A REPORT

ON

HELIBORNE MAGNETIC , ELECTROMAGNETIC & RADIOMETRIC SURVEYING

Iskut Area, B.C.
56°30'N, 130°30'W
NTS 104A/5, B/7,8,9,10,11,14 & 15

Survey Dates: July 19th – September 6th, 2007

FOR

HATHOR EXPLORATION LIMITED

Vancouver, B.C.

BY

PETER E. WALCOTT & ASSOCIATES LIMITED

Vancouver, British Columbia

OCTOBER 2008

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INTRODUCTION.

Between July 19th and September 6th, 2007 , Fugro Airborne Surveys carried out heliborne magnetic, electromagnetic and radiometric surveying over the glacier free areas of the vast holdings of Hathor Exploration Limited, held under the name of Mathew Mason, in the Iskut area of northwestern British Columbia.

The surveys were flown at a nominal helicopter terrain clearance of 60 metres on flight lines spaced 150 metres apart over five flight blocks, with the tie lines flown in the orthogonal direction at a spacing of 1500 metres.

The surveys were a continuation of the 2006 programme which was discontinued in October 2006 due to inclement weather with only 60% of the planned coverage completed.

The flight blocks and their respective line direction were laid out by Peter E. Walcott & Associates Limited, who planned, supervised and QC'd the surveys.

A Dighem multicoil, multifrequency E.M. system was employed, supplemented by a high sensitivity cesium magnetometer and a 256 channel spectrometer.

A GPS navigation system was employed to ensure accurate positioning of the geophysical data with respect to the topographic base maps.

The information from the respective geophysical sensors was used to produce maps that display the conductive, magnetic and radiometric properties of the survey areas. These maps are included in two reports on the respective blocks by P. Smith and I. Sram attached as Appendixes III and IV of this report.

The programme was terminated on September 6th after 14 days of no production due to inclement weather with some 200 line kilometers of coverage outstanding.

PROPERTY, LOCATION & ACCESS.

The property, known as Eskay Creek and/or Iskut River property, is located in the Liard and Skeena Mining Divisions of British Columbia. It consists of a large number of claims held under the name of Matthew Mason, alist of which is supplied in Appedix II.

It is situated in mountainous terrain with areas of glacial cover mainly to the east, south and west of the holdings of Barrick Gold and their Eskay Creek Mine, some 80 kilometres northwest of Stewart, B.C.

Due to the paucity of road access routes, access needs to be by helicopter. For this survey the helicopter and crew were base at the Bell II lodge on Hwy 37.

PREVIOUS WORK

Intermittent exploration has been carried out in the area since the original discovery and staking of the deposit by Tom Mackay in 1932 until the spectacular discovery by Prime Resources in 1988.

Since then numerous airborne geophysical surveys, ground geophysical and geochemical surveys, geological prospecting and diamond drill programmes have been carried out in the area, the results of which are mostly documented in numerous reports filed with the mines branch of the B.C. Government.

GEOLOGY.

Numerous publications exist on the geology of the Eskay Creek Mine and surrounding areas. The following is excerpted from a report by D. Kuran, P.Geo.

The Hathor claim area covers a large section of the Unuk River to Iskut River Area of north-western BC, centered on the Eskay Creek Mine, operated by Barrick Gold Corp.

The area is situated as to straddle older Asitka Group, Permian aged carbonates and volcanics to the west and upper Jurassic Bowser Group of post accretionary basinal sediments to the east. The area is described as lying with the Coast Mountains along the western margin of the Intermantaine tectonic belt, adjacent to the Coast Intrusive Complex. The stratigraphy belongs to the Stikine Terrain, composed of calcalkaline volcanics and coeval intrusive rocks and including stratigraphic equivalent sedimentary facies. The stratigraphy is deformed by open and upright D1 folds and associated faulting. The stratigraphy is described below.

The Paleozoic Stikine/Asitka assemblage consists of coralline limestones and intercalated mafic to felsic flows and volcaniclastic rocks, and siliceous siltstone, turbidite, chert and conglomerate. They exhibit local polyphase deformation. Mesozoic strata comprise mixed volcanic and volcanic-derived sedimentary rocks.

Upper Triassic Stuhini Group strata are dominantly sediments with minor pyroxene phyric flows and tuffs, and leucocratic dacitic tuffs. The sediments are siltstones, pebble to cobble conglomerates and wackes.

A Stuhini-Hazelton transitional unit of Hettangian age consists mainly of mixed sedimentary strata: black siltstones, heterolithic pebble to boulder conglomerates and wackes. Granitic stocks cut Stuhini Group rocks.

Lower to Middle Jurassic Hazelton Group volcanic and sedimentary rocks have been folded, faulted and weakly metamorphosed, mainly during Cretaceous time. Three episodes of intrusive activity produced small synvolcanic plutons, satellitic stocks of the Coast plutonic complex and minor dykes and sills.

The Unuk River Formation is of Hettangian to Pleinsbachian age. It consists primarily of andesitic tuffs with lesser black siltstone members. It is cut by the two-feldspar Premier porphyry.

The Betty Creek Formation is Pleinsbachian to Toarcian. It consists of interbedded tuffs, flows and hematitic sedimentary rocks. There are locally pillowed basaltic to dacitic crystal and lithic tuffs and flows, purple to maroon conglomerates, wackes, siltstones and mudstones, and minor black siltstone layers.

The Mount Dilworth Formation consists of felsic pyroclastics and flows. It consists of tuff breccias;

GEOLOGY cont'd

lapilli, ash and dust tuffs; and local welded ash flows. The unit is of Toarcian age.

Salmon River Formation, which is Toarcian to Bajocian in age, comprises a thick turbidite succession. It consists of dark siltstones with lesser sandstones, conglomerates, silty limestone and pale siliceous siltstones. Mafic pillow lava and minor intermediate distal tuff also crop out.

Middle to Upper Jurassic Bowser Lake Group strata are marine basin turbidites, black siltstones, fine-grained sandstones, and conglomerates. The Pliocene to Recent Stikine volcanics comprise basaltic flows, tuff and scoria.

Intrusive rocks in the area range from Late Triassic to Tertiary or Quaternary. The oldest is the Stikine plutonic suite of diorite and quartz diorite plutons. The Early Jurassic Texas Creek plutonic suite includes quartz diorite, monzodiorite, and quartz monzonite. The suite includes hypabyssal equivalents of the Hazelton Group. The Middle Jurassic Three Sisters suite consists of olivine-pyroxene gabbro and diorite. Rocks of the Coast plutonic complex are of Paleocene to Eocene age. Granitoid batholiths and stocks are characteristic. Rocks types include granodiorite, granite and dacite in dikes. Oligocene late-tectonic dikes are micro-diorite, andesite and lamprophyre. Basaltic dikes represent the Stikine volcanic suite.

The rich volcanogenic Eskay gold-silver-lead-zinc-copper mine and many other mineral occurrences are known in the area. Six types of veins are identified: base metal quartz, silver-rich base metal, precious and base metal quartz, precious metal quartz, carbonate, and barite. Other deposit types include: porphyry-style copper-molybdenum; disseminated gold (silver) in alteration zones; gold-bearing skarn; and stratabound pyritic zones.

PURPOSE.

As the Eskay Creek deposit is hosted by a bimodal felsic-mafic volcanic sequence, which is strongly potassically altered, the Snip mine by Triassic metasediments with a halo of biotite as a potassic alteration manifestation, and the Stonehouse – Johnny Mtn. – is a quartz – andaluria system with a potassic alteration signature, the purpose of the survey was to detect areas of potassic alteration, skarn mineralization and zones of conductive mineralization as well as to provide information that could be used to map geology and structure with the use of radiometric, magnetic and electromagnetic techniques.

SURVEY SPECIFICATIONS.

The magnetic survey was carried out using an optically pumped cesium vapour magnetometer mounted on the tail of the EM bird 28 metres below the helicopter. This instrument was manufactured by Scintrex Limited of Concord, Ontario. Corrections for the diurnal were made by comparison with a Fugro CFI base station employing a Geometrics, of San Jose, California, G822A sensor.

The electromagnetic survey was conducted using a Dighem V-BKS54 system - manufactured by Fugro – towed 30 metres below the helicopter. Coil separation is 8 metres for the 900 Hz coplanar, 1000 Hz coaxial, 5500 Hz coaxial, and 7200 Hz coplanar, and 6.3 metres for the 56,000 Hz coplanar configurations, with 5 inphase, 5 quadrature and 2 monitor channels recorded on a heliDAS digital data acquisition system also manufactured by Fugro.

The GR-820 spectrometer – manufactured by Exploranium – employs two downward looking crystals (1024 cu in) and one upward looking crystal (256 cu in). The downward crystals record the radiometric spectrum from 410 KeV to 3MeV over 256 discrete energy windows. From these 256 channels the standard Total Count, Potassium, Thorium, Uranium channels are extracted.

The upward looking crystal is used to measure and correct for Radon.

Navigation and flight path recovery were obtained using a Novatel OEMIV dual frequency 24 channel board with the antenna – Aero AT1675 – mounted on the tail of the helicopter. Post-survey differential correction was obtained by processing against the data from a similar unit at 10 Hz sampling rate, with a Marconi Allstar OEM, CMT – 1200 as a back-up.

The survey, as mentioned previously, was conducted on pre-programmed flight lines on the respective nine blocks.

In all some 2418 line kilometers were flown.

DATA PRESENTATION

Fugro Airborne computed and compiled the results of the data from the three sensors, and presented them on base maps of the local topography at a scale of 1:20,000 as listed in their reports.

The writers presented the 1:20,000 topography for Blocks 1, 3, 4, 5 & 6 with RGS assays and historic assays from Minfiles – elements Au, Ag & Cu – along with government geology sized to the airborne sheets for integration of the respective airborne anomalies/signatures with known mineral showings and geological features.

Also presented are 3D views of EM 1D inversions for Blocks 1 and 3.

DISCUSSION OF RESULTS.

The reports of Smith and Sram provide adequate coverage on the results obtained from the surveys and the writers will add no more at this time, as further studies of the results with more advanced software and imaging techniques are presently underway.

SUMMARY, CONCLUSIONS & RECOMMENDATIONS.

Between July 19th and September 6th, 2007, at the request of Hathor Exploration Limited, Fugro Airborne Surveys undertook to finish the combined magnetic, electromagnetic and radiometric survey programme over parts of the Eskay Creek property, located in the Iskut area of British Columbia, started in 2006.

The survey was suspended with only around 60% of the planned coverage completed due to the inclement weather that plagued most of northern B.C. for the summer and early fall of 2006.

All but some 200 kilometres of the planned and flyable coverage was completed when a decision to terminate the survey on account of the poor weather was made in early September.

The results as discussed in reports by Fugro personnel should be studied in conjunction with the known geology, the RGS data, the Minfile data and satellite imagery to generate a general prospecting- exploration strategy as well as possible targets for ground follow-up next year. Included in this study should be the additional processing of the geophysical results with sophisticated software and imaging techniques including leveling of the radiometric data for north and south exposures where the moisture content could vary considerably. Conductors and/or alteration zones in the vicinity of icefield margins should rank high as prospective targets due to possible ice retreat since previous mapping and prospecting.

Respectfully submitted,

PETER E. WALCOTT & ASSOCIATES LTD.

Alexander Walcott
Geophysicist

Peter E. Walcott, P.Eng.
Geophysicist

Vancouver, B.C.
October 2008

APPENDIX I

COST OF SURVEY.

Fugro Airborne undertook the survey on a kilometre basis with additional daily charges after forty odd days of non production. As the latter were incurred in the 2006 flying daily charges were billed for the 50 days at $2,500.00 per day and the 18 left over from the 2006 survey in addition to the 2417.9 kilometers at $106.00 per line kilometre for a total cost of $426,294.70.

Fuel for the helicopter was $8,163.22 with positioning costs by Vancouver Island Helicopters of $5,651.46.

Accommodation at Bell II lodge for Fugro personnel was $40,463.40.

Peter E. Walcott & Associates Limited managed the 2006 assessment filings and reported on the 2006 results at a cost of $8,000.00. They organized and supervised the 2007 work, and carried out ongoing GIS compilation of historic data and the 2006-2007 survey results at a cost of $36,000.00.

As a result the cost of the survey to date was $524,575.48.

PERSONNEL EMPLOYED ON SURVEY.

Name	Occupation	Address	Dates
Peter E. Walcott	Geophysicist	Peter E. Walcott & Assoc. 1529 W. 6th Ave., Vancouver, B.C.	Apr. 10th – Sept. 15th, 07 Oct. 12th -19th, 08
A. Walcott	“	“	Jun. 24th - 30th,07 Jan. 6th –Mar. 20th, Oct. 4th – 18th, 08
Fugro Airborne	Listed in their reports		July 19th -Sept. 6th 2007 Nov. 20th, 07 – Feb. 19th, 2008

CERTIFICATION.

I, Peter E. Walcott, of 605 Rutland Court, Coquitlam, British Columbia, hereby certify that:

1. I am graduate of the University of Toronto in 1962 with a B.A.Sc. in Engineering Physics, Geophysics Option.

2. I have been practicing my profession for the last forty seven years.

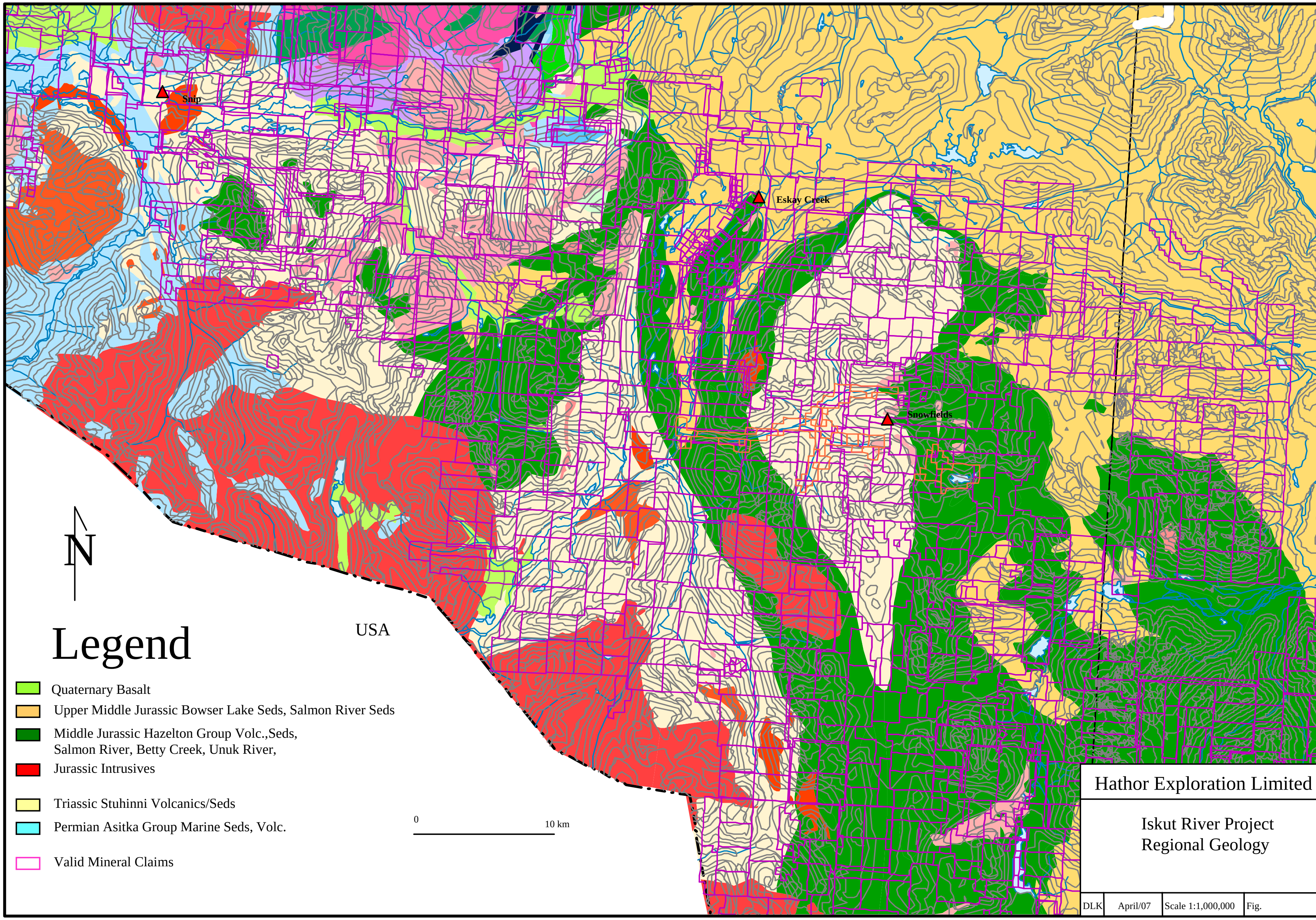
3. I am a member of the Association of Professional Engineers of British Columbia and Ontario.

4. I hold no interest, direct or indirect in Hathor Exploration Limited, nor do I expect to receive any.

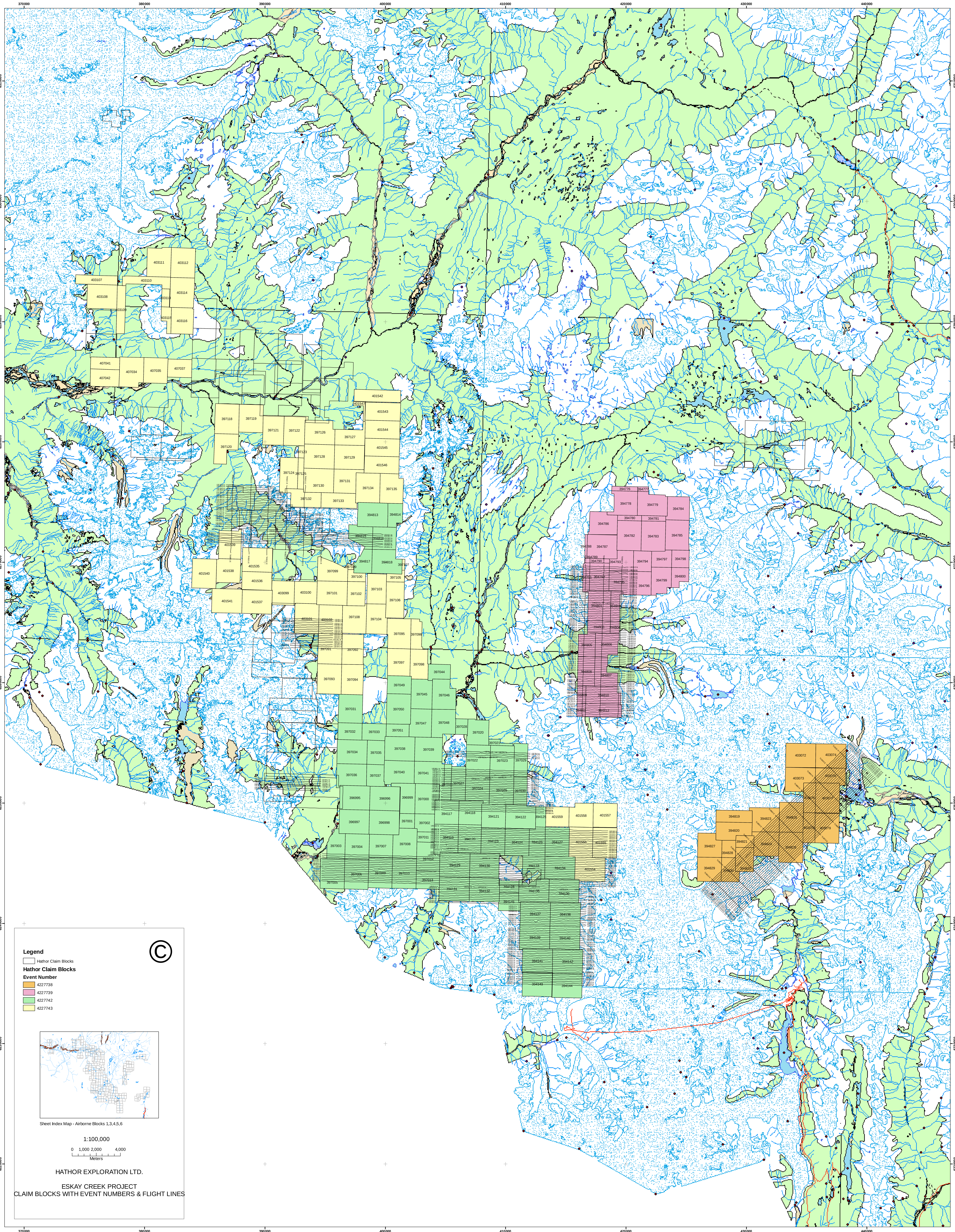
Peter E.Walcott, P.Eng.

Vancouver, B.C.

October 2008



Snip
Eskay Creek
Snowfields
N
USA
Legend
Quaternary Basalt
Upper Middle Jurassic Bowser Lake Seds, Salmon River Seds
Middle Jurassic Hazelton Group Volc.,Seds,
Salmon River, Betty Creek, Unuk River,
Jurassic Intrusives
Triassic Stuhinni Volcanics/Seds
Permian Asitka Group Marine Seds, Volc.
Valid Mineral Claims
0
10 km
Hathor Exploration Limited
Iskut River Project
Regional Geology
DLK
April/07
Scale 1:1,000,000
Fig.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Legend
Hathor Claim Blocks
Hathor Claim Blocks
Event Number
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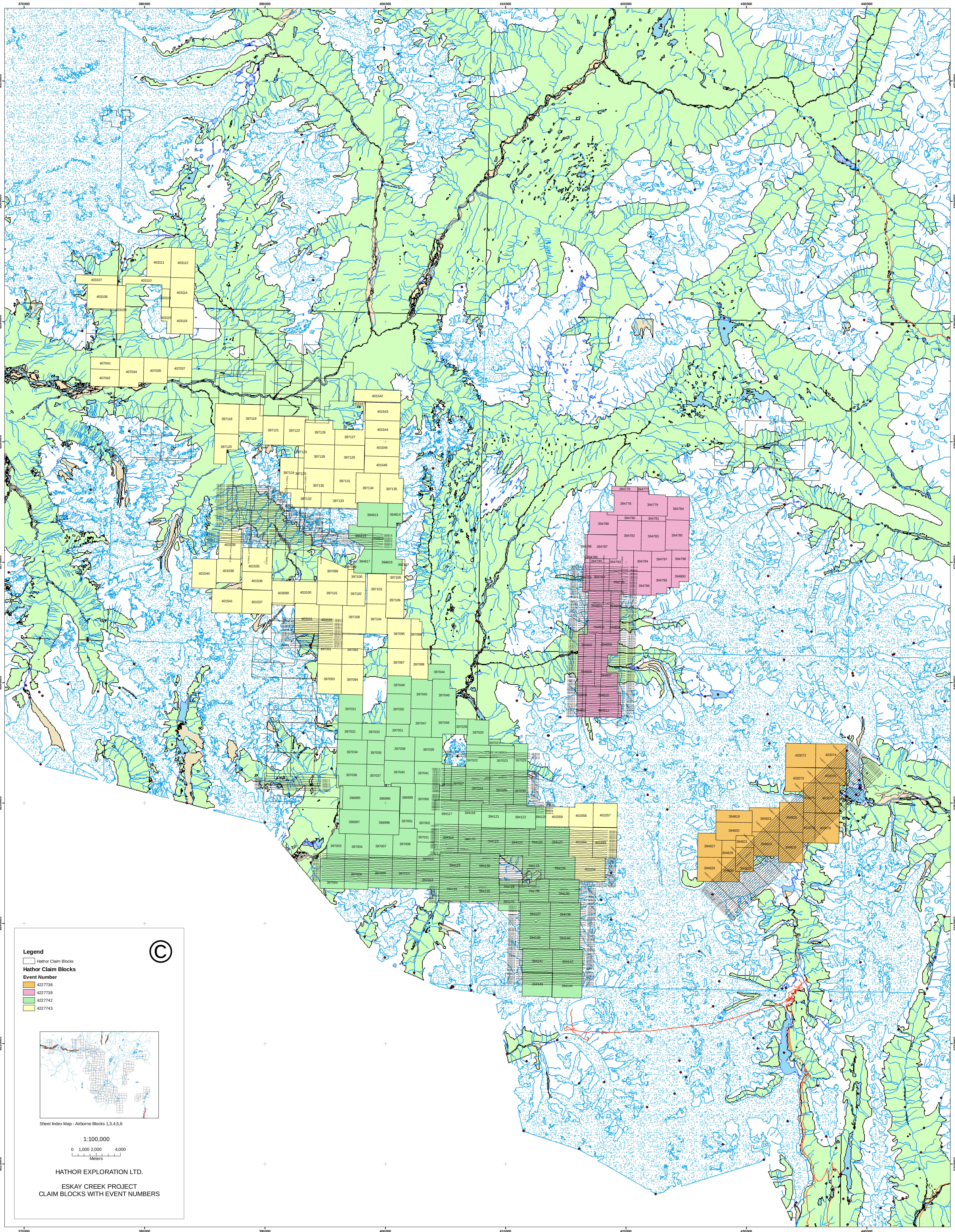
4227739
4227742
4227743
Sheet Index Map - Airborne Blocks 1,3,4,5,6
1:100,000
0 1,000 2,000 4,000
Meters
HATHOR EXPLORATION LTD.
ESKAY CREEK PROJECT
CLAIM BLOCKS WITH EVENT NUMBERS & FLIGHT LINES


Legend
Hathor Claim Blocks
Hathor Claim Blocks
Event Number
4227738
4227739
4227742
4227743
Sheet Index Map - Airborne Blocks 1,3,4,5,6
1:100,000
0 1,000 2,000 4,000
Meters
HATHOR EXPLORATION LTD.
ESKAY CREEK PROJECT
CLAIM BLOCKS WITH EVENT NUMBERS

APPENDIX II

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Hathor Holding - Eskay Area							
TEN_NO_ID	**TIMESTAMP_**	**CLAIM_NAME**	**OWNER**	**GOOD_TO_DATE**	**STATUS**	**MINING_DIV**	**AREA**
394825	20040930	DELTA 7	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
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394821	20040930	DELTA 4	143603 (100%)	2009/dec/11	GOOD	SKEENA	150
394819	20040930	DELTA 1	143603 (100%)	2009/dec/11	GOOD	SKEENA	300
394829	20040930	DELTA 12	143603 (100%)	2009/dec/11	GOOD	SKEENA	400
394827	20040930	DELTA 10	143603 (100%)	2009/dec/11	GOOD	SKEENA	400
394823	20040930	DELTA 6	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
394824	20040930	DELTA 8	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
394826	20040930	DELTA 9	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
394828	20040930	DELTA 11	143603 (100%)	2009/dec/11	GOOD	SKEENA	300
394830	20040930	DELTA 13	143603 (100%)	2009/dec/11	GOOD	SKEENA	300
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403074	20050117	KNIP 2	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
403075	20050117	KNIP 4	143603 (100%)	2009/dec/11	GOOD	SKEENA	375
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403077	20050117	KNIP 6	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
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394808	20040930	BJ 31A	143603 (100%)	2009/dec/11	GOOD	SKEENA	375
394810	20040930	BJ 33	143603 (100%)	2009/dec/11	GOOD	SKEENA	450
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394812	20040930	BJ 35	143603 (100%)	2010/jan/31	GOOD	SKEENA	450
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394780	20040930	BJ 5	143603 (100%)	2009/dec/11	GOOD	SKEENA	100
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394135	20040930	GRACEY 19	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397049	20040930	HAWILSON 6	143603 (100%)	2009/aug/11	GOOD	SKEENA	300
397044	20040930	HAWILSON 1	143603 (100%)	2009/aug/11	GOOD	SKEENA	300
397034	20040930	PEARLY 4	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394133	20040930	GRACEY 17	143603 (100%)	2009/aug/11	GOOD	SKEENA	400
397025	20040930	SUN 6	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397005	20040930	QUILLIAN 3	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394126	20040930	GRACEY 10	143603 (100%)	2009/aug/11	GOOD	SKEENA	375

394813	20040930	MACGOLD 1	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397045	20040930	HAWILSON 2	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394131	20040930	GRACEY 15	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397036	20040930	PEARLY 6	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394137	20040930	GRACEY 21	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
396999	20040930	FLORY 5	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397009	20040930	QUILLIAN 7	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397032	20040930	PEARLY 2	143603 (100%)	2009/aug/11	GOOD	SKEENA	300
396995	20040930	FLORY 1	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397002	20040930	FLORY 8	143603 (100%)	2009/aug/11	GOOD	SKEENA	300
397046	20040930	HAWILSON 3	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394817	20040930	MACGOLD 5	143603 (100%)	2009/aug/11	GOOD	LIARD	300
394144	20040930	GRACEY 28	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394132	20040930	GRACEY 16	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397024	20040930	SUN 5	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394119	20040930	GRACEY 3	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394118	20040930	GRACEY 2	143603 (100%)	2009/aug/11	GOOD	SKEENA	400
394117	20040930	GRACEY 1	143603 (100%)	2009/aug/11	GOOD	SKEENA	400
396997	20040930	FLORY 3	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394125	20040930	GRACEY 9	143603 (100%)	2009/aug/11	GOOD	SKEENA	200
397011	20040930	QUILLIAN 9	143603 (100%)	2009/aug/11	GOOD	SKEENA	200
397027	20040930	SUN 8	143603 (100%)	2009/aug/11	GOOD	SKEENA	450
397039	20040930	PEARLY 9	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397031	20040930	PEARLY 1	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394142	20040930	GRACEY 26	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397102	20040930	JULIAN 4	143603 (100%)	2009/aug/11	GOOD	LIARD	300
397135	20040930	SNIP 20	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397130	20040930	SNIP 15	143603 (100%)	2009/aug/11	GOOD	LIARD	500
397109	20040930	JULIAN 11	143603 (100%)	2009/aug/11	GOOD	LIARD	100
397118	20040930	SNIP 1	143603 (100%)	2009/aug/11	GOOD	LIARD	500
397124	20040930	SNIP 9	143603 (100%)	2009/aug/11	GOOD	LIARD	450
397119	20040930	SNIP 2	143603 (100%)	2009/aug/11	GOOD	LIARD	500
397134	20040930	SNIP 19	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397106	20040930	JULIAN 9	143603 (100%)	2009/aug/11	GOOD	SKEENA	450
397125	20040930	SNIP 10	143603 (100%)	2009/aug/11	GOOD	LIARD	150
397099	20040930	JULIAN 1	143603 (100%)	2009/aug/11	GOOD	LIARD	500
397101	20040930	JULIAN 3	143603 (100%)	2009/aug/11	GOOD	LIARD	500
397105	20040930	JULIAN 7	143603 (100%)	2009/aug/11	GOOD	SKEENA	150
397122	20040930	SNIP 5	143603 (100%)	2009/aug/11	GOOD	LIARD	500
397096	20040930	KING CREEK 6	143603 (100%)	2009/aug/11	GOOD	SKEENA	250
407041	20040930	IS 8	143603 (100%)	2009/aug/11	GOOD	LIARD	250
397133	20040930	SNIP 18	143603 (100%)	2009/aug/11	GOOD	LIARD	450
397126	20040930	SNIP 11	143603 (100%)	2009/aug/11	GOOD	LIARD	500
397132	20040930	SNIP 17	143603 (100%)	2009/aug/11	GOOD	LIARD	450
397123	20040930	SNIP 8	143603 (100%)	2009/aug/11	GOOD	LIARD	50
397094	20040930	KING CREEK 4	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397121	20040930	SNIP 4	143603 (100%)	2009/aug/11	GOOD	LIARD	500
397128	20040930	SNIP 13	143603 (100%)	2009/aug/11	GOOD	LIARD	500
397104	20040930	JULIAN 6	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397108	20040930	JULIAN 10	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
407042	20040930	IS 9	143603 (100%)	2009/aug/11	GOOD	LIARD	375
397098	20040930	KING CREEK 8	143603 (100%)	2009/aug/11	GOOD	SKEENA	375
397093	20040930	KING CREEK 3	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397092	20040930	KING CREEK 2	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397131	20040930	SNIP 16	143603 (100%)	2009/aug/11	GOOD	LIARD	500
397097	20040930	KING CREEK 7	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
401554	20051003	BURRARD 1	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
401555	20051003	BURRARD 2	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
401556	20051003	BURRARD 3	143603 (100%)	2009/aug/11	GOOD	SKEENA	500

397120	20040930	SNIP 3	143603 (100%)	2009/aug/11	GOOD	LIARD	500
401547	20040930	JACK 6	143603 (100%)	2009/aug/11	GOOD	LIARD	200
407037	20040930	IS 4	143603 (100%)	2009/aug/11	GOOD	LIARD	300
397091	20040930	KING CREEK 1	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
407035	20040930	IS 2	143603 (100%)	2009/aug/11	GOOD	LIARD	500
401557	20051005	BURRARD 4	143603 (100%)	2009/aug/11	GOOD	SKEENA	400
401558	20051005	BURRARD 5	143603 (100%)	2009/aug/11	GOOD	SKEENA	400
401559	20051005	BURRARD 6	143603 (100%)	2009/aug/11	GOOD	SKEENA	400
407034	20040930	IS 1	143603 (100%)	2009/aug/11	GOOD	LIARD	500
397129	20040930	SNIP 14	143603 (100%)	2009/aug/11	GOOD	LIARD	500
397103	20040930	JULIAN 5	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397095	20040930	KING CREEK 5	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397100	20040930	JULIAN 2	143603 (100%)	2009/aug/11	GOOD	LIARD	150
397107	20040930	JULIAN 8	143603 (100%)	2009/aug/11	GOOD	SKEENA	50
401542	20050111	JACK 1	143603 (100%)	2009/aug/11	GOOD	LIARD	400
401543	20050111	JACK 2	143603 (100%)	2009/aug/11	GOOD	LIARD	450
401535	20050111	GEORGIA 1	143603 (100%)	2009/aug/11	GOOD	LIARD	500
401536	20050111	GEORGIA 2	143603 (100%)	2009/aug/11	GOOD	LIARD	375
401537	20050111	GEORGIA 3	143603 (100%)	2009/aug/11	GOOD	LIARD	500
401538	20050111	GEORGIA 4	143603 (100%)	2009/aug/11	GOOD	LIARD	500
401539	20050111	GEORGIA 5	143603 (100%)	2009/aug/11	GOOD	LIARD	500
401540	20050111	GEORGIA 6	143603 (100%)	2009/aug/11	GOOD	LIARD	500
401541	20050111	GEORGIA 7	143603 (100%)	2009/aug/11	GOOD	LIARD	500
403099	20050111	NIP 1	143603 (100%)	2009/aug/11	GOOD	LIARD	400
403100	20050111	NIP 2	143603 (100%)	2009/aug/11	GOOD	LIARD	400
403101	20050111	NIP 3	143603 (100%)	2009/aug/11	GOOD	LIARD	500
403102	20050111	NIP 4	143603 (100%)	2009/aug/11	GOOD	LIARD	500
401544	20050111	JACK 3	143603 (100%)	2009/aug/11	GOOD	LIARD	450
401545	20050111	JACK 4	143603 (100%)	2009/aug/11	GOOD	LIARD	450
401546	20050111	JACK 5	143603 (100%)	2009/aug/11	GOOD	LIARD	450
403107	20050111	RET 1	143603 (100%)	2009/aug/11	GOOD	LIARD	350
403108	20050111	RET 2	143603 (100%)	2009/aug/11	GOOD	LIARD	500
403109	20050111	RET 3	143603 (100%)	2009/aug/11	GOOD	LIARD	400
403110	20050111	RET 4	143603 (100%)	2009/aug/11	GOOD	LIARD	400
403111	20050111	RET 5	143603 (100%)	2009/aug/11	GOOD	LIARD	500
403112	20050111	RET 6	143603 (100%)	2009/aug/11	GOOD	LIARD	500
403113	20050111	RET 7	143603 (100%)	2009/aug/11	GOOD	LIARD	150
403114	20050111	RET 8	143603 (100%)	2009/aug/11	GOOD	LIARD	500
403115	20050111	RET 9	143603 (100%)	2009/aug/11	GOOD	LIARD	250
403116	20050111	RET 10	143603 (100%)	2009/aug/11	GOOD	LIARD	500
397127	20040930	SNIP 12	143603 (100%)	2009/aug/11	GOOD	LIARD	500
407175	20040930	IS 29	143603 (100%)	2009/dec/11	GOOD	LIARD	300
407157	20040930	KING 1	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
407171	20040930	IS 25	143603 (100%)	2009/dec/11	GOOD	LIARD	500
407173	20040930	IS 27	143603 (100%)	2009/dec/11	GOOD	LIARD	500
407049	20040930	IS 16	143603 (100%)	2009/dec/11	GOOD	LIARD	500
407177	20040930	IS 31	143603 (100%)	2009/dec/11	GOOD	LIARD	375
522653	20051125	NEW	143603 (100%)	2009/dec/11	GOOD		427
522654	20051125	NEW	143603 (100%)	2009/dec/11	GOOD		427
522655	20051125	NEW	143603 (100%)	2009/dec/11	GOOD		71
407155	20040930	LEHUA 3	143603 (100%)	2009/dec/11	GOOD	LIARD	200
522498	20051122	NEW1	143603 (100%)	2009/dec/11	GOOD		426
522499	20051122	NEW2	143603 (100%)	2009/dec/11	GOOD		409
522500	20051122	NEW3	143603 (100%)	2009/nov/22	GOOD		426
522501	20051122	NEW4	143603 (100%)	2009/nov/22	GOOD		391
522540	20051123	NEW5	143603 (100%)	2009/dec/11	GOOD		426
522541	20051123	NEW6	143603 (100%)	2009/dec/11	GOOD		284
407156	20040930	LEHUA 4	143603 (100%)	2009/dec/11	GOOD	LIARD	300
407128	20040930	PIN 6	143603 (100%)	2009/dec/11	GOOD	LIARD	450

407160	20040930	KING 4	143603 (100%)	2009/dec/11	GOOD	SKEENA	450
529829	20060309	GLOBE	143603 (100%)	2009/dec/11	GOOD		18
407159	20040930	KING 3	143603 (100%)	2009/dec/11	GOOD	SKEENA	375
407047	20040930	IS 14	143603 (100%)	2009/dec/11	GOOD	LIARD	500
407129	20040930	PIN 7	143603 (100%)	2009/dec/11	GOOD	LIARD	500
407127	20040930	PIN 5	143603 (100%)	2009/dec/11	GOOD	LIARD	400
407123	20040930	PIN 1	143603 (100%)	2009/dec/11	GOOD	LIARD	350
407126	20040930	PIN 4	143603 (100%)	2009/dec/11	GOOD	LIARD	400
407050	20040930	IS 17	143603 (100%)	2009/dec/11	GOOD	LIARD	400
407132	20040930	PIN 10	143603 (100%)	2009/dec/11	GOOD	LIARD	500
407044	20040930	IS 11	143603 (100%)	2009/dec/11	GOOD	LIARD	500
407146	20040930	FEW 1	143603 (100%)	2009/dec/11	GOOD	SKEENA	400
407174	20040930	IS 28	143603 (100%)	2009/dec/11	GOOD	LIARD	500
407138	20040930	HELL 5	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
407141	20040930	HELL 8	143603 (100%)	2009/dec/11	GOOD	SKEENA	400
407158	20040930	KING 2	143603 (100%)	2009/dec/11	GOOD	SKEENA	100
407164	20040930	IS 18	143603 (100%)	2009/dec/11	GOOD	LIARD	150
407165	20040930	IS 19	143603 (100%)	2009/dec/11	GOOD	LIARD	450
407145	20040930	HELL 12	143603 (100%)	2009/dec/11	GOOD	SKEENA	400
407147	20040930	FEW 2	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
403117	20051003	PAC 1	143603 (100%)	2009/nov/14	GOOD	LIARD	500
403118	20051003	PAC 2	143603 (100%)	2009/nov/14	GOOD	LIARD	450
403119	20051003	PAC 3	143603 (100%)	2009/nov/14	GOOD	LIARD	500
403120	20051003	PAC 5	143603 (100%)	2009/nov/14	GOOD	LIARD	100
403121	20051003	PAC 4	143603 (100%)	2009/nov/14	GOOD	LIARD	500
403124	20051003	PAC 6	143603 (100%)	2009/nov/14	GOOD	LIARD	125
407131	20040930	PIN 9	143603 (100%)	2009/dec/11	GOOD	LIARD	225
407124	20040930	PIN 2	143603 (100%)	2009/dec/11	GOOD	LIARD	500
517580	20050712						0
517583	20050712						0
517586	20050712						0
407161	20040930	KING 5	143603 (100%)	2009/dec/11	GOOD	LIARD	300
407163	20040930	KING 7	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
407130	20040930	PIN 8	143603 (100%)	2009/dec/11	GOOD	LIARD	500
407125	20040930	PIN 3	143603 (100%)	2009/dec/11	GOOD	LIARD	300
407176	20040930	IS 30	143603 (100%)	2009/dec/11	GOOD	LIARD	225
407133	20040930	PIN 11	143603 (100%)	2009/dec/11	GOOD	LIARD	500
407142	20040930	HELL 9	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
407043	20040930	IS 10	143603 (100%)	2009/dec/11	GOOD	LIARD	500
407162	20040930	KING 6	143603 (100%)	2009/dec/11	GOOD	LIARD	500
407046	20040930	IS 13	143603 (100%)	2009/dec/11	GOOD	LIARD	500
522591	20051123	NEW7	143603 (100%)	2009/dec/11	GOOD		426
522593	20051123	NEW8	143603 (100%)	2009/dec/11	GOOD		426
522594	20051123	NEW9	143603 (100%)	2009/dec/11	GOOD		426
522595	20051123	NEW9	143603 (100%)	2009/dec/11	GOOD		142
407143	20040930	HELL 10	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
407140	20040930	HELL 7	143603 (100%)	2009/dec/11	GOOD	SKEENA	400
525297	20060113						0
407144	20040930	HELL 11	143603 (100%)	2009/dec/11	GOOD	SKEENA	400
522921	20051129	NEW	143603 (100%)	2009/dec/11	GOOD		430
522922	20051129	NEW	143603 (100%)	2009/dec/11	GOOD		430
522923	20051129	NEW	143603 (100%)	2009/dec/11	GOOD		394
522924	20051129	NEW	143603 (100%)	2009/dec/11	GOOD		430
403095	20050111	ZIP 1	143603 (100%)	2008/dec/11	GOOD	LIARD	500
403096	20050111	ZIP 2	143603 (100%)	2008/dec/11	GOOD	LIARD	500
403097	20050111	ZIP 4	143603 (100%)	2008/dec/11	GOOD	LIARD	150
403098	20050111	ZIP 3	143603 (100%)	2008/dec/11	GOOD	LIARD	350
403103	20050111	GRIZ 1	143603 (100%)	2008/dec/11	GOOD	LIARD	500
403104	20050111	GRIZ 2	143603 (100%)	2008/dec/11	GOOD	LIARD	500

403105	20050111	GRIZ 3	143603 (100%)	2008/dec/11	GOOD	LIARD	500
403106	20050111	GRIZ 4	143603 (100%)	2008/dec/11	GOOD	LIARD	500
401548	20050117	TINA 1	143603 (100%)	2008/dec/11	GOOD	SKEENA	500
401549	20050117	TINA 2	143603 (100%)	2008/dec/11	GOOD	SKEENA	500
401550	20050117	TINA 3	143603 (100%)	2008/dec/11	GOOD	SKEENA	500
401551	20050117	TINA 4	143603 (100%)	2008/dec/11	GOOD	SKEENA	500
401552	20050117	TINA 5	143603 (100%)	2008/dec/11	GOOD	SKEENA	500
401553	20050117	TINA 6	143603 (100%)	2008/dec/11	GOOD	SKEENA	250

Claims Surveys - Hathor Holdings Eskay Area							
TEN_NO_ID	TIMESTAMP_	CLAIM_NAME	OWNER	GOOD_TO_DA	STATUS	MINING_DIV	AREA
394825	20040930	DELTA 7	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
394822	20040930	DELTA 5	143603 (100%)	2009/dec/11	GOOD	SKEENA	300
394821	20040930	DELTA 4	143603 (100%)	2009/dec/11	GOOD	SKEENA	150
394829	20040930	DELTA 12	143603 (100%)	2009/dec/11	GOOD	SKEENA	400
394823	20040930	DELTA 6	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
394824	20040930	DELTA 8	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
394826	20040930	DELTA 9	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
394828	20040930	DELTA 11	143603 (100%)	2009/dec/11	GOOD	SKEENA	300
394830	20040930	DELTA 13	143603 (100%)	2009/dec/11	GOOD	SKEENA	300
403073	20050117	KNIP 3	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
403074	20050117	KNIP 2	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
403075	20050117	KNIP 4	143603 (100%)	2009/dec/11	GOOD	SKEENA	375
403076	20050117	KNIP 5	143603 (100%)	2009/dec/11	GOOD	SKEENA	250
403077	20050117	KNIP 6	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
403078	20050117	KNIP 7	143603 (100%)	2009/dec/11	GOOD	SKEENA	250
403079	20050117	KNIP 8	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
394805	20040930	BJ 29	143603 (100%)	2009/dec/11	GOOD	SKEENA	300
394808	20040930	BJ 31A	143603 (100%)	2009/dec/11	GOOD	SKEENA	375
394810	20040930	BJ 33	143603 (100%)	2009/dec/11	GOOD	SKEENA	450
394811	20040930	BJ 34	143603 (100%)	2010/dec/10	GOOD	SKEENA	150
394812	20040930	BJ 35	143603 (100%)	2010/jan/31	GOOD	SKEENA	450
394802	20040930	BJ 26	143603 (100%)	2009/dec/11	GOOD	SKEENA	250
394806	20040930	BJ 30	143603 (100%)	2009/dec/11	GOOD	SKEENA	400
394790	20040930	BJ 14	143603 (100%)	2009/dec/11	GOOD	SKEENA	100
394807	20040930	BJ 31	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
394801	20040930	BJ 25	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
394792	20040930	BJ 16	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
394804	20040930	BJ 28	143603 (100%)	2009/dec/11	GOOD	SKEENA	100
394795	20040930	BJ 19	143603 (100%)	2009/dec/11	GOOD	SKEENA	500
394791	20040930	BJ 15	143603 (100%)	2009/dec/11	GOOD	SKEENA	250
394793	20040930	BJ 17	143603 (100%)	2009/dec/11	GOOD	SKEENA	400
394803	20040930	BJ 27	143603 (100%)	2009/dec/11	GOOD	SKEENA	200
394789	20040930	BJ 13A	143603 (100%)	2009/dec/11	GOOD	SKEENA	25
394809	20040930	BJ 32	143603 (100%)	2009/dec/11	GOOD	SKEENA	150
397013	20040930	QUILLIAN 11	143603 (100%)	2009/aug/11	GOOD	SKEENA	300
397041	20040930	PEARLY 11	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394124	20040930	GRACEY 8	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397010	20040930	QUILLIAN 8	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394141	20040930	GRACEY 25	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397006	20040930	QUILLIAN 4	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394127	20040930	GRACEY 11	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394140	20040930	GRACEY 24	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397003	20040930	QUILLIAN 1	143603 (100%)	2009/aug/11	GOOD	SKEENA	375
394129	20040930	GRACEY 13	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394136	20040930	GRACEY 20	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397030	20040930	SUN 11	143603 (100%)	2009/aug/11	GOOD	SKEENA	375
394123	20040930	GRACEY 7	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394134	20040930	GRACEY 18	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397004	20040930	QUILLIAN 2	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394139	20040930	GRACEY 23	143603 (100%)	2009/aug/11	GOOD	SKEENA	500

394128	20040930	GRACEY 12	143603 (100%)	2009/aug/11	GOOD	SKEENA	200
394120	20040930	GRACEY 4	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394143	20040930	GRACEY 27	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394122	20040930	GRACEY 6	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397022	20040930	SUN 3	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394138	20040930	GRACEY 22	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394121	20040930	GRACEY 5	143603 (100%)	2009/aug/11	GOOD	SKEENA	400
394816	20040930	MACGOLD 4	143603 (100%)	2009/aug/11	GOOD	LIARD	400
397007	20040930	QUILLIAN 5	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397023	20040930	SUN 4	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397008	20040930	QUILLIAN 6	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397012	20040930	QUILLIAN 10	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394145	20040930	GRACEY 29	143603 (100%)	2009/aug/11	GOOD	SKEENA	300
397026	20040930	SUN 7	143603 (100%)	2009/aug/11	GOOD	SKEENA	350
394815	20040930	MACGOLD 3	143603 (100%)	2009/aug/11	GOOD	LIARD	400
397029	20040930	SUN 10	143603 (100%)	2009/aug/11	GOOD	SKEENA	450
394130	20040930	GRACEY 14	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394135	20040930	GRACEY 19	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394133	20040930	GRACEY 17	143603 (100%)	2009/aug/11	GOOD	SKEENA	400
397025	20040930	SUN 6	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397005	20040930	QUILLIAN 3	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394126	20040930	GRACEY 10	143603 (100%)	2009/aug/11	GOOD	SKEENA	375
394131	20040930	GRACEY 15	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394137	20040930	GRACEY 21	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397009	20040930	QUILLIAN 7	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394144	20040930	GRACEY 28	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394132	20040930	GRACEY 16	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397024	20040930	SUN 5	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394119	20040930	GRACEY 3	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
394118	20040930	GRACEY 2	143603 (100%)	2009/aug/11	GOOD	SKEENA	400
394117	20040930	GRACEY 1	143603 (100%)	2009/aug/11	GOOD	SKEENA	400
394125	20040930	GRACEY 9	143603 (100%)	2009/aug/11	GOOD	SKEENA	200
397027	20040930	SUN 8	143603 (100%)	2009/aug/11	GOOD	SKEENA	450
394142	20040930	GRACEY 26	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397092	20040930	KING CREEK 2	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
401554	20051003	BURRARD 1	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
401555	20051003	BURRARD 2	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
401556	20051003	BURRARD 3	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
397091	20040930	KING CREEK 1	143603 (100%)	2009/aug/11	GOOD	SKEENA	500
401539	20050111	GEORGIA 5	143603 (100%)	2009/aug/11	GOOD	LIARD	500
403101	20050111	NIP 3	143603 (100%)	2009/aug/11	GOOD	LIARD	500
403102	20050111	NIP 4	143603 (100%)	2009/aug/11	GOOD	LIARD	500

APPENDIX III

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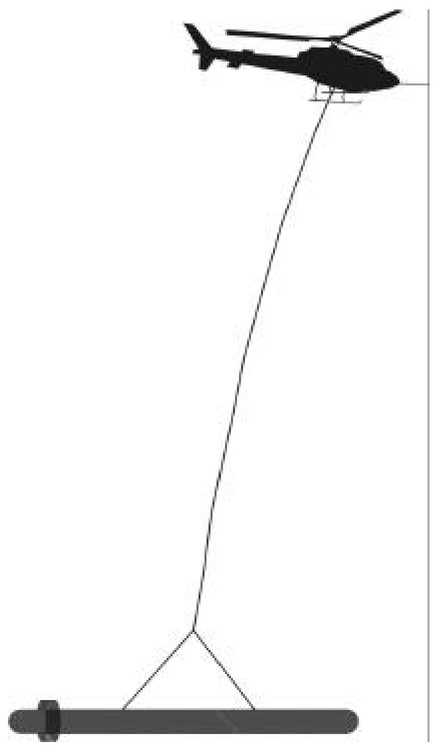
Report # 06041-1&3

DIGHEM SURVEY
FOR
HATHOR EXPLORATION LIMITED
ESKAY AREA BLOCKS 1&3,
NORTHWESTERN BRITISH COLUMBIA

NTS: 104A/5; 104B/8,9



Fugro Airborne Surveys Corp.
Mississauga, Ontario

Fugro Airborne Surveys, 2270 Argentia Road, Unit 2, Mississauga, Ontario, Canada, L5N 6A6
Phone: 1 905 812 0212, Fax: 1 905 812 1504

February 21, 2008

SUMMARY

This report describes the logistics, data acquisition, processing and presentation of results of a DIGHEM airborne geophysical survey carried out for Hathor Exploration Limited, over two properties located near Eskay Creek, British Columbia. Total coverage for Blocks 1 and 3 amounted to 800 km. The survey was flown from July 19th to September 5th, 2007.

The purpose of the survey was to detect zones of conductive mineralization, to locate zones of potassic alteration and to provide information that could be used to map the geology and structure of the survey areas. This was accomplished by using a DIGHEM multi-coil, multi-frequency electromagnetic system, supplemented by a high sensitivity cesium magnetometer, and a 256 channel spectrometer. The information from these sensors was processed to produce maps that display the magnetic, radiometric, and conductive properties of the survey areas. A GPS electronic navigation system ensured accurate positioning of the geophysical data with respect to the base maps.

The survey data were processed and compiled in the Fugro Airborne Surveys Toronto office. Map products and digital data were provided in accordance with the scales and formats specified in the Survey Agreement.

The survey properties contain several anomalous features, many of which are considered to be of moderate to high priority as exploration targets. Many of the inferred bedrock conductors appear to warrant further investigation using appropriate surface exploration

techniques. Areas of interest may be assigned priorities on the basis of supporting geophysical, geochemical and/or geological information. After initial investigations have been carried out, it may be necessary to re-evaluate the remaining anomalies based on information acquired from the follow-up program.

CONTENTS

APPENDICES

1. INTRODUCTION

A DIGHEM electromagnetic/resistivity/magnetic/radiometric survey was flown for Hathor Exploration Ltd., from July 19th to September 5th, 2007, over two survey blocks located near Eskay Creek, northwestern British Columbia. The survey areas can be located on NTS map sheets 104 A/5 and 104 B/8,9 (Figure 2).

Survey coverage consisted of approximately 800 line-km, including 78line-km of tie lines. Flight lines for Block 1 were flown in an azimuthal direction of 45°/225°, and flight lines for Block 3 were flown in an azimuthal direction of 90°/270°, both with a line separation of 150 metres. Tie lines were flown orthogonal to the traverse lines with a line separation of 1500 meters.

Summary of Line Km for Block 1 and Block 3

Block 1	439km
Block 3	361km

The survey employed the DIGHEM electromagnetic system. Ancillary equipment consisted of a magnetometer, radar and barometric altimeters, video camera, analog and digital recorders, a 256-channel spectrometer and an electronic navigation system. The instrumentation was installed in an AS350B3 turbine helicopter (Registration C-FQDA) that was provided by Great Slave Helicopters Ltd. The helicopter flew at an average airspeed of 90 km/h with an EM sensor height of approximately 30 metres. The spectrometer crystal package was housed within the helicopter, with a nominal terrain clearance of 58 metres.

In some portions of the survey areas, the steep topography forced the pilot to exceed normal terrain clearance for safety reasons. It is possible that some weak conductors may have escaped detection in areas where the bird height exceeded 120 m. In difficult areas where near-vertical climbs were necessary, the forward speed of the helicopter was reduced to a level that permitted excessive bird swinging. This problem, combined with the severe stresses to which the bird was subjected, gave rise to aerodynamic noise levels that are slightly higher than normal on some lines. Where warranted, reflights were carried out to minimize these adverse effects.

Figure 1: Fugro Airborne Surveys DIGHEM EM bird with AS350-B3

2. SURVEY OPERATIONS

The base of operations for the survey was established at Bell II Lodge, British Columbia.

The survey areas can be located on NTS map sheets 104A/5 and 104B/8,9(Figures 2a,2b).

Table 2-1 lists the corner coordinates of the survey areas in NAD83, UTM Zone 9 North, central meridian 129° West.

Table 2-1

Nad83 Utm Zone 9

Block	Corners	X-UTM (E)	Y-UTM (N)
06041-1	1	426810	6243319
Block 1	2	438144	6254553
	3	440723	6251951
	4	429389	6240717
06041-3	1	416243	6269766
Block 3	2	420093	6269662
	3	419752	6257064
	4	415902	6257168

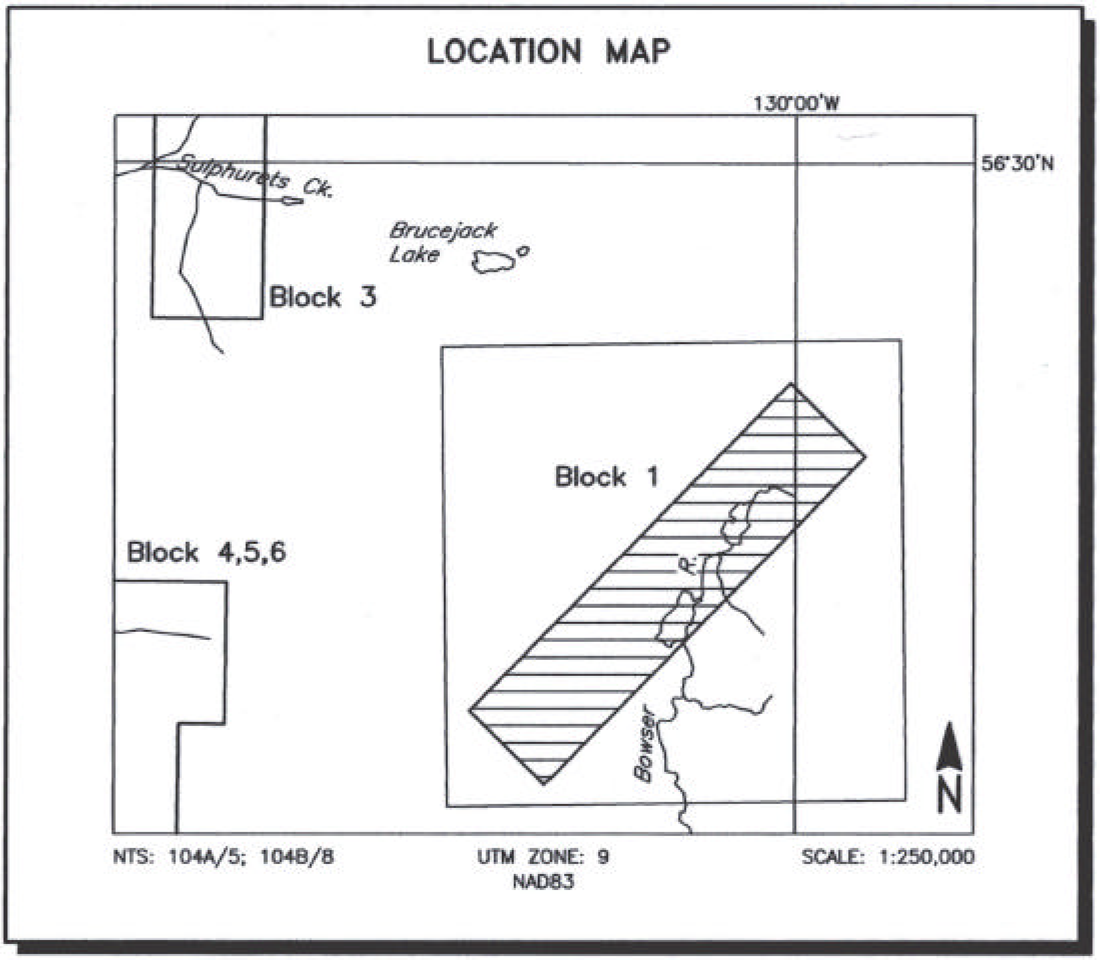


Figure 2a
Location Map and Sheet Layout
Eskay Claims Survey Area
Block 1
Job # 06041-1

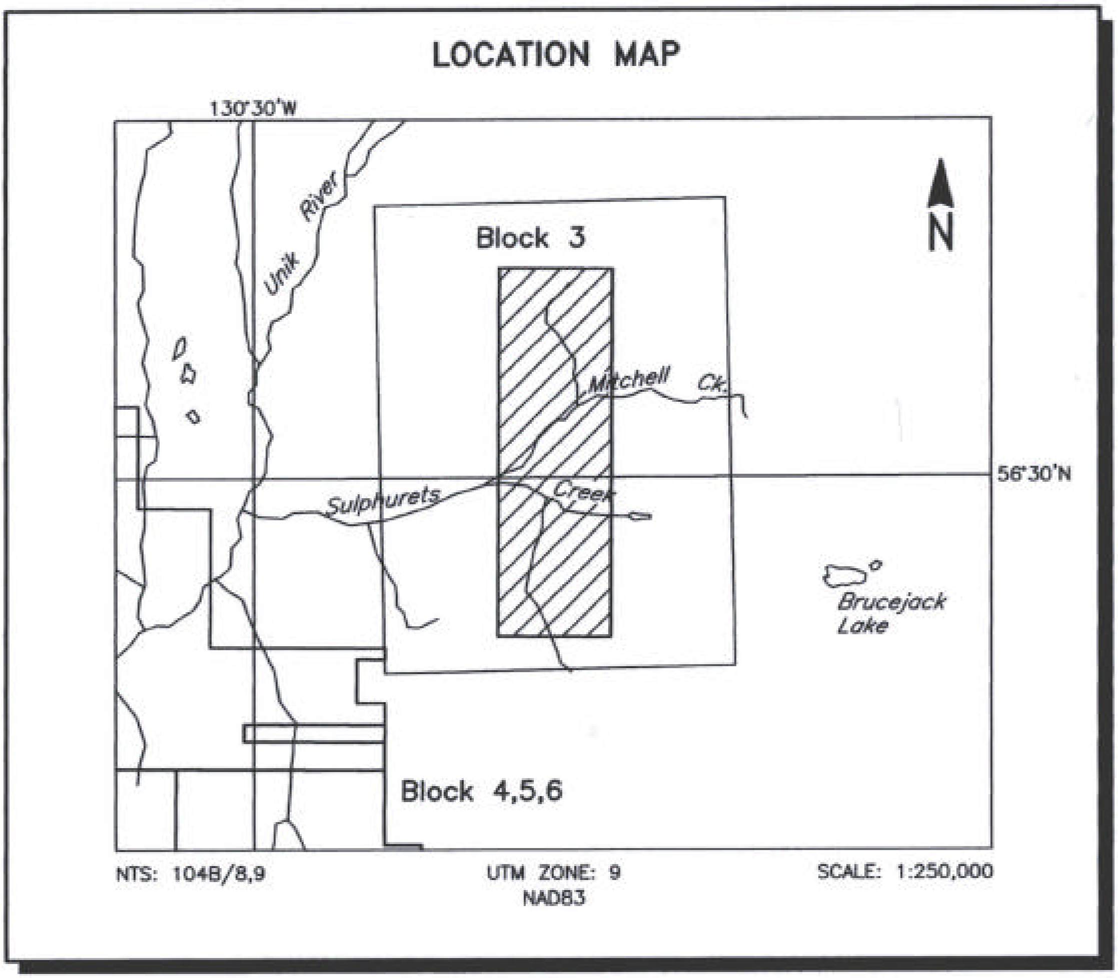


Figure 2b
Location Map and Sheet Layout
Eskay Claims Survey Area
Block 3
Job # 06041-3

The survey specifications were as follows:

Block 1

Parameter	Specifications
Traverse line direction	45°/225°
Traverse line spacing	150 m
Tie line direction	135°/315°,
Tie line spacing	1500 m
Sample interval	10 Hz, 2.5 m @ 90 km/h
Aircraft mean terrain clearance	58 m
EM sensor mean terrain clearance	30 m
Mag sensor mean terrain clearance	30 m
Spectrometer crystal pack	58 m
Average speed	77 km/h
Navigation (guidance)	±5 m, Real-time GPS
Post-survey flight path	±2 m, Differential GPS

Block 3

Parameter	Specifications
Traverse line direction	90°/270°
Traverse line spacing	150 m
Tie line direction	180°/360°,
Tie line spacing	1500 m
Sample interval	10 Hz, 2.5 m @ 90 km/h
Aircraft mean terrain clearance	58 m
EM sensor mean terrain clearance	30 m
Mag sensor mean terrain clearance	30 m
Spectrometer crystal pack	58 m
Average speed	60 km/h
Navigation (guidance)	±5 m, Real-time GPS
Post-survey flight path	±2 m, Differential GPS

3. SURVEY EQUIPMENT

This section provides a brief description of the geophysical instruments used to acquire the survey data and the calibration procedures employed. The geophysical equipment was installed in an AS350B3 helicopter. This aircraft provides a safe and efficient platform for surveys of this type.

Electromagnetic System

Model: DIGHEM V – BKS54

Type: Towed bird, symmetric dipole configuration operated at a nominal survey altitude of 30 metres. Coil separation is 8 metres for 900 Hz, 1000 Hz, 5500 Hz and 7200 Hz, and 6.3 metres for the 56,000 Hz coil-pair.

Coil orientations, frequencies and dipole moments

Atm^2	orientation		nominal	actual
211	coaxial	/	1000 Hz	1125 Hz
211	coplanar	/	900 Hz	875 Hz
67	coaxial	/	5500 Hz	5462 Hz
56	coplanar	/	7200 Hz	7150 Hz
15	coplanar	/	56,000 Hz	56400 Hz

Channels recorded:
5 in-phase channels
5 quadrature channels
2 monitor channels

Sensitivity:
0.06 ppm at 1000 Hz Cx
0.12 ppm at 900 Hz Cp
0.12 ppm at 5,500 Hz Cx
0.24 ppm at 7,200 Hz Cp
0.60 ppm at 56,000 Hz Cp

Sample rate:	10 per second, equivalent to 1 sample every 2.5 m, at a survey speed of 90 km/h.

The electromagnetic system utilizes a multi-coil coaxial/coplanar technique to energize conductors in different directions. The coaxial coils are vertical with their axes in the flight direction. The coplanar coils are horizontal. The secondary fields are sensed simultaneously by means of receiver coils that are maximum coupled to their respective transmitter coils. The system yields an in-phase and a quadrature channel from each transmitter-receiver coil-pair.

In-Flight EM System Calibration

Calibration of the system during the survey uses the Fugro AutoCal automatic, internal calibration process. At the beginning and end of each flight, and at intervals during the flight, the system is flown up to high altitude to remove it from any “ground effect” (response from the earth). Any remaining signal from the receiver coils (base level) is measured as the zero level, and is removed from the data collected until the time of the next calibration. Following the zero level setting, internal calibration coils, for which the response phase and amplitude have been determined at the factory, are automatically triggered – one for each frequency. The on-time of the coils is sufficient to determine an accurate response through any ambient noise. The receiver response to each calibration coil “event” is compared to the expected response (from the factory calibration) for both phase angle and amplitude, and any phase and gain corrections are automatically applied to bring the data to the correct value.

In addition, the outputs of the transmitter coils are continuously monitored during the survey, and the gains are adjusted to correct for any change in transmitter output. Because the internal calibration coils are calibrated at the factory (on a resistive halfspace) ground calibrations using external calibration coils on-site are not necessary for system calibration. A check calibration may be carried out on-site to ensure all systems are working correctly. All system calibrations will be carried out in the air, at sufficient altitude that there will be no measurable response from the ground.

The internal calibration coils are rigidly positioned and mounted in the system relative to the transmitter and receiver coils. In addition, when the internal calibration coils are calibrated at the factory, a rigid jig is employed to ensure accurate response from the external coils.

Using real time Fast Fourier Transforms and the calibration procedures outlined above, the data are processed in real time, from measured total field at a high sampling rate, to in-phase and quadrature values at 10 samples per second.

Airborne Magnetometer

Model:	Scintrex CS3 sensor
Type:	Optically pumped cesium vapour

Sensitivity: 0.01 nT

Sample rate: 10 per second

The magnetometer sensor was mounted inside the centre of the EM bird, 28 m below the helicopter.

Magnetic Base Station

Primary

Model: Fugro CF1 base station with timing provided by integrated GPS

Sensor type: Scintrex CS3

Counter specifications:	Accuracy:	±0.1 nT
	Resolution:	0.01 nT
	Sample rate	1 Hz
GPS specifications:	Model:	Marconi Allstar
	Type:	Code and carrier tracking of L1 band, 12-channel, C/A code at 1575.42 MHz
	Sensitivity:	-90 dBm, 1.0 second update
	Accuracy:	Manufacturer's stated accuracy for differential corrected GPS is 2 metres

Environmental
Monitor specifications: Temperature:

- Accuracy: ±1.5ºC max
- Resolution: 0.0305ºC
- Sample rate: 1 Hz
- Range: -40ºC to +75ºC

Barometric pressure:

- Model: Motorola MPXA4115A
- Accuracy: ±3.0º kPa max (-20ºC to 105ºC temp. ranges)
- Resolution: 0.013 kPa

- Sample rate: 1 Hz
- Range: 55 kPa to 108 kPa

<u>Backup</u>

Model:	GEM Systems GSM-19T
Type:	Digital recording proton precession
Sensitivity:	0.10 nT
Sample rate:	3 second intervals

A digital recorder is operated in conjunction with the base station magnetometer to record the diurnal variations of the earth's magnetic field. The clock of the base station is synchronized with that of the airborne system, using GPS time, to permit subsequent removal of diurnal drift. The Fugro CF1 was the primary magnetic base station. It was located at Bell II Lodge, at latitude 56°44'41.56093" N, longitude 129°47'45.88900" W, at an elevation of 554.6 metres above the ellipsoid.

Figure 3-1: Fugro CF1

Navigation (Global Positioning System)

Airborne Receiver for Real-time Navigation & Guidance

Model:	Novatel OEM IV.
Type:	Code and carrier tracking of L1-C/A code at 1575.42 MHz and L2-P code at 1227.0 MHz. Dual frequency, 24-channel.
Sample rate:	10 Hz update.
Accuracy:	Better than 1 metre in differential mode.
Antenna:	Aero AT1675 mounted on tail of aircraft

Primary Base Station for Post-Survey Differential Correction

Model:	Novatel OEM IV
Type:	Code and carrier tracking of L1-C/A code at 1575.42 MHz and L2-P code at 1227.0 MHz. Dual frequency, 24-channel.
Sample rate:	10 Hz update.
Accuracy:	Better than 1 metre in differential mode.

Secondary GPS Base Station

Model:	Marconi Allstar OEM, CMT-1200
Type:	Code and carrier tracking of L1 band, 12-channel, C/A code at 1575.42 MHz
Sensitivity:	-90 dBm, 1.0 second update
Accuracy:	Manufacturer’s stated accuracy for differential corrected GPS is 2 metres.

The Novatel OEM IV is a line of sight, satellite navigation system that utilizes time-coded signals from at least four of forty-eight available satellites. Both Russian GLONASS and American NAVSTAR satellite constellations are used to calculate the position and to provide real time guidance to the helicopter. A similar system was used as the primary base station receiver. The mobile and base station raw XYZ data were recorded, thereby permitting post-survey differential corrections for theoretical accuracies of better than 2 metres. A Marconi Allstar GPS unit, part of the CF-1, was used as a secondary (back-up) base station.

Each base station receiver is able to calculate its own latitude and longitude. For this survey, the primary GPS station was located at Bell II Lodge, latitude 56° 44' 42.776" N, longitude 129° 47' 45.547" W, at an elevation of 554.6 metres above the ellipsoid. The GPS records data relative to the WGS84 ellipsoid, which is the basis of the revised North American Datum (NAD83). Conversion software is used to transform the WGS84 coordinates to the NAD83 UTM system displayed on the maps.

Figure3-2: Fugro Primary GPS base station

Radar Altimeter

Manufacturer:	Sperry
Model:	RT220
Type:	Short pulse modulation, 4.3 GHz
Sensitivity:	0.3 m
Sample rate:	2 per second

The radar altimeter measures the vertical distance between the helicopter and the ground. This information is used in the processing algorithm that determines conductor depth.

Barometric Pressure and Temperature Sensors

Model:	DIGHEM D 1300	
Type:	Motorola MPX4115AP analog pressure sensor AD592AN high-impedance remote temperature sensors	
Sensitivity:	Pressure: Temperature:	150 mV/kPa 100 mV/°C or 10 mV/°C (selectable)
Sample rate:	10 per second	

The D1300 circuit is used in conjunction with one barometric sensor and up to three temperature sensors. Two sensors (baro and temp) are installed in the EM console in the aircraft, to monitor pressure (KPA), and internal (TEMP_INT) operating temperature. A third sensor is installed in the bird to monitor the external (TEMP_EXT) temperature.

Digital Data Acquisition System

Manufacturer:	Fugro
Model:	HeliDAS
Recorder:	Ultra II Compact Flash Memory Card

The stored data are downloaded to the field workstation PC at the survey base, for verification, backup and preparation of in-field products.

Video Flight Path Recording System

Type:	Panasonic WVCD322 Colour Video Camera
Recorder:	Axis 241S Video Server and Tablet Computer
Format:	Digital (*.BIN/*.BDX)

Fiducial numbers are recorded continuously and are displayed on the margin of each image. This procedure ensures accurate correlation of data with respect to visible features on the ground.

Spectrometer

Manufacturer:	Exploranium
Model:	GR-820
Type:	256 Multichannel, Potassium stabilized
Accuracy:	1 count/sec.
Update:	1 integrated sample/sec.

The GR-820 Airborne Spectrometer employs two downward looking crystals (1024 cu.in.-16.8 L) and one upward looking crystal (256 cu.in.- 4.2 L). The downward crystal records the radiometric spectrum from 410 KeV to 3 MeV over 256 discrete energy windows, as well as a cosmic ray channel, which detects photons with energy levels above 3.0 MeV. From these 256 channels, the standard Total Count, Potassium, Uranium and Thorium channels are extracted. The upward crystal is used to measure and correct for Radon.

The shock-protected Sodium Iodide (Thallium) crystal package is unheated, and is automatically stabilized with respect to the Thorium peak. The GR-820 provides raw or Compton stripped data that has been automatically corrected for gain, base level, ADC offset and dead time.

The system is calibrated before and after each flight using three accurately positioned hand-held sources. Additionally, fixed-site test lines are flown to determine if there are any differences in background. This procedure allows corrections to be applied to each survey flight, to eliminate any differences that might result from changes in temperature or humidity.

4. QUALITY CONTROL AND IN-FIELD PROCESSING

Digital data for each flight were transferred to the field workstation, in order to verify data quality and completeness. A database was created and updated using Geosoft Oasis Montaj and proprietary Fugro Atlas software. This allowed the field personnel to calculate, display and verify both the positional (flight path) and geophysical data on a screen or printer. Records were examined as a preliminary assessment of the data acquired for each flight.

In-field processing of Fugro survey data consists of differential corrections to the airborne GPS data, verification of EM calibrations, drift correction of the raw airborne EM data, spike rejection and filtering of all geophysical and ancillary data, verification of flight videos, calculation of preliminary resistivity data, diurnal correction, and preliminary leveling of magnetic data.

All data, including base station records, were checked on a daily basis, to ensure compliance with the survey contract specifications. Reflights were required if any of the following specifications were not met.

Navigation - Positional (x,y) accuracy of better than 10 m, with a CEP (circular error of probability) of 95%.

Flight Path	-	No lines to exceed ±25% departure from nominal line spacing over a continuous distance of more than 1 km, except for reasons of safety.
Clearance	-	Mean terrain sensor clearance of 30 m, ±10 m, except where precluded by safety considerations, e.g., restricted or populated areas, severe topography, obstructions, tree canopy, aerodynamic limitations, etc.
Airborne Mag	-	The non-normalized 4^{th} difference will not exceed 1.6 nT over a continuous distance of 1 kilometre excluding areas where this specification is exceeded due to natural anomalies.
Base Mag	-	Diurnal variations not to exceed 10 nT over a straight line time chord of 1 minute.
EM	-	Spheric pulses may occur having strong peaks but narrow widths. The EM data area considered acceptable when their occurrence is less than 10 spheric events exceeding the stated noise specification for a given frequency per 100 samples continuously over a distance of 2,000 metres.

Frequency	Coil Orientation	Peak to Peak Noise Envelope (ppm)
900 Hz	horizontal coplanar	10.0
1000 Hz	vertical coaxial	5.0
5500 Hz	vertical coaxial	10.0
7200 Hz	horizontal coplanar	20.0
56,000 Hz	horizontal coplanar	40.0

5. DATA PROCESSING

Flight Path Recovery

The raw range data from at least four satellites are simultaneously recorded by both the base and mobile GPS units. The geographic positions of both units, relative to the model ellipsoid, are calculated from this information. Differential corrections, which are obtained from the base station, are applied to the mobile unit data to provide a post-flight track of the aircraft, accurate to within 2 m. Speed checks of the flight path are also carried out to determine if there are any spikes or gaps in the data.

The corrected WGS84 latitude/longitude coordinates are transformed to the coordinate system used on the final maps. Images or plots are then created to provide a visual check of the flight path.

Electromagnetic Data

EM data are processed at the recorded sample rate of 10 samples/second. Sferic rejection median and Hanning filters are then applied to reduce noise to acceptable levels. EM test profiles are then created to allow the interpreter to select the most appropriate EM anomaly picking controls for a given survey area. The EM picking parameters depend on several factors but are primarily based on the dynamic range of the resistivities within the survey area, and the types and expected geophysical responses of the targets being sought.

Anomalous electromagnetic responses are selected and analysed by computer to provide a preliminary electromagnetic anomaly map. The automatic selection algorithm is intentionally oversensitive to assure that no meaningful responses are missed. Using the preliminary map in conjunction with the multi-parameter stacked profiles, the interpreter then classifies the anomalies according to their source and eliminates those that are not substantiated by the data. The final interpreted EM anomaly map includes bedrock, surficial and cultural conductors. A map containing only bedrock conductors can be generated, if desired.

Apparent Resistivity

The apparent resistivities in ohm-m are generated from the in-phase and quadrature EM components for all of the coplanar frequencies, using a pseudo-layer half-space model. The inputs to the resistivity algorithm are the in-phase and quadrature amplitudes of the secondary field. The algorithm calculates the apparent resistivity in ohm-m, and the apparent height of the bird above the conductive source. Any difference between the apparent height and the true height, as measured by the radar altimeter, is called the pseudo-layer and reflects the difference between the real geology and a homogeneous halfspace. This difference is often attributed to the presence of a highly resistive upper layer. Any errors in the altimeter reading, caused by heavy tree cover, are included in the pseudo-layer and do not affect the resistivity calculation. The apparent depth estimates, however, will reflect the altimeter errors. Apparent resistivities calculated in this manner may differ from those calculated using other models.

In areas where the effects of magnetic permeability or dielectric permittivity have suppressed the in-phase responses, the calculated resistivities will be erroneously high. Various algorithms and inversion techniques can be used to partially correct for the effects of permeability and permittivity.

Apparent resistivity maps portray all of the information for a given frequency over the entire survey area. This full coverage contrasts with the electromagnetic anomaly map, which provides information only over interpreted conductors. The large dynamic range afforded by the multiple frequencies makes the apparent resistivity parameter an excellent mapping tool.

The preliminary apparent resistivity maps and images are carefully inspected to identify any lines or line segments that might require base level adjustments. Subtle changes between in-flight calibrations of the system can result in line-to-line differences that are more recognizable in resistive (low signal amplitude) areas. If required, manual level adjustments are carried out to eliminate or minimize resistivity differences that can be attributed, in part, to changes in operating temperatures. These leveling adjustments are usually very subtle, and do not result in the degradation of discrete anomalies.

After the manual leveling process is complete, revised resistivity grids are created. The resulting grids can be subjected to a microleveling technique in order to smooth the data for contouring. The coplanar resistivity parameter has a broad 'footprint' that requires very little filtering.

The calculated resistivities for the 900 Hz, 7200 Hz and 56000 Hz coplanar frequencies are included in the XYZ and grid archives. Values are in ohm-metres on all final products.

Dielectric Permittivity and Magnetic Permeability Corrections[1]

In resistive areas having magnetic rocks, the magnetic and dielectric effects will both generally be present in high-frequency EM data, whereas only the magnetic effect will exist in low-frequency data.

The magnetic permeability is first obtained from the EM data at the lowest frequency, because the ratio of the magnetic response to conductive response is maximized and because displacement currents are negligible. The homogeneous half-space model is used. The computed magnetic permeability is then used along with the in-phase and quadrature response at the highest frequency to obtain the relative dielectric permittivity, again using the homogeneous half-space model. The highest frequency is used because the ratio of dielectric response to conductive response is maximized. The resistivity can

[1] Huang, H. and Fraser, D.C., 2001 Mapping of the Resistivity, Susceptibility, and Permittivity of the Earth Using a Helicopter-borne Electromagnetic System: Geophysics 106 pg 148-157.

then be determined from the measured in-phase and quadrature components of each frequency, given the relative magnetic permeability and relative dielectric permittivity.

Resistivity-depth Sections (optional)

The apparent resistivities for all frequencies can be displayed simultaneously as coloured resistivity-depth sections. Usually, only the coplanar data are displayed as the close frequency separation between the coplanar and adjacent coaxial data tends to distort the section. The sections can be plotted using the topographic elevation profile as the surface. The digital terrain values, in metres a.m.s.l., can be calculated from the GPS Z-value or barometric altimeter, minus the aircraft radar altimeter.

Resistivity-depth sections can be generated in three formats:

(1) Sengpiel resistivity sections, where the apparent resistivity for each frequency is plotted at the depth of the centroid of the in-phase current flow[2]; and,

(2) Differential resistivity sections, where the differential resistivity is plotted at the differential depth[3].

(3) Occam[4] or Multi-layer[5] inversion.

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[2] Sengpiel, K.P., 1988, Approximate Inversion of Airborne EM Data from Multilayered Ground: Geophysical Prospecting 36, 446-459.

[3] Huang, H. and Fraser, D.C., 1993, Differential Resistivity Method for Multi-frequency Airborne EM Sounding: presented at Intern. Airb. EM Workshop, Tucson, Ariz.

Both the Sengpiel and differential methods are derived from the pseudo-layer half-space model. Both yield a coloured resistivity-depth section that attempts to portray a smoothed approximation of the true resistivity distribution with depth. Resistivity-depth sections are most useful in conductive layered situations, but may be unreliable in areas of moderate to high resistivity where signal amplitudes are weak. In areas where in-phase responses have been suppressed by the effects of magnetite, or adversely affected by cultural features, the computed resistivities shown on the sections may be unreliable.

Both the Occam and multi-layer inversions compute the layered earth resistivity model that would best match the measured EM data. The Occam inversion uses a series of thin, fixed layers (usually 20 x 5m and 10 x 10m layers) and computes resistivities to fit the EM data. The multi-layer inversion computes the resistivity and thickness for each of a defined number of layers (typically 3-5 layers) to best fit the data.

Total Magnetic Field

A fourth difference editing routine was applied to the magnetic data to remove any spikes. The aeromagnetic data were corrected for diurnal variation using the magnetic base station data. The results were then leveled using tie and traverse line intercepts. Manual adjustments were applied to any lines that required leveling, as indicated by shadowed

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[4] Constable et al, 1987, Occam's inversion: a practical algorithm for generating smooth models from electromagnetic sounding data: Geophysics, 52, 289-300.

[5] Huang H., and Palacky, G.J., 1991, Damped least-squares inversion of time domain airborne EM data based on singular value decomposition: Geophysical Prospecting, 39, 827-844.

images of the gridded magnetic data. The manually leveled data were then subjected to a microleveling filter.

Calculated Vertical Magnetic Gradient

The diurnally-corrected total magnetic field data were subjected to a processing algorithm that enhances the response of magnetic bodies in the upper 500 m and attenuates the response of deeper bodies. The resulting vertical gradient map provides better definition and resolution of near-surface magnetic units. It also identifies weak magnetic features that may not be evident on the total field map. However, regional magnetic variations and changes in lithology may be better defined on the total magnetic field map.

EM Magnetite (optional)

The apparent percent magnetite by weight is computed wherever magnetite produces a negative in-phase EM response. This calculation is more meaningful in resistive areas.

Magnetic Derivatives (optional)

The total magnetic field data can be subjected to a variety of filtering techniques to yield maps or images of the following:

enhanced magnetics

second vertical derivative

reduction to the pole/equator

magnetic susceptibility with reduction to the pole

upward/downward continuations

analytic signal

All of these filtering techniques improve the recognition of near-surface magnetic bodies, with the exception of upward continuation. Any of these parameters can be produced on request.

Digital Elevation (optional)

The radar altimeter values (ALTR – aircraft to ground clearance) are subtracted from the differentially corrected and de-spiked GPS-Z values to produce profiles of the height above the ellipsoid along the survey lines. These values are gridded to produce contour maps showing approximate elevations within the survey area. The calculated digital terrain data are then tie-line leveled and adjusted to mean sea level. Any remaining subtle line-to-line discrepancies are manually removed. After the manual corrections are applied, the digital terrain data are filtered with a microleveling algorithm.

The accuracy of the elevation calculation is directly dependent on the accuracy of the two input parameters, ALTR and GPS-Z. The ALTR value may be erroneous in areas of heavy tree cover, where the altimeter reflects the distance to the tree canopy rather than the ground. The GPS-Z value is primarily dependent on the number of available satellites. Although post-processing of GPS data will yield X and Y accuracies in the order of 1-2 metres, the accuracy of the Z value is usually much less, sometimes in the ±10 metre range. Further inaccuracies may be introduced during the interpolation and gridding process.

Because of the inherent inaccuracies of this method, no guarantee is made or implied that the information displayed is a true representation of the height above sea level. Although this product may be of some use as a general reference, THIS PRODUCT MUST NOT BE USED FOR NAVIGATION PURPOSES.

Contour, Colour and Shadow Map Displays

The geophysical data are interpolated onto a regular grid using a modified Akima spline technique. The resulting grid is suitable for image processing and generation of contour maps. The grid cell size is 20% of the line interval.

Colour maps are produced by interpolating the grid down to the pixel size. The parameter is then incremented with respect to specific amplitude ranges to provide colour "contour" maps.

Monochromatic shadow maps or images are generated by employing an artificial sun to cast shadows on a surface defined by the geophysical grid. There are many variations in the shadowing technique. These techniques can be applied to total field or enhanced magnetic data, magnetic derivatives, resistivity, etc. The shadowing technique is also used as a quality control method to detect subtle changes between lines.

Multi-channel Stacked Profiles

Distance-based profiles of the digitally recorded geophysical data are generated and plotted at an appropriate scale. These profiles also contain the calculated parameters that are used in the interpretation process. These are produced as worksheets prior to interpretation, and are also presented in the final corrected form after interpretation. The profiles display electromagnetic anomalies with their respective interpretive symbols. Table 5-1 shows the parameters and scales for the multi-channel stacked profiles.

In Table 5-1, the log resistivity scale of 0.06 decade/mm means that the resistivity changes by an order of magnitude in 16.6 mm. The resistivities at 0, 33 and 67 mm up from the bottom of the digital profile are respectively 1, 100 and 10,000 ohm-m.

Table 5-1. Multi-channel Stacked Profiles

Channel Name (Freq)	Observed Parameters	Scale Units/mm
MAGF	total magnetic field (fine)	5 nT
MAGF	total magnetic field (coarse)	50 nT
ALTBIRDM	EM sensor height above ground	6 m
TC	Total Counts	50 cps
K	Potassium counts	10 cps
TH	Thorium counts	2 cps
U	Uranium counts	2 cps
CXI1000	vertical coaxial coil-pair in-phase (1000 Hz)	2 ppm
CXQ1000	vertical coaxial coil-pair quadrature (1000 Hz)	2 ppm
CPI900	horizontal coplanar coil-pair in-phase (900 Hz)	4 ppm
CPQ900	horizontal coplanar coil-pair quadrature (900 Hz)	4 ppm
CXI5500	vertical coaxial coil-pair in-phase (5500 Hz)	4 ppm
CXQ5500	vertical coaxial coil-pair quadrature (5500 Hz)	4 ppm
CPI7200	horizontal coplanar coil-pair in-phase (7200 Hz)	10 ppm
CPQ7200	horizontal coplanar coil-pair quadrature (7200 Hz)	10 ppm
CPI56K	horizontal coplanar coil-pair in-phase (56,000 Hz)	10 ppm
CPQ56K	horizontal coplanar coil-pair quadrature (56,000 Hz)	10 ppm
CXSP	coaxial spherics monitor	
	Computed Parameters	
DIFI (mid freq.)	difference function in-phase from CXI and CPI	5 ppm
DIFQ (mid freq.)	difference function quadrature from CXQ and CPQ	5 ppm
RES900	log resistivity	.06 decade
RES7200	log resistivity	.06 decade
RES56K	log resistivity	.06 decade
DEP900	apparent depth	6 m
DEP7200	apparent depth	6 m
DEP56K	apparent depth	6 m

Radiometrics

All radiometric data reductions performed by Fugro rigorously follow the procedures described in the IAEA Technical Report[6].

All processing of radiometric data was undertaken at the natural sampling rate of the spectrometer, i.e., one second. The data were not interpolated to match the fundamental 0.1 second interval of the EM and magnetic data.

The following sections describe each step in the process.

Pre-filtering

The radar altimeter data were processed with a 15-point median filter to remove spikes.

Reduction to Standard Temperature and Pressure

The radar altimeter data were converted to effective height (h_e) in feet using the acquired temperature and pressure data, according to the following formula:

[6] Exploranium, I.A.E.A. Report, Airborne Gamma-Ray Spectrometer Surveying, Technical Report No. 323, 1991.

$$h_e = h * \frac{273.15}{T + 273.15} * \frac{P}{1013.25}$$

where: *h* is the observed crystal to ground distance in feet

T is the measured air temperature in degrees Celsius

P is the barometric pressure in millibars

Live Time Correction

The spectrometer, an Exploranium GR-820, uses the notion of "live time" to express the relative period of time the instrument was able to register new pulses per sample interval. This is the opposite of the traditional "dead time", which is an expression of the relative period of time the system was unable to register new pulses per sample interval.

The GR-820 measures the live time electronically, and outputs the value in milliseconds. The live time correction is applied to the total count, potassium, uranium, thorium, upward uranium and cosmic channels. The formula used to apply the correction is as follows:

$$C_{lt} = C_{raw} * \frac{1000.0}{L}$$

where: C_{lt} is the live time corrected channel in counts per second

C_{raw} is the raw channel data in counts per second

L is the live time in milliseconds

Intermediate Filtering

Two parameters were filtered, but not returned to the database:

- Radar altimeter was smoothed with a 3-point Hanning filter (h_{ef}).
- The Cosmic window was smoothed with a 9-point Hanning filter (Cos_f).

Aircraft and Cosmic Background

Aircraft background and cosmic stripping corrections were applied to the total count, potassium, uranium, thorium and upward uranium channels using the following formula:

$$C_{ac} = C_{lt} - (a_c + b_c * \mathrm{Cos}_f)$$

where: C_{ac} is the background and cosmic corrected channel

C_{lt} is the live time corrected channel

a_c is the aircraft background for this channel

b_c is the cosmic stripping coefficient for this channel

Cos_f is the filtered Cosmic channel

Radon Background

The determination of calibration constants that enable the stripping of the effects of atmospheric radon from the downward-looking detectors through the use of an upward-looking detector is divided into two parts:

1) Determine the relationship between the upward- and downward-looking detector count rates for radiation originating from the ground.

2) Determine the relationship between the upward- and downward-looking detector count rates for radiation due to atmospheric radon.

The procedures to determine these calibration factors are documented in IAEA Report #323 on airborne gamma-ray surveying. The calibrations for the first part were determined as outlined in the report.

The latter case normally requires many over-water measurements where there is no contribution from the ground. Where this is not possible, it is standard procedure to establish a test line over which a series of repeat measurements are acquired. From these repeat flights, any change in the downward uranium window due to variations in radon background would be directly related to variations in the upward window and the other downward windows.

The validity of this technique rests on the assumption that the radiation from the ground is essentially constant from flight to flight. Inhomogeneities in the ground, coupled with deviations in the flight path between test runs, add to the inaccuracy of the accumulated results. Variations in flying heights and other environmental factors also contribute to the uncertainty.

The use of test lines is a common solution for a fixed-wing acquisition platform. The ability of rotary wing platforms to hover at a constant height over a fixed position eliminates a number of the variations which degrade the accuracy of the results required for this calibration.

A test site was established in or near the survey area. The tests were carried out at the start and end of each day, and at the end of each flight. Data were acquired over a four-minute period at the nominal survey altitude (60 m). The data were then corrected for live time, aircraft background and cosmic activity.

Once the survey was completed, the relationships between the counts in the downward uranium window and in the other four windows due to atmospheric radon were determined using linear regression for each of the hover sites. The following equations were used:

$$u_r = a_u Ur + b_u$$

$$K_r = a_K U_r + b_K$$

$$T_r = a_T U_r + b_T$$

$$I_r = a_I U_r + b_I$$

where: u_r is the radon component in the upward uranium window

K_r, U_r, T_r and I_r are the radon components in the various windows of the downward detectors

the various "a" and "b" coefficients are the required calibration constants

In practice, only the "a" constants were used in the final processing. The "b" constants, which are normally near zero for over-water calibrations, were of no value as they reflected the local distribution of the ground concentrations measured in the five windows.

Compton Stripping

Following the radon correction, the potassium, uranium and thorium are corrected for spectral overlap. First, α,β and γ the stripping ratios, are modified according to altitude. Then an adjustment factor based on a, the reversed stripping ratio, uranium into thorium, is calculated. (Note: the stripping ratio altitude correction constants are expressed in change per metre. A constant of 0.3048 is required to conform to the internal usage of height in feet):

$$\alpha_h = \alpha + h_{ef} * 0.00049$$

$$\alpha_r = \frac{1.0}{1.0 - a * \alpha_h}$$

$$\beta_h = \beta + h_{ef} * 0.00065$$

$$\gamma_h = \gamma + h_{ef} * 0.00069$$

where: α, β, γ are the Compton stripping coefficients

α_h, β_h, γ_h are the height corrected Compton stripping coefficients

h_{ef} is the height above ground in metres

α_r is the scaling factor correcting for back scatter

a is the reverse stripping ratio

The stripping corrections are then carried out using the following formulas:

$$Th_c = (Th_{rc} - a * U_{rc}) * \alpha_r$$

$$K_c = K_{rc} - \gamma_h * U_c - \beta_h * Th_c$$

$$U_c = (U_{rc} - \alpha_h * Th_{rc}) * \alpha_r$$

where: U_c, Th_c and K_c are corrected uranium, thorium and potassium

α_h, β_h, γ_h are the height corrected Compton stripping coefficients

U_{rc}, Th_{rc} and K_{rc} are radon-corrected uranium, thorium and potassium

α_r is the backscatter correction

Attenuation Corrections

The total count, potassium, uranium and thorium data are then corrected to a nominal survey altitude, in this case 200 feet. This is done according to the equation:

$$C_a = C * e^{m(h_{ef} - ho)}$$

where: C_a is the output altitude corrected channel

C is the input channel

e^{μ} is the attenuation correction for that channel

h_{ef} is the effective altitude

h_0 is the nominal survey altitude to correct to

6. PRODUCTS

This section lists the final maps and products that have been provided under the terms of the survey agreement. Other products can be prepared from the existing dataset, if requested. These include magnetic enhancements or derivatives, percent magnetite, resistivities corrected for magnetic permeability and/or dielectric permittivity, digital terrain, resistivity-depth sections, inversions, and overburden thickness. Most parameters can be displayed as contours, profiles, or in colour.

Base Maps

Base maps of the survey area were produced by scanning published topographic maps to a bitmap (.bmp) format. This process provides a relatively accurate, distortion-free base that facilitates correlation of the navigation data to the map coordinate system. The topographic files were combined with geophysical data for plotting the final maps. All maps were created using the following parameters:

Projection Description:

Datum:	NAD 83
Ellipsoid:	GRS80
Projection:	UTM (Zone: 9 North)
Central Meridian:	129 ° West
False Northing:	0
False Easting:	500000
Scale Factor:	0.9996
WGS84 to Local Conversion:	Molodensky
Datum Shifts:	DX: 0 DY: 0 DZ: 0

The following parameters are presented on 2 separate map sheets, at a scale of 1:20,000. All maps include flight lines and topography, unless otherwise indicated. Preliminary products are not listed.

Final Products

	No. of Map Sets		
	Mylar	Blackline	Colour
EM Anomalies		2 x 2	
Total Magnetic Field			2 x 2
Calculated Vertical Magnetic Gradient			2 x 2
Apparent Resistivity 7200 Hz			2 x 2
Apparent Resistivity 56,000 Hz			2 x 2
Radiometrics - Total Count			2 x 2
- Potassium			2 x 2
- Uranium			2 x 2
- Thorium			2 x 2

<u>Additional Products</u>

Digital Archive (see Archive Description)	1 CD-ROM
Survey Report	2 copies
Multi-channel Stacked Profiles	All lines
Flight Path Video (DVD)	9 DVDs

7. SURVEY RESULTS

General Discussion

Tables 7-1 through 7-2 summarize the EM responses in the two survey areas, with respect to conductance grade and interpretation. The apparent conductance and depth values shown in the EM Anomaly lists appended to this report have been calculated from “local” in-phase and quadrature amplitudes of the Coaxial 5500 Hz frequency. The picking and interpretation procedure relies on several parameters and calculated functions. For this survey, the Coaxial 5500 Hz responses and the mid-frequency difference channels were used as two of the main picking criteria. The 7200 Hz coplanar results were also weighted to provide picks over wider or flat-dipping sources. The quadrature channels provided picks in areas where the in-phase responses might have been suppressed by magnetite.

The anomalies shown on the electromagnetic anomaly maps are based on a near-vertical, half plane model. This model best reflects "discrete" bedrock conductors. Wide bedrock conductors or flat-lying conductive units, whether from surficial or bedrock sources, may give rise to very broad anomalous responses on the EM profiles. These may not appear on the electromagnetic anomaly map if they have a regional character rather than a locally anomalous character.

TABLE 7-1 EM ANOMALY STATISTICS

ESKAY BLOCK 1

CONDUCTOR GRADE	CONDUCTANCE RANGE SIEMENS (MHOS)	NUMBER OF RESPONSES
7	>10	3
6	50 - 100	1
5	20 - 50	2
4	10 - 20	6
3	5 - 10	18
2	1 - 5	254
1	<1	275
INDETERMINATE		43
TOTAL		602

CONDUCTOR MODEL	MOST LIKELY SOURCE	NUMBER OF RESPONSES
D	DISCRETE BEDROCK CONDUCTOR	97
B	DISCRETE BEDROCK CONDUCTOR	195
S	CONDUCTIVE COVER	64
H	ROCK UNIT OR THICK COVER	197
E	EDGE OF WIDE CONDUCTOR	47
L	CULTURE	2
TOTAL		602

(SEE EM MAP LEGEND FOR EXPLANATIONS)

TABLE 7-2 EM ANOMALY STATISTICS

ESKAY BLOCK 3

CONDUCTOR GRADE	CONDUCTANCE RANGE SIEMENS (MHOS)	NUMBER OF RESPONSES
7	>100	4
6	50 - 100	1
5	20 - 50	18
4	10 - 20	40
3	5 - 10	110
2	1 - 5	380
1	<1	134
*	INDETERMINATE	45
TOTAL		732

CONDUCTOR MODEL	MOST LIKELY SOURCE	NUMBER OF RESPONSES
D	DISCRETE BEDROCK CONDUCTOR	291
B	DISCRETE BEDROCK CONDUCTOR	252
S	CONDUCTIVE COVER	21
H	ROCK UNIT OR THICK COVER	137
E	EDGE OF WIDE CONDUCTOR	31
L	CULTURE	0
TOTAL		732

(SEE EM MAP LEGEND FOR EXPLANATIONS)

These broad conductors, which more closely approximate a half-space model, will be maximum coupled to the horizontal (coplanar) coil-pair and should be more evident on the resistivity parameter. Resistivity maps, therefore, may be more valuable than the electromagnetic anomaly maps, in areas where broad or flat-lying conductors are considered to be of importance. Contoured resistivity maps, based on the 7200 Hz and 56kHz coplanar data are included with this report.

Excellent resolution and discrimination of conductors was accomplished by using a fast sampling rate of 0.1 sec and by employing a “common” frequency (5500/7200 Hz) on two orthogonal coil-pairs (coaxial and coplanar). The resulting difference channel parameters often permit differentiation of bedrock and surficial conductors, even though they may exhibit similar conductance values.

Anomalies that occur near the ends of the survey lines (i.e., outside the survey area), should be viewed with caution. Some of the weaker anomalies could be due to aerodynamic noise, i.e., bird bending, which is created by abnormal stresses to which the bird is subjected during the climb and turn of the aircraft between lines. Such aerodynamic noise is usually manifested by an anomaly on the coaxial in-phase channel only, although severe stresses can affect the coplanar in-phase channels as well.

Magnetics

A Fugro CF-1 cesium vapour magnetometer was operated at the survey base to record diurnal variations of the earth's magnetic field. The clock of the base station was synchronized with that of the airborne system to permit subsequent removal of diurnal drift.

The total magnetic field data have been presented as contours on the base maps using a contour interval of 5 nT where gradients permit. The maps show the magnetic properties of the rock units underlying the survey areas.

The total magnetic field data have been subjected to a processing algorithm to produce maps of the calculated vertical gradient. This procedure enhances near-surface magnetic units and suppresses regional gradients. It also provides better definition and resolution of magnetic units and displays weak magnetic features that may not be clearly evident on the total field maps.

There is some evidence on the magnetic maps that suggests that the survey areas have been subjected to deformation and/or alteration. These structural complexities are evident on the contour maps as variations in magnetic intensity, irregular patterns, and as offsets or changes in strike direction. If a specific magnetic intensity can be assigned to the rock type that is believed to host the target mineralization, it may be possible to select areas of higher priority on the basis of the total field magnetic data. This is based on the assumption that the magnetite content of the host rocks will give rise to a limited range of contour values that will permit differentiation of various lithological units.

The magnetic results, in conjunction with the other geophysical parameters, have provided valuable information that can be used to effectively map the geology and structure in the survey areas.

Apparent Resistivity

Apparent resistivity maps, which display the conductive properties of the survey areas, were produced from the 7200 Hz and 56,000 Hz coplanar data. The maximum resistivity values, which are calculated for each frequency, are 8,000 and 20,000 ohm-m respectively. These cutoffs eliminate the erratic higher resistivities that would result from unstable ratios of very small EM amplitudes.

In general, the resistivity patterns show moderately poor agreement with the magnetic trends. This suggests that at least some of the resistivity lows are probably related to conductive cover in the valleys, rather than bedrock sources. However, most of the stronger lows are obviously due to bedrock conductors that vary from thin discrete sources to broader flat-dipping units.

Several resistivity highs are due to glacial cover, resistive rock units, or excessive flying heights, while others are at least partially due to magnetic suppression.

Electromagnetic Anomalies

The EM anomalies resulting from this survey appear to fall within one of three general categories. The first type consists of discrete, well-defined anomalies that yield marked inflections on the difference channels. These anomalies are usually attributed to conductive sulphides or graphite and are generally given a "B", "T" or "D" interpretive symbol, denoting a bedrock source.

The second class of anomalies comprises moderately broad responses that exhibit the characteristics of a half-space and do not yield well-defined inflections on the difference channels. Anomalies in this category are usually given an "S" or "H" interpretive symbol. The lack of a difference channel response usually implies a broad or flat-lying conductive source such as overburden. Some of these anomalies could reflect conductive rock units, zones of deep weathering, the weathered tops of plugs or pipes, or broad alteration zones, all of which can yield “non-discrete” signatures.

The effects of conductive overburden are evident over portions of the survey areas. Although the difference channels (DIFI and DIFQ) are extremely valuable in detecting bedrock conductors that are partially masked by conductive overburden, sharp undulations in the bedrock/overburden interface can yield anomalies in the difference channels which may be interpreted as possible bedrock conductors. Such anomalies usually fall into the "S?" or "B?" classification but may also be given an "E" interpretive symbol, denoting a resistivity contrast at the edge of a conductive unit.

The "?" symbol does not question the validity of an anomaly, but instead indicates some degree of uncertainty as to which is the most appropriate EM source model. This ambiguity results from the combination of effects from two or more conductive sources, such as overburden and bedrock, gradational changes, or moderately shallow dips. The presence of a conductive upper layer has a tendency to mask or alter the characteristics of bedrock conductors, making interpretation difficult. This problem is further exacerbated in the presence of magnetite.

The third anomaly category includes responses that are associated with magnetite. Magnetite can cause suppression or polarity reversals of the in-phase components, particularly at the lower frequencies in resistive areas. The effects of magnetite-rich rock units are usually evident on the multi-parameter geophysical data profiles as negative excursions of the lower frequency in-phase channels. These are evident primarily on Block 8.

In areas where EM responses are evident primarily on the quadrature components, zones of poor conductivity are indicated. Where these responses are coincident with magnetic anomalies, it is possible that the in-phase component amplitudes have been suppressed by the effects of magnetite. Poorly-conductive magnetic features can give rise to resistivity anomalies that are only slightly below or slightly above background. If it is expected that poorly-conductive economic mineralization could be associated with magnetite-rich units, most of these weakly anomalous features will be of interest. In areas where magnetite causes the in-phase components to become negative, the apparent conductance and depth of EM anomalies will be unreliable. Magnetite effects usually give rise to overstated (higher) resistivity values and understated (shallow) depth calculations.

As potential targets within the area may be associated with massive to weakly disseminated sulphides, which may or may not be hosted by magnetite-rich rocks, it is impractical to assess the relative merits of EM anomalies on the basis of conductance. It is recommended that an attempt be made to compile a suite of geophysical "signatures" over any known areas of interest. Anomaly characteristics are clearly defined on the multi-parameter geophysical data profiles that are supplied as one of the survey products.

Potential Targets in the Survey Areas

The electromagnetic anomaly maps show the anomaly locations with the interpreted conductor type, dip, conductance and depth being indicated by symbols. Direct magnetic correlation is also shown if it exists. The strike direction and length of the conductors are indicated only where anomalies can be correlated from line to line with a reasonable degree of confidence.

In areas where several conductors or conductive trends appear to be related to a common geological unit, these have been outlined as "zones" on the EM anomaly maps. The zone outlines usually approximate the limits of conductive units defined by the 7200 Hz resistivity contours.

Although zones of massive sulphide mineralization on the property should yield a distinct EM anomaly, any disseminated (porphyry) zones might not be conductive or resistive enough to enough to exhibit a well-defined contrast with the surrounding units. At least some of the porphyry deposits in B.C. yield relative resistivity highs, rather than lows. The Mt. Milligan deposit is one such example. The Mt. Milligan zone also hosts three areas of slightly elevated magnetic susceptibility. Therefore, any plug-like resistive units in the project areas should obviously be considered potential targets, particularly those that exhibit weak to moderate magnetic correlation.

Any vein-type mineralization on the properties may not be conductive enough to override the opposing effects of the more resistive quartz-carbonate host, and would be unlikely to yield resistivity lows. However, if the unweathered quartz-rich units are thick enough, it is possible that they could give rise to relative resistivity highs. Conversely, faults and shear zones can often be moderately conductive due to the increased porosity or development of alteration products. Because of these factors, it is impractical to assess the relative merits of EM anomalies on the basis of conductance. It is recommended that an attempt be made to compile a suite of geophysical "signatures" over any known areas of interest. Anomaly characteristics are clearly defined on the multi-parameter geophysical data profiles that are supplied as one of the survey products.

It is beyond the scope of this report to attempt to describe the 1334 anomalies detected by the survey. The following paragraphs provide a very brief description of some of the more discrete (sulphide-type) conductors, and a few other responses that appear to be associated with possible faults, shears or non-magnetic intrusions that can be inferred from the magnetic data. The discussion does not include any of the plug-like resistive or weakly conductive units that could reflect porphyritic intrusions. These larger zones should be more evident on the high frequency resistivity map.

Many of the magnetite associated responses also give rise to resistivity highs. These are usually evident on the low frequency 900Hz profiles as negative excursions of the in-phase component. If these negatives correlate with anomalous (positive) responses on the quadrature parameter or high frequencies, they often carry an “S?” symbol. However, they could reflect skarn-type mineralization, rather than conductive overburden.

Block 1

Magnetic relief varies from a low of 56,360 nT to a high of more than 57,210 nT. The southwestern half of the property exhibits lower susceptibilities than the units to the northeast. The magnetic amplitudes underlying the Frank Mackie Glacier in the southwest have been suppressed by the increased thickness of the overlying ice. This smoothness is also evident in the northeast, under the Knipple Glacier. However, the more erratic magnetic values in the west central region suggest that the icefield in this area is probably much thinner than those in the northeast and southwest.

There is very little direct correlation between magnetic units and resistivity patterns except for the general indirect correlation in between the relative magnetic lows and high resistivities associated with the ice-covered areas. Magnetic trends suggest the area is underlain by rather complex geology, with linear magnetic trends varying in the strike from east to south-southeast.

Although the Bowser River valley is moderately conductive, there are at least five highly conductive zones on the property that comprise broad half-space type conductive units. These have been outlined on the EM Anomaly Map as Zones A through F. The zone outlines approximate the 250 ohm-m contour taken from the 7200 Hz resistivity maps. These flat lying zones host several discrete conductors that reflect thinner, more vertical bedrock sources. Dips are variable, and sometimes appear to reflect synclinal or anticlinal structures with converging or opposing dips, as indicated by 10150 E and 10150 G, 10150 K and 10150 L, and 10230 B and 10230 E.

Most of these conductive zones are close to surface, but the low frequency results show that they often continue at depth beneath the glaciers, or into the hillside. One such example is evident southwest of anomaly 10180 A, where the 900 Hz coplanar channel indicates that the source continues to a depth of more that 120 m, beneath the Frank Mackie Glacier.

Nearly all of the bedrock conductors on this block are contained within one of the six main conductive zones. Although, most of the discrete sources appear to exhibit strikes towards the southeast, no attempt has been made to correlate conductor axes from line to line, because of the close proximity of the multi-conductor sources and the apparent inconsistencies in the magnetic correlation.

Many of the anomalous responses reflect broad buried sources that have been attributed to conductive, flat-dipping zones, some of which increase in conductance at depth. Others clearly define thin sources, many of which are quite close to surface.

No attempt has been made to assess the relative importance of the numerous conductors on the property. The following paragraphs describe one or more conductor types that give rise to, or are contained within, the main conductive zones outlined on the EM Anomaly map.

Zone A occurs near the southeastern edge of the Frank Mackie Glacier. On line 10240, at least five separate thin sources have been defined. Although the conductor proximity precludes accurate dip estimates, there is an indication that conductors 10240 A and E show converging dips to the NE and SW respectively. With the possible exception of 10230 C, nearly all of the conductors in this zone are non-magnetic. The most conductive portion is near 10240 C, where resistivity values of less than 6 ohm-m have been observed.

Zone B is a broad resistivity low located north of the Frank Mackie Glacier. Most of the anomalies comprising this zone have been attributed to discrete bedrock sources, although there are a few that indicate broad buried units. Nearly all of the conductors in Zone B are non-magnetic, and generally exhibit strikes towards the southeast. Dips vary from NE to SW.

Within this zone, there are a few "pods" of highly conductive material as indicated by the resistivity lows associated with anomalies 10060 I, 10060 N, 10090 H, 10150 D and 10170 H. All of these appear to be very close to surface.

Zone C closely follows the area covered by a lake and has been attributed primarily to conductive lake bottom material. However, anomalies 10200 C, 10200 H, 10220 D, 10220 G and 10230 F all yield direct magnetic correlation. In addition, anomalies 10220 D and 10230 F are on land, beyond the southwestern shore of the lake. Anomaly 10200 I occurs at the contact of a magnetite rich zone while 10230 G overlies, or is contained within, a magnetic unit.

The western lobe of Zone D occurs within a lake, and could be due to conductive lake bottom material. However the resistivity low is on strike with Zone E and could be a SW continuation of this unit. The eastern lobe of Zone D hosts broad, half-space type anomalies in the south, with more discrete thinner sources in the north, between 10150 K and 10250 O. This zone remains open to the east and southeast.

Dips, where indicated, are towards the SW, as indicated by anomalies 10150 L, 10170 P, 10190 M, 10230 K and 10250 O. However, anomaly 10150 K suggests a think source with a probable dip to the NE, opposite to that for 10150 L. The most conductive portions of this zone are near 10150 K, 10210 H and 10240 H.

Zone E is located southwest of the Knipple Glacier. This complex resistivity low hosts both broad sources and more discrete thinner conductors. Dips are generally towards the southwest, although there are exceptions at 10100 R and 10120 S. All of the conductors in this zone are non-magnetic except for 10170 S. However, there is a moderately strong magnetic high near the SW edge of the glacier near 10120 U. Anomaly 10160 X, to the SW of the conductive zone, also yields a direct magnetic correlation of 138 nT. This very sharp EM anomaly, that is coincident with a well-defined dipolar magnetic response, suggests the presence of a cultural object near surface. A check of the video for flight 8, at fiducial 4534, did not reveal any visible cultural cause. Therefore this is considered to be a small, but very attractive anomaly that should be investigated.

The most conductive portion of Zone E is at its eastern edge, along the western margin of the Knipple Glacier. Resistivity values of less than 25 ohm-m are not uncommon between anomalies 10020 W and 10100 W. The most conductive portions are near 10030 AB, 10050 AE and 10060 AC, where the conductors appear to be due to thin SW-dipping sources that are very close to surface.

This Zone hosts one or two main conductors, although as many as seven separate sources are indicated on line 10100 from 10100 R to 10100 Y. At the western edge of Zone E, most of the anomalous responses between 10040 L and 10070 N indicate probable dips to northeast, suggesting the possibility of a synclinal or basin shaped structure.

Zone F is a strong, well-defined resistivity low that abuts the eastern edge of the Knipple Glacier. This zone hosts at least two thin conductors and is open to the east, beyond the limits of the survey block. This zone is relatively non-magnetic, but it occurs east of a strong dipolar magnetic anomaly that underlies the central axis of the Knipple Glacier. Dips appear to be towards the northeast, opposite to those observed in Zone E on the southwest edge of the glacier. Resistivities of less than 15 ohm-m are observed at the property boundary, near anomaly 10180 U.

The two strong anomalies at 10210 K and 10220 O are due to metal culverts under the road, as indicated on the flight video.

There are a few other anomalous responses on the property that occur as weak or isolated responses that lie outside of the limits of the six main conductive zones. Anomalies 10250 A and 10250 I are two such examples. Anomaly 10250 A is extremely weak and non-magnetic and lies in close proximity to a creek. Anomaly 10250 I, however, is much stronger. This response indicates a thin SW–dipping conductor located near a magnetic contact. It is considered to be a moderately attractive target that could continue to the southeast, beyond the limits of the current survey coverage.

Block 3

Block 3 covers an area of moderately low topographic relief near the confluence of McTagg Creek, Gingras Creek, Mitchell Creek, Sulphurets Creek and a fifth creek that flows north in the southern portion of the property. Resistivity patterns at the higher frequencies show a general correlation with the main valleys, and appear to be partially caused by weakly conductive alluvial material. However, the lower frequency (900 Hz) resistivity shows a south-trending conductive zone that is not restricted to the main valleys in the northern half of the property.

South of line 30400, the 900 Hz resistivity shows five or more parallel bands of conductive material that strike south-southeast. Most of these bands are associated with a zone of relatively low magnetic susceptibility that dominates the central and southern portions of the property. However the vertical gradient map shows that the southernmost conductive zone, through anomaly30710C, appears to correlate with a weak magnetic high, south of line 30700. Nearly all of the other conductive zones are associated with relatively non-magnetic units.

The conductive zones outlines shown on the EM Anomaly Map approximate the 250 ohm-m contour taken from the 7200 Hz resistivity maps. These conductive zones underlie nearly 50 % of the property.

It is difficult to determine which anomalies within these multi-conductor zones might be of greater interest. If there are any known zones of mineralization on the property, the geophysical profiles over these areas should be analysed, in order to determine their geophysical signatures. If no such information is available, higher priorities might be assigned to the more discrete responses that yield magnetic correlation, or appear to be related to contacts or zones of structural deformation.

Zone A comprises three main S-trending sub-parallel bands, each of which hosts from one to three distinct conductors. Although it is difficult to determine dip directions from closely-spaced thin sources, it is evident that dips vary between conductors and along strike. Opposing or converging dips are indicated between 30050 C and 30050 E, 30070 D and 30070 I, 30240A and 30240 D, 30590 A and 30590 C, 30620 A and 30620 D and 30700 G and 30700 H.

The main conductor axes in Zones A1 and A2 generally follow the contacts of the central magnetic low that dominates the north-central portion of the property. Most of the conductors are non-magnetic, although roughly 10% of the anomalous responses yield apparent magnetic correlation. Examples include 30040 H, 30420 E, 30450 G, 30540 H, 30570 B, 30620 A, 30750 D and 30840 E. These anomalies are more likely to host magnetic sulphides, rather than graphite only.

Any anomalous responses that appear to be related to probable contacts, faults, folds, or non-magnetic intrusions, are also considered to be of higher priority than those that are not. These contact-related features are evident on the vertical gradient map. Some of the conductors that are in close proximity to inferred structural breaks, include 30110 D, 30130 B, 30170 F, 30180 I, 30210 A, 30220 H, 30250 F, 30300 G, 30330 E, 30340 E, 30360 D, 30460 F, 30460 G, 30470 D, 30550 C, 30580 G, 30600 G, 30630 D, 30630 H, 30710 B, 30730 G and 30740 A.

If conductance can be used as a criterion for locating areas of interest, the following anomalies yield resistivity lows that suggest local concentrations of conductive material: 30010 G, 30040 H, 30090 J, 30120 D, 30140 A, 30180 B, 30250 H, 30260 A, 30270 H, 30300 C, 30320 E, 30360 E, 30370 B, 30430 B, 30440 A, 30440 C, 30440 D, 30440 F, 30490 D, 30530 B, 30550 D, 30570 D, 30610 C, 30610 G, 30660 A, 30700 D, 30740 D, 30800 F, and 30840 E. All of the anomalies in this group yield resistivities of less than 10 ohm-m at the 900 Hz frequency. Some, such as 30360 E, reflect broad, highly conductive, flat-dipping sources at depths of up to 60 m. Others are more discrete and closer to surface.

In addition to the numerous conductors in Zones A1-A2, there are two smaller pods of conductive material shown on the EM anomaly map as Zone B and Zone C. There are also a few shorter or isolated conductors that occur outside of the main conductive units.

Anomalies 30020 C, 30030 A and 30070 D all reflect thin, non-magnetic sources of limited strike extent. Anomaly 30070 D dips to the west. Anomaly 30060 A is extremely weak, but is one of the few anomalies that yields direct magnetic correlation.

Anomalies 30190 B and 30200 B define a 200 m – long thin conductor that is about 200 m east of a stronger east-dipping source in Zone A1. Anomaly 30214 A is a short thin, isolated conductor with a 40 nT magnetic correlation, about 300 m west of Zone A1.

Three or more conductors are associated with a weak magnetic high that is located in a moderately resistive zone between A1 and A2. Two thin conductors strike south from anomalies 30250 D and 30250 F, to line 30270. There are no discrete conductors observed on line 30280, but anomalies 30290 C and 30300 E may be related to the same causative sources. All anomalies in this group reflect thin conductors, with 30260 D and 30270 D yielding weak magnetic correlation.

Anomaly 30310 B is a short, weak, thin conductor near the western edge of Zone A1. The conductor defined by 30360 A to 30380 A is associated with a south-trending magnetic contact that is parallel to the western edge of Zone A1 in this area. This thin conductor exhibits a probable strike length of about 350 m.

In the southeastern quadrant of the sheet, weak anomalies are evident at 30660 F, 30670 J, 30670 K and 30670 L. These anomalies suggest short, poorly conductive, thin sources that are associated with subtle magnetic lows.

Zone B hosts two conductors separated by about 100 m. They combine to yield a strong oblate resistivity low with a probable SSE strike. This attractive zone is non-magnetic, but occurs on the western flank of a weak magnetic unit. Dips are uncertain, but the strong coplanar response suggests a probable dip to the west. The 900 Hz resistivity parameter indicates an increase in conductance with depth, which tends to enhance the significance of this interesting zone. Additional work is recommended to check the causative source(s) of Zone B.

Zone C is a similarly strong resistivity low in the southwest corner, of slightly larger dimensions. High flying on line 30811 precluded accurate resistivity calculations in this area, but this dual conductor source is probably at least 450 m long. It is possible that the conductor extends north, to include anomalies 30750 A and 30740 A, where similar east-dipping thin sources are indicated. However, the northern extension of this zone is non-magnetic while the southern portion, at 30780 A and 30790 D, is magnetic. Note the strong, well-defined magnetic low at 30760 A and the magnetite-hosted response at 30770 A on the adjacent line. The erratic magnetic responses suggest an area of complex structure.

A single-line response at 30720 A reflects an extremely weak quadrature anomaly that is associated with an east-trending creek bed. This anomaly is not strong enough to yield a resistivity low.

8. CONCLUSIONS AND RECOMMENDATIONS

This report provides a very brief description of the survey results and describes the equipment, data processing procedures and logistics of the survey over two blocks flown in the Eskay Creek area in 2007.

There are numerous anomalies in the survey blocks that are typical of graphitic or massive sulphide responses. The survey was also successful in locating a few moderately strong or broad conductors that may also warrant additional work. The various maps included with this report display the magnetic, radiometric and conductive properties of the survey areas. It is recommended that a complete assessment and detailed evaluation of the survey results be carried out, in conjunction with all available geophysical, geological and geochemical information. Particular reference should be made to the multi-parameter data profiles that clearly define the characteristics of the individual anomalies.

In addition to the six main multi-conductor resistivity lows observed on Block 1, there are a few other interesting conductors that are considered to be potential areas for further investigation. Although most of the conductors on the property are non-magnetic, there are a few, such as 10160 X, that yield direct magnetic correlation. Several others appear to be related to zones of structural deformation, which tends to enhance their significance.

Portions of the conductive Zones A and B appear to partially underlie the Frank Mackie Glacier, while portions of Zones E and F also abut or underlie the edges of the Knipple Glacier.

Block 3 is underlain by a relatively non-magnetic south-trending core unit, the edges of which coincide with highly conductive bedrock sources. The multi-conductor zones strike south to Mitchell Creek, and then tend to display five or more parallel conductive bands that strike more towards the SE.

The highly conductive, non-magnetic characteristics tend to suggest graphite as a like contributing factor. However there are several conductors that yield weak magnetic correlation that could indicate the presence of magnetic sulphides. Most of the anomalies in the latter category are considered to be moderately attractive geophysical targets that warrant further investigation.

The interpreted bedrock conductors and anomalous targets defined by the survey should be subjected to further investigation, using appropriate surface exploration techniques. Anomalies that are currently considered to be of moderately low priority may require upgrading if follow-up results are favourable or if they occur in areas of anomalous geochemistry or favourable geology.

It is also recommended that additional processing of existing geophysical data be considered, in order to extract the maximum amount of information from the survey results.

Current software and imaging techniques often provide valuable information on structure and lithology, which may not be clearly evident on the contour and colour maps. These techniques can yield images that define subtle, but significant, structural details. In addition, ratios of the various radiometric channels might help to eliminate or minimize anomalous responses that are partially due to changes in sensor height or variations in overburden thickness or composition. The K/Th or K/U ratios are often helpful in locating alteration zones as well as mapping rock units that exhibit higher Potassium concentrations.

Respectfully submitted,

FUGRO AIRBORNE SURVEYS CORP.

APPENDIX A

LIST OF PERSONNEL

The following personnel were involved in the acquisition, processing, interpretation and presentation of data, relating to a DIGHEM airborne geophysical survey carried out for Hathor Exploration Ltd., over Blocks 1 and 3, in the Eskay Creek Area, northwestern British Columbia.

David Miles	Manager, Helicopter Operations
Emily Farquhar	Manager, Data Processing and Interpretation
Delvin Masilamani	Geophysical Operator
Lendl Mendes	Geophysical Operator
Darcy McGill	Field Geophysicist
Dima Amine	Field Geophysicist
Greg Charbonneau	Helicopter Pilot
Al Sweet	Helicopter Pilot
Scott McRae	Helicopter Mechanic
Igor Sram	Data Processor/ Interpretation Geophysicist
Paul Smith	Interpretation Supervisor
Lyn Vanderstarren	Drafting Supervisor
Susan Pothiah	Word Processing Operator
Albina Tonello	Secretary/Expeditor

The survey consisted of 800km of coverage, flown from July 19th to September 5th, 2007.

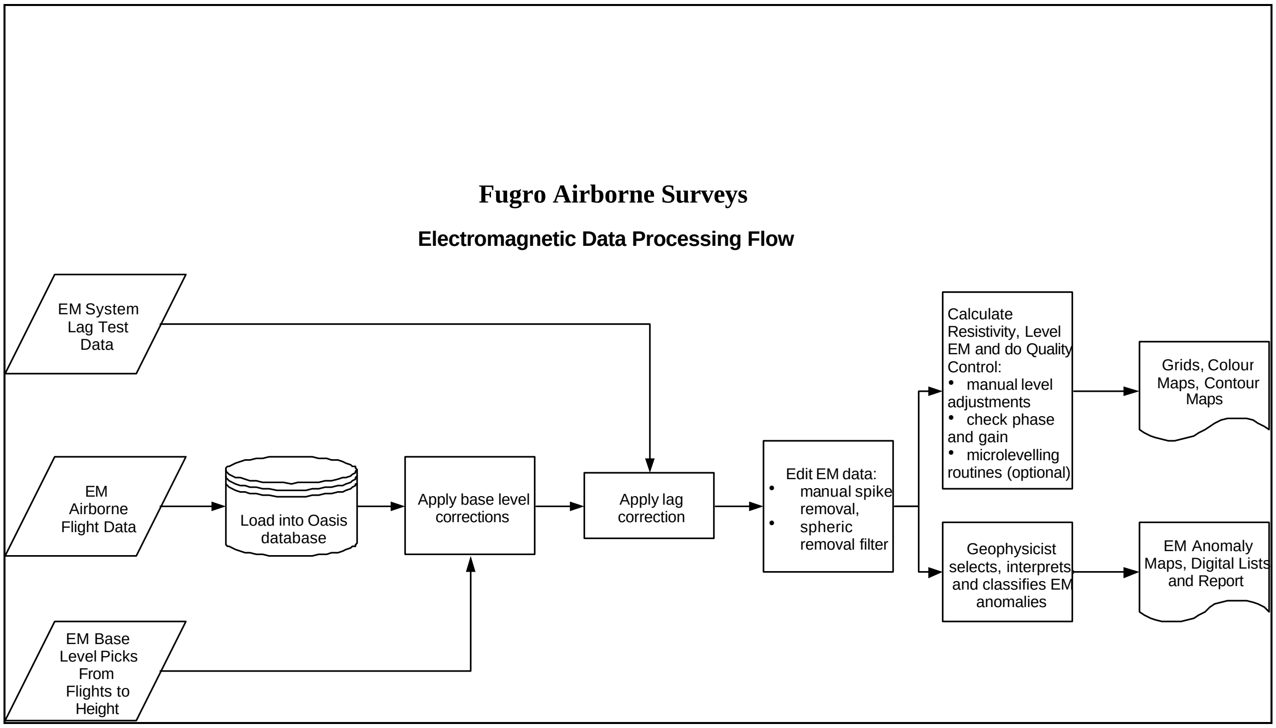
All personnel are employees of Fugro Airborne Surveys, except for the pilots and engineer who are employees of Great Slave Helicopters Ltd.

APPENDIX B

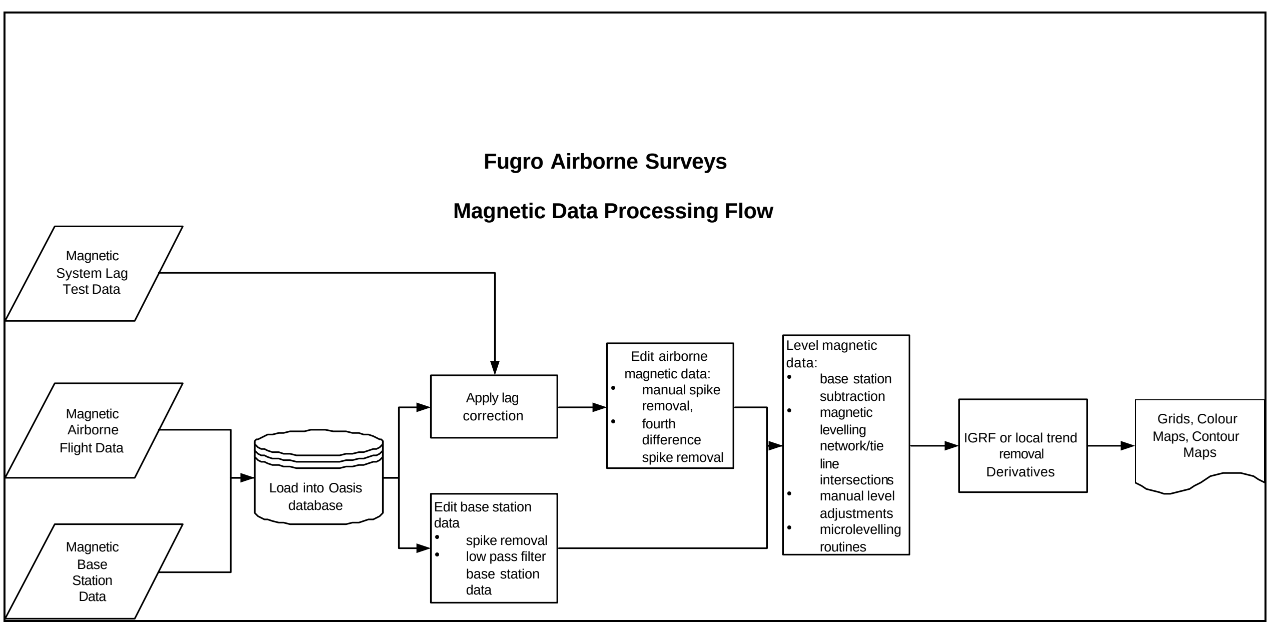
DATA PROCESSING FLOWCHARTS

APPENDIX B

Processing Flow Chart - Electromagnetic Data



Processing Flow Chart - Magnetic Data



APPENDIX C

BACKGROUND INFORMATION

BACKGROUND INFORMATION

Electromagnetics

Fugro electromagnetic responses fall into two general classes, discrete and broad. The discrete class consists of sharp, well-defined anomalies from discrete conductors such as sulphide lenses and steeply dipping sheets of graphite and sulphides. The broad class consists of wide anomalies from conductors having a large horizontal surface such as flatly dipping graphite or sulphide sheets, saline water-saturated sedimentary formations, conductive overburden and rock, kimberlite pipes and geothermal zones. A vertical conductive slab with a width of 200 m would straddle these two classes.

The vertical sheet (half plane) is the most common model used for the analysis of discrete conductors. All anomalies plotted on the geophysical maps are analyzed according to this model. The following section entitled **Discrete Conductor Analysis** describes this model in detail, including the effect of using it on anomalies caused by broad conductors such as conductive overburden.

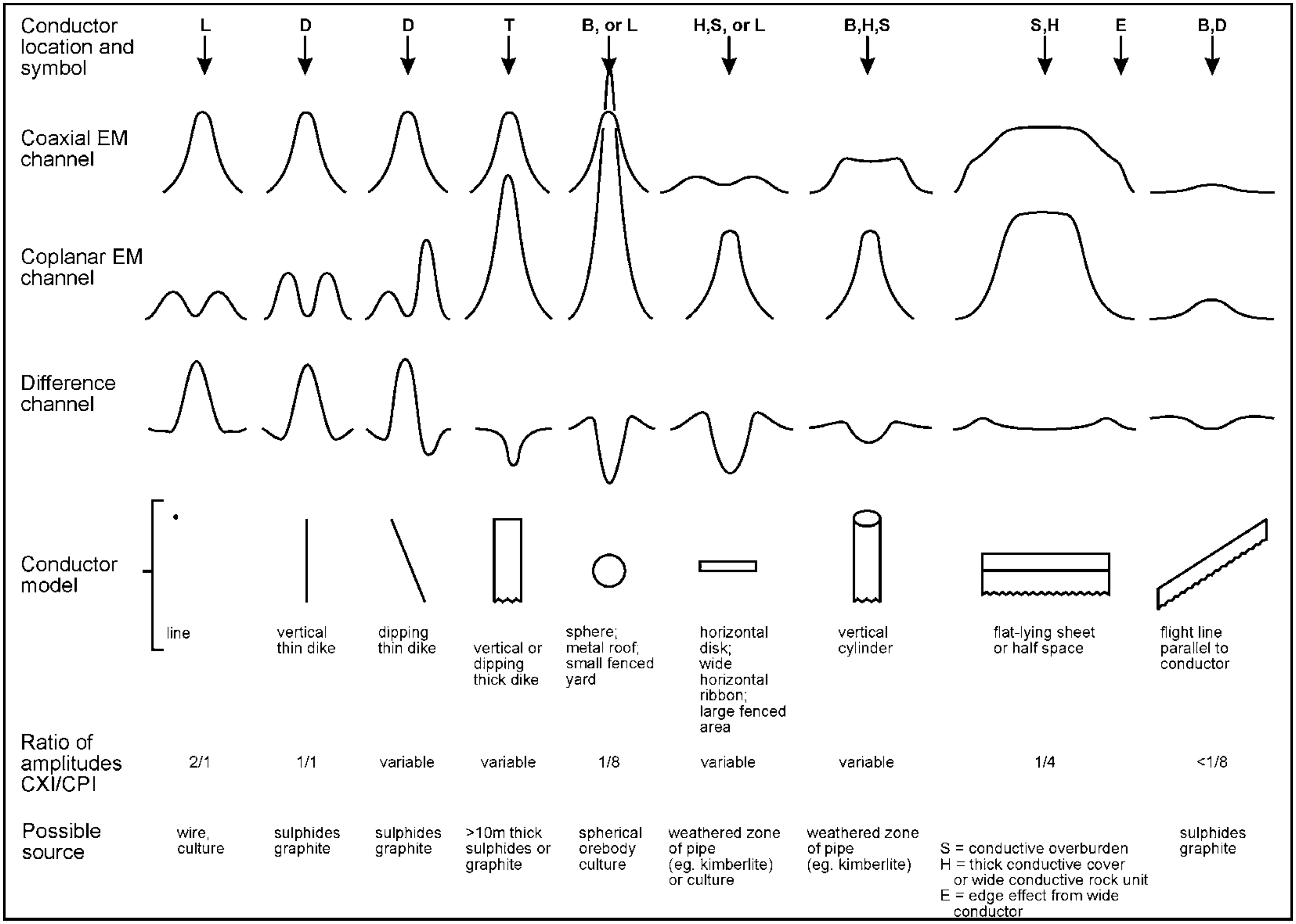
The conductive earth (half-space) model is suitable for broad conductors. Resistivity contour maps result from the use of this model. A later section entitled **Resistivity Mapping** describes the method further, including the effect of using it on anomalies caused by discrete conductors such as sulphide bodies.

Geometric Interpretation

The geophysical interpreter attempts to determine the geometric shape and dip of the conductor. Figure C-1 shows typical HEM anomaly shapes which are used to guide the geometric interpretation.

Discrete Conductor Analysis

The EM anomalies appearing on the electromagnetic map are analyzed by computer to give the conductance (i.e., conductivity-thickness product) in siemens (mhos) of a vertical sheet model. This is done regardless of the interpreted geometric shape of the conductor. This is not an unreasonable procedure, because the computed conductance increases as the electrical quality of the conductor increases, regardless of its true shape. DIGHEM anomalies are divided into seven grades of conductance, as shown in Table C-1. The conductance in siemens (mhos) is the reciprocal of resistance in ohms.



Typical HEM anomaly shapes

Figure C-1

The conductance value is a geological parameter because it is a characteristic of the conductor alone. It generally is independent of frequency, flying height or depth of burial, apart from the averaging over a greater portion of the conductor as height increases. Small anomalies from deeply buried strong conductors are not confused with small anomalies from shallow weak conductors because the former will have larger conductance values.

Table C-1. EM Anomaly Grades

Anomaly Grade	Siemens
7	> 100
6	50 - 100
5	20 - 50
4	10 - 20
3	5 - 10
2	1 - 5
1	< 1

Conductive overburden generally produces broad EM responses which may not be shown as anomalies on the geophysical maps. However, patchy conductive overburden in otherwise resistive areas can yield discrete anomalies with a conductance grade (cf. Table C-1) of 1, 2 or even 3 for conducting clays which have resistivities as low as 50 ohm-m. In areas where ground resistivities are below 10 ohm-m, anomalies caused by weathering variations and similar causes can have any conductance grade. The anomaly shapes from the multiple coils often allow such conductors to be recognized, and these are indicated by the letters S, H, and sometimes E on the geophysical maps (see EM legend on maps).

For bedrock conductors, the higher anomaly grades indicate increasingly higher conductances. Examples: the New Insco copper discovery (Noranda, Canada) yielded a grade 5 anomaly, as did the neighbouring copper-zinc Magusi River ore body; Mattabi (copper-zinc, Sturgeon Lake, Canada) and Whistle (nickel, Sudbury, Canada) gave grade 6; and the Montcalm nickel-copper discovery (Timmins, Canada) yielded a grade 7 anomaly. Graphite and sulphides can span all grades but, in any particular survey area, field work may show that the different grades indicate different types of conductors.

Strong conductors (i.e., grades 6 and 7) are characteristic of massive sulphides or graphite. Moderate conductors (grades 4 and 5) typically reflect graphite or sulphides of a less massive character, while weak bedrock conductors (grades 1 to 3) can signify poorly connected graphite or heavily disseminated sulphides. Grades 1 and 2 conductors may not respond to ground EM equipment using frequencies less than 2000 Hz.

The presence of sphalerite or gangue can result in ore deposits having weak to moderate conductances. As an example, the three million ton lead-zinc deposit of Restigouche Mining Corporation near Bathurst, Canada, yielded a well-defined grade 2 conductor. The 10 percent by volume of sphalerite occurs as a coating around the fine grained massive pyrite, thereby inhibiting electrical conduction. Faults, fractures and shear zones may produce anomalies that typically have low conductances (e.g., grades 1 to 3). Conductive rock formations can yield anomalies of any conductance grade. The conductive materials in such rock formations can be salt water, weathered products such as clays, original depositional clays, and carbonaceous material.

For each interpreted electromagnetic anomaly on the geophysical maps, a letter identifier and an interpretive symbol are plotted beside the EM grade symbol. The horizontal rows of dots, under the interpretive symbol, indicate the anomaly amplitude on the flight record. The vertical column of dots, under the anomaly letter, gives the estimated depth. In areas where anomalies are crowded, the letter identifiers, interpretive symbols and dots may be obliterated. The EM grade symbols, however, will always be discernible, and the obliterated information can be obtained from the anomaly listing appended to this report.

The purpose of indicating the anomaly amplitude by dots is to provide an estimate of the reliability of the conductance calculation. Thus, a conductance value obtained from a large ppm anomaly (3 or 4 dots) will tend to be accurate whereas one obtained from a small ppm anomaly (no dots) could be quite inaccurate. The absence of amplitude dots indicates that the anomaly from the coaxial coil-pair is 5 ppm or less on both the in-phase and quadrature channels. Such small anomalies could reflect a weak conductor at the surface or a stronger conductor at depth. The conductance grade and depth estimate illustrates which of these possibilities fits the recorded data best.

The conductance measurement is considered more reliable than the depth estimate. There are a number of factors that can produce an error in the depth estimate, including the averaging of topographic variations by the altimeter, overlying conductive overburden, and the location and attitude of the conductor relative to the flight line. Conductor location and attitude can provide an erroneous depth estimate because the stronger part of the conductor may be deeper or to one side of the flight line, or because it has a shallow dip. A heavy tree cover can also produce errors in depth estimates. This is because the depth estimate is computed as the distance of bird from conductor, minus the altimeter reading. The altimeter can lock onto the top of a dense forest canopy. This situation yields an erroneously large depth estimate but does not affect the conductance estimate.

Dip symbols are used to indicate the direction of dip of conductors. These symbols are used only when the anomaly shapes are unambiguous, which usually requires a fairly resistive environment.

A further interpretation is presented on the EM map by means of the line-to-line correlation of bedrock anomalies, which is based on a comparison of anomaly shapes on adjacent lines. This provides conductor axes that may define the geological structure over portions of the survey area. The absence of conductor axes in an area implies that anomalies could not be correlated from line to line with reasonable confidence.

The electromagnetic anomalies are designed to provide a correct impression of conductor quality by means of the conductance grade symbols. The symbols can stand alone with geology when planning a follow-up program. The actual conductance values are printed in the attached anomaly list for those who wish quantitative data. The anomaly ppm and depth are indicated by inconspicuous dots which should not distract from the conductor patterns, while being helpful to those who wish this information. The map provides an interpretation of conductors in terms of length, strike and dip, geometric shape, conductance, depth, and thickness. The accuracy is comparable to an interpretation from a high quality ground EM survey having the same line spacing.

The appended EM anomaly list provides a tabulation of anomalies in ppm, conductance, and depth for the vertical sheet model. No conductance or depth estimates are shown for weak anomalous responses that are not of sufficient amplitude to yield reliable calculations.

Since discrete bodies normally are the targets of EM surveys, local base (or zero) levels are used to compute local anomaly amplitudes. This contrasts with the use of true zero levels which are used to compute true EM amplitudes. Local anomaly amplitudes are shown in the EM anomaly list and these are used to compute the vertical sheet parameters of conductance and depth.

Questionable Anomalies

The EM maps may contain anomalous responses that are displayed as asterisks (*). These responses denote weak anomalies of indeterminate conductance, which may reflect one of the following: a weak conductor near the surface, a strong conductor at depth (e.g., 100 to 120 m below surface) or to one side of the flight line, or aerodynamic noise. Those responses that have the appearance of valid bedrock anomalies on the flight profiles are indicated by appropriate interpretive symbols (see EM legend on maps). The others probably do not warrant further investigation unless their locations are of considerable geological interest.

The Thickness Parameter

A comparison of coaxial and coplanar shapes can provide an indication of the thickness of a steeply dipping conductor. The amplitude of the coplanar anomaly (e.g., CPI channel) increases relative to the coaxial anomaly (e.g., CXI) as the apparent thickness increases, i.e., the thickness in the horizontal plane. (The thickness is equal to the conductor width if the conductor dips at 90 degrees and strikes at right angles to the flight line.) This report refers to a conductor as <u>thin</u> when the thickness is likely to be less than 3 m, and <u>thick</u> when in excess of 10 m. Thick conductors are indicated on the EM map by parentheses "(

)". For base metal exploration in steeply dipping geology, thick conductors can be high priority targets because many massive sulphide ore bodies are thick. The system cannot sense the thickness when the strike of the conductor is subparallel to the flight line, when the conductor has a shallow dip, when the anomaly amplitudes are small, or when the resistivity of the environment is below 100 ohm-m.

Resistivity Mapping

Resistivity mapping is useful in areas where broad or flat lying conductive units are of interest. One example of this is the clay alteration which is associated with Carlin-type deposits in the south west United States. The resistivity parameter was able to identify the clay alteration zone over the Cove deposit. The alteration zone appeared as a strong resistivity low on the 900 Hz resistivity parameter. The 7,200 Hz and 56,000 Hz resistivities showed more detail in the covering sediments, and delineated a range front fault. This is typical in many areas of the south west United States, where conductive near surface sediments, which may sometimes be alkalic, attenuate the higher frequencies.

Resistivity mapping has proven successful for locating diatremes in diamond exploration. Weathering products from relatively soft kimberlite pipes produce a resistivity contrast with the unaltered host rock. In many cases weathered kimberlite pipes were associated with thick conductive layers that contrasted with overlying or adjacent relatively thin layers of lake bottom sediments or overburden.

Areas of widespread conductivity are commonly encountered during surveys. These conductive zones may reflect alteration zones, shallow-dipping sulphide or graphite-rich units, saline ground water, or conductive overburden. In such areas, EM amplitude changes can be generated by decreases of only 5 m in survey altitude, as well as by increases in conductivity. The typical flight record in conductive areas is characterized by in-phase and quadrature channels that are continuously active. Local EM peaks reflect either increases in conductivity of the earth or decreases in survey altitude. For such conductive areas, apparent resistivity profiles and contour maps are necessary for the correct interpretation of the airborne data. The advantage of the resistivity parameter is that anomalies caused by altitude changes are virtually eliminated, so the resistivity data reflect only those anomalies caused by conductivity changes. The resistivity analysis also helps the interpreter to differentiate between conductive bedrock and conductive overburden. For example, discrete conductors will generally appear as narrow lows on the contour map and broad conductors (e.g., overburden) will appear as wide lows.

The apparent resistivity is calculated using the pseudo-layer (or buried) half-space model defined by Fraser (1978)[7]. This model consists of a resistive layer overlying a conductive

[7] Resistivity mapping with an airborne multicoil electromagnetic system: Geophysics, v. 43, p.144-172

half-space. The depth channels give the apparent depth below surface of the conductive material. The apparent depth is simply the apparent thickness of the overlying resistive layer. The apparent depth (or thickness) parameter will be positive when the upper layer is more resistive than the underlying material, in which case the apparent depth may be quite close to the true depth.

The apparent depth will be negative when the upper layer is more conductive than the underlying material, and will be zero when a homogeneous half-space exists. The apparent depth parameter must be interpreted cautiously because it will contain any errors that might exist in the measured altitude of the EM bird (e.g., as caused by a dense tree cover). The inputs to the resistivity algorithm are the in-phase and quadrature components of the coplanar coil-pair. The outputs are the apparent resistivity of the conductive half-space (the source) and the sensor-source distance. The flying height is not an input variable, and the output resistivity and sensor-source distance are independent of the flying height when the conductivity of the measured material is sufficient to yield significant in-phase as well as quadrature responses. The apparent depth, discussed above, is simply the sensor-source distance minus the measured altitude or flying height. Consequently, errors in the measured altitude will affect the apparent depth parameter but not the apparent resistivity parameter.

The apparent depth parameter is a useful indicator of simple layering in areas lacking a heavy tree cover. Depth information has been used for permafrost mapping, where positive apparent depths were used as a measure of permafrost thickness. However, little quantitative use has been made of negative apparent depths because the absolute value of the negative depth is not a measure of the thickness of the conductive upper layer and, therefore, is not meaningful physically. Qualitatively, a negative apparent depth estimate usually shows that the EM anomaly is caused by conductive overburden. Consequently, the apparent depth channel can be of significant help in distinguishing between overburden and bedrock conductors.

Interpretation in Conductive Environments

Environments having low background resistivities (e.g., below 30 ohm-m for a 900 Hz system) yield very large responses from the conductive ground. This usually prohibits the recognition of discrete bedrock conductors. However, Fugro data processing techniques produce three parameters that contribute significantly to the recognition of bedrock conductors in conductive environments. These are the in-phase and quadrature difference channels (DIFI and DIFQ, which are available only on systems with “common” frequencies on orthogonal coil pairs), and the resistivity and depth channels (RES and DEP) for each coplanar frequency.

The EM difference channels (DIFI and DIFQ) eliminate most of the responses from conductive ground, leaving responses from bedrock conductors, cultural features (e.g., telephone lines, fences, etc.) and edge effects. Edge effects often occur near the perimeter of broad conductive zones. This can be a source of geologic noise. While edge effects yield anomalies on the EM difference channels, they do not produce resistivity anomalies. Consequently, the resistivity channel aids in eliminating anomalies due to edge effects. On the other hand, resistivity anomalies will coincide with the most highly conductive sections of conductive ground, and this is another source of geologic noise. The recognition of a bedrock conductor in a conductive environment therefore is based on the anomalous responses of the two difference channels (DIFI and DIFQ) and the resistivity channels (RES). The most favourable situation is where anomalies coincide on all channels.

The DEP channels, which give the apparent depth to the conductive material, also help to determine whether a conductive response arises from surficial material or from a conductive zone in the bedrock. When these channels ride above the zero level on the depth profiles (i.e., depth is negative), it implies that the EM and resistivity profiles are responding primarily to a conductive upper layer, i.e., conductive overburden. If the DEP channels are below the zero level, it indicates that a resistive upper layer exists, and this usually implies the existence of a bedrock conductor. If the low frequency DEP channel is below the zero level and the high frequency DEP is above, this suggests that a bedrock conductor occurs beneath conductive cover.

Reduction of Geologic Noise

Geologic noise refers to unwanted geophysical responses. For purposes of airborne EM surveying, geologic noise refers to EM responses caused by conductive overburden and magnetic permeability. It was mentioned previously that the EM difference channels (i.e., channel DIFI for in-phase and DIFQ for quadrature) tend to eliminate the response of conductive overburden.

Magnetite produces a form of geological noise on the in-phase channels. Rocks containing less than 1% magnetite can yield negative in-phase anomalies caused by magnetic permeability. When magnetite is widely distributed throughout a survey area, the in-phase EM channels may continuously rise and fall, reflecting variations in the magnetite percentage, flying height, and overburden thickness. This can lead to difficulties in recognizing deeply buried bedrock conductors, particularly if conductive overburden also exists. However, the response of broadly distributed magnetite generally vanishes on the in-phase difference channel DIFI. This feature can be a significant aid in the recognition of conductors that occur in rocks containing accessory magnetite.

EM Magnetite Mapping

The information content of HEM data consists of a combination of conductive eddy current responses and magnetic permeability responses. The secondary field resulting from conductive eddy current flow is frequency-dependent and consists of both in-phase and quadrature components, which are positive in sign. On the other hand, the secondary field resulting from magnetic permeability is independent of frequency and consists of only an in-phase component which is negative in sign. When magnetic permeability manifests itself by decreasing the measured amount of positive in-phase, its presence may be difficult to recognize. However, when it manifests itself by yielding a negative in-phase anomaly (e.g., in the absence of eddy current flow), its presence is assured. In this latter case, the negative component can be used to estimate the percent magnetite content.

A magnetite mapping technique, based on the low frequency coplanar data, can be complementary to magnetometer mapping in certain cases. Compared to magnetometry, it is far less sensitive but is more able to resolve closely spaced magnetite zones, as well as providing an estimate of the amount of magnetite in the rock. The method is sensitive to 1/4% magnetite by weight when the EM sensor is at a height of 30 m above a magnetitic half-space. It can individually resolve steep dipping narrow magnetite-rich bands which are separated by 60 m. Unlike magnetometry, the EM magnetite method is unaffected by remanent magnetism or magnetic latitude.

The EM magnetite mapping technique provides estimates of magnetite content which are usually correct within a factor of 2 when the magnetite is fairly uniformly distributed. EM magnetite maps can be generated when magnetic permeability is evident as negative in-phase responses on the data profiles.

Like magnetometry, the EM magnetite method maps only bedrock features, provided that the overburden is characterized by a general lack of magnetite. This contrasts with resistivity mapping which portrays the combined effect of bedrock and overburden.

The Susceptibility Effect

When the host rock is conductive, the positive conductivity response will usually dominate the secondary field, and the susceptibility effect[8] will appear as a reduction in the in-phase, rather than as a negative value. The in-phase response will be lower than would be predicted by a model using zero susceptibility. At higher frequencies the in-phase conductivity response also gets larger, so a negative magnetite effect observed on the low frequency might not be observable on the higher frequencies, over the same body. The susceptibility effect is most obvious over discrete magnetite-rich zones, but also occurs over uniform geology such as a homogeneous half-space.

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[8] Magnetic susceptibility and permeability are two measures of the same physical property. Permeability is generally given as relative permeability, μ_r, which is the permeability of the substance divided by the permeability of free space ($4 \pi \times 10^{-7}$). Magnetic susceptibility *k* is related to permeability by $k=\mu^r-1$. Susceptibility is a unitless measurement, and is usually reported in units of 10^{-6}. The typical range of susceptibilities is –1 for quartz, 130 for pyrite, and up to 5×10^5 for magnetite, in 10^{-6} units (Telford et al, 1986).

High magnetic susceptibility will affect the calculated apparent resistivity, if only conductivity is considered. Standard apparent resistivity algorithms use a homogeneous half-space model, with zero susceptibility. For these algorithms, the reduced in-phase response will, in most cases, make the apparent resistivity higher than it should be. It is important to note that there is nothing wrong with the data, nor is there anything wrong with the processing algorithms. The apparent difference results from the fact that the simple geological model used in processing does not match the complex geology.

Measuring and Correcting the Magnetite Effect

Theoretically, it is possible to calculate (forward model) the combined effect of electrical conductivity and magnetic susceptibility on an EM response in all environments. The difficulty lies, however, in separating out the susceptibility effect from other geological effects when deriving resistivity and susceptibility from EM data.

Over a homogeneous half-space, there is a precise relationship between in-phase, quadrature, and altitude. These are often resolved as phase angle, amplitude, and altitude. Within a reasonable range, any two of these three parameters can be used to calculate the half space resistivity. If the rock has a positive magnetic susceptibility, the in-phase component will be reduced and this departure can be recognized by comparison to the other parameters.

The algorithm used to calculate apparent susceptibility and apparent resistivity from HEM data, uses a homogeneous half-space geological model. Non half-space geology, such as horizontal layers or dipping sources, can also distort the perfect half-space relationship of the three data parameters. While it may be possible to use more complex models to calculate both rock parameters, this procedure becomes very complex and time-consuming. For basic HEM data processing, it is most practical to stick to the simplest geological model.

Magnetite reversals (reversed in-phase anomalies) have been used for many years to calculate an “FeO” or magnetite response from HEM data (Fraser, 1981). However, this technique could only be applied to data where the in-phase was observed to be negative, which happens when susceptibility is high and conductivity is low.

Applying Susceptibility Corrections

Resistivity calculations done with susceptibility correction may change the apparent resistivity. High-susceptibility conductors, that were previously masked by the susceptibility effect in standard resistivity algorithms, may become evident. In this case the susceptibility corrected apparent resistivity is a better measure of the actual resistivity of the earth. However, other geological variations, such as a deep resistive layer, can also reduce the in-phase by the same amount. In this case, susceptibility correction would not be the best method. Different geological models can apply in different areas of the same data set. The effects of susceptibility, and other effects that can create a similar response, must be considered when selecting the resistivity algorithm.

Susceptibility from EM vs Magnetic Field Data

The response of the EM system to magnetite may not match that from a magnetometer survey. First, HEM-derived susceptibility is a rock property measurement, like resistivity. Magnetic data show the total magnetic field, a measure of the potential field, not the rock property. Secondly, the shape of an anomaly depends on the shape and direction of the source magnetic field. The electromagnetic field of HEM is much different in shape from the earth's magnetic field. Total field magnetic anomalies are different at different magnetic latitudes; HEM susceptibility anomalies have the same shape regardless of their location on the earth.

In far northern latitudes, where the magnetic field is nearly vertical, the total magnetic field measurement over a thin vertical dike is very similar in shape to the anomaly from the HEM-derived susceptibility (a sharp peak over the body). The same vertical dike at the magnetic equator would yield a negative magnetic anomaly, but the HEM susceptibility anomaly would show a positive susceptibility peak.

Effects of Permeability and Dielectric Permittivity

Resistivity algorithms that assume free-space magnetic permeability and dielectric permittivity, do not yield reliable values in highly magnetic or highly resistive areas. Both magnetic polarization and displacement currents cause a decrease in the in-phase component, often resulting in negative values that yield erroneously high apparent resistivities. The effects of magnetite occur at all frequencies, but are most evident at the lowest frequency. Conversely, the negative effects of dielectric permittivity are most evident at the higher frequencies, in resistive areas.

The table below shows the effects of varying permittivity over a resistive (10,000 ohm-m) half space, at frequencies of 56,000 Hz (DIGHEM^{V}) and 102,000 Hz (RESOLVE).

Apparent Resistivity Calculations

Effects of Permittivity on In-phase/Quadrature/Resistivity

Freq (Hz)	Coil	Sep (m)	Thres (ppm)	Alt (m)	In Phase	Quad Phase	App Res	App Depth (m)	Permittivity
56,000	CP	6.3	0.1	30	7.3	35.3	10118	-1.0	1 Air
56,000	CP	6.3	0.1	30	3.6	36.6	19838	-13.2	5 Quartz
56,000	CP	6.3	0.1	30	-1.1	38.3	81832	-25.7	10 Epidote
56,000	CP	6.3	0.1	30	-10.4	42.3	76620	-25.8	20 Granite

56,000	CP	6.3	0.1	30	-19.7	46.9	71550	-26.0	30 Diabase
56,000	CP	6.3	0.1	30	-28.7	52.0	66787	-26.1	40 Gabbro
102,000	CP	7.86	0.1	30	32.5	117.2	9409	-0.3	1 Air
102,000	CP	7.86	0.1	30	11.7	127.2	25956	-16.8	5 Quartz
102,000	CP	7.86	0.1	30	-14.0	141.6	97064	-26.5	10 Epidote
102,000	CP	7.86	0.1	30	-62.9	176.0	83995	-26.8	20 Granite
102,000	CP	7.86	0.1	30	-107.5	215.8	73320	-27.0	30 Diabase
102,000	CP	7.86	0.1	30	-147.1	259.2	64875	-27.2	40 Gabbro

Methods have been developed (Huang and Fraser, 2000, 2001) to correct apparent resistivities for the effects of permittivity and permeability. The corrected resistivities yield more credible values than if the effects of permittivity and permeability are disregarded.

Recognition of Culture

Cultural responses include all EM anomalies caused by man-made metallic objects. Such anomalies may be caused by inductive coupling or current gathering. The concern of the interpreter is to recognize when an EM response is due to culture. Points of consideration used by the interpreter, when coaxial and coplanar coil-pairs are operated at a common frequency, are as follows:

1. Channels CXPL and CPPL monitor 60 Hz radiation. An anomaly on these channels shows that the conductor is radiating power. Such an indication is normally a guarantee that the conductor is cultural. However, care must be taken to ensure that the conductor is not a geologic body that strikes across a power line, carrying leakage currents.

2. A flight that crosses a "line" (e.g., fence, telephone line, etc.) yields a centre-peaked coaxial anomaly and an m-shaped coplanar anomaly.[9] When the flight crosses the cultural line at a high angle of intersection, the amplitude ratio of coaxial/coplanar response is 2. Such an EM anomaly can only be caused by a line. The geologic body that yields anomalies most closely resembling a line is the vertically dipping thin dike. Such a body, however, yields an amplitude ratio of 1 rather than 2. Consequently, an m-shaped coplanar anomaly with a CXI/CPI amplitude ratio of 2 is virtually a guarantee that the source is a cultural line.

3. A flight that crosses a sphere or horizontal disk yields centre-peaked coaxial and coplanar anomalies with a CXI/CPI amplitude ratio (i.e., coaxial/coplanar) of 1/8. In the absence of geologic bodies of this geometry, the most likely conductor is a

[9] See Figure C-1 presented earlier.

metal roof or small fenced yard.[10] Anomalies of this type are virtually certain to be cultural if they occur in an area of culture.

4. A flight that crosses a horizontal rectangular body or wide ribbon yields an m-shaped coaxial anomaly and a centre-peaked coplanar anomaly. In the absence of geologic bodies of this geometry, the most likely conductor is a large fenced area.[5] Anomalies of this type are virtually certain to be cultural if they occur in an area of culture.
5. EM anomalies that coincide with culture, as seen on the camera film or video display, are usually caused by culture. However, care is taken with such coincidences because a geologic conductor could occur beneath a fence, for example. In this example, the fence would be expected to yield an m-shaped coplanar anomaly as in case #2 above. If, instead, a centre-peaked coplanar anomaly occurred, there would be concern that a thick geologic conductor coincided with the cultural line.

6. The above description of anomaly shapes is valid when the culture is not conductively coupled to the environment. In this case, the anomalies arise from inductive coupling to the EM transmitter. However, when the environment is quite conductive (e.g., less than 100 ohm-m at 900 Hz), the cultural conductor may be conductively coupled to the environment. In this latter case, the anomaly shapes tend to be governed by current gathering. Current gathering can completely distort the anomaly shapes, thereby complicating the identification of cultural anomalies. In such circumstances, the interpreter can only rely on the radiation channels and on the camera film or video records.

Magnetic Responses

The measured total magnetic field provides information on the magnetic properties of the earth materials in the survey area. The information can be used to locate magnetic bodies of direct interest for exploration, and for structural and lithological mapping.

The total magnetic field response reflects the abundance of magnetic material in the source. Magnetite is the most common magnetic mineral. Other minerals such as ilmenite, pyrrhotite, franklinite, chromite, hematite, arsenopyrite, limonite and pyrite are also magnetic, but to a lesser extent than magnetite on average.

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[10] It is a characteristic of EM that geometrically similar anomalies are obtained from: (1) a planar conductor, and (2) a wire which forms a loop having dimensions identical to the perimeter of the equivalent planar conductor.

In some geological environments, an EM anomaly with magnetic correlation has a greater likelihood of being produced by sulphides than one which is non-magnetic. However, sulphide ore bodies may be non-magnetic (e.g., the Kidd Creek deposit near Timmins, Canada) as well as magnetic (e.g., the Mattabi deposit near Sturgeon Lake, Canada).

Iron ore deposits will be anomalously magnetic in comparison to surrounding rock due to the concentration of iron minerals such as magnetite, ilmenite and hematite.

Changes in magnetic susceptibility often allow rock units to be differentiated based on the total field magnetic response. Geophysical classifications may differ from geological classifications if various magnetite levels exist within one general geological classification. Geometric considerations of the source such as shape, dip and depth, inclination of the earth's field and remanent magnetization will complicate such an analysis.

In general, mafic lithologies contain more magnetite and are therefore more magnetic than many sediments which tend to be weakly magnetic. Metamorphism and alteration can also increase or decrease the magnetization of a rock unit.
Textural differences on a total field magnetic contour, colour or shadow map due to the frequency of activity of the magnetic parameter resulting from inhomogeneities in the distribution of magnetite within the rock, may define certain lithologies. For example, near surface volcanics may display highly complex contour patterns with little line-to-line correlation.

Rock units may be differentiated based on the plan shapes of their total field magnetic responses. Mafic intrusive plugs can appear as isolated "bulls-eye" anomalies. Granitic intrusives appear as sub-circular zones, and may have contrasting rings due to contact metamorphism. Generally, granitic terrain will lack a pronounced strike direction, although granite gneiss may display strike.

Linear north-south units are theoretically not well-defined on total field magnetic maps in equatorial regions due to the low inclination of the earth's magnetic field. However, most stratigraphic units will have variations in composition along strike that will cause the units to appear as a series of alternating magnetic highs and lows.

Faults and shear zones may be characterized by alteration that causes destruction of magnetite (e.g., weathering) that produces a contrast with surrounding rock. Structural breaks may be filled by magnetite-rich, fracture filling material as is the case with diabase dikes, or by non-magnetic felsic material.

Faulting can also be identified by patterns in the magnetic total field contours or colours. Faults and dikes tend to appear as lineaments and often have strike lengths of several kilometres. Offsets in narrow, magnetic, stratigraphic trends also delineate structure. Sharp contrasts in magnetic lithologies may arise due to large displacements along strike-slip or dip-slip faults.

Gamma Ray Spectrometry

Radioelement concentrations are measures of the abundance of radioactive elements in the rock. The original abundance of the radioelements in any rock can be altered by the subsequent processes of metamorphism and weathering.

Gamma radiation in the range that is measured in the thorium, potassium, uranium and total count windows is strongly attenuated by rock, overburden and water. Almost all of the total radiation measured from rock and overburden originates in the upper .5 metres. Moisture in soil and bodies of water will mask the radioactivity from underlying rock. Weathered rock materials that have been displaced by glacial, water or wind action will not reflect the general composition of the underlying bedrock. Where residual soils exist, they may reflect the composition of underlying rock except where equilibrium does not exist between the original radioelement and the products in its decay series.

Radioelement counts (expressed as counts per second) are the rates of detection of the gamma radiation from specific decaying particles corresponding to products in each radioelements decay series. The radiation source for uranium is bismuth (Bi-214), for thorium it is thallium (Tl-208) and for potassium it is potassium (K-40).

The uranium and thorium radioelement concentrations are dependent on a state of equilibrium between the parent and daughter products in the decay series. Some daughter products in the uranium decay are long lived and could be removed by processes such as leaching. One product in the series, radon (Rn-222), is a gas which can easily escape. Both of these factors can affect the degree to which the calculated uranium concentrations reflect the actual composition of the source rock. Because the daughter products of thorium are relatively short lived, there is more likelihood that the thorium decay series is in equilibrium.

Lithological discrimination can be based on the measured relative concentrations and total, combined, radioactivity of the radioelements. Feldspar and mica contain potassium. Zircon, sphene and apatite are accessory minerals in igneous rocks that are sources of uranium and thorium. Monazite, thorianite, thorite, uraninite and uranothorite are also sources of uranium and thorium which are found in granites and pegmatites.

In general, the abundance of uranium, thorium and potassium in igneous rock increases with acidity. Pegmatites commonly have elevated concentrations of uranium relative to thorium. Sedimentary rocks derived from igneous rocks may have characteristic signatures that are influenced by their parent rocks, but these will have been altered by subsequent weathering and alteration.

Metamorphism and alteration will cause variations in the abundance of certain radioelements relative to each other. For example, alterative processes may cause uranium enrichment to the extent that a rock will be of economic interest. Uranium anomalies are more likely to be economically significant if they consist of an increase in the uranium relative to thorium and potassium, rather than a sympathetic increase in all three radioelements.

Faults can exhibit radioactive highs due to increased permeability which allows radon migration, or as lows due to structural control of drainage and fluvial sediments which attenuate gamma radiation from the underlying rocks. Faults can also be recognized by sharp contrasts in radiometric lithologies due to large strike-slip or dip-slip displacements. Changes in relative radioelement concentrations due to alteration will also define faults.

Similar to magnetics, certain rock types can be identified by their plan shapes if they also produce a radiometric contrast with surrounding rock. For example, granite intrusions will appear as sub-circular bodies, and may display concentric zonations. They will tend to lack a prominent strike direction. Offsets of narrow, continuous, stratigraphic units with contrasting radiometric signatures can identify faulting, and folding of stratigraphic trends will also be apparent.

APPENDIX D

DATA ARCHIVE DESCRIPTION

APPENDIX D

ARCHIVE DESCRIPTION

Reference: CDVD00275
Disc 1 of 1
Archive Date: February 19, 2008

This archive contains FINAL DATA ARCHIVES of an airborne geophysical survey conducted by FUGRO AIRBORNE SURVEYS CORP. over the Eskay Creek Areas, British Columbia on behalf of Hathor Exploration Ltd. during July 19 to September 5, 2007.

Job # 06041-1,3

******* Disc 1 of 1 *******

\README.TXT - this file

GRIDS\
NOTE: _# indicates block number.

Grids in Geosoft binary (float) format

RES900_1.GRD	- Apparent Resistivity 900 Hz coplanar
RES7200_1.GRD	- Apparent Resistivity 7200 Hz coplanar
RES56K_1.GRD	- Apparent Resistivity 56000 Hz coplanar
MAG_1.GRD	- Total Magnetic Intensity nT
CVG_1.GRD	- Calculated Vertical gradient from TMI grid nT/m
K_1.GR	- Potasium Counts (cps)
U_1.GRD	- Uranium Counts (cps)
TH_1.GRD	- Thorium Counts (cps)
TC_1.GRD	- Total Counts (cps)
RES900_3.GRD	- Apparent Resistivity 900 Hz coplanar
RES7200_3.GRD	- Apparent Resistivity 7200 Hz coplanar
RES56K_3.GRD	- Apparent Resistivity 56000 Hz coplanar
MAG_3.GRD	- Total Magnetic Intensity nT
CVG_3.GRD	- Calculated Vertical gradient from TMI grid nT/m
K_3.GRD	- Potasium Counts (cps)
U_3.GRD	- Uranium Counts (cps)
TH_3.GRD	- Thorium Counts (cps)
TC_3.GRD	- Total Counts (cps)

- Appendix D.2 -

XYZ\

Block1.XYZ	- ASCII line data archive in Geosoft XYZ format
anBlock1.XYZ	- Geosoft Anomaly ASCII data archive
Block3.XYZ	- ASCII line data archive in Geosoft XYZ format
anBlock3.XYZ	- Geosoft Anomaly ASCII data archive

ArchiveSummary.txt - Summary of Channel Names in the ASCII line data archive

MAPS\

Block 1 Maps

aem_block1.pdf	- Electromagnetic Anomalies map
cvg_block1.pdf	- Calculated Vertical Gradient map
mag_block1.pdf	- Total Magnetic Field map
res56K_block1.pdf	- Apparent Resistivity Map 56 KHz
res7200_block1.pdf	- Apparent Resistivity Map 7200 Hz
res900_block1.pdf	- Apparent Resistivity Map 900 Hz
tc_block1.pdf	- Radiometric Total Count map
th_block1.pdf	- Radiometric Thorium counts map
k_block1.pdf	- Radiometric Potassium counts map
u_block1.pdf	- Radiometric Uranium counts map

Block 3 Maps

aem_block3.pdf	- Electromagnetic Anomalies map
cvg_block3.pdf	- Calculated Vertical Gradient map
mag_block3.pdf	- Total Magnetic Field map
res56K_block3.pdf	- Apparent Resistivity Map 56 KHz
res7200_block3.pdf	- Apparent Resistivity Map 7200 Hz
res900_block3.pdf	- Apparent Resistivity Map 900 Hz
tc_block3.pdf	- Radiometric Total Count map
th_block3.pdf	- Radiometric Thorium counts map
k_block3.pdf	- Radiometric Potassium counts map
u_block3.pdf	- Radiometric Uranium counts map

- Appendix D.3 -

Geosoft XYZ ARCHIVE SUMMARY

JOB TITLE: 06041-1,-3

TYPE OF SURVEY   :Fugro DIGHEM V EM, Magnetics, Resistivity, Radiometrics
AREA   :Eskay Creek Areas, Blocks 1 and 3, British Columbia
CLIENT   :Hathor Exploration Ltd.

****

NUMBER OF DATA FIELDS :   43

#	CHANNAME	TIME	UNITS / DESCRIPTION	
1	X	0.1	m	UTME-NAD83 (ZONE-9N)
2	Y	0.1	m	UTMN-NAD83 (ZONE-9N)
3	LAT	0.1	deg.m	Latitude NAD83
4	LON	0.1	deg.m	Longitude NAD83
5	ALTBIRDM	0.1	m	Bird height above ground
6	ALTHELIM	0.1	m	Heli height above ground
7	FID	0.1	s	Fiducial
8	DIURNAL	0.1	nT	Diurnal correction
9	MAGR	0.1	nT	Lagged and diurnal corrected Total Magnetic Field
10	MAGF	0.1	nT	Final Total Magnetic Field
11	CPI900	0.1	ppm	INPHASE-COPLANAR 872 HZ
12	CPQ900	0.1	ppm	QUADRATURE- COPLANAR 872 HZ
13	CXI1000	0.1	ppm	INPHASE-COAXIAL 1116 HZ
14	CXQ1000	0.1	ppm	QUAD- COAXIAL 1116 HZ
15	CXI5500	0.1	ppm	INPHASE -COAXIAL 5666 HZ
16	CXQ5500	0.1	ppm	QUAD -COAXIAL 5666 HZ
17	CPI7200	0.1	ppm	INPHASE -COPLANAR 7233 HZ
18	CPQ7200	0.1	ppm	QUAD -COPLANAR 7233 HZ
19	CPI56K	0.1	ppm	INPHASE-COPLANAR 55460 HZ
20	CPQ56K	0.1	ppm	QUAD-COPLANAR 55460 HZ
21	RES900	0.1	ohm-m	APPARENT RESISTIVITY - 872 Hz
22	RES7200	0.1	ohm-m	APPARENT RESISTIVITY - 7233 Hz
23	RES56K	0.1	ohm-m	APPARENT RESISTIVITY - 55460 Hz
24	DEP900	0.1	m	APPARENT DEPTH - 872 Hz
25	DEP7200	0.1	m	APPARENT DEPTH - 7233 Hz
26	DEP56K	0.1	m	APPARENT DEPTH - 55460 Hz
27	COSMIC	1.0	counts/s	Cosmic counts
28	LIVE_TIME	1.0	ms	Spectrometer live time
29	URANUP	1.0	counts/s	Upward Uranium window
30	TC_RAW	1.0	counts/s	Total Count window - raw
31	TH_RAW	1.0	counts/s	Thorium window - raw
32	U_RAW	1.0	counts/s	Uranium window - raw
33	K_RAW	1.0	counts/s	Potassium window - raw
34	TC	1.0	counts/s	Total Count window - corrected
35	TH	1.0	counts/s	Thorium window - corrected
36	U	1.0	counts/s	Uranium window - corrected
37	K	1.0	counts/s	Potassium window - corrected

```
 38 PRESSURE    0.1    kpa         Air pressure
 39 TEMPERATURE 0.1    Celsius     Outside air temperature
 40 Z           0.1    m           Height above mean sea level
 41 DTM         0.1    m           Digital Terrain Model
 42 FLT         0.1                Survey flight number
 43 DATE        0.1    Y/M/D       Date of the survey line
************************************************************************
ISSUE DATE         :February 19, 2008
FOR WHOM           :Hathor Exploration Ltd.
BY  WHOM           :FUGRO AIRBORNE SURVEYS
                    2270 ARGENTIA ROAD, UNIT 2
                    MISSISSAUGA, ONTARIO,
                    CANADA  L5N 6A6
                    TEL. (905) 812-0212
                    FAX (905) 812-1504
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APPENDIX E

EM ANOMALY LIST

EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 10010		FLIGHT 6											
A	1531.4	B	430110	6246519	28.4	44.6	79.3	135.5	3.9	34.6	1.2	0	0
B	1520.1	D	430198	6246616	12.6	11.7	21.9	44.7	1.2	12.1	1.6	17	0
C	1503.7	S?	430362	6246770	16.8	42.6	87.6	259.2	6.9	50.8	0.7	0	0
D	1479.1	B?	430813	6247237	108.6	163.1	659.4	661.4	72.1	258.6	1.9	0	0
E	1469.1	E	430949	6247366	11.5	14.8	28.2	23.0	11.7	21.3	1.1	21	0
F	1441.4	B	431232	6247669	9.3	69.6	98.8	279.8	18.1	70.7	0.2	0	0
G	1425.1	H	431437	6247863	12.2	15.7	58.9	74.4	11.6	26.0	1.1	8	0
H	1417.8	S?	431517	6247945	3.4	27.2	34.1	218.5	9.6	48.2	0.2	0	0
I	1410.8	B	431591	6248022	14.1	45.5	62.4	218.5	18.8	48.2	0.5	0	0
J	1405.8	E	431662	6248091	13.9	17.2	69.5	67.0	18.8	45.8	1.2	13	0
K	1373.9	S	432140	6248568	20.0	21.8	142.6	132.5	15.2	50.1	1.5	0	0
L	1356.4	B	432400	6248813	22.5	18.2	91.9	90.0	16.0	42.2	2.3	7	0
M	1337.1	S?	432576	6248981	7.0	7.5	43.1	59.0	7.9	9.4	1.1	11	0
N	1325.8	E	432662	6249066	10.3	23.9	74.3	104.4	3.2	27.3	0.6	0	0
O	1172.7	S?	434606	6251015	0.5	0.9	1.1	13.1	0.0	1.6	---	---	0
P	1154.1	S	434790	6251197	2.7	2.5	9.8	13.2	9.5	2.4	---	---	0
Q	1060.8	E	436194	6252578	18.9	25.7	102.1	126.1	4.8	38.9	1.2	0	0
R	1051.0	H	436417	6252791	35.5	41.1	248.6	276.8	32.1	105.3	1.7	3	0
S	1044.2	B	436544	6252925	25.7	27.2	158.4	226.4	32.1	102.9	1.7	4	0
T	1029.8	B	436753	6253148	7.3	10.6	67.5	48.2	15.8	26.5	0.8	4	0
U	1017.1	S	437025	6253384	4.8	6.8	34.8	25.3	4.2	2.0	0.7	18	0
V	1008.3	S	437207	6253557	2.9	39.7	79.2	270.4	2.8	46.2	0.1	0	0
W	948.4	B	437529	6253912	20.1	24.9	78.3	155.9	29.4	28.6	1.3	0	0
X	934.9	B	437687	6254065	29.1	10.6	135.5	61.4	51.8	69.3	6.9	17	0
LINE 10020		FLIGHT 6											
A	2071.0	S	427794	6244032	1.9	3.6	5.6	27.1	1.6	5.6	---	---	0
B	2231.0	S?	430009	6246228	6.7	16.7	18.8	65.7	0.3	8.7	0.5	14	0
C	2256.9	B?	430226	6246443	7.0	12.4	35.1	59.4	5.3	17.2	0.7	11	0
D	2280.0	B	430481	6246693	74.8	87.7	311.4	419.9	24.4	143.3	2.2	0	0
E	2282.9	B	430524	6246739	76.9	110.2	311.4	419.9	9.8	143.3	1.8	0	0
F	2291.2	D	430664	6246883	10.8	24.5	0.6	13.9	3.3	2.9	0.6	0	33
G	2304.3	B	430930	6247134	66.7	99.6	475.7	482.9	48.9	188.4	1.7	0	0
H	2308.2	D	430975	6247175	19.0	6.0	475.7	482.9	48.9	188.4	7.3	24	0
I	2337.1	H	431184	6247392	14.3	19.1	126.1	116.7	23.9	52.4	1.1	5	0
J	2342.7	B	431250	6247458	9.0	14.5	126.1	0.0	23.9	52.4	0.8	1	0
K	2354.4	B	431395	6247609	19.3	14.8	50.8	69.3	0.7	23.0	2.3	8	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 10020		FLIGHT 6											
L	2368.0	B	431563	6247779	38.9	69.8	379.7	430.0	16.1	125.6	1.1	0	0
M	2376.5	H	431710	6247917	3.7	11.2	2.8	0.0	11.9	0.0	0.3	8	0
N	2410.7	B	432309	6248502	25.4	44.8	110.4	128.4	16.3	46.2	1.0	0	0
O	2422.4	B	432473	6248664	24.9	29.9	145.0	148.0	25.2	61.3	1.5	0	0
P	2500.2	S	433437	6249627	1.5	18.0	4.0	52.1	1.7	8.1	---	---	0
Q	2606.4	S?	434727	6250918	1.9	1.3	1.7	11.8	0.0	1.6	---	---	0
R	2722.9	E	436401	6252563	17.8	20.2	79.6	164.8	2.4	40.9	1.4	9	0
S	2730.8	H	436539	6252701	9.4	12.6	65.6	83.2	16.4	27.5	1.0	20	0
T	2741.8	B	436713	6252883	16.5	43.0	124.3	240.4	11.6	57.9	0.6	0	0
U	2770.8	S	437288	6253454	3.9	2.9	42.3	108.4	1.9	20.4	1.4	54	0
V	2812.2	B	437660	6253825	14.8	28.9	87.3	56.0	13.2	28.3	0.8	0	0
W	2831.1	B	437826	6253977	70.1	31.4	227.5	150.8	70.4	105.5	7.0	0	0
LINE 10030		FLIGHT 6											
A	3746.4	B	430669	6246662	86.9	109.5	187.7	368.7	3.7	78.9	2.1	0	0
B	3731.0	B	430772	6246764	6.0	23.3	115.7	97.8	4.8	43.9	0.3	2	0
C	3725.9	B	430815	6246802	3.3	2.0	115.7	181.5	5.6	43.9	1.8	63	0
D	3713.8	B	430882	6246878	0.0	1.3	38.7	125.4	4.3	19.0	0.1	21	0
E	3706.2	B	430914	6246918	3.8	4.8	15.1	0.0	11.2	12.7	0.8	24	0
F	3700.1	H	430976	6246987	25.5	49.6	115.6	157.8	15.5	50.2	0.9	0	0
G	3692.0	B	431071	6247084	89.1	242.6	358.2	761.6	26.2	184.7	1.1	0	0
H	3680.7	B	431200	6247209	10.8	36.5	79.8	155.2	7.1	41.8	0.4	0	0
I	3673.6	B	431282	6247288	14.1	28.3	113.6	150.2	38.4	63.5	0.7	2	0
J	3647.8	H	431608	6247604	7.9	12.6	39.1	111.8	3.2	10.8	0.8	9	0
K	3625.7	H	431876	6247888	5.6	11.3	35.0	83.8	6.3	23.5	0.5	5	0
L	3594.9	H	432268	6248256	10.0	13.0	20.0	38.7	8.2	14.9	1.0	22	0
M	3587.2	B	432360	6248368	37.6	44.1	175.2	180.7	57.2	66.4	1.8	0	0
N	3583.0	B	432435	6248439	30.0	12.8	299.7	287.2	67.4	130.8	---	---	0
O	3578.2	B	432528	6248524	49.6	52.7	299.7	287.2	67.4	130.8	2.1	0	0
P	3575.3	H	432580	6248575	40.0	25.9	299.7	287.2	25.2	130.8	3.6	5	0
Q	3570.2	H?	432664	6248658	18.6	39.8	62.2	125.5	16.3	46.7	0.8	0	0
R	3563.1	B	432775	6248769	23.2	17.2	48.0	29.7	13.8	20.7	2.5	7	0
S	3556.3	B	432898	6248888	11.1	12.7	107.5	241.4	6.0	44.7	1.2	19	0
T	3553.6	B	432950	6248937	18.4	57.1	107.5	241.4	3.5	44.7	0.6	0	0
U	3488.0	S	433797	6249754	0.1	2.5	2.3	22.2	0.0	3.9	---	---	0
V	3290.2	B	436542	6252511	15.7	22.7	89.4	129.3	14.1	43.8	1.1	3	0
W	3278.4	H	436757	6252714	5.0	21.5	62.3	74.7	11.9	33.3	0.3	0	0
X	3272.4	B	436856	6252800	32.4	67.0	212.7	301.5	18.4	90.0	1.0	0	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 10030		FLIGHT 6											
Y	3214.4	B	437763	6253718	22.3	41.7	131.9	224.2	7.5	60.8	0.9	2	0
Z	3207.2	B	437813	6253761	16.2	7.6	205.0	244.5	11.5	76.7	4.1	27	0
AA	3189.2	B	437899	6253839	29.5	41.8	127.1	137.9	21.5	56.9	1.3	0	0
AB	3165.6	B	438009	6253957	113.8	60.5	631.4	343.8	203.9	306.5	6.6	0	0
LINE 10040		FLIGHT 6											
A	4404.3	S?	429956	6245743	1.0	18.0	11.2	49.5	12.0	6.4	---	---	46
B	4419.1	B	430195	6245984	14.3	52.8	72.3	267.0	5.1	48.6	0.5	0	0
C	4423.5	H	430274	6246061	3.3	9.7	72.3	267.0	5.1	48.6	0.3	2	0
D	4475.3	B	430826	6246604	38.9	109.6	244.9	379.7	12.7	99.8	0.8	0	0
E	4481.3	B	430873	6246647	38.8	91.3	222.2	379.7	12.7	99.8	0.9	0	14
F	4497.4	H	431004	6246782	5.4	43.6	67.0	155.2	7.0	38.3	0.2	0	0
G	4510.6	D	431192	6246971	63.6	55.7	277.8	237.4	64.2	122.6	2.9	0	0
H	4515.7	B	431270	6247047	9.8	22.4	218.8	143.3	62.7	108.5	0.6	2	0
I	4522.7	B	431326	6247113	18.9	13.6	71.9	74.7	10.0	30.4	2.5	18	0
J	4532.3	B	431399	6247187	14.2	20.8	150.9	124.9	39.6	68.3	1.0	5	0
K	4557.7	B	431685	6247468	32.7	45.2	212.2	237.5	27.8	81.2	1.4	0	0
L	4563.5	B?	431761	6247546	17.4	27.5	212.2	237.5	27.8	81.2	1.0	6	0
M	4579.2	H	431990	6247775	10.4	21.7	40.0	63.7	6.4	18.4	0.6	3	0
N	4596.4	H	432314	6248088	32.5	18.2	52.4	22.2	42.8	18.9	4.0	9	0
O	4603.7	B	432452	6248224	42.6	60.3	275.5	279.2	41.7	109.5	1.5	0	0
P	4610.9	B	432573	6248343	40.9	27.0	218.2	131.6	65.8	101.8	3.5	0	0
Q	4623.4	H	432738	6248527	1.5	11.1	64.6	68.0	12.3	27.5	0.1	0	0
R	4627.5	S?	432797	6248584	10.8	18.6	64.6	68.0	7.3	27.4	0.8	0	0
S	4644.4	S?	433065	6248833	8.6	31.9	98.0	167.6	6.8	39.7	0.4	0	0
T	4699.0	S?	433797	6249563	2.0	10.1	4.9	39.9	0.3	5.6	---	---	0
U	4925.8	B	436681	6252425	25.1	28.4	121.7	119.4	22.3	57.3	1.6	0	0
V	4936.8	H	436830	6252575	10.0	11.5	111.3	119.6	22.9	57.1	1.1	19	0
W	4947.7	B	436952	6252693	21.0	53.6	151.8	342.7	12.5	77.3	0.7	0	0
X	4951.9	H	437014	6252759	12.0	30.1	151.8	342.7	12.5	77.3	0.6	0	0
Y	5004.2	S?	437868	6253583	4.6	32.4	80.6	264.1	4.2	45.6	0.2	0	0
Z	5034.0	H	438097	6253845	7.2	0.5	21.0	3.2	24.8	18.3	49.9	0	0
AA	5041.4	B	438181	6253920	41.8	24.8	108.4	81.3	21.3	47.7	4.1	0	0
LINE 10050		FLIGHT 6											
A	5938.3	D	430303	6245899	14.6	43.4	86.4	172.5	6.7	38.3	0.6	0	0
B	5933.4	H	430410	6246009	6.7	18.7	86.4	172.5	6.7	38.3	0.4	0	0
C	5931.0	H	430469	6246067	13.3	18.7	70.6	142.0	6.7	38.3	1.0	9	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 10050		FLIGHT 6											
D	5891.3	H	431009	6246576	5.6	27.0	106.0	196.5	4.2	19.3	0.3	0	0
E	5881.0	B	431074	6246654	10.5	17.4	114.9	168.9	14.6	50.8	0.8	13	0
F	5860.0	B	431194	6246775	20.9	49.9	95.3	151.1	12.1	45.0	0.7	0	0
G	5850.1	B	431300	6246897	43.9	46.5	157.8	176.8	39.3	66.8	2.1	0	0
H	5846.3	H?	431371	6246960	6.0	11.6	157.8	176.8	40.7	66.8	0.6	0	0
I	5839.6	D	431469	6247058	69.8	87.5	315.6	279.7	71.6	143.0	2.0	0	0
J	5816.6	B	431697	6247288	12.2	17.6	4.7	50.2	0.0	3.3	1.0	1	0
K	5807.2	D	431803	6247388	28.8	39.2	102.3	104.4	8.8	29.9	1.4	0	0
L	5797.3	B	431912	6247506	17.2	41.9	184.7	229.2	20.8	71.1	0.7	0	0
M	5760.8	H	432412	6247999	42.2	20.7	388.9	220.2	119.8	170.9	5.2	0	0
N	5756.6	B	432490	6248069	43.6	52.5	388.9	220.2	119.8	170.9	1.8	0	0
O	5747.7	B	432632	6248193	12.2	55.0	142.5	200.9	65.8	84.6	0.4	0	0
P	5737.2	B	432744	6248292	39.9	46.6	218.6	119.2	45.6	83.8	1.8	9	0
Q	5729.2	H	432800	6248349	47.3	52.7	201.2	229.5	20.4	79.6	2.0	0	0
R	5719.1	B	432933	6248492	34.2	79.8	258.8	402.9	9.2	99.1	0.9	0	0
S	5717.2	B	432968	6248532	39.8	81.1	258.8	402.9	9.2	99.1	1.0	0	0
T	5709.2	B	433130	6248703	10.0	39.7	116.8	221.9	3.5	46.8	0.4	0	0
U	5706.2	H	433194	6248767	18.9	44.6	116.8	221.9	3.5	46.8	0.7	0	0
V	5453.7	D	436799	6252351	49.4	57.4	180.4	217.6	3.9	71.7	1.9	0	0
W	5445.8	H	436944	6252484	13.5	7.3	93.5	59.1	23.3	34.1	3.2	17	0
X	5434.4	D	437086	6252611	8.4	11.9	62.8	81.7	10.4	25.9	0.9	14	0
Y	5427.8	H	437166	6252694	8.3	16.8	99.1	111.3	11.6	40.4	0.6	6	0
Z	5411.8	E	437501	6253023	8.0	28.4	86.6	130.5	7.0	38.3	0.4	0	0
AA	5402.9	H	437692	6253214	17.6	28.6	114.8	175.0	9.4	46.7	1.0	0	0
AB	5381.2	B	437948	6253486	7.5	29.9	82.3	222.4	5.3	41.5	0.3	0	0
AC	5369.0	B	438012	6253565	9.3	27.4	75.8	164.2	9.1	35.8	0.5	0	0
AD	5356.0	B	438060	6253612	7.1	25.2	67.0	100.8	14.4	27.5	0.4	0	0
AE	5331.7	D	438154	6253701	7.4	0.0	410.7	203.1	194.0	225.1	908.9	47	0
AF	5324.5	B	438220	6253763	40.9	35.6	410.7	203.1	68.5	225.1	2.5	3	0
LINE 10051		FLIGHT 7											
A	2114.2	S	428459	6244058	1.1	19.5	19.9	101.8	2.3	16.7	---	---	0
B	2020.0	S?	429568	6245167	3.4	10.5	10.0	25.8	1.0	4.4	---	---	0
LINE 10060		FLIGHT 7											
A	1536.5	S?	430103	6245484	0.1	2.3	3.3	33.4	0.3	5.3	---	---	0
B	1491.9	H	430499	6245897	5.9	34.2	101.4	223.3	8.2	48.7	0.2	0	0
C	1490.4	B	430528	6245922	8.6	14.8	101.4	223.3	8.2	48.7	0.7	2	0

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 shallow dip or magnetite/overburden effects

EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 10060			FLIGHT 7										
D	1447.7	E	431216	6246566	1.5	3.3	50.6	51.6	7.8	18.2	0.3	29	0
E	1435.0	B	431267	6246634	11.9	19.2	65.5	126.7	6.3	32.9	0.9	7	0
F	1422.9	D	431299	6246675	8.4	35.7	118.2	74.1	21.5	53.0	0.3	0	0
G	1414.8	B	431339	6246720	26.7	35.6	121.0	150.0	2.6	47.4	1.4	2	0
H	1401.3	H	431463	6246831	58.3	71.5	140.7	222.8	33.6	63.5	1.9	0	0
I	1390.4	D	431648	6247012	68.7	40.5	340.2	145.3	115.4	159.7	4.9	0	0
J	1361.6	B	431996	6247383	27.1	53.4	258.5	245.2	40.6	109.4	0.9	0	0
K	1358.0	B	432057	6247439	46.7	55.6	258.5	245.2	40.6	109.4	1.9	0	0
L	1343.7	H	432281	6247637	8.3	11.5	3.5	0.0	0.0	1.8	0.9	12	0
M	1329.8	H	432472	6247832	57.5	34.1	370.1	121.5	146.2	167.2	4.5	0	0
N	1326.4	B	432514	6247882	22.2	7.1	367.2	106.6	146.2	166.6	7.7	10	0
O	1321.5	B	432573	6247943	83.0	87.5	437.3	342.0	87.0	200.0	2.6	0	0
P	1305.6	D	432732	6248085	0.0	3.2	369.6	8.3	135.0	183.4	0.1	14	0
Q	1302.0	B	432781	6248126	52.4	33.1	369.6	282.4	135.0	183.4	4.1	2	0
R	1297.9	E	432848	6248183	81.6	86.7	342.6	282.4	59.5	147.1	2.5	0	0
S	1288.9	H	433013	6248350	15.4	37.1	34.9	75.2	3.5	13.3	0.7	0	0
T	1167.7	S?	434461	6249795	1.1	0.3	15.5	24.3	21.3	2.6	---	---	0
U	997.7	E	436888	6252204	28.7	59.3	154.9	237.4	6.9	53.9	0.9	0	0
V	995.3	H	436935	6252256	13.2	15.5	154.9	237.4	14.7	53.9	1.2	7	0
W	982.6	B	437141	6252457	23.4	49.3	113.9	117.4	19.2	50.7	0.8	0	0
X	950.5	B?	437715	6253035	25.3	41.7	198.9	222.9	16.0	75.5	1.1	0	0
Y	923.1	B	437979	6253295	10.0	15.7	91.1	105.9	12.3	38.1	0.8	12	0
Z	900.4	B	438087	6253401	11.8	20.4	120.4	155.9	13.8	48.9	0.8	8	0
AA	890.7	B	438128	6253445	0.0	10.6	32.8	66.0	24.0	13.3	0.1	23	0
AB	875.4	B	438192	6253508	47.7	16.4	731.5	28.8	175.1	344.1	8.8	7	0
AC	868.8	B	438236	6253551	141.4	82.5	747.2	391.5	175.1	344.1	6.2	0	0
AD	856.8	D	438312	6253617	11.7	22.8	58.9	71.7	21.2	24.4	0.7	0	0
AE	845.0	D	438397	6253709	15.7	11.2	83.1	58.2	24.3	41.4	2.3	0	0
LINE 10070			FLIGHT 7										
A	2408.6	H	430617	6245772	10.2	30.8	70.9	139.7	7.7	33.4	0.5	0	0
B	2413.2	H	430695	6245857	6.4	14.1	70.9	139.7	9.8	25.3	0.5	0	0
C	2453.5	H	431317	6246466	6.6	14.5	51.6	62.1	2.7	19.2	0.5	0	0
D	2460.8	D	431391	6246542	19.3	30.9	50.3	73.1	6.2	19.6	1.0	0	0
E	2471.1	B	431492	6246649	45.2	50.8	207.1	175.6	32.2	77.5	2.0	0	0
F	2482.2	B	431628	6246786	79.6	118.5	202.8	192.3	50.0	90.0	1.8	0	0
G	2490.4	B	431755	6246918	53.1	99.8	266.5	364.0	61.7	122.9	1.2	0	0
H	2518.0	H	432105	6247244	18.7	19.0	145.6	93.7	36.8	63.5	1.6	2	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 10070			FLIGHT 7										
I	2529.6	B?	432373	6247504	13.7	26.6	49.5	72.9	7.6	18.9	0.8	4	0
J	2538.4	B	432532	6247671	58.2	61.4	440.0	296.8	141.9	192.0	2.3	0	0
K	2550.0	B	432681	6247823	81.7	54.1	529.4	279.2	167.0	262.2	4.4	0	0
L	2562.4	B	432909	6248042	84.6	59.6	393.1	308.6	108.5	173.8	4.2	0	0
M	2565.0	E	432960	6248099	72.8	73.0	393.1	308.6	23.4	173.8	2.6	0	0
N	2833.0	D	437120	6252209	26.1	30.7	141.7	206.0	10.4	58.4	1.6	1	0
O	2847.5	B	437265	6252365	17.9	27.9	84.0	123.7	10.2	37.6	1.0	0	0
P	2873.4	S?	437602	6252712	4.8	0.0	75.3	197.5	13.3	44.7	---	---	0
Q	2899.8	S?	438002	6253095	5.0	43.1	78.4	219.3	3.4	38.2	0.2	0	0
R	2911.5	H	438112	6253192	9.1	20.4	22.3	76.3	7.1	8.8	0.6	0	0
S	2927.1	B	438265	6253358	52.1	45.5	606.4	561.0	88.5	236.3	2.7	0	0
T	2930.6	B	438307	6253400	179.1	197.9	606.4	561.0	88.5	236.3	3.2	0	0
LINE 10080			FLIGHT 7										
A	3804.4	H?	430774	6245717	3.8	15.0	65.3	120.5	2.5	31.3	0.3	1	0
B	3797.9	H	430860	6245809	12.7	30.5	65.3	121.1	7.6	29.0	0.6	0	0
C	3775.2	H	431291	6246220	6.4	21.8	65.5	161.4	9.8	36.4	0.4	0	0
D	3765.3	B	431473	6246394	19.6	34.8	160.6	190.6	10.5	55.7	0.9	0	0
E	3744.7	B	431659	6246602	26.7	30.8	80.1	67.1	21.7	34.2	1.6	0	0
F	3734.4	H	431711	6246652	39.6	93.8	273.4	383.6	52.0	139.1	0.9	0	0
G	3724.3	B	431748	6246686	73.7	84.8	472.6	357.2	65.6	184.3	2.2	0	0
H	3718.9	B	431769	6246709	23.1	47.8	655.2	560.5	94.3	273.9	0.9	0	0
I	3705.9	B	431938	6246878	54.0	80.4	221.1	144.0	40.0	91.4	1.5	0	0
J	3690.2	H	432170	6247113	10.8	27.5	121.1	99.6	48.5	56.5	0.6	0	0
K	3687.0	B?	432219	6247160	16.0	33.0	121.1	254.0	48.5	56.5	0.8	0	0
L	3662.9	H	432563	6247498	32.0	42.9	124.5	196.9	66.5	65.4	1.4	0	0
M	3655.1	D	432660	6247584	25.3	20.5	129.7	52.5	111.0	64.4	2.3	2	0
N	3642.0	B	432828	6247764	48.3	71.2	334.4	507.1	122.0	216.3	1.5	0	0
O	3640.4	B?	432851	6247790	79.9	92.0	436.1	507.1	122.0	236.8	2.3	0	0
P	3633.3	H	432957	6247893	51.9	20.1	411.2	160.9	117.5	184.5	7.7	5	0
Q	3618.8	E	433145	6248083	13.3	27.6	36.3	105.9	8.7	26.5	0.7	0	0
R	3366.4	H?	436793	6251668	2.0	7.3	26.0	71.2	1.2	11.8	---	---	0
S	3342.7	H	437288	6252189	13.4	8.3	62.3	59.3	5.3	26.0	2.6	14	0
T	3332.9	H	437489	6252363	8.1	12.5	18.2	22.8	11.9	12.3	0.8	6	0
U	3319.3	B	437725	6252608	12.4	33.6	140.8	221.2	13.9	58.4	0.6	0	0
V	3314.0	B	437813	6252707	7.9	20.7	124.1	192.2	13.9	51.0	0.5	0	0
W	3294.3	S?	438052	6252960	11.9	45.0	109.2	292.6	0.8	52.4	0.4	0	0
X	3263.1	B	438236	6253123	1.1	7.5	91.4	124.5	8.5	35.3	0.1	0	0

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EM Anomaly List

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LINE 10080		FLIGHT 7											
Y	3258.0	B	438260	6253144	1.8	4.8	53.7	81.7	8.3	19.5	0.3	11	0
Z	3238.9	D	438363	6253251	31.9	17.8	173.9	98.1	57.2	85.4	4.0	10	0
AA	3228.9	B	438420	6253316	43.3	30.3	349.1	278.5	43.8	141.9	3.3	0	0
LINE 10090		FLIGHT 7											
A	4365.6	H?	430880	6245612	9.8	17.7	48.6	134.0	7.3	26.2	0.7	6	0
B	4370.0	H	430981	6245714	1.9	12.9	40.8	66.4	8.4	17.8	0.1	0	0
C	4403.3	H	431684	6246407	14.1	26.3	44.1	114.4	5.7	20.3	0.8	0	0
D	4418.4	B	431876	6246601	103.1	105.6	577.8	451.5	114.2	268.9	2.9	0	0
E	4424.6	B?	431965	6246690	40.1	28.6	0.0	0.0	28.2	0.0	3.2	0	0
F	4436.1	B	432140	6246857	39.8	69.0	276.4	509.7	13.3	119.3	1.2	0	0
G	4442.8	H	432232	6246946	28.5	32.2	245.0	143.1	4.6	37.9	1.7	0	0
H	4475.6	D	432785	6247478	67.1	0.0	516.6	308.4	264.5	255.5	999.0	0	0
I	4479.6	B?	432854	6247541	22.5	17.9	235.5	204.5	264.5	134.5	2.3	5	0
J	4486.9	B	432951	6247628	78.6	70.6	180.7	181.3	6.7	77.8	3.0	0	0
K	4503.0	B?	433148	6247854	129.6	117.8	243.5	223.6	29.4	102.1	3.5	0	0
L	4510.6	H?	433269	6247972	22.3	18.0	59.5	34.5	3.2	25.1	2.3	0	0
M	4529.9	E	433665	6248357	2.2	11.7	15.3	40.0	0.3	6.4	---	---	0
N	4735.3	H	436717	6251397	7.7	15.2	82.5	131.7	7.6	34.7	0.6	1	0
O	4742.7	H	436846	6251528	4.3	21.9	48.4	122.2	7.4	25.2	0.2	0	0
P	4758.8	S?	437051	6251736	10.1	21.2	40.2	101.7	0.0	7.0	0.6	1	0
Q	4779.0	H	437408	6252076	12.5	10.2	108.0	66.9	14.4	42.5	1.8	22	0
R	4787.9	B?	437518	6252197	9.1	2.5	34.6	41.8	7.7	9.5	7.0	46	0
S	4804.7	B	437761	6252443	26.9	23.5	137.6	154.9	11.5	48.1	2.2	10	0
T	4817.4	B?	437947	6252621	7.9	6.5	43.2	0.7	12.5	20.4	1.6	19	0
U	4859.9	H	438313	6252971	10.2	15.7	37.5	46.2	10.0	7.6	0.9	0	0
V	4881.2	D	438521	6253200	18.2	19.3	88.7	105.8	11.8	32.2	1.5	0	0
W	4883.8	E	438552	6253241	22.5	30.6	88.7	105.8	8.0	32.2	1.3	0	0
LINE 10100		FLIGHT 7											
A	5772.4	H?	430255	6244785	3.5	10.3	13.9	17.2	3.0	2.9	0.3	9	0
B	5706.7	H	431264	6245796	3.2	5.1	22.1	9.2	7.1	6.3	0.6	21	0
C	5687.7	H	431642	6246165	7.5	13.1	50.4	83.0	5.8	24.2	0.7	2	0
D	5666.4	D	431924	6246437	58.7	49.3	343.8	247.2	82.5	162.2	3.0	0	26
E	5653.2	B	432023	6246531	163.1	276.5	1144.5	1452.7	152.4	537.0	2.0	0	0
F	5645.2	B	432086	6246595	47.0	43.5	203.3	247.4	18.3	78.8	2.5	3	0
G	5592.6	E	432850	6247370	58.5	65.5	438.0	203.9	188.0	204.1	2.1	0	0
H	5588.5	B	432913	6247427	31.9	36.9	380.4	203.9	188.0	204.1	1.7	0	0

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EM Anomaly List

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LINE 10100		FLIGHT 7											
I	5575.4	B	433051	6247567	32.8	38.6	248.1	127.3	185.1	181.9	1.7	0	0
J	5567.8	B	433171	6247671	55.6	19.6	274.0	56.9	178.2	154.6	9.0	0	0
K	5555.8	D	433334	6247838	23.9	19.6	70.1	41.4	13.0	29.1	2.3	0	34
L	5323.0	H	436696	6251160	23.5	16.4	190.3	125.8	17.1	63.3	2.7	17	0
M	5316.0	H?	436855	6251337	13.5	25.5	73.6	117.2	16.3	51.5	0.8	4	0
N	5287.7	H	437254	6251721	6.1	21.3	103.1	105.2	4.1	36.1	0.4	0	0
O	5284.8	H	437295	6251762	8.0	18.4	103.1	105.2	5.2	36.1	0.6	1	0
P	5257.2	H	437676	6252142	7.2	14.8	43.7	78.2	6.5	22.6	0.6	7	0
Q	5240.8	H	437907	6252396	15.0	11.6	39.9	31.2	8.5	16.3	2.1	6	0
R	5229.4	D	438070	6252566	17.9	29.4	62.5	129.8	5.0	27.2	1.0	0	0
S	5217.0	D	438204	6252688	3.8	7.2	0.2	0.0	1.3	0.0	0.5	22	0
T	5204.9	B	438297	6252772	9.8	16.4	112.9	154.3	13.2	45.2	0.8	11	0
U	5192.8	B	438374	6252829	14.4	11.1	63.5	104.3	19.8	23.7	2.1	22	0
V	5185.0	B	438398	6252856	11.0	29.2	178.4	195.4	40.2	88.2	0.5	0	0
W	5178.9	B	438420	6252876	30.9	0.0	140.8	169.7	34.2	62.8	999.0	26	0
X	5164.0	B	438514	6252964	36.1	19.6	232.7	53.7	64.1	111.8	4.3	0	0
Y	5155.3	B	438607	6253063	38.7	74.2	246.4	431.1	10.8	98.6	1.1	0	0
LINE 10110		FLIGHT 7											
A	6232.3	E	430890	6245208	5.1	11.7	30.0	48.2	3.9	12.5	0.5	5	0
B	6255.5	H	431445	6245759	9.4	8.6	53.9	48.2	6.6	17.6	1.5	18	0
C	6267.6	H	431714	6246033	5.1	1.2	3.4	0.0	6.8	9.2	7.1	60	0
D	6276.4	H?	431886	6246194	13.6	28.4	54.3	105.8	16.7	24.6	0.7	0	0
E	6289.9	B	432098	6246405	87.6	85.2	376.3	301.6	69.1	163.3	2.9	0	0
F	6292.5	B	432133	6246436	80.4	65.6	376.3	301.6	25.9	163.3	3.4	0	0
G	6340.6	H	432877	6247163	5.7	22.4	95.0	72.5	25.9	48.4	0.3	0	0
H	6348.7	B	432980	6247261	19.3	24.1	85.9	44.5	34.3	52.1	1.3	6	0
I	6358.2	B	433149	6247431	29.2	38.9	148.6	91.1	56.9	73.6	1.4	0	0
J	6363.3	B	433251	6247532	25.0	20.4	116.4	52.7	25.6	52.5	2.3	7	0
K	6369.3	B?	433375	6247657	18.7	16.9	65.0	66.2	2.0	23.5	1.9	9	0
L	6409.7	S?	434308	6248585	3.8	4.6	8.5	15.1	7.0	2.6	---	---	0
M	6543.3	E	436489	6250757	9.9	13.5	52.4	83.5	4.6	18.3	1.0	16	0
N	6548.5	B	436602	6250868	38.8	58.3	234.4	309.7	9.1	80.5	1.4	0	0
O	6553.5	H	436714	6250975	14.0	16.4	136.6	118.9	20.7	44.7	1.3	15	0
P	6586.1	H	437383	6251634	5.6	11.8	61.4	83.6	10.4	27.2	0.5	10	0
Q	6589.8	H	437441	6251692	6.2	12.6	57.5	83.6	7.1	27.2	0.6	19	0
R	6606.8	B?	437643	6251894	4.4	2.2	42.4	35.2	8.1	16.9	2.4	50	0
S	6619.6	H	437793	6252053	5.1	10.1	51.2	69.5	10.4	21.7	0.5	12	0

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LINE 10110		FLIGHT 7											
T	6645.6	H	438208	6252448	2.0	3.3	75.1	113.2	7.6	33.7	0.5	29	0
U	6653.8	D?	438323	6252564	11.8	14.9	13.2	7.1	3.6	7.1	1.1	0	0
V	6657.4	B	438353	6252601	8.2	12.9	45.5	76.4	4.3	20.2	0.8	16	0
W	6673.0	B	438473	6252721	41.7	39.0	92.9	68.1	24.2	51.0	2.3	4	0
X	6680.9	B	438541	6252797	75.3	86.1	407.9	138.9	41.9	86.9	2.3	0	0
LINE 10120		FLIGHT 8											
A	1458.9	H	430601	6244715	2.2	8.1	4.6	61.2	0.9	10.8	---	---	0
B	1406.7	H	431453	6245545	9.3	10.2	47.9	59.8	9.3	18.0	1.2	6	0
C	1386.9	B?	431838	6245932	16.2	23.1	147.5	132.3	17.4	56.2	1.1	0	0
D	1367.2	H	432126	6246211	9.9	5.5	77.1	30.0	28.2	39.8	2.8	27	0
E	1359.2	D	432203	6246291	99.3	88.8	414.4	397.5	63.3	179.5	3.3	0	0
F	1317.0	E	432893	6246986	7.9	18.2	78.4	161.6	3.8	34.0	0.5	1	0
G	1311.2	D	432968	6247047	21.5	22.5	89.8	161.6	1.4	29.1	1.7	12	0
H	1296.3	B	433052	6247140	11.0	6.8	120.1	64.3	22.2	57.5	2.5	24	0
I	1283.1	D	433210	6247303	98.3	58.4	319.2	168.3	101.2	160.9	5.4	0	0
J	1274.4	H	433389	6247479	2.2	6.1	92.8	61.8	11.5	39.0	0.3	12	0
K	1271.1	D	433448	6247544	20.3	16.4	88.6	54.5	11.3	38.9	2.2	8	0
L	1243.3	S?	433889	6247952	3.6	4.4	12.0	12.4	15.7	2.4	---	---	0
M	1099.8	H?	436088	6250160	3.4	14.6	72.4	86.1	3.1	25.7	0.2	0	0
N	1076.6	H	436575	6250624	17.3	14.2	109.4	69.2	15.9	45.9	2.0	16	0
O	1068.8	H	436732	6250776	26.9	33.7	164.5	132.1	15.5	68.8	1.5	0	0
P	1031.5	S?	437430	6251492	12.6	45.9	68.9	222.2	2.0	43.0	0.4	0	0
Q	1005.9	H	437827	6251873	7.2	10.8	32.1	53.8	6.7	13.7	0.8	17	0
R	1000.3	H	437920	6251968	7.6	8.6	28.4	23.3	7.8	11.7	1.1	16	0
S	957.0	D	438524	6252559	5.0	9.4	38.3	65.5	1.0	15.1	0.6	10	0
T	944.1	D	438684	6252708	18.6	15.5	153.8	102.8	4.6	24.3	2.0	11	0
U	941.2	E	438728	6252752	23.6	20.6	31.9	84.0	7.9	13.8	2.1	0	0
LINE 10130		FLIGHT 8											
A	1955.1	H	431502	6245388	9.7	21.1	129.6	61.1	22.7	45.3	0.6	0	0
B	1960.1	D	431600	6245485	33.5	51.5	129.6	209.3	0.0	45.3	1.3	3	0
C	1967.1	H	431720	6245611	9.3	9.6	39.0	43.2	15.3	20.0	1.3	12	0
D	1982.4	H	431906	6245784	7.6	8.4	109.6	15.9	6.1	34.4	1.1	9	0
E	1988.0	D	431999	6245865	26.2	38.8	109.6	115.2	6.1	34.4	1.2	0	0
F	1999.7	D	432210	6246074	50.5	39.1	200.3	140.9	39.4	88.7	3.1	2	0
G	2047.5	E	433071	6246934	10.2	14.3	60.3	94.4	1.8	23.4	0.9	16	0
H	2052.3	H?	433158	6247023	6.7	18.0	60.3	94.4	2.7	23.4	0.5	0	0

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LINE 10130		FLIGHT 8											
I	2073.8	D	433545	6247422	16.3	20.0	75.1	86.4	2.1	26.0	1.3	0	0
J	2097.3	S?	433950	6247796	2.8	1.2	12.7	1.8	16.7	1.2	---	---	0
K	2201.7	H?	435619	6249474	2.6	10.6	7.5	33.4	0.7	6.2	---	---	17
L	2214.9	H	435865	6249734	2.6	9.2	50.5	133.8	1.7	17.0	0.3	11	0
M	2218.2	H	435933	6249798	8.2	5.1	23.7	133.8	4.1	17.0	2.3	33	0
N	2220.7	H	435981	6249845	9.7	26.4	23.7	0.0	4.1	10.5	0.5	1	0
O	2230.2	H	436174	6250033	17.5	17.9	82.4	151.9	3.4	33.3	1.6	14	45
P	2232.6	H	436227	6250086	3.2	17.9	82.4	151.9	3.5	33.3	0.2	0	44
Q	2248.2	H	436590	6250433	1.0	4.1	6.7	23.7	9.9	9.4	0.2	9	0
R	2287.9	H	437499	6251342	1.8	6.0	37.3	63.2	5.7	12.8	0.3	8	0
S	2319.4	H	438008	6251840	0.0	2.4	32.1	46.6	7.9	17.1	0.1	24	0
T	2340.1	H	438316	6252143	1.0	8.7	43.5	61.3	4.9	16.4	0.1	0	0
U	2357.8	B?	438579	6252389	7.2	17.9	131.1	219.2	8.3	59.3	0.5	0	0
V	2363.6	H?	438661	6252475	8.4	35.6	64.5	244.1	1.8	59.3	0.3	0	0
W	2410.6	B	439273	6253087	15.4	37.9	50.1	162.4	2.4	32.2	0.7	0	14
X	2422.5	B	439354	6253182	2.9	7.3	0.9	5.9	2.6	2.3	0.4	16	0
LINE 10140		FLIGHT 8											
A	3189.1	H	430750	6244478	0.1	13.7	34.6	84.8	20.8	14.8	0.1	20	0
B	3146.3	D	431488	6245140	28.1	43.9	152.9	198.5	15.7	57.8	1.2	0	0
C	3138.1	H	431625	6245293	6.6	38.4	32.5	104.6	5.7	20.5	0.2	0	16
D	3125.6	H	431835	6245513	5.4	10.4	35.4	133.5	7.5	21.8	0.6	16	0
E	3101.4	H	432190	6245859	18.5	6.1	211.5	160.9	41.6	101.4	6.9	28	0
F	3094.9	D	432304	6245975	71.0	79.2	315.4	352.5	35.4	126.4	2.3	0	0
G	3030.8	H	433267	6246916	11.0	38.0	16.2	106.4	1.2	16.1	0.4	0	0
H	2863.2	H?	435761	6249391	8.6	10.9	12.9	18.2	0.8	4.4	1.0	0	13
I	2855.3	H	435951	6249598	4.1	12.4	112.5	198.7	6.1	53.0	0.4	11	0
J	2826.5	S?	436672	6250298	1.7	10.7	59.3	156.4	4.2	27.2	0.1	0	0
K	2816.8	D	436777	6250402	8.1	34.7	30.8	222.4	0.0	27.9	0.3	0	0
L	2738.0	H	438261	6251891	6.4	12.0	48.5	69.5	4.1	19.6	0.6	15	0
M	2726.1	B?	438476	6252091	1.2	4.0	41.2	34.5	17.1	20.1	0.2	11	0
N	2714.5	B	438637	6252253	8.8	34.2	87.2	135.4	7.3	38.5	0.4	0	0
O	2702.7	H?	438819	6252435	5.8	24.6	33.7	99.1	1.2	19.0	0.3	0	0
P	2638.7	D	439460	6253066	15.7	18.6	134.2	124.2	39.0	70.0	1.3	0	0
Q	2630.3	D	439563	6253162	15.3	13.0	5.4	0.5	9.3	5.4	1.9	7	0
LINE 10150		FLIGHT 8											
A	3617.0	H	430937	6244406	1.2	2.3	18.8	12.7	10.8	7.6	0.3	46	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 10150		FLIGHT 8											
B	3626.9	E	431130	6244610	34.9	44.4	378.9	256.7	149.9	172.5	1.6	0	0
C	3630.3	B	431201	6244684	46.6	57.8	378.9	256.7	149.9	172.5	1.8	0	0
D	3642.3	B	431468	6244940	199.4	144.5	1335.7	647.7	502.2	669.6	5.3	0	0
E	3681.1	D	432069	6245515	21.6	25.7	108.4	49.1	9.0	34.9	1.4	1	0
F	3686.1	B?	432165	6245616	25.2	13.2	137.2	78.6	50.6	55.3	4.0	12	0
G	3695.5	D	432327	6245776	36.8	71.9	382.5	425.6	41.5	177.3	1.0	0	0
H	3830.5	S	434494	6247941	1.9	6.3	53.2	76.3	2.3	19.6	0.2	7	0
I	3864.1	E	435287	6248715	2.0	10.7	32.1	66.6	16.7	13.5	0.2	0	0
J	3907.1	H	435972	6249411	2.8	1.3	74.5	169.0	5.4	21.2	2.2	78	0
K	3933.9	D	436568	6249986	27.3	35.7	230.9	260.5	24.9	92.8	1.4	0	0
L	3943.9	D	436710	6250137	10.4	9.4	129.2	127.7	5.5	61.5	1.5	20	0
M	3950.7	H	436795	6250206	6.3	16.6	90.1	129.6	9.7	42.1	0.5	3	0
N	3974.1	H	437084	6250462	4.3	7.7	18.8	4.1	4.3	3.6	0.5	0	0
O	3980.3	H	437171	6250560	2.7	10.1	32.9	79.6	4.3	14.8	0.3	5	0
P	4022.5	H	438012	6251426	2.8	2.4	30.1	24.2	4.4	11.3	1.0	54	0
Q	4066.7	D	438614	6252035	39.3	48.3	163.7	168.3	12.1	56.3	1.7	0	0
R	4074.2	B	438741	6252157	7.4	21.1	51.7	197.8	3.0	33.6	0.5	0	0
S	4184.5	D	439449	6252848	61.9	78.0	494.1	497.7	31.7	172.2	1.9	0	0
T	4196.8	D	439579	6252976	86.9	94.8	473.6	457.8	121.0	199.2	2.5	0	0
LINE 10160		FLIGHT 8											
A	4955.9	E	431313	6244603	45.6	26.3	234.1	62.5	179.5	209.7	4.4	9	0
B	4952.2	B	431361	6244652	46.0	43.7	471.0	307.0	179.5	209.8	2.4	0	0
C	4944.3	B	431485	6244762	53.9	79.7	495.3	352.6	229.7	210.1	---	---	0
D	4937.7	E	431591	6244857	54.4	13.4	80.3	18.4	35.0	160.2	14.9	18	0
E	4918.3	H	431867	6245125	5.4	9.8	36.6	69.2	5.4	13.9	0.6	12	0
F	4896.2	E	432107	6245357	26.2	26.1	109.1	116.6	19.6	44.6	1.9	1	0
G	4888.4	H?	432218	6245478	30.4	24.2	272.8	156.0	64.2	119.9	2.5	7	0
H	4886.4	D	432251	6245512	35.3	25.5	272.8	156.0	86.5	119.9	3.0	7	0
I	4873.9	D	432433	6245681	65.8	62.5	276.9	298.9	49.9	100.9	2.7	1	0
J	4868.1	B	432485	6245728	18.0	21.4	150.7	239.8	38.9	70.8	1.3	9	0
K	4862.1	B	432529	6245776	69.1	78.9	439.4	421.3	52.1	184.3	---	---	0
L	4767.2	S	433906	6247129	3.4	0.7	17.2	0.0	25.0	1.2	---	---	0
M	4755.9	E	434166	6247396	3.9	4.1	32.1	72.4	25.2	11.4	---	---	0
N	4742.3	H	434479	6247709	4.4	4.2	46.4	123.1	4.3	17.7	1.1	39	55
O	4673.7	S	435902	6249104	3.8	18.8	53.6	125.3	9.0	22.2	0.2	0	57
P	4667.3	S	436036	6249235	4.7	6.9	63.2	186.8	4.0	25.5	0.7	31	0
Q	4663.4	S	436121	6249320	9.9	29.6	63.2	186.8	3.7	34.4	0.5	2	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 10160			FLIGHT 8										
R	4642.7	H	436554	6249761	18.2	60.8	139.1	180.0	5.4	46.4	0.5	0	0
S	4636.2	H	436672	6249881	9.8	28.6	139.1	136.5	5.1	34.2	0.5	0	0
T	4624.3	H	436886	6250093	8.5	15.0	65.1	59.3	7.8	19.8	0.7	10	0
U	4594.8	B	437158	6250357	3.1	7.7	63.2	122.8	0.7	26.9	0.4	25	0
V	4584.9	B	437191	6250394	8.0	19.7	98.2	98.6	4.1	32.7	0.5	0	0
W	4568.4	H	437308	6250520	2.9	14.3	0.0	33.4	4.4	5.3	0.2	0	0
X	4533.4	B?	437945	6251153	9.5	6.2	55.1	20.6	53.6	15.0	2.2	32	138
Y	4521.6	H	438195	6251407	3.4	3.6	63.5	42.9	10.9	23.3	0.9	37	0
Z	4507.6	H	438423	6251635	3.7	8.2	9.1	74.4	0.5	6.6	0.4	18	0
AA	4499.3	D	438575	6251778	26.3	47.5	152.5	209.6	15.9	70.6	1.0	0	0
AB	4493.7	D	438696	6251893	38.2	43.2	190.7	170.5	17.1	72.0	1.8	0	11
AC	4428.3	B?	439751	6252906	16.9	6.4	139.9	40.4	61.6	67.8	5.4	0	0
LINE 10170			FLIGHT 8										
A	5480.0	H	431521	6244569	10.0	3.8	40.1	13.1	19.6	22.0	4.6	41	0
B	5484.0	H	431590	6244642	7.7	3.1	40.1	9.6	19.6	22.0	3.8	41	0
C	5502.7	H	431945	6244992	16.1	15.3	105.1	87.7	28.1	53.3	1.7	18	0
D	5517.3	B	432154	6245205	28.8	51.2	228.6	265.2	27.6	92.4	1.0	0	0
E	5522.7	B	432232	6245278	51.9	105.7	213.7	432.5	6.2	79.6	1.1	0	0
F	5532.0	D	432378	6245411	85.7	88.9	403.3	257.2	72.5	158.8	2.6	0	0
G	5538.0	D	432460	6245487	45.4	56.5	403.3	299.0	72.5	158.8	1.8	0	0
H	5546.4	D	432549	6245578	17.4	1.9	222.3	129.1	63.3	109.0	34.0	23	0
I	5551.1	D	432604	6245635	74.2	73.2	318.6	265.3	48.8	136.3	2.7	0	0
J	5611.8	E	433399	6246427	3.4	8.8	30.4	60.2	34.9	10.6	---	---	0
K	5639.3	E	433988	6247003	21.8	68.5	158.7	347.7	22.4	66.3	0.6	0	295
L	5644.3	S	434105	6247114	7.5	29.9	158.7	347.7	22.7	66.3	0.3	0	0
M	5653.6	S	434319	6247336	3.6	23.3	44.3	141.2	1.8	23.9	0.2	0	0
N	5669.2	S	434675	6247700	3.6	15.2	26.3	49.7	4.8	12.1	0.3	0	0
O	5706.1	S	435602	6248597	1.4	9.5	34.3	44.4	1.4	11.3	---	---	0
P	5799.3	D	437251	6250217	8.9	14.2	57.9	60.9	3.7	22.5	0.8	9	0
Q	5809.4	D	437403	6250367	13.6	9.8	26.6	15.1	0.0	10.8	2.2	6	0
R	5823.2	E	437592	6250562	7.4	7.4	16.7	63.2	1.3	8.7	1.2	15	0
S	5851.9	H	438270	6251248	10.2	10.0	95.2	119.8	13.8	39.5	1.4	29	14
T	5854.7	B	438326	6251304	14.0	26.6	95.2	119.8	13.8	39.5	0.8	0	0
U	5870.5	D	438540	6251515	22.6	33.9	83.1	161.5	8.1	27.5	1.1	0	0
V	5877.9	H	438639	6251616	9.0	13.4	23.0	93.8	3.4	16.1	0.8	19	0
W	5893.0	D	438805	6251783	26.4	26.2	72.2	65.5	4.8	22.5	1.9	0	0
X	6054.4	B	439871	6252825	64.0	61.6	447.7	268.7	112.1	198.8	2.6	0	0

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LINE 10180		FLIGHT 8											
A	6723.0	B?	432181	6245018	32.4	51.6	302.5	328.7	35.0	125.2	1.2	0	0
B	6719.6	D	432242	6245079	30.5	31.5	305.1	408.7	35.0	118.9	1.9	0	0
C	6714.3	B	432332	6245173	47.3	102.3	305.1	408.7	18.9	118.9	1.1	0	0
D	6704.4	D	432491	6245335	73.5	22.5	393.1	271.3	103.3	166.3	12.0	3	0
E	6700.8	B	432554	6245389	15.1	37.9	393.1	271.3	103.3	166.3	0.6	0	0
F	6692.1	D	432679	6245499	29.5	5.7	174.8	159.8	30.3	86.9	17.4	16	0
G	6687.4	E	432721	6245541	37.2	56.9	279.9	306.6	32.1	114.8	1.3	0	0
H	6643.4	S	433507	6246330	12.1	14.3	137.1	192.1	20.5	47.4	1.2	10	0
I	6629.5	S?	433855	6246654	10.4	8.0	111.0	52.5	8.1	25.2	1.8	29	0
J	6615.1	H	434195	6247002	18.6	37.8	137.0	185.2	5.4	46.7	0.8	2	0
K	6606.2	S	434393	6247199	6.2	29.7	67.1	250.9	2.5	44.6	0.3	0	0
L	6530.3	S	435720	6248511	2.5	16.0	52.3	188.0	0.8	31.8	0.2	0	0
M	6480.7	H	436610	6249390	3.3	15.9	35.6	109.9	3.1	19.2	0.2	0	0
N	6439.0	B	437328	6250100	6.9	1.0	64.8	72.4	7.3	23.8	15.6	37	0
O	6434.1	B	437404	6250174	6.9	10.6	42.7	72.1	7.3	20.4	0.8	16	0
P	6419.3	B	437507	6250280	0.9	0.0	66.9	129.8	2.7	28.6	---	---	0
Q	6408.6	B?	437568	6250355	9.9	10.3	59.9	38.9	6.4	18.7	1.3	10	0
R	6355.5	D	438541	6251312	32.5	59.3	181.6	341.9	9.9	68.4	1.1	0	0
S	6336.6	D	438866	6251647	48.8	83.9	223.4	369.2	5.3	84.0	1.3	0	0
T	6290.5	S?	439532	6252304	2.3	9.1	14.7	48.2	1.8	9.0	---	---	0
U	6251.1	B	440007	6252752	43.9	16.4	214.2	75.5	92.0	105.3	7.7	0	0
LINE 10190		FLIGHT 8											
A	7378.9	B	432455	6245088	63.3	103.9	364.9	410.0	48.7	144.9	1.5	0	0
B	7389.4	H?	432598	6245223	16.9	46.5	136.4	242.0	4.3	46.3	0.6	0	0
C	7398.6	D	432743	6245347	47.6	35.1	189.4	181.0	29.6	80.2	3.2	0	0
D	7402.7	E	432818	6245419	24.9	39.1	51.8	181.0	23.7	22.6	1.1	0	0
E	7418.1	S	433091	6245711	11.2	34.4	52.2	164.5	26.3	27.4	0.5	0	36
F	7430.9	S	433420	6246019	13.6	16.9	91.4	113.5	2.7	30.4	1.2	11	0
G	7440.6	H?	433680	6246278	6.6	3.8	126.1	24.7	16.2	42.2	2.3	45	0
H	7447.5	H?	433866	6246474	3.9	4.7	70.9	22.4	7.2	29.5	0.8	40	0
I	7457.2	S	434130	6246743	15.1	11.3	32.3	3.4	6.1	11.9	2.2	17	76
J	7463.5	H	434307	6246913	14.0	19.6	120.0	178.3	7.0	43.1	1.1	5	85
K	7482.7	E	434821	6247409	2.4	7.1	21.0	66.9	25.2	12.9	---	---	0
L	7633.6	H	437101	6249675	5.2	6.0	41.3	64.4	4.4	17.3	0.9	12	0
M	7657.6	D	437515	6250071	2.4	12.8	29.2	33.6	0.0	13.7	0.2	0	0
N	7672.2	H	437710	6250283	5.6	5.1	43.6	53.4	4.7	12.6	1.2	22	0

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LINE 10190		FLIGHT 8											
O	7677.8	H	437819	6250381	6.4	13.3	45.7	98.7	3.9	17.2	0.6	2	0
P	7711.4	H	438611	6251171	8.0	11.2	90.9	167.0	6.1	39.0	0.9	22	0
Q	7733.6	D	439015	6251580	20.8	78.7	94.5	317.6	0.4	57.2	0.5	0	0
R	7852.6	H	439769	6252299	5.1	10.4	91.8	119.8	3.2	28.4	0.5	10	0
LINE 10200		FLIGHT 8											
A	8490.6	E	432566	6244982	4.4	28.0	75.0	115.8	20.5	36.8	0.2	0	0
B	8485.7	D	432669	6245082	13.3	12.4	61.2	106.8	16.1	27.8	1.6	4	0
C	8463.7	H?	433172	6245565	17.2	16.3	71.3	147.3	4.5	29.8	1.7	14	91
D	8452.5	H	433443	6245825	3.1	7.8	78.9	79.3	12.3	18.0	0.4	11	11
E	8439.5	H	433750	6246132	8.4	15.4	125.7	119.9	14.1	50.0	0.7	12	0
F	8437.3	H	433803	6246183	6.4	12.4	125.7	119.9	14.1	50.0	0.6	17	0
G	8429.5	H	433988	6246370	5.8	13.2	45.2	73.8	9.2	23.7	0.5	15	0
H	8411.7	H	434393	6246766	14.2	35.5	257.9	453.8	46.5	95.2	0.6	3	36
I	8406.9	E	434497	6246868	19.2	67.8	71.8	445.3	61.1	90.4	0.5	0	0
J	8399.9	S	434639	6247010	10.9	13.6	8.7	55.0	5.5	9.1	---	---	0
K	8390.5	S	434822	6247195	0.4	3.5	16.4	42.2	17.1	5.8	---	---	0
L	8275.2	H	437023	6249382	4.5	4.6	56.7	30.6	6.7	18.8	1.0	33	0
M	8270.2	H	437137	6249492	5.5	4.5	28.3	24.1	4.4	13.3	1.4	37	0
N	8248.1	H	437508	6249863	6.6	11.6	34.3	24.2	4.2	12.9	0.6	7	0
O	8202.5	E	438006	6250365	4.4	24.6	74.1	106.0	5.1	27.5	0.2	0	0
P	8176.1	S	438580	6250937	2.5	11.9	45.5	101.2	2.5	20.1	0.2	2	0
Q	8171.6	S	438691	6251053	4.0	7.3	71.6	138.3	3.0	30.6	0.5	22	0
LINE 10210		FLIGHT 8											
A	8973.8	E	432711	6244908	3.2	5.2	21.2	17.4	7.7	11.3	0.6	36	0
B	8978.7	H	432836	6245037	5.2	19.9	49.5	173.8	9.5	32.1	0.3	0	16
C	9009.2	H	433656	6245842	4.6	7.1	114.3	15.5	11.5	46.4	0.7	22	0
D	9033.3	H	434337	6246514	9.6	11.7	195.4	243.3	9.1	62.2	1.1	20	39
E	9041.5	E	434568	6246735	3.3	23.3	10.6	33.9	4.6	6.5	---	---	0
F	9156.3	H	437039	6249191	8.6	16.4	95.8	93.2	14.1	40.5	0.7	3	0
G	9161.1	H	437144	6249307	3.2	6.8	95.8	11.4	14.1	40.5	0.4	13	0
H	9214.3	H	438040	6250169	15.3	19.1	144.4	109.1	20.1	51.9	1.2	0	0
I	9218.0	H	438112	6250242	11.6	14.2	144.4	139.5	18.8	53.9	1.1	3	0
J	9255.8	E	439024	6251154	5.6	16.9	12.8	62.8	1.6	20.8	0.4	0	0
K	9273.6	L	439328	6251458	9.1	19.7	32.6	88.8	33.9	14.1	0.6	5	102

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 10220		FLIGHT 9											
A	1268.1	S	430078	6242076	4.8	13.7	7.3	34.6	0.8	4.7	0.4	4	0
B	1193.4	H	431469	6243452	4.4	1.7	12.8	4.7	10.1	5.2	3.4	49	0
C	1116.3	H	433003	6244976	4.9	11.8	51.7	159.5	7.6	30.0	0.5	9	0
D	1086.3	H	433583	6245548	8.1	11.3	98.0	65.8	5.6	29.1	0.9	19	85
E	1069.7	H	433897	6245873	5.9	13.6	85.6	151.6	13.8	35.2	0.5	9	0
F	1065.6	H	433978	6245941	8.8	24.9	197.0	255.2	13.8	47.3	0.5	4	0
G	1053.1	E	434213	6246164	22.3	90.5	34.6	475.3	31.1	89.8	0.5	0	60
H	870.4	H	437177	6249119	12.4	21.5	119.4	140.2	12.5	47.6	0.8	0	0
I	862.4	H	437348	6249291	5.9	14.8	7.5	22.8	1.8	5.3	0.5	0	0
J	831.3	H?	437802	6249729	9.7	14.0	20.6	23.5	1.9	8.8	0.9	12	0
K	806.9	D?	437947	6249890	3.6	10.4	0.0	0.0	0.8	0.0	0.4	2	0
L	779.7	B	438144	6250108	26.6	30.8	188.2	186.4	28.0	78.5	1.6	0	10
M	771.6	H	438292	6250240	10.0	46.8	106.9	187.8	7.9	49.9	0.3	0	0
N	732.2	S	439045	6250981	3.2	5.5	51.3	114.7	5.1	22.6	0.5	35	0
O	714.5	L	439457	6251367	6.6	8.0	40.4	102.2	45.0	16.3	1.0	23	136
LINE 10230		FLIGHT 9											
A	1631.4	S	430195	6241981	6.4	16.9	9.5	41.2	2.0	7.6	0.5	0	0
B	1692.4	B	431278	6243047	20.1	38.8	143.6	171.8	7.7	49.7	0.9	0	0
C	1694.9	B	431320	6243091	15.0	29.0	143.6	171.8	6.3	49.7	0.8	6	22
D	1706.6	D	431541	6243318	88.8	62.9	199.2	169.1	65.1	88.0	4.2	0	0
E	1776.7	H	433109	6244883	4.2	16.9	49.7	171.0	6.8	29.6	0.3	0	0
F	1797.5	B?	433613	6245378	8.5	29.7	90.4	198.5	14.8	38.0	---	---	114
G	1823.3	B?	434126	6245864	9.4	39.1	78.2	354.3	5.2	60.6	0.4	0	0
H	1976.9	H	437166	6248905	15.5	11.7	50.6	44.5	5.2	21.3	2.2	15	0
I	1984.7	H	437372	6249098	9.1	12.0	59.4	61.1	13.2	27.2	1.0	5	0
J	2000.8	H	437761	6249474	7.1	6.0	29.9	18.8	7.1	11.9	1.5	14	0
K	2045.9	D	438371	6250104	11.0	14.8	70.4	58.8	8.0	25.8	1.0	1	0
L	2055.0	H?	438562	6250288	3.5	6.5	1.1	9.2	5.8	2.1	0.5	8	0
M	2065.6	S	438811	6250527	4.7	18.3	81.9	184.4	5.5	34.5	0.3	5	27
N	2094.6	E	439535	6251249	2.1	3.6	4.1	15.8	2.1	4.2	---	---	0
LINE 10240		FLIGHT 9											
A	2936.8	D	431430	6242995	23.7	29.2	94.2	119.8	8.5	37.2	1.4	0	0
B	2924.7	D	431591	6243161	64.9	67.4	259.8	278.0	26.4	110.1	2.4	0	0
C	2914.1	B	431716	6243292	65.5	51.1	433.9	199.7	279.3	244.8	3.4	0	0
D	2910.2	B	431770	6243343	135.1	34.6	433.9	199.7	279.3	244.8	19.0	0	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 10240		FLIGHT 9											
E	2898.7	D	431935	6243494	34.6	62.1	138.1	208.5	5.8	53.9	1.1	0	0
F	2781.0	S?	434183	6245711	4.6	19.4	20.7	80.0	20.8	11.5	---	---	0
G	2594.4	E	437285	6248785	18.5	22.2	106.7	105.9	6.6	46.1	1.4	8	0
H	2591.2	D	437341	6248843	15.1	22.7	106.7	105.9	15.9	46.1	1.0	0	0
I	2585.1	B	437461	6248968	8.9	33.5	73.5	141.7	15.9	33.4	0.4	0	0
J	2571.4	H	437736	6249255	9.2	16.1	61.3	100.3	4.9	27.7	0.7	5	0
K	2554.1	D	437999	6249505	8.9	8.1	8.5	46.6	6.5	4.8	---	---	0
L	2545.0	D	438069	6249568	11.6	15.1	101.2	161.2	4.6	42.6	1.1	1	0
M	2541.2	B	438099	6249602	8.3	14.8	101.2	166.0	4.7	42.6	0.7	6	0
N	2510.7	H	438241	6249759	1.0	7.4	6.1	23.8	0.7	4.8	0.1	0	0
O	2481.2	B	438487	6249996	9.9	39.0	103.6	241.7	6.8	50.1	0.4	0	0
P	2471.8	B	438628	6250137	2.8	30.8	89.8	246.0	1.2	50.8	0.1	0	0
Q	2445.4	S	438972	6250472	4.2	2.4	58.3	166.9	3.7	32.9	2.0	59	0
R	2435.8	E	439173	6250673	3.7	37.1	40.2	204.8	2.3	35.4	---	---	76
S	2415.6	S	439523	6251032	3.1	17.3	41.9	181.3	2.3	30.4	0.2	0	0
LINE 10250		FLIGHT 9											
A	3213.3	B?	430473	6241836	5.9	15.1	5.6	39.2	1.8	6.4	---	---	0
B	3265.2	B?	431401	6242751	26.9	55.7	92.5	245.9	2.2	62.8	0.9	0	0
C	3271.4	B	431498	6242844	25.1	10.2	198.0	199.5	18.5	63.6	5.7	19	0
D	3276.8	B	431586	6242936	56.4	57.2	271.2	199.5	146.5	137.9	2.4	0	0
E	3289.0	B	431801	6243150	244.6	179.8	746.0	516.9	248.7	379.3	---	---	0
F	3318.3	H	432396	6243730	1.3	3.3	9.9	10.7	12.2	4.7	0.3	32	0
G	3328.0	H	432655	6243991	0.1	11.5	23.6	99.3	10.7	20.6	---	---	0
H	3351.9	H	433233	6244575	4.0	19.1	0.0	124.3	5.7	25.4	0.2	0	0
I	3362.7	D	433425	6244762	35.4	52.5	129.3	197.4	4.5	51.5	1.3	0	0
J	3580.0	E	437391	6248694	16.8	12.1	89.9	63.1	4.9	36.3	2.4	13	0
K	3584.0	H	437486	6248788	12.2	13.8	97.9	72.0	14.5	35.3	1.2	0	0
L	3597.6	H?	437842	6249144	13.1	12.8	84.0	113.5	4.6	31.6	1.5	0	0
M	3612.6	H	438170	6249462	8.4	14.4	29.2	59.2	2.3	12.0	0.7	2	0
N	3623.7	D	438313	6249583	13.0	9.7	32.3	35.0	2.4	10.4	2.1	13	0
O	3652.4	D	438743	6250038	12.9	39.7	69.1	151.4	2.5	30.1	0.5	0	0
P	3658.5	H	438843	6250130	6.0	24.1	39.2	59.7	3.7	11.2	0.3	0	0
Q	3670.1	H	439037	6250325	4.3	18.4	35.7	159.2	4.0	27.5	0.3	0	0
R	3693.2	S	439525	6250809	1.4	19.9	53.4	209.7	2.3	34.2	0.1	0	0
LINE 19020		FLIGHT 10											
A	4801.7	S?	430472	6242427	0.8	10.8	4.5	55.4	0.0	9.0	---	---	23

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 19030			FLIGHT 10										
A	4566.0	S	430120	6244915	3.7	11.0	5.2	12.2	1.1	3.0	---	---	0
B	4661.7	B	431695	6243307	72.7	49.0	782.8	281.1	412.0	423.2	4.2	0	0
C	4670.7	B	431789	6243214	23.8	13.4	232.2	188.3	147.8	105.0	3.6	11	0
D	4679.9	D	431880	6243119	33.7	21.9	320.9	83.0	121.6	178.3	3.4	5	0
LINE 19040			FLIGHT 10										
A	4212.0	D	430424	6246734	48.6	69.3	140.7	168.7	12.5	57.0	1.6	0	0
B	4202.8	D	430541	6246631	14.3	17.4	23.5	61.8	6.0	15.7	1.2	16	0
C	4120.6	H	431364	6245797	9.4	7.0	44.4	16.1	4.3	11.9	1.9	20	0
D	4089.4	E	431653	6245515	5.7	15.8	51.2	93.4	7.9	26.9	0.4	0	0
E	4083.2	B?	431740	6245436	16.8	17.8	98.8	112.4	15.9	40.9	1.5	2	0
F	4037.7	E	432133	6245019	26.3	31.0	153.5	112.2	38.8	69.9	1.6	0	0
LINE 19050			FLIGHT 10										
A	3691.4	D	431505	6247758	10.7	17.8	151.9	270.8	4.3	48.7	0.8	12	0
B	3698.3	D	431572	6247694	16.8	27.1	151.9	206.7	4.3	48.7	1.0	1	0
C	3711.0	H	431706	6247555	8.6	5.6	68.5	55.7	11.1	25.0	2.1	25	0
D	3717.8	D	431787	6247477	17.5	19.7	77.3	126.9	10.2	25.0	1.4	4	0
E	3724.8	D	431878	6247398	15.1	26.6	77.3	126.9	10.2	25.0	0.8	0	0
F	3733.4	B	431986	6247296	24.8	27.6	95.5	62.1	24.8	45.3	1.6	0	0
G	3747.5	B	432159	6247100	16.0	20.1	226.4	127.5	56.2	107.7	1.2	1	0
H	3754.4	E	432268	6246988	51.6	53.1	193.4	169.0	4.8	74.8	2.3	0	0
I	3837.2	H	433529	6245727	11.2	14.3	226.6	315.7	17.2	90.6	1.1	17	80
LINE 19060			FLIGHT 10										
A	5582.5	B?	432562	6248820	11.9	42.8	49.1	199.6	2.8	38.4	0.4	0	0
B	5599.3	H	432728	6248653	11.2	17.9	44.4	61.4	6.3	22.1	0.9	0	0
C	5619.5	D	432935	6248465	56.5	97.6	203.8	344.4	9.5	75.3	1.4	0	0
D	5655.3	H?	433338	6248054	10.6	24.2	50.3	172.3	1.8	30.2	0.6	0	0
E	5722.7	H	434204	6247193	5.7	23.1	89.8	261.2	12.7	50.3	0.3	0	0
F	5731.0	H	434360	6247029	6.2	8.0	89.8	244.8	3.5	32.5	0.9	25	0
LINE 19070			FLIGHT 10										
A	3212.8	H	435102	6248402	5.9	19.8	66.9	259.4	8.3	44.0	0.4	0	0
LINE 19080			FLIGHT 10										
A	2848.7	H	435928	6249696	5.2	8.5	99.0	214.0	5.3	42.4	0.6	24	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 19080			FLIGHT 10										
B	2862.5	E	436226	6249394	4.6	16.6	17.1	107.6	0.9	6.3	0.3	0	0
LINE 19090			FLIGHT 10										
A	2422.6	D	436670	6251086	38.2	35.6	176.7	140.9	19.2	69.3	2.3	0	12
B	2386.3	H	437269	6250474	4.5	12.6	14.8	40.2	0.6	7.3	0.4	0	0
C	2379.3	H	437322	6250425	12.9	24.2	42.1	37.9	2.5	12.4	0.8	2	0
D	2337.1	D	437962	6249774	10.7	20.0	43.1	68.3	0.9	16.6	0.7	0	0
E	2315.0	H	438219	6249522	10.9	30.5	47.3	92.9	2.3	23.0	0.5	0	0
LINE 19100			FLIGHT 10										
A	2015.7	H	436753	6253114	1.1	6.0	32.9	60.0	3.0	16.6	0.1	0	0
B	2047.1	H	437237	6252640	6.4	14.2	50.0	92.9	6.9	21.5	0.5	5	0
C	2056.5	D	437348	6252522	13.1	28.6	38.5	121.2	1.4	19.8	0.7	0	0
D	2098.0	H	437874	6251988	7.2	12.1	36.1	48.4	9.1	16.2	0.7	11	0
E	2137.7	D	438353	6251506	15.4	13.8	45.0	29.5	5.6	18.2	1.8	5	0
F	2145.4	D	438443	6251421	8.4	5.6	45.0	8.2	6.3	18.2	2.1	35	0
G	2153.0	D	438521	6251349	14.0	15.1	53.8	41.1	2.8	10.5	1.4	0	0
H	2157.7	B?	438578	6251288	7.0	1.3	53.8	123.7	4.1	14.9	11.7	46	0
I	2173.4	S?	438898	6250973	1.4	12.2	50.7	115.4	1.9	21.8	0.1	0	0
LINE 19110			FLIGHT 10										
A	1889.5	B	438037	6253954	151.1	144.8	1171.1	747.0	214.6	522.4	3.5	0	0
B	1883.4	D	438118	6253875	60.9	6.7	553.6	258.5	150.8	401.9	51.6	9	0
C	1868.5	D	438243	6253758	59.5	108.2	361.2	380.6	55.5	154.4	1.3	0	0
D	1861.3	E	438281	6253716	43.6	65.7	309.9	297.4	37.8	128.8	1.4	0	0
E	1768.6	B?	439636	6252346	13.7	25.0	48.7	84.0	0.9	16.8	0.8	3	0

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Anomalies Summary
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Conductor Grade	No, of Responses
7	3
6	1
5	2
4	6
3	18
2	254
1	275
0	43
Total	602

Conductor Model	No, of Responses
E	47
B	195
D	97
S	64
L	2
H	197
Total	602

EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 30010		FLIGHT 13											
A	1513.4	D	417184	6269664	18.9	11.2	53.0	33.1	18.9	27.5	3.1	0	0
B	1422.5	D	418061	6269645	18.7	5.4	36.2	32.5	12.3	18.9	8.3	3	0
C	1384.3	E	418326	6269616	35.6	43.7	354.4	274.3	94.3	155.2	1.6	5	0
D	1376.5	D	418372	6269618	30.7	23.4	354.4	274.3	94.3	136.7	2.7	3	0
E	1368.1	D	418454	6269624	27.5	129.1	281.2	307.0	82.0	133.2	0.5	0	0
F	1364.9	B	418503	6269629	72.9	129.1	281.2	348.9	82.0	133.2	1.4	0	0
G	1351.1	B	418805	6269622	156.1	72.0	476.5	153.4	284.8	214.1	8.8	0	0
H	1342.8	D	418981	6269623	11.8	5.3	1.9	28.2	10.0	0.9	3.8	15	344
I	1336.3	D	419127	6269627	31.7	33.9	64.7	58.2	7.1	23.2	1.8	0	140
J	1307.2	D	419612	6269600	10.1	4.1	22.6	28.5	3.9	9.8	4.2	0	0
LINE 30020		FLIGHT 13											
A	1682.0	H?	416837	6269526	6.6	4.8	16.0	19.0	2.6	4.0	---	---	0
B	1697.5	D	417152	6269515	25.2	9.5	52.0	27.8	19.6	24.1	6.3	0	0
C	1711.0	D	417360	6269498	8.7	6.4	5.4	6.0	2.5	1.3	1.8	32	0
D	1762.5	D	418064	6269497	19.6	14.7	64.1	50.5	12.7	26.3	2.4	0	0
E	1770.9	B	418184	6269478	6.8	7.9	25.9	12.3	10.9	8.8	1.0	9	0
F	1785.8	D	418464	6269500	44.2	31.8	272.5	217.9	82.5	123.9	3.3	0	0
G	1789.8	D	418552	6269491	63.2	63.8	272.5	217.9	82.5	123.9	2.5	0	0
H	1791.7	B	418600	6269489	47.0	63.8	272.5	217.9	82.5	123.9	1.6	0	0
I	1799.3	B	418813	6269475	77.4	34.1	356.9	151.4	171.4	167.6	7.4	0	0
J	1802.6	E	418903	6269471	79.6	35.0	356.9	151.4	171.4	167.6	7.5	0	0
K	1825.6	H	419358	6269455	3.0	6.9	32.9	16.2	15.7	19.2	0.4	14	0
L	1830.6	D	419474	6269448	13.6	2.8	32.9	16.2	15.7	19.2	12.1	17	0
M	1839.1	H?	419688	6269428	8.3	11.2	33.8	36.0	3.1	11.1	0.9	0	0
LINE 30030		FLIGHT 13											
A	2157.2	D	416874	6269386	9.2	8.2	18.8	14.5	6.1	7.0	1.5	0	0
B	2146.1	D	417136	6269387	23.7	9.6	63.0	29.9	22.0	29.8	5.6	0	0
C	2070.3	B	418071	6269339	11.2	8.7	24.8	47.2	5.0	12.6	1.9	13	0
D	2048.6	D	418222	6269320	7.2	9.0	29.7	33.3	3.1	13.5	0.9	23	0
E	2023.3	D	418558	6269320	61.7	50.4	110.2	91.3	19.2	48.4	3.1	0	0
F	2017.4	B	418710	6269316	64.2	44.9	378.1	264.4	153.7	159.9	3.8	0	0
G	2010.4	B	418896	6269310	35.9	9.1	183.6	264.4	153.7	85.5	12.3	11	0
H	2000.5	D	419114	6269305	6.8	16.8	52.1	53.5	50.6	25.9	0.5	1	0
I	1995.7	B	419204	6269302	5.3	9.8	59.6	53.5	50.6	25.9	0.6	11	0
J	1986.1	B?	419375	6269307	15.4	18.7	125.6	35.1	87.7	66.2	1.3	1	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 30030		FLIGHT 13											
K	1972.6	D	419623	6269310	19.5	11.0	36.1	27.5	14.4	19.1	3.4	10	0
L	1966.6	S?	419725	6269315	6.7	5.0	59.6	42.9	11.3	22.8	1.6	2	0
LINE 30040		FLIGHT 13											
A	2490.8	S?	416873	6269231	7.8	8.3	30.9	30.1	5.7	12.3	1.1	0	0
B	2499.1	B?	417015	6269213	8.2	13.1	48.7	27.1	12.8	21.9	0.8	0	0
C	2503.7	D	417121	6269214	12.2	7.3	48.7	24.9	12.8	21.9	2.7	0	0
D	2578.3	D	418155	6269173	15.8	15.7	100.9	103.3	23.0	49.1	1.6	5	0
E	2583.7	D	418278	6269181	29.4	29.5	100.9	103.3	23.0	49.1	1.9	0	0
F	2587.6	H?	418391	6269171	5.5	14.5	100.9	103.3	23.0	49.1	0.4	0	0
G	2599.0	B	418744	6269133	28.1	12.1	174.2	48.0	113.0	79.1	5.4	15	0
H	2602.3	B	418831	6269139	29.0	12.1	174.2	48.0	113.0	79.1	5.7	16	83
I	2621.6	H	419249	6269192	8.1	2.0	53.2	6.7	50.1	22.4	7.5	47	0
J	2648.6	H	419759	6269136	5.4	2.6	9.3	8.6	2.7	3.3	2.6	46	18
LINE 30050		FLIGHT 13											
A	2913.5	D	416916	6269081	17.1	20.2	82.7	81.5	19.0	33.2	1.3	0	0
B	2909.6	D	417008	6269086	12.1	20.8	82.7	81.5	19.0	33.2	0.8	0	0
C	2905.6	D	417115	6269083	17.2	7.1	53.8	33.9	19.0	25.6	4.9	0	0
D	2841.0	H	417886	6269053	6.8	8.3	17.5	33.0	2.3	8.1	0.9	12	0
E	2811.4	D	418161	6269025	40.7	22.3	281.8	165.6	12.1	129.9	4.5	5	0
F	2805.9	B	418212	6269029	93.2	60.9	281.8	165.6	104.5	129.9	4.7	0	0
G	2795.8	H?	418414	6269025	14.7	7.3	2.9	26.5	0.3	0.5	3.6	6	0
H	2783.0	E	418678	6269005	57.5	54.0	378.8	168.0	32.8	173.4	2.6	0	16
I	2776.6	B	418785	6269015	74.5	15.8	384.3	168.0	215.8	178.8	20.4	0	11
J	2771.5	B	418863	6269024	42.7	11.0	384.3	168.0	215.8	178.8	12.9	2	11
K	2761.8	B?	419002	6269015	58.8	21.9	159.8	67.2	95.3	74.9	8.5	0	0
L	2753.0	H	419153	6269014	22.5	3.2	67.1	10.4	60.9	27.8	24.8	20	0
M	2722.7	H	419745	6269024	4.3	1.9	14.8	7.5	8.5	6.6	2.7	55	0
LINE 30060		FLIGHT 13											
A	3091.1	B?	416556	6268929	6.1	12.4	27.7	33.5	2.9	10.9	0.6	0	205
B	3112.0	H	416915	6268918	5.2	5.8	47.6	29.8	18.3	23.4	1.0	11	0
C	3119.6	D	417080	6268920	14.3	9.6	52.9	22.6	18.3	23.4	2.4	0	0
D	3149.5	H	417567	6268903	8.9	4.8	16.4	21.3	0.6	5.0	2.7	7	0
E	3191.4	D	418172	6268881	16.9	3.8	30.0	15.4	11.1	14.2	11.5	0	0
F	3216.2	B	418642	6268877	4.4	10.4	48.7	74.2	12.3	23.4	0.4	11	0
G	3223.8	B	418703	6268875	0.0	4.4	26.3	33.3	11.8	12.7	0.1	23	0

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LINE 30060			FLIGHT 13										
H	3229.0	B?	418749	6268873	5.9	5.4	26.3	33.3	11.8	12.7	1.3	38	0
I	3255.4	B	419125	6268866	17.6	16.9	81.5	73.9	25.0	37.9	1.7	11	0
J	3264.3	H	419327	6268859	12.9	17.9	36.8	42.5	6.3	13.3	1.0	5	61
K	3291.3	H	419914	6268812	10.6	16.4	42.9	56.7	7.6	18.7	0.9	11	0
LINE 30070			FLIGHT 13										
A	3646.0	D	416603	6268787	13.6	9.2	37.1	50.1	5.6	11.7	2.4	0	0
B	3616.6	D	416938	6268763	12.8	0.2	100.6	75.2	55.3	80.5	502.4	31	0
C	3607.2	B	417055	6268764	50.2	51.2	171.0	138.2	55.3	80.5	2.3	0	0
D	3561.1	D	417583	6268761	15.0	12.0	31.5	39.8	4.4	11.5	2.0	2	0
E	3507.1	B	418022	6268735	18.0	22.8	34.8	71.6	18.1	16.0	1.3	11	0
F	3495.7	D	418180	6268753	27.6	10.0	57.4	66.4	19.5	28.2	6.8	7	0
G	3481.4	H?	418394	6268720	7.2	7.6	23.2	0.7	1.3	1.8	1.1	8	0
H	3466.1	B?	418554	6268733	16.4	18.8	26.2	24.2	3.5	9.8	1.4	0	0
I	3450.3	D	418702	6268718	29.8	18.5	83.7	30.6	34.1	45.6	3.4	2	0
LINE 30080			FLIGHT 13										
A	4052.6	B	416833	6268630	113.0	77.5	458.1	259.7	139.8	211.6	4.7	0	0
B	4054.9	B	416878	6268630	107.5	77.5	458.1	259.7	139.8	211.6	4.4	0	0
C	4064.9	E	417090	6268619	36.5	48.5	193.0	136.8	27.6	70.9	1.5	0	0
D	4101.6	D	417606	6268599	21.0	18.2	46.5	29.7	13.5	21.6	2.0	0	0
E	4122.9	D	417938	6268580	36.7	23.1	132.4	104.0	17.2	53.4	3.6	0	0
F	4126.1	B?	418016	6268579	17.4	23.1	132.4	104.0	17.2	53.4	1.2	0	0
G	4131.9	D	418162	6268577	16.0	15.0	63.1	68.8	14.6	27.2	1.7	7	0
H	4139.0	H?	418267	6268582	8.3	15.3	45.6	68.8	6.5	19.5	0.7	8	0
I	4152.4	D	418372	6268590	16.4	17.0	11.6	23.9	1.9	3.7	1.5	7	0
J	4179.2	B	418551	6268569	64.1	43.2	262.1	192.7	40.2	107.0	4.0	0	0
K	4193.4	B	418651	6268568	93.4	36.7	552.4	251.5	222.8	296.3	9.2	0	0
L	4205.8	E	418737	6268574	17.1	7.4	86.9	7.1	65.5	42.8	4.6	15	0
LINE 30090			FLIGHT 13										
A	4632.6	H	416615	6268483	4.7	12.8	31.3	34.8	0.9	7.0	0.4	14	101
B	4619.9	H	416816	6268468	8.0	12.2	48.5	59.0	34.8	51.1	0.8	10	120
C	4612.2	D	417008	6268463	38.4	17.9	104.7	53.5	34.8	51.1	5.4	0	0
D	4569.8	B	417648	6268459	19.4	16.9	145.0	109.1	17.0	50.2	2.0	3	0
E	4560.3	B	417690	6268464	24.1	18.0	63.9	59.8	9.6	27.7	2.5	14	0
F	4535.9	B?	417950	6268449	41.9	55.3	103.4	178.9	16.1	48.8	1.6	0	0
G	4530.5	B	418062	6268450	8.0	18.5	103.4	110.0	14.2	48.8	0.6	0	0

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LINE 30090			FLIGHT 13										
H	4524.4	H	418156	6268447	9.2	13.7	23.8	110.0	10.3	36.1	0.9	3	0
I	4489.2	D	418585	6268428	74.5	44.3	190.5	88.7	105.2	106.4	4.9	0	0
J	4484.1	B	418647	6268424	31.3	10.6	190.5	88.7	105.2	106.4	7.9	9	0
LINE 30100			FLIGHT 13										
A	4736.0	H	416518	6268328	4.3	11.7	19.3	39.2	3.7	10.5	0.4	0	16
B	4745.7	H?	416770	6268321	13.4	13.3	76.4	77.5	13.9	22.3	1.5	11	0
C	4756.1	B	417028	6268321	74.8	36.9	447.9	213.6	160.6	227.7	6.3	0	0
D	4758.2	B	417076	6268320	67.3	36.9	447.9	213.6	160.6	227.7	5.3	0	0
E	4761.0	B	417137	6268319	85.5	62.6	447.9	213.6	160.6	227.7	4.0	0	0
F	4790.0	D	417644	6268311	40.7	23.7	174.0	87.3	50.7	80.3	4.1	0	0
G	4794.1	D	417736	6268306	22.2	21.3	174.0	87.3	56.1	80.3	1.8	0	0
H	4796.0	D	417784	6268300	24.4	21.3	174.0	87.3	56.1	80.3	2.1	0	0
I	4800.3	B	417881	6268286	16.0	19.7	174.0	86.1	56.1	80.3	1.3	0	0
J	4820.1	H	418112	6268281	5.8	15.6	23.9	63.5	4.9	14.2	0.4	0	0
K	4855.6	D	418499	6268279	75.2	51.0	251.5	154.3	108.2	124.5	4.2	0	0
L	4861.1	B	418564	6268279	20.1	15.9	251.5	154.3	108.2	124.5	2.2	14	0
M	4870.7	H	418726	6268271	19.1	4.1	112.2	14.1	87.1	45.0	12.7	26	0
LINE 30110			FLIGHT 13										
A	5283.7	H	416714	6268191	7.3	17.2	44.4	62.7	8.4	22.4	0.5	0	0
B	5271.4	D	417013	6268174	38.4	27.9	174.7	124.0	18.3	33.3	3.1	4	176
C	5262.7	B	417223	6268178	158.1	49.1	542.0	263.7	250.1	286.9	15.2	0	0
D	5258.3	B	417325	6268174	42.7	58.4	334.5	349.4	250.1	124.0	1.6	0	0
E	5234.5	B	417638	6268150	165.8	72.4	511.0	209.9	227.5	254.0	9.6	0	0
F	5224.2	H	417832	6268143	4.6	20.3	73.0	103.9	9.2	39.3	0.3	0	0
G	5212.9	D	418001	6268154	5.0	5.2	14.3	16.1	1.6	5.7	1.0	29	0
H	5170.6	D	418570	6268123	77.3	51.2	150.0	108.6	60.5	76.1	4.3	0	0
LINE 30120			FLIGHT 13										
A	5617.9	B	416912	6268025	20.1	20.2	89.3	36.7	13.4	36.8	1.7	0	0
B	5623.2	D	417028	6268030	19.5	24.8	89.3	84.4	13.4	36.8	1.3	0	284
C	5625.8	D	417083	6268030	27.8	22.4	89.3	84.4	13.4	36.8	2.4	0	284
D	5648.4	B	417608	6268005	206.8	91.9	640.7	255.8	293.8	312.2	10.1	0	0
E	5677.8	H?	418001	6267989	2.2	13.2	6.1	25.4	4.4	5.6	0.2	0	0
F	5722.5	H	418564	6267977	8.3	7.5	20.4	15.7	9.3	8.5	1.4	22	0
G	5728.6	D	418674	6267971	5.0	0.2	25.3	10.5	9.4	12.6	---	---	0
H	5760.4	H	419208	6267951	3.6	5.3	10.7	25.2	1.3	3.9	0.6	37	46

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LINE 30130		FLIGHT 13											
A	6084.3	D	416991	6267869	11.1	9.4	35.1	17.9	17.5	13.3	1.7	23	146
B	6076.5	D	417157	6267865	146.1	103.5	506.3	363.9	157.6	242.5	4.9	0	0
C	6055.3	B	417613	6267858	183.7	101.4	629.3	276.1	301.7	281.9	7.3	0	0
D	6050.9	B	417704	6267849	132.0	53.6	599.1	236.4	320.8	294.0	9.9	0	0
E	6047.7	E	417769	6267843	124.0	59.0	488.4	236.4	320.8	294.0	7.8	0	0
F	6027.9	B?	418102	6267847	10.8	23.5	13.1	30.4	2.6	5.8	0.6	0	0
G	5989.8	H	418682	6267818	13.2	9.0	34.3	33.2	8.3	17.4	2.3	4	0
LINE 30140		FLIGHT 13											
A	6270.8	D	417362	6267706	58.3	18.6	151.7	37.2	133.0	63.2	10.5	11	0
B	6284.8	B	417622	6267701	272.9	153.6	872.0	532.5	251.1	416.3	8.1	0	0
C	6295.1	D	417848	6267700	34.3	37.9	100.6	114.4	5.1	38.3	1.8	0	25
D	6310.6	D	418092	6267692	3.9	3.6	22.4	28.2	7.1	13.8	1.1	44	0
E	6354.8	B	418621	6267674	27.2	18.1	94.0	76.3	26.0	44.2	3.0	0	0
F	6357.8	B	418669	6267672	17.8	19.5	94.0	76.3	26.0	44.2	1.5	9	0
G	6389.8	H	419123	6267657	4.6	8.3	18.6	45.6	2.7	11.0	0.6	20	0
LINE 30150		FLIGHT 13											
A	6878.7	B	417166	6267589	29.8	24.3	118.8	74.5	41.7	53.6	2.5	1	0
B	6869.0	D	417395	6267565	64.1	40.7	212.1	130.4	64.1	95.6	4.3	1	0
C	6854.6	B	417640	6267540	64.6	35.8	252.7	109.7	115.3	126.7	5.1	0	0
D	6851.7	B	417704	6267539	45.3	33.8	252.7	109.7	115.3	126.7	3.1	0	50
E	6847.7	B?	417807	6267536	11.5	13.2	252.7	91.1	115.3	126.7	1.2	11	55
F	6842.9	D	417939	6267539	7.4	13.9	40.2	90.1	3.7	20.5	0.6	3	0
G	6836.8	D	418075	6267543	13.3	24.4	56.4	96.6	7.5	26.5	0.8	0	0
H	6828.4	D	418219	6267551	10.6	15.6	13.9	33.9	1.9	8.4	0.9	0	0
I	6805.0	B	418603	6267529	31.0	16.1	108.6	56.5	43.8	53.9	4.4	0	0
J	6800.3	B	418676	6267528	15.6	14.1	107.8	56.5	43.8	53.5	1.7	20	0
K	6775.6	H	419019	6267521	7.6	9.4	19.1	14.8	5.4	7.7	1.0	17	41
LINE 30160		FLIGHT 14											
A	921.7	H	416949	6267249	4.0	7.3	10.7	23.7	1.9	5.5	---	---	0
B	949.1	D	417251	6267259	44.3	47.5	61.2	81.1	11.2	28.9	2.0	1	0
C	964.7	D	417492	6267244	9.4	16.3	17.9	24.5	4.7	8.3	---	---	0
D	982.4	D	417803	6267238	95.0	49.1	240.1	92.6	106.8	111.8	6.4	0	0
E	993.4	D	417995	6267246	6.7	14.9	34.1	66.8	0.0	7.4	0.5	7	0
F	1001.6	B?	418178	6267233	8.8	21.3	34.1	53.5	5.6	7.9	0.5	0	0

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EM Anomaly List

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LINE 30160			FLIGHT 14										
G	1015.2	D	418367	6267219	35.7	38.3	64.6	64.0	26.8	24.5	1.9	2	0
H	1026.6	B	418443	6267220	10.3	9.5	62.6	23.2	6.7	21.5	1.5	24	0
I	1044.4	B	418642	6267226	56.3	59.3	251.5	208.0	70.7	119.0	2.3	0	0
LINE 30170			FLIGHT 14										
A	1527.1	D	417192	6267422	32.1	21.2	52.4	40.9	15.9	22.0	3.2	6	0
B	1482.2	B	417688	6267400	56.4	25.9	194.0	116.7	80.7	91.6	6.3	3	0
C	1477.8	B	417767	6267392	59.7	22.1	194.0	116.7	80.7	91.6	8.6	0	89
D	1469.3	D	417970	6267379	11.6	23.4	41.8	80.3	0.1	17.7	0.7	0	0
E	1465.0	B?	418075	6267381	10.6	26.1	41.8	80.3	1.0	17.7	---	---	0
F	1444.3	D	418407	6267385	14.2	12.4	59.2	8.4	28.1	30.5	1.8	12	0
G	1438.0	B	418496	6267387	20.6	12.5	59.2	8.4	28.1	30.5	3.1	4	0
H	1432.3	B	418561	6267378	1.1	0.7	79.3	28.7	36.0	37.9	1.2	95	0
I	1424.6	B	418645	6267366	15.3	21.9	63.0	38.2	22.2	29.5	1.1	3	0
J	1419.0	D	418712	6267368	19.2	7.8	63.0	38.2	22.2	29.5	5.1	10	0
K	1405.0	D	418897	6267367	11.0	14.0	38.9	23.8	13.8	14.2	1.1	0	0
L	1402.6	B?	418934	6267364	11.0	5.9	38.9	23.8	13.8	14.2	3.0	13	0
M	1384.4	H?	419176	6267342	12.9	19.9	51.6	72.1	3.4	23.4	---	---	0
N	1374.9	H?	419298	6267331	3.9	12.7	16.5	46.9	1.3	10.0	---	---	0
LINE 30180			FLIGHT 14										
A	1772.7	D	417295	6267107	17.8	21.2	22.0	24.6	6.8	9.7	1.3	0	0
B	1806.7	B	417787	6267103	180.6	146.9	532.5	295.2	222.7	253.5	4.5	0	0
C	1813.7	B	417889	6267088	89.3	36.9	532.5	295.2	71.4	253.5	---	---	32
D	1822.4	B?	418037	6267087	1.1	2.8	32.1	84.3	0.1	20.3	0.3	34	0
E	1830.2	H	418218	6267088	13.0	25.8	42.0	84.3	38.1	20.3	0.7	0	17
F	1838.7	D	418388	6267082	46.0	29.4	133.0	65.5	38.1	58.3	3.8	2	0
G	1848.5	B	418527	6267073	74.9	60.0	288.7	203.4	87.8	136.2	3.4	0	0
H	1881.9	H	418812	6267062	1.9	8.6	28.7	51.9	5.1	14.8	---	---	19
LINE 30190			FLIGHT 14										
A	2394.5	D	417292	6266986	33.6	29.8	75.3	100.0	16.8	36.0	2.3	2	0
B	2381.2	D	417456	6266955	16.1	12.8	12.6	20.5	16.8	0.8	2.1	0	0
C	2365.0	B	417716	6266958	29.7	33.1	89.7	63.9	40.6	42.3	1.7	3	0
D	2350.9	D	417846	6266951	51.8	55.0	122.6	73.7	45.3	51.9	2.2	0	0
E	2338.7	D	417927	6266947	47.7	34.3	127.6	64.8	64.2	55.8	3.3	0	0
F	2314.8	B?	418121	6266931	12.9	17.4	28.5	54.7	2.1	11.5	1.1	7	17
G	2298.5	B	418492	6266930	73.8	71.8	266.6	169.0	81.3	131.2	2.7	0	0

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LINE 30190			FLIGHT 14										
H	2283.3	H	418729	6266924	6.1	7.0	16.2	30.5	3.8	9.3	---	---	17
LINE 30200			FLIGHT 14										
A	2620.1	D	417201	6266812	128.4	127.7	296.6	225.0	86.5	124.4	3.2	0	0
B	2635.6	D	417456	6266814	18.1	10.0	18.8	21.4	3.8	8.5	3.4	16	0
C	2656.5	D	417736	6266806	54.0	40.7	196.4	100.7	90.5	89.6	3.3	0	0
D	2663.7	D	417838	6266793	22.5	26.8	193.4	115.8	90.5	88.7	---	---	0
E	2669.3	D	417907	6266796	24.6	17.3	117.9	107.0	23.5	51.3	2.8	10	0
F	2672.7	E	417944	6266799	33.7	22.1	71.7	41.4	24.1	30.7	3.3	4	0
G	2677.8	H?	418002	6266795	11.4	7.2	15.7	0.7	21.1	9.8	2.4	21	26
H	2687.5	H	418159	6266794	7.2	9.2	22.2	33.4	2.7	9.3	0.9	5	0
I	2701.1	B	418479	6266798	50.0	33.0	204.6	197.1	49.0	89.8	3.8	0	0
LINE 30210			FLIGHT 14										
A	3034.2	B	417982	6266643	34.4	22.9	111.1	91.9	27.7	48.9	3.3	9	0
B	2991.6	B?	418233	6266637	23.4	22.3	34.6	59.6	3.2	17.5	1.9	0	0
C	2987.0	D	418290	6266627	17.9	32.4	147.3	146.8	25.4	64.6	0.9	0	0
D	2984.8	B	418327	6266625	16.2	39.3	147.3	146.8	25.4	64.6	0.7	0	0
E	2978.7	H	418464	6266632	21.3	6.8	67.3	146.8	39.5	32.8	7.5	0	0
LINE 30214			FLIGHT 14										
A	3145.3	D	416883	6266668	8.0	12.1	24.3	26.8	6.0	11.8	0.8	5	40
B	3133.8	H	417155	6266671	4.2	7.4	63.2	62.3	12.4	25.2	0.6	12	154
C	3129.8	D	417261	6266660	22.6	12.2	63.2	62.3	10.6	25.2	3.8	7	0
D	3104.1	H	417767	6266638	16.6	9.3	64.2	35.3	34.1	29.3	3.2	12	0
LINE 30220			FLIGHT 14										
A	3304.7	S?	416518	6266527	2.1	9.8	1.0	25.6	0.5	2.8	---	---	0
B	3371.2	D	417325	6266501	22.0	21.9	36.9	38.5	10.0	17.2	1.8	7	0
C	3411.0	B	417781	6266491	71.0	44.5	288.3	111.0	132.8	139.6	4.5	0	0
D	3415.0	D	417843	6266493	65.4	42.4	288.3	111.0	132.8	139.6	4.2	0	0
E	3428.7	D	417997	6266486	47.6	35.4	68.8	52.7	28.1	34.2	3.2	0	29
F	3455.9	B	418303	6266478	44.6	57.2	222.3	250.5	30.2	101.2	1.7	0	0
G	3462.1	B	418398	6266485	9.9	18.4	228.1	212.4	119.5	93.4	0.7	10	0
H	3468.6	B	418502	6266488	53.1	51.7	380.2	210.9	119.5	188.8	2.4	0	0
I	3471.7	B	418547	6266486	86.3	50.0	380.2	220.5	119.5	188.8	5.3	0	0

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LINE 30231		FLIGHT 23											
A	1879.0	B	417330	6266361	8.8	13.1	93.4	90.9	12.3	44.0	0.8	13	0
B	1870.9	B	417386	6266361	20.4	19.3	93.4	90.9	14.6	44.0	1.8	11	0
C	1810.2	H	417916	6266342	7.1	1.0	75.6	30.9	31.7	35.4	18.2	41	0
D	1795.0	D	418027	6266339	15.4	8.8	37.0	23.9	9.2	14.1	3.0	16	16
E	1768.0	D	418176	6266323	30.9	17.7	59.0	46.9	25.3	27.0	3.8	0	0
F	1743.6	B	418493	6266318	32.2	17.8	132.2	46.3	47.3	64.2	4.1	0	0
G	1739.4	B	418581	6266319	33.2	20.7	132.2	64.3	47.3	64.2	3.5	0	0
LINE 30240		FLIGHT 23											
A	2145.5	D	417326	6266197	36.0	21.7	83.8	41.1	21.9	37.2	3.8	0	0
B	2184.4	D	417953	6266190	19.2	4.5	89.6	38.2	43.6	44.1	11.1	17	0
C	2188.5	D	418026	6266190	25.5	12.3	89.6	28.0	43.6	44.1	4.5	0	16
D	2198.7	D	418191	6266176	23.3	10.7	17.0	12.8	24.2	10.1	4.7	0	0
E	2213.3	D	418480	6266197	19.5	8.1	113.7	22.0	49.5	56.4	5.0	0	0
F	2220.3	D	418620	6266172	30.4	14.1	113.7	50.9	49.5	56.4	5.1	0	0
LINE 30250		FLIGHT 23											
A	2625.2	B	417220	6266062	51.1	48.0	489.4	260.5	109.2	226.4	2.5	0	0
B	2619.8	B	417255	6266062	88.3	62.6	489.4	260.5	109.2	226.4	4.2	0	0
C	2612.9	B	417300	6266062	20.0	11.1	283.6	172.8	75.5	43.9	3.4	20	0
D	2580.1	D	417496	6266055	8.7	5.1	25.4	10.1	0.2	7.8	2.4	34	0
E	2572.6	B	417546	6266052	0.0	0.4	25.4	25.5	3.4	7.8	0.1	62	0
F	2565.1	D	417624	6266051	17.6	21.7	25.4	31.9	2.2	8.3	1.3	1	0
G	2540.8	D	417911	6266037	76.4	53.4	473.2	156.6	256.0	224.5	4.0	0	0
H	2530.2	B	418055	6266044	117.5	46.2	473.2	201.7	256.0	224.5	9.9	0	0
I	2520.0	D	418222	6266024	71.9	45.3	267.6	131.0	84.6	134.7	4.5	0	0
J	2500.8	B	418503	6266016	20.5	10.3	65.7	31.1	28.6	33.0	4.0	0	0
LINE 30260		FLIGHT 23											
A	2995.6	B	417164	6265906	98.8	64.3	269.6	125.5	117.8	129.9	4.8	0	0
B	3006.1	D	417292	6265906	70.0	65.2	168.7	111.8	88.9	89.9	2.8	0	0
C	3027.4	D	417549	6265900	8.9	14.6	26.9	32.2	3.7	10.9	0.8	14	0
D	3038.9	D	417686	6265894	9.7	10.4	0.9	10.0	2.6	0.0	1.2	14	10
E	3061.9	D	417966	6265893	41.4	35.3	181.2	106.9	70.0	82.5	2.6	0	0
F	3068.8	D	418052	6265890	71.0	61.8	256.3	137.5	106.5	119.6	3.0	0	0
G	3077.6	B?	418172	6265887	29.9	24.2	176.1	134.2	106.5	119.6	2.5	3	0
H	3086.7	D	418314	6265888	89.7	65.6	159.6	102.0	60.0	83.3	4.0	0	0

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LINE 30260			FLIGHT 23										
I	3101.3	H	418547	6265876	18.4	9.2	62.5	45.0	20.0	29.3	3.8	6	0
LINE 30270			FLIGHT 17										
A	1147.6	D	417180	6265760	53.0	42.5	129.5	83.4	39.1	64.6	3.0	3	0
B	1157.7	D	417327	6265753	12.0	9.9	8.6	14.2	3.6	6.3	1.8	16	0
C	1179.3	B	417611	6265755	7.3	11.5	16.6	28.5	2.1	7.1	0.8	14	0
D	1188.3	D	417722	6265757	16.3	39.5	17.0	34.7	3.0	8.9	0.7	0	16
E	1214.1	D	418065	6265741	33.4	9.1	150.8	73.5	59.1	70.4	10.9	3	0
F	1219.8	D	418143	6265736	25.0	23.6	150.8	73.5	59.1	70.4	2.0	10	0
G	1230.2	B?	418284	6265727	68.9	41.9	179.9	121.4	77.3	101.9	4.7	0	0
H	1236.5	B	418362	6265731	128.4	103.3	263.7	122.5	139.8	125.4	4.1	0	0
I	1249.6	H?	418562	6265726	15.4	4.2	44.9	14.0	19.8	21.3	8.4	5	0
LINE 30280			FLIGHT 17										
A	947.4	H	416314	6265631	12.7	8.1	48.8	23.8	18.3	22.6	2.5	2	0
B	906.9	D	417150	6265611	24.7	21.9	64.8	48.6	14.6	29.5	2.1	6	0
C	892.5	B?	417356	6265603	5.7	4.6	17.4	15.8	1.6	3.9	1.4	35	0
D	837.5	E	417956	6265595	14.2	12.6	31.8	53.9	14.9	37.2	1.7	10	0
E	818.5	D	418147	6265574	15.7	5.4	150.4	77.5	65.6	67.4	6.1	18	0
F	798.0	D	418384	6265578	24.6	11.7	91.9	34.0	41.4	47.6	4.6	8	0
G	770.8	B	418581	6265573	30.7	19.4	139.1	71.6	58.5	61.6	3.4	0	0
LINE 30290			FLIGHT 17										
A	415.3	B	416317	6265489	37.6	35.7	156.3	88.5	46.5	69.1	2.2	0	0
B	470.9	D	417041	6265467	40.1	63.5	78.2	225.6	13.3	44.3	1.3	0	0
C	533.9	D	417811	6265439	7.6	15.9	25.4	27.6	8.7	11.1	0.6	16	0
D	550.5	B	418047	6265436	15.1	7.8	107.0	40.8	58.1	58.1	3.5	21	0
E	557.2	D	418141	6265434	59.2	27.5	107.0	48.1	58.1	58.1	6.3	1	0
F	577.2	D	418457	6265432	22.0	13.3	69.3	33.4	24.8	32.5	3.2	9	0
G	586.8	D	418615	6265431	11.7	5.5	66.7	10.7	41.4	35.0	3.6	17	0
LINE 30300			FLIGHT 16										
A	4827.6	D	416192	6265348	27.0	20.3	83.8	81.9	26.5	38.4	2.6	0	0
B	4818.5	B?	416313	6265342	14.5	15.7	50.9	54.2	22.2	38.4	1.4	10	55
C	4780.6	B	416657	6265333	34.9	20.7	151.2	34.4	97.7	65.3	3.8	0	0
D	4767.6	D	416961	6265331	25.8	30.3	124.8	123.6	18.5	50.1	1.5	0	11
E	4702.1	D	417702	6265286	6.1	13.9	11.3	21.1	2.4	5.7	0.5	7	0
F	4692.4	D	417808	6265284	11.5	24.6	30.8	32.6	7.5	14.5	0.7	4	0

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LINE 30300		FLIGHT 16											
G	4676.3	B	418032	6265294	58.4	42.9	282.0	174.3	111.4	135.4	3.5	0	0
H	4671.6	H?	418118	6265289	54.3	12.5	282.0	144.9	111.4	135.4	16.4	0	0
I	4657.6	D	418330	6265287	20.5	4.8	73.6	28.3	32.4	36.2	11.7	19	0
J	4648.8	D	418494	6265287	13.0	2.3	48.8	11.3	40.8	22.5	15.0	25	0
LINE 30310		FLIGHT 16											
A	4320.7	B?	416101	6265191	96.5	81.1	211.6	189.2	76.6	98.4	3.5	0	0
B	4344.3	D	416440	6265173	8.0	12.5	13.7	31.5	0.5	0.0	0.8	3	0
C	4357.9	D	416704	6265175	15.6	4.3	53.3	8.2	27.4	22.5	8.4	0	0
D	4440.1	E	417886	6265142	61.4	36.5	229.7	115.2	103.5	104.5	4.6	0	0
E	4444.4	D	417965	6265141	36.0	34.2	229.7	87.0	103.5	104.5	---	---	0
F	4448.0	D	418037	6265140	44.8	6.6	167.8	78.2	62.9	81.5	---	---	0
G	4465.8	H?	418334	6265131	25.7	11.7	97.0	30.4	40.1	49.1	4.9	3	0
H	4474.2	D	418469	6265131	27.5	25.5	16.1	6.9	18.2	10.3	2.0	5	45
I	4486.6	D	418641	6265121	21.6	8.8	67.0	29.1	36.2	33.0	5.4	6	0
LINE 30320		FLIGHT 16											
A	4123.1	H?	416494	6265013	5.7	7.2	3.2	28.1	0.0	3.4	0.9	11	44
B	4102.8	B	416681	6265019	12.6	5.6	72.9	20.0	27.9	34.0	4.0	0	0
C	4098.7	B	416754	6265020	19.1	5.4	72.9	24.7	27.9	34.0	8.7	0	0
D	4000.9	D	417864	6264987	24.3	11.0	64.8	49.9	73.6	40.4	4.9	5	0
E	3993.0	B	418006	6264991	57.4	23.6	206.5	89.0	87.0	102.9	7.3	0	0
F	3976.7	D	418428	6264993	21.5	8.4	87.8	22.1	61.3	43.2	5.7	12	0
LINE 30330		FLIGHT 16											
A	3699.7	H	416692	6264862	6.2	2.4	17.9	4.2	6.2	6.9	3.8	0	0
B	3776.8	D	417825	6264835	24.3	11.2	55.2	30.6	45.7	29.3	4.7	15	0
C	3786.2	B	418030	6264834	115.0	48.8	313.9	150.5	179.0	150.3	8.9	0	0
D	3799.0	D	418318	6264831	15.9	5.0	58.6	16.7	37.1	21.8	7.0	16	0
E	3822.9	H	418722	6264819	6.5	17.7	44.9	91.9	7.8	15.9	0.4	0	0
F	3835.4	H?	418937	6264808	6.1	20.0	47.3	92.0	0.4	21.6	0.4	0	0
LINE 30340		FLIGHT 16											
A	3481.6	D	416732	6264730	9.7	7.9	44.9	38.6	17.3	21.0	1.7	0	0
B	3402.5	E	417589	6264686	14.3	8.2	47.9	16.0	17.1	21.3	3.0	17	0
C	3399.0	H	417656	6264689	5.8	4.3	47.9	16.0	17.1	21.3	1.6	19	0
D	3385.5	B	417943	6264704	43.1	21.9	188.5	72.5	91.3	91.2	---	---	0
E	3384.1	B	417987	6264705	43.1	21.9	188.5	72.5	91.3	91.2	5.0	0	19

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EM Anomaly List

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LINE 30350			FLIGHT 16										
A	3104.8	B	416701	6264563	2.7	3.2	19.4	11.3	7.3	9.6	0.7	0	0
B	3162.2	B	417619	6264544	34.1	15.9	122.9	62.9	77.3	55.3	5.2	0	0
C	3163.9	B	417659	6264544	22.3	23.2	122.9	62.9	77.3	55.3	1.7	0	0
D	3168.6	D	417785	6264539	10.5	2.2	32.2	31.0	24.7	20.4	10.8	23	0
E	3171.5	B?	417872	6264533	11.5	1.9	32.2	0.0	24.7	20.4	16.4	39	0
F	3185.2	H	418329	6264532	9.0	1.2	62.7	23.1	52.3	34.3	20.5	36	0
G	3189.5	D	418479	6264529	10.6	6.7	62.7	23.1	52.3	34.3	2.3	18	0
H	3193.1	E	418590	6264527	15.6	9.3	51.6	24.1	17.3	34.3	2.9	14	0
LINE 30360			FLIGHT 16										
A	2855.8	D	416573	6264421	6.1	12.4	17.6	25.2	3.1	3.9	0.6	11	0
B	2844.6	H	416685	6264434	2.7	7.7	35.5	36.0	14.5	19.5	0.3	0	0
C	2777.0	D	417584	6264393	21.0	3.5	96.0	31.4	48.9	46.9	19.4	13	0
D	2771.0	D	417737	6264398	20.8	3.5	48.1	10.0	38.7	24.1	18.8	0	0
E	2754.7	H	418326	6264385	9.0	3.1	54.5	11.4	50.9	27.1	5.1	7	0
F	2716.0	H	419114	6264366	3.3	5.7	1.9	6.1	1.6	1.4	0.5	21	33
LINE 30370			FLIGHT 16										
A	2447.7	D	416566	6264270	9.5	13.2	34.6	44.6	10.5	11.9	0.9	7	0
B	2506.8	B	417555	6264238	28.0	8.4	87.8	24.6	66.8	40.7	9.1	4	0
C	2513.7	D	417717	6264231	13.0	4.8	31.7	11.6	27.0	19.0	5.1	25	0
D	2516.9	D	417808	6264230	17.0	7.6	31.7	27.3	27.0	19.0	4.4	0	0
E	2530.8	H	418218	6264226	6.6	2.5	52.3	17.9	42.6	27.3	4.1	35	0
F	2582.7	H	419142	6264197	1.4	7.6	21.0	27.0	1.6	7.3	0.2	0	33
LINE 30380			FLIGHT 16										
A	2202.6	D	416527	6264137	10.1	9.0	26.9	21.7	3.9	10.6	1.6	19	0
B	2183.2	D	416806	6264135	9.7	5.3	28.6	26.2	10.1	14.8	2.8	0	0
C	2136.6	B	417528	6264111	17.0	3.9	100.6	21.5	63.8	49.1	10.9	14	0
D	2125.1	D	417789	6264086	17.3	13.3	44.2	61.6	34.0	18.1	2.2	4	0
E	2108.0	H	418176	6264083	6.3	0.2	74.7	39.6	27.0	35.2	---	---	0
LINE 30390			FLIGHT 14										
A	4216.6	H	416527	6263989	5.5	10.9	27.0	45.5	5.2	12.3	0.5	0	68
B	4190.0	D	416841	6263976	37.1	21.9	77.9	72.7	13.0	34.5	3.9	0	0
C	4152.8	B?	417499	6263964	32.5	11.0	91.1	30.7	50.6	41.4	7.9	9	0
D	4144.2	B	417708	6263934	21.7	6.7	82.3	21.7	90.6	33.2	7.9	23	0

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LINE 30390			FLIGHT 14										
E	4131.5	H	417977	6263935	2.2	7.4	8.0	32.4	0.5	3.8	0.3	0	0
F	4118.7	B?	418279	6263941	20.9	10.0	90.5	44.0	40.0	43.6	4.3	10	0
LINE 30400			FLIGHT 14										
A	4334.2	S?	416367	6263828	6.3	9.1	13.1	16.0	0.4	5.0	0.8	22	29
B	4358.6	E	416693	6263827	6.3	10.6	12.7	29.7	7.0	7.5	0.7	15	0
C	4368.0	B	416840	6263821	76.1	56.8	176.7	86.3	83.1	85.1	3.7	0	0
D	4410.0	B	417682	6263791	4.1	3.5	103.6	18.9	86.3	43.0	1.2	31	0
E	4413.9	B	417793	6263792	18.6	1.4	103.6	11.4	86.3	29.0	62.5	17	0
F	4431.0	B	418304	6263801	27.0	7.8	100.2	23.6	60.7	45.6	9.4	9	39
LINE 30410			FLIGHT 17										
A	1771.8	H	416300	6263686	8.0	12.7	35.4	38.2	2.4	14.6	0.8	7	0
B	1745.9	B	416800	6263668	19.2	8.3	80.0	33.5	35.4	38.7	4.7	5	0
C	1693.2	E	417556	6263646	27.1	11.0	77.5	19.5	60.4	40.6	5.8	8	0
D	1679.5	B	417767	6263640	24.3	8.8	198.6	27.7	155.3	91.7	6.5	17	0
E	1643.4	B	418478	6263625	30.6	26.0	142.9	75.2	78.6	73.0	2.4	0	0
LINE 30420			FLIGHT 17										
A	1983.7	B	416075	6263533	4.4	6.2	5.8	25.6	8.9	0.0	0.7	25	0
B	2011.7	B?	416705	6263525	14.2	5.5	68.6	35.9	33.7	28.3	5.0	13	0
C	2072.9	B	417847	6263488	22.6	0.0	134.7	34.9	112.8	60.4	999.0	18	0
D	2076.9	B	417959	6263484	15.9	1.8	109.5	24.9	112.8	37.5	30.3	25	0
E	2111.2	B	418642	6263470	8.1	10.9	212.4	77.7	86.5	106.6	0.9	20	43
F	2115.4	B	418712	6263467	13.1	9.2	212.4	95.2	87.0	106.6	2.2	21	0
G	2119.2	E	418776	6263465	31.1	19.8	212.6	95.2	10.9	106.6	3.4	8	0
LINE 30430			FLIGHT 17										
A	2446.5	B	416044	6263400	12.2	1.1	49.2	20.2	41.5	26.6	42.7	31	0
B	2431.9	B	416481	6263379	24.4	9.6	177.6	27.6	137.0	73.8	5.9	8	0
C	2349.6	D	417796	6263344	13.9	1.3	137.9	47.2	81.9	71.7	42.3	32	0
D	2343.3	B	417894	6263344	25.9	5.0	144.2	34.5	172.5	48.4	16.8	19	0
E	2337.8	E	418000	6263337	24.4	3.3	132.6	24.7	170.4	57.6	28.2	14	30
F	2296.2	B	418768	6263317	47.0	31.9	235.6	85.3	147.2	115.0	3.6	1	0
LINE 30440			FLIGHT 17										
A	2490.1	H	416053	6263231	3.7	2.4	50.3	10.9	35.3	19.0	1.6	55	0
B	2497.3	D	416220	6263236	23.3	6.0	27.8	14.0	8.8	15.8	10.5	21	0

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LINE 30440			FLIGHT 17										
C	2509.5	E	416507	6263227	46.9	19.9	268.7	66.2	188.6	116.8	6.6	14	0
D	2594.1	B	417780	6263187	35.7	6.8	173.4	48.9	120.5	82.6	18.9	16	0
E	2603.0	D	418010	6263177	29.4	8.3	108.4	36.4	103.2	43.9	10.0	16	0
F	2642.0	B	418826	6263163	33.2	13.3	192.6	83.0	115.2	100.0	6.3	16	0
LINE 30450			FLIGHT 17										
A	2918.7	B	416181	6263084	20.2	10.7	128.6	36.6	83.4	49.8	3.7	2	0
B	2907.0	B?	416560	6263075	26.5	10.5	188.3	49.9	129.4	80.6	6.0	20	0
C	2863.3	E	417652	6263046	13.2	5.3	89.4	11.3	80.7	33.9	4.7	30	0
D	2855.6	B	417781	6263046	48.2	11.2	194.7	62.2	166.9	89.2	15.5	6	0
E	2847.9	B	417925	6263040	31.8	8.5	131.2	51.3	166.9	52.6	11.0	7	0
F	2840.5	B?	418120	6263032	8.1	0.8	66.8	6.7	81.8	34.1	33.3	44	52
G	2809.1	B	418863	6263012	24.7	19.6	167.5	86.0	96.4	84.4	2.4	9	98
H	2806.0	B	418932	6263010	26.9	21.2	167.5	86.0	4.0	84.4	2.5	5	103
LINE 30460			FLIGHT 17										
A	2975.3	B	416183	6262932	15.8	7.4	85.3	26.1	64.5	33.6	4.0	27	0
B	2978.8	D	416303	6262929	11.7	3.1	85.3	26.1	64.5	33.6	7.8	33	0
C	2986.6	B	416577	6262926	12.6	3.0	139.0	24.4	105.7	58.8	9.5	37	0
D	3021.0	E	417615	6262895	19.2	5.2	95.6	22.6	118.3	36.3	9.1	25	0
E	3025.5	B	417734	6262894	30.2	4.8	165.5	32.8	149.6	76.6	23.5	19	0
F	3030.4	B	417883	6262888	30.8	3.0	143.9	38.3	149.6	49.9	48.8	15	0
G	3042.2	B?	418240	6262879	16.4	7.1	88.7	48.1	41.1	45.0	4.6	26	0
H	3064.7	D	418890	6262858	11.0	7.0	106.9	53.9	34.4	43.6	2.4	22	0
I	3068.6	D	418992	6262855	16.7	14.6	106.9	53.9	17.0	45.5	1.9	10	0
LINE 30470			FLIGHT 17										
A	3446.7	H	416214	6262796	9.2	1.9	41.6	7.7	37.9	22.7	11.1	43	0
B	3433.3	B	416627	6262780	15.4	4.6	151.5	41.1	92.0	72.5	7.4	29	0
C	3395.1	B	417682	6262733	24.6	6.4	159.4	25.3	117.9	64.7	10.4	18	0
D	3374.3	H	418208	6262733	3.8	6.4	13.4	22.7	5.1	3.0	0.6	25	0
E	3341.5	B	418986	6262715	11.5	13.0	159.3	63.9	55.5	82.8	1.2	14	0
LINE 30480			FLIGHT 17										
A	3498.7	H?	416278	6262633	13.7	0.7	10.1	14.7	26.1	0.0	90.0	5	0
B	3505.8	D	416532	6262618	24.7	7.0	126.7	64.0	83.6	61.9	9.4	6	0
C	3509.8	D	416664	6262616	13.9	12.0	126.7	48.1	83.6	61.9	---	---	0
D	3541.5	B	417690	6262593	39.0	10.7	209.1	55.7	132.5	97.0	11.3	13	0

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LINE 30480		FLIGHT 17											
E	3591.4	H	418986	6262556	5.0	5.1	34.3	38.3	2.2	13.0	1.0	33	0
LINE 30490		FLIGHT 17											
A	3785.1	B?	416135	6262490	18.2	12.2	220.1	64.5	194.1	84.1	2.6	24	0
B	3782.1	B	416247	6262492	57.9	2.9	220.1	0.0	194.1	84.1	166.3	3	0
C	3774.6	B	416528	6262487	64.9	22.8	260.6	98.0	129.0	146.6	9.5	2	0
D	3769.1	D	416739	6262472	34.1	27.1	270.9	179.4	117.6	137.5	2.6	1	0
E	3747.0	B	417617	6262450	34.0	10.3	184.8	40.0	126.4	88.4	9.5	12	0
LINE 30500		FLIGHT 18											
A	829.2	B?	416275	6262336	6.4	1.5	33.5	18.5	11.7	13.4	8.1	38	0
B	846.4	D	416814	6262311	18.7	7.6	75.4	56.0	39.7	37.9	5.1	17	0
C	848.3	D	416877	6262308	14.1	7.4	75.4	56.0	39.7	37.9	3.3	28	0
D	855.7	B?	417142	6262302	8.0	16.8	77.3	159.6	0.0	29.9	0.6	0	0
E	869.1	B	417616	6262302	21.5	3.8	156.2	33.8	118.9	75.1	17.7	0	0
F	872.1	B	417711	6262301	22.8	4.4	156.2	33.8	118.9	75.1	16.1	13	0
LINE 30510		FLIGHT 18											
A	1142.1	D	416362	6262186	4.4	1.5	13.4	14.9	4.1	5.5	4.2	47	0
B	1123.5	B	416887	6262167	8.7	4.7	54.7	24.8	28.2	25.8	2.7	25	0
C	1112.4	B	417203	6262164	11.8	31.1	43.8	151.1	4.0	23.2	0.6	0	0
D	1103.7	D	417490	6262151	33.3	19.4	105.5	22.6	79.2	48.8	3.9	20	0
E	1100.4	B	417606	6262148	6.8	2.4	105.5	22.6	79.2	48.8	4.5	49	0
F	1096.8	D	417741	6262148	13.0	1.5	81.8	6.7	80.1	36.7	28.1	30	71
LINE 30520		FLIGHT 18											
A	1210.2	B	416035	6262038	0.1	0.0	34.3	18.4	13.2	14.6	216.8	365	0
B	1212.6	B	416109	6262038	8.2	5.4	34.3	18.4	13.2	14.6	2.1	27	0
C	1222.9	D	416451	6262028	18.1	4.1	83.6	28.9	46.7	41.2	11.6	22	0
D	1238.0	B	416939	6262012	29.0	11.5	148.9	61.9	75.9	69.7	6.2	14	0
E	1241.9	D	417072	6262010	18.8	9.8	144.9	8.1	75.9	68.4	---	---	0
F	1255.9	D	417529	6262000	47.2	25.8	339.6	274.6	133.8	152.3	4.7	0	0
G	1258.7	B	417620	6261995	13.8	18.1	339.6	274.6	133.8	152.3	1.1	2	0
LINE 30530		FLIGHT 18											
A	1530.9	D	416117	6261893	26.3	12.3	38.9	29.2	30.8	14.5	4.8	15	0
B	1518.0	D	416484	6261879	22.8	6.6	118.8	28.3	89.6	54.1	---	---	0
C	1501.1	D	416932	6261870	15.2	2.4	69.6	25.5	35.5	31.1	18.7	31	0

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LINE 30530			FLIGHT 18										
D	1498.1	D	417014	6261864	11.1	5.2	69.6	25.5	35.5	31.1	3.6	22	0
E	1482.3	H?	417434	6261851	11.3	15.0	88.7	108.3	19.5	34.4	1.0	0	0
F	1472.3	H	417741	6261847	10.3	8.6	107.4	64.1	47.9	44.0	1.7	21	0
G	1467.5	E	417918	6261844	7.4	5.3	112.4	64.6	68.9	48.1	1.8	26	0
LINE 30540			FLIGHT 18										
A	1608.6	D	416216	6261748	12.8	5.4	55.0	33.0	22.1	23.7	4.3	24	17
B	1619.8	B	416497	6261731	14.4	8.4	102.8	50.9	35.2	46.0	2.9	17	0
C	1624.0	B	416614	6261723	7.8	8.2	102.8	50.9	35.2	46.0	1.2	23	0
D	1631.8	H	416852	6261711	9.6	6.0	45.4	31.7	33.0	25.2	2.3	34	0
E	1637.4	D	417033	6261705	5.7	0.8	55.8	17.3	35.1	26.7	---	---	0
F	1641.1	B?	417155	6261704	11.4	5.0	55.8	15.9	35.1	26.7	4.0	22	0
G	1650.7	H	417474	6261696	8.9	11.5	60.7	74.2	10.7	23.5	1.0	2	0
H	1669.8	D	418055	6261684	11.4	2.3	55.3	48.1	41.5	27.4	---	---	117
LINE 30550			FLIGHT 18										
A	1922.4	D	416304	6261578	19.1	10.3	101.3	42.1	50.0	48.6	3.6	17	0
B	1914.8	D	416473	6261572	14.8	8.9	9.9	17.6	5.5	2.8	2.8	16	29
C	1887.7	D	416827	6261574	9.0	5.3	60.8	27.9	13.0	30.8	2.5	33	0
D	1877.0	B	417060	6261562	14.0	5.9	74.7	41.4	39.7	36.7	4.4	19	0
E	1865.7	H	417359	6261562	7.0	5.2	41.9	35.4	43.6	21.1	1.7	27	0
F	1840.2	S	418153	6261545	4.1	9.1	43.1	87.1	8.7	16.5	0.4	0	0
G	1818.6	S?	418960	6261522	3.7	5.4	17.5	27.8	1.6	7.3	0.6	26	0
LINE 30560			FLIGHT 18										
A	2155.2	D	416381	6261436	13.0	13.7	109.6	68.3	39.8	52.5	1.4	13	88
B	2162.2	D	416504	6261429	26.7	13.8	89.5	41.8	39.8	40.4	4.2	10	54
C	2182.8	D	416868	6261407	17.6	9.4	95.4	40.5	46.3	44.0	3.5	17	0
D	2189.8	B?	416992	6261416	14.5	7.9	93.0	50.4	42.9	29.8	3.2	27	0
E	2195.9	D	417123	6261417	10.9	4.1	75.0	44.1	45.5	33.4	4.7	35	0
F	2208.5	D	417406	6261407	11.5	4.4	82.4	51.2	65.2	37.4	4.7	10	0
G	2224.9	H	417738	6261401	2.3	1.0	15.1	8.5	9.6	5.9	2.5	87	0
H	2263.1	S	418940	6261360	6.2	6.0	58.7	37.4	3.1	16.2	1.2	22	0
I	2268.9	S	419128	6261361	3.1	3.4	58.7	35.0	2.7	16.2	0.8	33	0
LINE 30570			FLIGHT 18										
A	2484.7	D	416420	6261282	17.5	7.9	102.6	47.7	43.9	51.3	4.4	20	0
B	2468.3	D	416538	6261278	6.2	2.9	47.9	21.9	25.5	21.9	3.0	44	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 30570			FLIGHT 18										
C	2435.3	D	416893	6261269	12.2	6.1	59.9	32.7	11.2	32.1	3.4	31	0
D	2417.2	B	417209	6261269	12.2	5.7	130.4	18.9	113.0	55.2	3.7	23	0
E	2403.2	B	417700	6261251	5.1	0.6	19.3	7.0	3.5	7.9	22.8	60	0
F	2367.9	S	418964	6261205	5.4	3.8	35.4	30.3	2.6	9.2	1.6	43	0
G	2365.0	S	419074	6261204	3.1	2.0	35.4	25.7	2.3	9.2	1.6	60	0
LINE 30580			FLIGHT 20										
A	2140.6	D	415975	6261126	7.6	5.1	25.3	0.3	18.2	12.7	2.0	10	0
B	2177.5	B	416523	6261116	12.0	3.6	95.4	30.7	62.6	47.0	6.8	21	0
C	2198.0	H?	416851	6261111	5.6	6.3	6.4	8.9	1.9	2.7	1.0	24	29
D	2208.8	H	417049	6261112	8.5	3.5	67.7	24.6	30.7	35.9	3.9	35	0
E	2223.6	H	417390	6261115	9.6	5.9	62.4	26.9	51.7	23.5	2.4	1	0
F	2237.9	B	417788	6261090	6.5	3.2	28.3	19.8	6.1	13.4	2.7	41	0
G	2275.4	H?	418943	6261061	2.8	7.2	17.2	36.8	1.3	6.8	0.4	10	0
LINE 30590			FLIGHT 20										
A	2539.2	D	416006	6260997	15.0	10.7	34.6	43.4	11.4	14.7	2.3	7	0
B	2510.1	H	416465	6260974	7.1	5.6	31.5	9.6	17.7	14.7	1.6	29	0
C	2497.9	D	416604	6260967	13.8	4.1	51.2	34.4	27.2	29.2	7.2	29	0
D	2483.6	D	416755	6260965	4.7	2.7	0.0	5.8	13.9	1.5	2.0	43	0
E	2468.3	D	416916	6260964	7.9	3.8	19.6	17.9	5.8	8.2	3.1	33	20
F	2443.4	H	417327	6260953	11.0	5.8	25.8	21.1	20.9	7.6	3.1	23	0
G	2426.6	E	417854	6260933	12.1	7.8	62.2	39.6	7.4	29.2	2.4	20	0
H	2388.6	H?	418943	6260911	5.2	6.2	14.4	30.2	2.0	7.7	0.9	14	0
LINE 30600			FLIGHT 20										
A	2613.8	H	416085	6260831	5.0	1.8	19.5	16.3	1.7	6.6	4.0	42	15
B	2629.5	B?	416395	6260823	2.6	0.4	58.4	29.2	31.2	26.9	12.3	79	0
C	2633.7	D	416465	6260818	23.2	14.2	58.4	29.2	14.6	26.9	3.2	8	14
D	2640.0	B	416570	6260817	0.4	0.4	19.5	1.2	16.5	6.1	0.5	132	0
E	2650.5	D	416733	6260809	34.9	19.7	123.8	52.3	51.8	62.6	4.1	11	0
F	2654.7	B	416803	6260813	24.8	11.2	107.6	32.5	53.1	53.6	4.9	7	0
G	2662.0	D	416929	6260815	8.3	2.0	13.0	17.5	5.8	3.4	8.0	41	0
H	2692.7	H?	417660	6260813	8.0	1.9	18.0	16.9	23.2	12.1	8.2	36	0
I	2700.3	D	417844	6260802	3.5	4.6	56.4	33.7	23.1	26.3	0.7	37	0
LINE 30610			FLIGHT 20										
A	3068.7	D	416176	6260695	15.6	9.0	59.1	26.9	19.7	25.5	3.1	18	29

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EM Anomaly List

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LINE 30610			FLIGHT 20										
B	3064.8	D	416267	6260694	9.2	8.4	59.1	26.9	19.7	25.5	1.4	20	0
C	3030.0	B	416679	6260663	6.6	5.2	46.2	20.2	35.5	21.0	1.6	33	0
D	3020.4	B	416802	6260665	4.9	1.0	42.6	17.5	17.7	20.4	9.4	53	0
E	3006.2	D	416981	6260663	5.5	0.4	35.1	9.3	18.0	18.8	37.1	52	0
F	2982.8	H	417285	6260662	11.9	5.8	52.5	37.7	21.2	26.9	3.4	30	0
G	2967.9	H	417624	6260648	4.4	0.1	25.8	5.7	32.0	12.6	150.7	64	0
H	2962.2	H?	417749	6260646	9.4	3.6	24.6	14.3	30.8	12.6	4.4	37	0
I	2947.0	D	418043	6260646	8.4	5.6	47.6	32.9	14.6	22.7	2.1	24	0
LINE 30620			FLIGHT 20										
A	3358.6	D	416281	6260529	37.1	35.3	96.1	105.6	23.9	42.4	2.2	0	0
B	3382.6	H	416638	6260516	8.9	5.9	34.1	12.1	11.3	15.2	2.1	25	18
C	3393.1	B?	416810	6260510	10.4	4.6	41.9	10.7	26.8	17.0	3.8	24	0
D	3401.7	D	416966	6260518	7.3	1.7	14.9	0.7	17.7	3.4	8.2	38	0
E	3414.8	H	417199	6260518	7.5	5.9	21.3	34.3	6.3	10.6	1.6	13	0
F	3420.6	D	417338	6260513	5.7	6.3	34.5	41.2	11.8	16.8	1.0	28	0
G	3459.8	D	418112	6260491	6.7	4.8	21.8	6.6	2.8	4.5	1.8	24	0
LINE 30630			FLIGHT 20										
A	3892.6	D	416363	6260391	18.8	21.4	79.0	67.7	40.0	39.2	1.4	7	66
B	3881.1	H?	416496	6260386	3.2	3.1	46.2	37.0	24.7	25.2	1.0	38	10
C	3846.5	D	416856	6260362	15.3	1.5	34.8	12.5	22.8	17.8	36.7	25	0
D	3824.8	D	417162	6260360	9.1	9.1	50.0	68.5	15.1	22.8	1.3	18	0
E	3818.1	H?	417304	6260357	4.7	5.9	50.0	68.5	14.7	22.8	0.8	33	0
F	3795.7	H	417666	6260346	3.6	3.9	16.5	7.4	11.3	7.7	0.9	38	0
G	3787.8	H?	417803	6260339	10.1	3.4	10.9	10.5	9.1	4.4	5.4	35	20
H	3769.9	E	418153	6260339	5.1	7.0	35.1	35.9	12.0	15.6	0.8	22	11
LINE 30640			FLIGHT 20										
A	4032.8	D	416494	6260216	26.5	13.2	79.2	43.7	19.0	38.2	4.4	0	0
B	4066.2	B	417067	6260202	17.4	7.5	123.3	57.7	95.9	51.1	4.6	6	0
C	4101.0	D	417691	6260169	8.1	6.6	82.0	30.5	47.7	38.8	---	---	0
D	4108.4	D	417826	6260168	10.5	6.4	82.0	30.5	47.7	38.8	2.5	18	0
E	4134.3	H	418246	6260173	4.4	8.1	15.0	26.2	0.8	4.1	0.5	25	0
LINE 30650			FLIGHT 20										
A	4492.1	H	416753	6260076	15.9	14.3	81.3	83.8	13.4	33.6	1.8	4	0
B	4470.9	B	417170	6260066	20.2	7.3	149.0	43.9	111.8	65.6	6.2	0	0

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LINE 30650			FLIGHT 20										
C	4440.5	B	417786	6260032	12.5	3.6	70.1	24.2	43.0	31.2	7.4	25	0
LINE 30660			FLIGHT 20										
A	4691.5	B	417199	6259916	25.3	4.5	124.1	37.1	110.3	59.5	18.9	3	17
B	4710.2	B?	417407	6259905	9.2	6.2	58.0	45.8	17.6	28.2	2.1	27	0
C	4746.7	B	417814	6259878	23.1	15.8	105.4	39.2	62.8	48.1	2.8	15	0
D	4753.4	D	417932	6259880	16.9	8.0	105.4	25.6	62.8	48.1	4.0	13	0
E	4809.7	S?	418575	6259862	5.1	7.5	13.6	45.9	3.6	7.3	0.7	26	17
F	4836.1	B?	419175	6259854	5.4	20.0	24.9	51.9	1.3	9.9	0.3	0	0
G	4854.1	S	419436	6259849	5.4	14.5	20.5	51.8	1.4	11.1	0.4	0	0
LINE 30670			FLIGHT 20										
A	5368.4	H	416148	6259792	3.6	0.2	29.6	27.3	6.2	11.3	47.5	60	0
B	5356.8	H	416264	6259793	7.4	8.1	20.7	18.8	4.5	11.0	1.1	16	0
C	5277.4	D	417082	6259767	11.5	3.1	61.8	44.0	38.1	25.9	7.8	38	62
D	5269.3	B	417263	6259755	16.6	13.7	68.5	23.2	55.3	23.8	2.0	0	0
E	5263.2	B	417348	6259753	28.4	14.5	68.5	23.2	55.3	34.8	4.4	17	0
F	5251.2	D	417489	6259746	28.6	13.0	25.8	35.5	9.9	13.6	5.1	11	0
G	5219.8	D	417960	6259741	14.0	9.1	53.1	36.3	20.9	20.9	2.5	0	20
H	5215.5	D	418041	6259738	10.6	11.6	53.1	36.3	20.9	20.9	1.2	3	20
I	5168.4	E	418684	6259728	6.9	15.9	75.8	120.7	0.6	25.7	0.5	5	0
J	5162.9	B	418767	6259725	1.3	16.0	75.8	120.7	1.5	25.7	0.1	0	0
K	5158.4	D	418833	6259725	17.2	25.3	75.8	120.7	1.4	25.7	1.1	0	0
L	5107.0	D	419461	6259694	14.6	33.5	41.3	75.8	4.1	16.8	0.7	0	0
LINE 30681			FLIGHT 21										
A	882.3	D	415905	6259633	8.6	18.3	61.7	68.1	3.5	13.1	0.6	0	0
B	889.2	B?	415999	6259636	6.2	19.7	61.7	68.1	8.4	27.3	0.4	0	18
C	892.3	D	416044	6259636	6.2	9.4	61.7	68.1	13.8	27.3	0.7	0	0
D	905.9	D	416243	6259639	24.4	17.2	54.9	34.4	23.1	24.8	2.7	1	0
E	916.6	D	416403	6259630	10.6	2.4	31.1	4.6	23.9	11.5	10.1	30	0
F	919.4	D	416441	6259624	12.9	6.0	31.1	4.6	23.9	11.5	3.8	30	0
G	945.6	E	417020	6259622	17.0	15.9	91.6	81.3	31.4	42.2	1.7	21	30
H	949.7	D	417139	6259621	21.2	1.8	91.6	81.3	39.0	42.2	54.8	20	34
I	974.2	B	417390	6259608	6.0	3.0	61.1	27.3	38.0	22.5	2.6	50	0
J	983.5	B	417453	6259604	2.0	1.4	91.1	34.1	51.3	45.4	1.2	60	0
K	989.3	D	417509	6259597	14.9	9.8	91.1	34.2	51.3	45.4	2.5	23	0
L	1031.0	D	417966	6259583	14.1	3.9	67.8	57.0	20.0	30.2	7.9	7	0

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LINE 30681		FLIGHT 21											
M	1035.9	D	418077	6259579	20.0	19.6	67.8	57.0	20.0	17.9	1.7	8	0
N	1110.2	H?	418951	6259552	2.3	9.9	29.7	76.5	0.5	13.1	---	---	0
O	1120.1	S	419136	6259553	1.7	16.4	10.4	54.4	0.0	8.8	---	---	0
P	1147.9	S	419537	6259552	6.0	11.4	26.0	39.9	4.9	8.2	---	---	0
LINE 30690		FLIGHT 21											
A	1596.5	H?	416294	6259494	5.1	3.0	33.3	6.5	18.6	14.9	---	---	0
B	1567.6	D	416462	6259476	11.2	6.7	37.6	35.4	6.5	16.5	2.6	20	0
C	1550.4	B	416530	6259472	8.7	9.1	88.0	36.9	52.7	46.1	1.2	21	0
D	1503.8	B	417180	6259452	51.5	22.5	178.2	84.8	82.6	80.3	6.5	0	0
E	1487.8	D	417437	6259463	13.4	12.1	79.9	40.5	38.2	36.3	1.7	12	0
F	1483.4	D	417501	6259461	24.2	14.8	79.9	40.5	38.2	36.3	3.3	12	22
G	1449.0	B	418010	6259424	17.3	5.0	74.9	21.1	38.1	35.7	8.0	0	0
H	1336.2	S	419618	6259392	12.6	29.5	62.8	130.5	3.9	25.7	---	---	0
LINE 30700		FLIGHT 21											
A	1722.3	D	416312	6259337	14.9	24.1	66.9	64.4	33.0	32.0	0.9	6	18
B	1729.6	D	416426	6259337	12.5	1.9	67.8	64.4	33.0	32.0	18.1	19	17
C	1741.9	D	416608	6259321	50.1	42.1	151.1	102.5	67.3	78.7	2.8	0	0
D	1764.8	B	417222	6259301	61.6	25.0	277.4	113.7	167.5	122.8	7.7	0	0
E	1775.9	E	417364	6259303	11.6	9.6	11.7	23.3	10.4	5.9	1.8	8	0
F	1805.7	H	417527	6259293	3.2	3.5	17.7	8.5	4.1	8.2	---	---	0
G	1845.3	D	417877	6259289	21.4	8.6	55.8	21.0	31.5	27.0	5.5	16	0
H	1862.5	D	418223	6259281	14.8	14.5	63.1	63.1	37.4	32.3	1.6	0	0
I	1975.2	S	419634	6259246	6.4	15.0	21.8	44.9	10.0	8.9	0.5	0	0
LINE 30710		FLIGHT 22											
A	1132.6	B	416544	6259177	33.2	13.0	146.6	39.6	95.4	72.0	6.5	10	15
B	1140.6	B?	416675	6259180	22.4	16.8	116.2	58.2	75.8	59.5	2.5	0	0
C	1143.3	B	416730	6259180	31.1	4.6	116.2	93.1	75.8	59.5	25.9	3	28
D	1158.1	B	417121	6259159	61.6	16.4	323.3	81.7	197.6	154.3	13.8	5	0
E	1162.1	B	417205	6259162	65.5	26.4	323.3	129.2	197.6	154.3	7.9	2	0
F	1233.0	B	417816	6259145	53.2	34.0	107.7	112.8	19.1	47.7	4.0	5	0
G	1244.6	B	417965	6259141	14.2	13.0	53.0	14.7	25.8	5.8	---	---	0
H	1265.3	D	418364	6259132	21.5	23.9	116.3	125.8	14.0	51.5	1.5	3	0
I	1364.7	S	419708	6259102	8.3	10.9	18.4	30.4	5.5	8.1	---	---	18

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LINE 30720		FLIGHT 22											
A	1727.0	D	416011	6259056	7.3	7.0	13.8	61.6	0.9	9.9	---	---	0
B	1664.8	D	416590	6259026	78.0	41.3	203.9	129.2	79.8	92.2	5.8	0	16
C	1656.0	D	416718	6259026	2.7	2.1	96.0	99.5	79.8	92.2	---	---	0
D	1651.8	B?	416827	6259021	36.3	23.2	96.0	99.5	79.8	39.3	3.5	7	76
E	1638.4	D	417165	6259016	99.9	61.3	283.2	224.1	120.7	130.4	5.2	0	21
F	1633.6	B	417249	6259011	54.5	54.7	234.5	118.0	125.8	106.9	2.4	0	21
G	1630.5	E	417300	6259010	48.5	54.7	234.5	118.0	125.8	106.9	2.0	0	0
H	1594.7	D	417849	6259003	43.3	34.0	60.7	38.2	23.1	29.2	2.9	0	0
I	1554.2	H	418463	6258981	10.6	14.6	44.4	63.6	31.0	23.6	---	---	0
J	1467.0	S	419645	6258954	6.3	1.4	15.2	0.0	10.5	1.3	---	---	0
K	1455.7	S	419758	6258964	9.9	9.3	43.4	50.8	9.1	13.2	---	---	22
LINE 30730		FLIGHT 22											
A	1887.4	D	416680	6258886	32.2	31.2	199.6	248.7	92.7	111.7	2.1	0	0
B	1893.3	D	416832	6258877	44.3	42.5	202.9	248.7	113.2	104.1	2.3	5	39
C	1898.5	D	416977	6258877	2.3	0.0	202.9	248.7	113.2	104.1	---	---	40
D	1905.8	B	417152	6258863	64.8	51.3	353.7	207.4	126.9	161.0	3.3	0	0
E	1909.2	D	417207	6258858	78.1	48.0	353.7	207.4	126.9	161.0	4.8	0	0
F	1920.0	D	417306	6258858	23.0	13.4	60.9	56.0	16.9	26.7	3.4	0	0
G	1951.6	D	417658	6258837	14.5	4.1	17.2	17.0	13.8	10.0	7.8	15	0
H	1959.8	D	417842	6258824	13.0	11.3	53.1	46.9	27.2	29.3	1.7	19	17
I	1965.9	B	417909	6258835	7.3	11.7	53.1	46.9	27.2	29.3	0.7	21	19
J	1974.1	D	417978	6258844	30.8	19.1	40.3	40.8	4.9	18.7	3.5	6	15
K	1993.5	H	418189	6258839	7.4	18.2	18.3	52.1	1.8	14.3	0.5	6	0
L	2059.8	B	419073	6258808	31.6	28.7	265.8	127.5	138.3	126.4	2.2	3	0
M	2068.4	B?	419204	6258806	37.7	41.0	183.3	173.7	9.9	70.2	1.9	0	0
LINE 30740		FLIGHT 22											
A	2481.5	D	416467	6258720	2.1	0.0	16.8	44.6	2.9	10.9	---	---	0
B	2467.2	B	416664	6258725	0.0	15.1	104.9	104.8	16.8	45.4	---	---	0
C	2462.7	D	416794	6258725	44.6	21.5	104.9	104.8	196.5	45.4	5.4	5	83
D	2453.8	D	417041	6258716	92.9	49.3	302.1	186.1	196.5	134.5	6.1	5	0
E	2442.3	D	417246	6258714	45.6	10.1	166.3	73.9	99.1	68.3	16.3	0	11
F	2434.4	D	417361	6258715	16.3	18.6	95.0	43.0	54.8	44.5	1.4	9	10
G	2410.5	H?	417722	6258710	8.2	2.4	6.1	6.3	4.0	2.0	6.3	27	24
H	2395.6	D	418049	6258685	32.5	9.7	84.9	53.6	23.0	39.8	9.5	0	24
I	2328.5	D	419119	6258668	41.7	32.7	218.7	165.6	91.9	102.3	2.9	5	0

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EM Anomaly List

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LINE 30740			FLIGHT 22										
J	2323.5	D	419214	6258659	46.3	43.0	218.7	165.6	91.9	102.3	2.4	0	0
LINE 30750			FLIGHT 22										
A	2747.8	D	416589	6258575	9.1	9.4	33.7	172.7	7.3	34.1	1.3	1	0
B	2754.8	E	416757	6258576	3.2	40.6	67.9	172.7	39.7	26.1	0.1	0	0
C	2760.0	D	416885	6258570	41.8	0.7	230.5	63.5	163.4	95.0	---	---	85
D	2766.1	D	417022	6258564	55.1	21.7	222.5	27.9	159.0	83.4	7.7	2	79
E	2769.7	D	417092	6258566	48.5	16.9	205.5	71.4	159.0	87.0	8.7	6	79
F	2779.3	D	417216	6258569	68.0	33.2	250.5	152.2	146.1	111.4	6.2	2	0
G	2788.4	E	417279	6258566	18.8	17.6	28.1	13.9	17.7	15.5	1.8	10	0
H	2836.2	D	417718	6258528	8.2	5.6	17.6	18.2	9.5	8.9	2.0	20	0
I	2849.5	B?	417993	6258522	83.7	56.7	299.4	185.4	108.1	141.5	4.3	0	18
J	2913.5	H	419128	6258504	2.5	1.4	16.6	4.6	12.7	5.0	1.7	72	0
LINE 30760			FLIGHT 22										
A	3334.1	H?	416555	6258428	17.6	35.6	58.5	143.4	23.3	31.9	0.8	0	0
B	3329.9	H	416664	6258424	12.3	35.6	58.5	143.4	34.4	31.9	0.5	0	51
C	3319.8	D	416951	6258409	48.7	12.4	85.8	51.9	90.0	40.2	13.6	5	84
D	3312.7	B	417118	6258401	33.4	20.3	116.4	51.9	96.3	50.4	3.7	0	83
E	3310.4	B	417162	6258404	33.8	20.3	116.4	53.6	96.3	50.2	3.7	2	0
F	3304.2	D	417256	6258411	21.2	17.9	85.5	47.2	52.9	35.1	2.1	0	23
G	3250.1	D	417977	6258379	99.6	61.6	271.5	158.1	84.6	129.3	5.2	0	0
H	3160.0	S	419691	6258356	4.5	6.4	2.7	21.2	0.7	5.4	0.7	23	0
LINE 30770			FLIGHT 22										
A	3568.3	D	416556	6258291	23.9	56.6	81.7	247.8	20.6	48.9	0.8	0	0
B	3575.3	B?	416679	6258287	5.1	10.6	81.7	44.5	21.6	48.9	0.5	4	0
C	3602.3	D	417031	6258253	110.7	45.2	302.9	192.7	151.1	145.5	9.2	3	0
D	3604.0	B	417067	6258253	110.7	60.2	302.9	192.7	151.1	145.5	6.3	0	68
E	3616.2	B	417296	6258243	5.5	7.2	46.0	27.3	29.4	19.2	---	---	0
F	3668.6	D	417881	6258237	31.9	20.1	131.8	82.0	62.2	66.0	3.4	5	13
G	3671.4	B	417939	6258234	16.7	10.2	131.8	82.0	62.2	66.0	2.9	18	0
LINE 30780			FLIGHT 23										
A	3599.4	D	416626	6258134	9.5	3.1	79.7	110.6	5.6	38.0	5.5	34	59
B	3609.4	D	416743	6258139	8.1	17.3	79.7	113.9	1.2	38.0	0.6	5	0
C	3657.1	D	417065	6258093	34.5	12.0	71.7	20.1	13.7	18.7	7.8	13	0
D	3665.3	B	417153	6258089	43.9	30.5	237.5	67.5	162.1	111.5	3.4	11	0

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LINE 30780		FLIGHT 23											
E	3741.9	D	417891	6258091	13.8	15.0	59.0	53.4	30.0	31.1	1.4	18	0
F	3748.4	B	417981	6258087	8.6	10.3	59.0	53.4	30.0	31.1	1.1	22	0
LINE 30790		FLIGHT 23											
A	4185.2	H?	416362	6257986	4.0	2.1	27.5	14.8	12.2	12.0	2.3	57	0
B	4174.9	H	416474	6257977	8.7	14.7	74.1	140.5	8.7	32.6	0.7	0	20
C	4170.4	D	416550	6257974	3.8	20.0	74.1	140.5	12.8	46.5	0.2	0	64
D	4161.1	B?	416671	6257966	17.8	23.7	88.7	140.5	8.7	46.5	1.2	0	72
E	4112.9	D	417152	6257968	18.6	7.4	43.3	23.4	16.8	18.4	5.3	27	0
F	4102.2	B?	417254	6257965	13.5	6.0	60.0	23.4	39.6	24.7	4.1	14	16
G	4060.3	D	417824	6257948	21.8	16.8	95.8	71.1	33.8	42.2	2.4	10	10
H	4053.6	D	417907	6257937	43.9	29.8	112.2	71.1	33.8	49.8	3.5	1	0
I	4047.6	D	417981	6257930	41.5	39.2	112.2	75.7	29.7	49.8	2.3	7	0
LINE 30800		FLIGHT 23											
A	4365.2	H	416086	6257834	5.4	9.8	23.5	35.7	12.5	11.1	0.6	8	0
B	4388.5	H	416287	6257838	11.8	2.2	18.2	7.9	23.5	5.2	13.2	9	0
C	4404.1	B?	416528	6257825	7.5	12.1	39.9	64.1	7.0	20.9	0.7	0	0
D	4411.0	B?	416621	6257827	3.0	7.3	39.9	64.1	7.5	20.9	0.4	1	0
E	4503.5	D	417256	6257797	16.6	12.7	42.3	58.6	25.8	46.8	2.2	5	0
F	4514.3	B	417382	6257802	30.7	11.4	167.2	58.6	96.5	67.0	6.9	0	31
G	4522.8	D	417512	6257801	20.1	19.1	104.7	79.6	51.5	43.5	1.8	1	0
H	4563.8	D	417876	6257787	86.6	58.2	109.4	121.1	43.0	50.3	4.4	0	0
I	4576.8	E	417974	6257787	14.4	16.2	81.3	52.5	24.0	35.5	1.3	17	0
LINE 30811		FLIGHT 65											
A	1131.4	H?	417384	6257636	1.5	0.8	17.3	0.3	12.7	5.1	---	---	0
B	1167.6	D	417900	6257644	47.2	27.1	101.9	78.0	24.7	49.5	4.4	0	0
LINE 30821		FLIGHT 65											
A	1610.2	H	417364	6257518	4.2	1.5	9.2	9.5	4.7	2.6	---	---	0
LINE 30830		FLIGHT 23											
A	5980.9	H	416732	6257386	15.9	21.6	38.5	28.5	22.4	12.6	1.1	0	0
B	5900.8	D	417384	6257350	40.2	30.0	65.4	64.9	49.6	39.9	3.0	0	0
C	5884.1	B	417507	6257342	44.2	16.8	228.9	110.7	136.1	98.0	7.5	0	20
D	5880.1	D	417561	6257343	37.9	10.8	228.9	110.7	136.1	98.0	10.6	0	20
E	5860.2	D	417883	6257347	37.4	61.0	79.8	62.2	28.8	35.6	1.2	0	0

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LINE 30830			FLIGHT 23										
F	5851.1	E	418001	6257347	8.2	10.7	38.2	18.6	9.4	12.2	0.9	19	0
LINE 30840			FLIGHT 23										
A	6146.0	S	416012	6257245	4.5	15.6	14.7	23.6	7.9	7.0	0.3	0	71
B	6230.1	H	416767	6257192	27.7	30.0	65.3	82.1	20.9	26.6	1.7	2	0
C	6301.6	D	417367	6257209	24.0	46.5	219.2	141.2	95.4	109.1	0.9	0	0
D	6309.4	B	417453	6257211	76.7	45.0	219.2	141.2	95.4	109.1	5.1	8	0
E	6315.2	B	417528	6257212	52.2	24.2	321.1	136.0	173.4	147.2	6.1	0	31
F	6322.6	D	417647	6257212	28.6	19.0	154.8	100.4	117.0	69.8	3.1	6	29
G	6327.8	D	417727	6257207	57.5	41.1	154.8	100.4	117.0	69.8	3.6	0	0
H	6347.8	B?	417871	6257188	26.2	36.5	81.5	65.9	30.0	35.0	1.3	3	0
LINE 39010			FLIGHT 23										
A	9015.0	H?	416657	6268891	5.6	13.4	24.3	58.5	1.7	12.9	0.5	12	0
B	9002.4	H?	416643	6268782	2.6	3.7	0.0	0.1	2.7	7.3	0.6	46	0
C	8981.3	H	416639	6268579	1.4	4.0	47.2	72.3	10.3	16.8	0.3	23	159
D	8961.8	H	416630	6268367	2.5	4.4	6.1	13.0	1.9	2.9	0.5	32	0
E	8952.5	H	416631	6268272	3.1	4.6	22.5	48.0	4.5	11.6	0.6	23	0
F	8818.7	D	416573	6265439	29.7	20.0	216.2	80.3	131.9	93.8	3.1	4	0
G	8814.4	B	416572	6265384	23.0	14.0	216.2	80.3	131.9	93.8	3.2	2	0
H	8702.8	B	416500	6263306	3.5	4.0	131.3	21.9	129.5	53.0	0.8	40	0
I	8696.4	B	416494	6263135	0.0	4.9	131.3	21.9	68.9	28.9	0.1	20	0
J	8694.0	B	416489	6263071	11.0	4.9	68.3	10.2	68.9	28.9	3.8	30	0
K	8683.8	H	416477	6262759	9.2	3.9	58.3	24.9	35.9	29.7	3.8	30	0
L	8677.9	H	416471	6262548	18.0	13.7	66.1	65.3	28.7	29.7	2.3	0	0
M	8661.4	B	416451	6261918	15.1	3.8	91.4	26.1	71.4	35.3	9.4	22	0
N	8648.0	E	416436	6261549	11.2	9.8	54.1	17.4	30.5	24.8	1.6	17	0
O	8640.9	D	416428	6261408	11.7	2.6	64.8	43.5	16.0	35.8	10.4	32	142
P	8639.0	D	416428	6261370	12.0	6.2	64.8	37.7	16.0	35.8	3.2	28	139
Q	8627.9	B	416444	6261135	9.8	7.2	101.0	32.9	47.8	53.4	1.9	19	0
R	8614.8	D	416436	6260786	15.8	8.8	65.7	28.6	33.1	31.7	3.2	21	22
S	8600.4	H	416415	6260376	7.9	5.4	73.5	27.6	43.3	37.6	2.0	28	0
T	8593.2	E	416423	6260163	11.4	5.0	58.7	24.7	20.1	31.3	4.0	23	0
U	8567.1	D	416388	6259319	24.5	11.2	62.1	35.9	36.9	31.0	4.8	10	0
V	8540.8	H?	416376	6258601	7.7	7.3	19.7	14.3	6.7	8.3	1.3	19	0
W	8527.4	H	416363	6258224	6.9	12.5	11.5	19.9	8.0	5.2	0.6	1	0
X	8514.9	D	416351	6257795	20.3	19.3	48.4	46.9	27.2	26.4	1.8	6	48

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LINE 39020		FLIGHT 23											
A	8314.5	H	417859	6258235	4.0	4.2	21.3	29.8	5.5	10.7	0.9	41	0
B	8271.1	H	417875	6258915	7.8	9.9	41.8	35.9	6.5	19.8	1.0	15	0
C	8258.7	B?	417873	6259161	1.9	6.1	57.5	14.8	19.9	26.5	0.3	5	0
D	8248.5	H	417880	6259390	6.6	5.7	17.4	38.0	2.2	10.9	1.4	30	0
E	8217.2	B	417893	6259865	10.1	6.5	107.1	43.2	53.1	50.4	2.3	13	0
F	8179.3	D	417925	6260869	10.7	7.0	67.5	38.2	16.1	31.0	2.3	27	0
G	8148.1	H	417948	6261815	15.3	8.8	87.0	52.4	55.7	43.6	3.1	24	0
H	8107.9	H	417974	6262939	13.2	7.0	96.5	42.3	43.4	39.8	3.2	23	0
I	8098.4	B	417987	6263208	14.9	5.7	151.3	22.6	120.0	73.4	5.2	28	0
J	8045.3	B	418043	6264790	24.4	19.7	196.8	98.9	76.6	95.3	2.3	0	0
K	8039.3	B?	418042	6264953	22.6	26.9	199.4	135.8	65.3	97.3	1.5	0	59
L	8036.9	B	418041	6265009	18.9	25.0	199.4	135.8	65.3	97.3	1.2	15	0
M	8028.5	D	418035	6265175	23.9	12.4	0.0	0.0	57.2	0.0	4.0	6	0
N	8021.9	B	418032	6265287	76.0	59.4	306.4	171.7	110.6	147.4	3.5	0	0
O	7992.4	D	418054	6265877	26.0	18.3	175.3	105.1	79.8	84.1	2.8	9	0
P	7987.9	H?	418058	6265991	18.7	22.0	175.3	105.1	79.8	84.1	1.4	0	0
Q	7950.6	B	418126	6266886	10.0	15.0	91.3	106.0	14.4	40.0	0.9	11	0
R	7931.7	H	418119	6267426	4.0	8.4	32.1	69.7	0.6	15.1	0.5	17	0
S	7866.7	H	418136	6268534	5.3	9.7	37.7	69.2	13.6	16.7	0.6	9	0
T	7858.7	H	418148	6268756	9.6	13.2	53.1	53.0	12.2	26.1	0.9	10	0
U	7843.5	D	418145	6269090	9.9	14.3	38.0	53.3	3.0	15.4	0.9	13	0
V	7839.3	B?	418153	6269168	11.5	16.8	29.9	52.4	5.7	15.3	0.9	7	33
W	7818.5	H	418155	6269505	9.8	5.0	10.6	5.7	5.8	6.6	3.0	9	0
X	7800.3	B	418161	6269752	4.3	4.7	8.3	4.1	5.7	1.9	0.9	44	0
LINE 39030		FLIGHT 23											
A	7623.2	B	419682	6269690	11.4	12.5	110.0	88.4	19.2	49.5	1.3	0	0
B	7593.2	D	419644	6269382	24.6	20.9	46.6	74.1	1.1	14.4	2.2	4	0
C	7238.1	H?	419539	6265143	12.3	13.0	59.7	53.1	17.5	24.4	1.4	0	23
D	7017.3	H	419441	6261295	3.8	11.8	18.0	54.3	1.0	10.6	---	---	0
E	6997.4	H?	419411	6260757	3.6	5.7	13.7	31.4	0.4	6.8	---	---	0
F	6865.8	H	419356	6258628	4.4	2.5	24.0	33.6	1.8	8.5	---	---	0

CX = COAXIAL
CP = COPLANAR

Note:EM values shown above are local amplitudes

*Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

Anomalies Summary
ÄÄÄÄÄÄÄÄÄÄÄÄÄÄÄÄÄ

Conductor Grade	No, of Responses
7	4
6	1
5	18
4	40
3	110
2	380
1	134
0	45
Total	732

Conductor Model	No, of Responses
E	31
B	252
D	291
S	21
H	137
Total	732

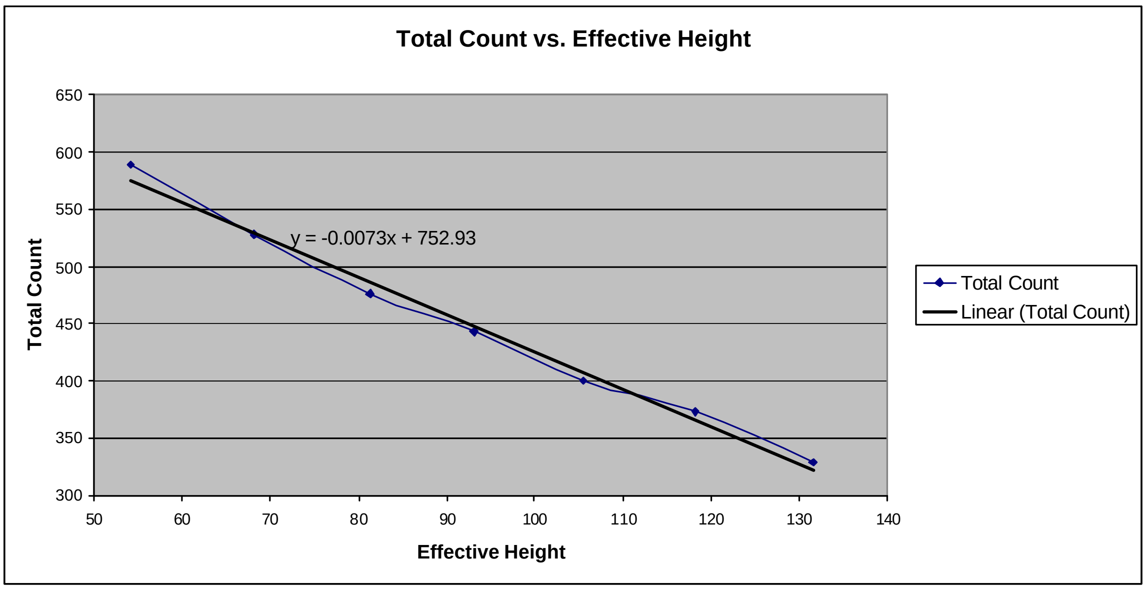
APPENDIX F

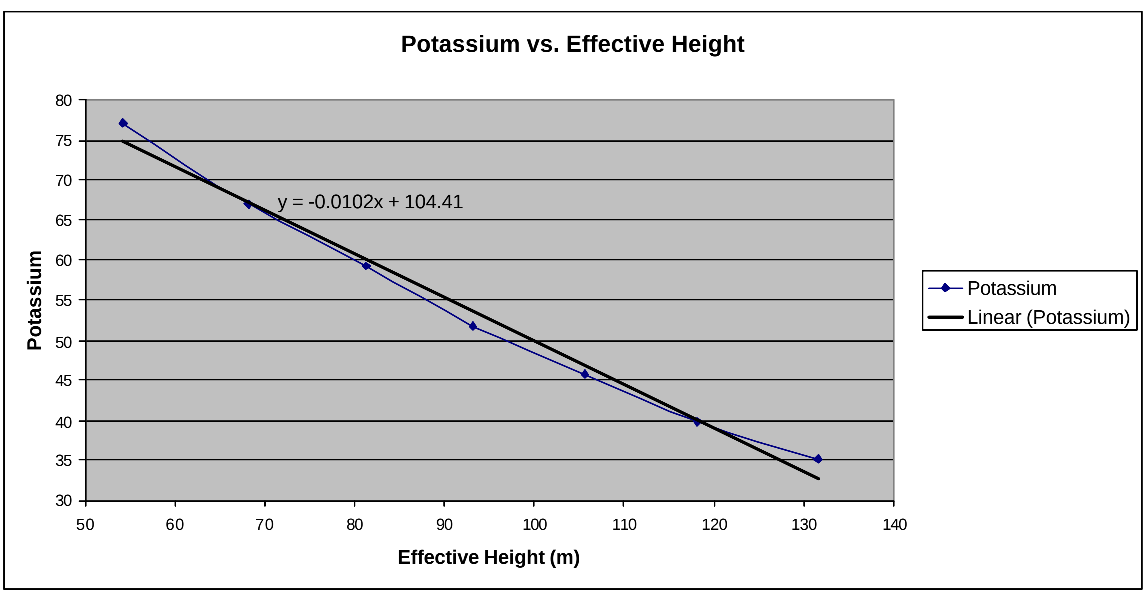
TESTS AND CALIBRATIONS

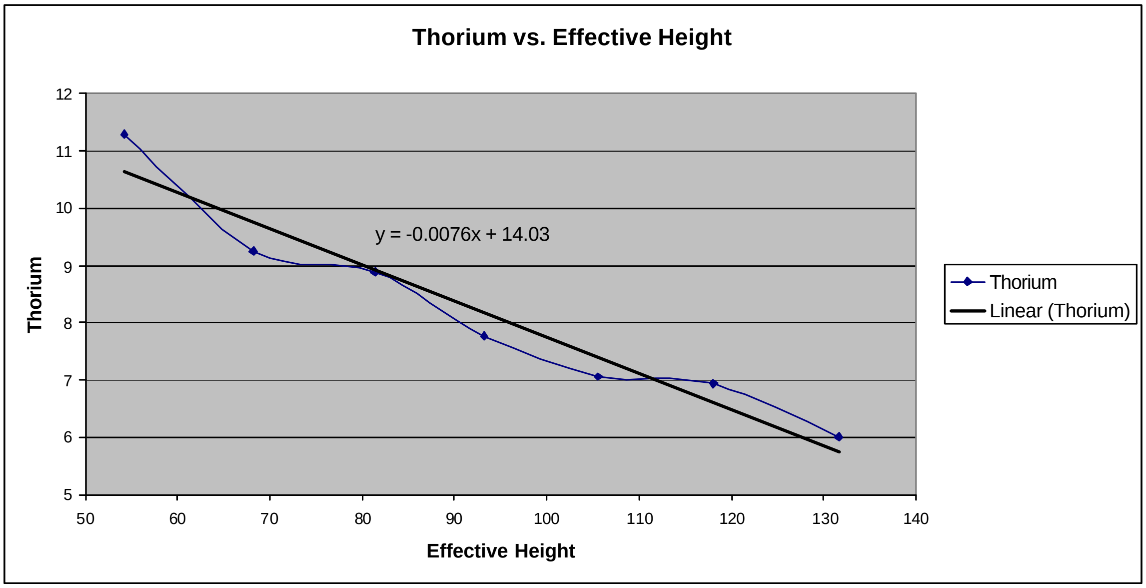
APPENDIX F

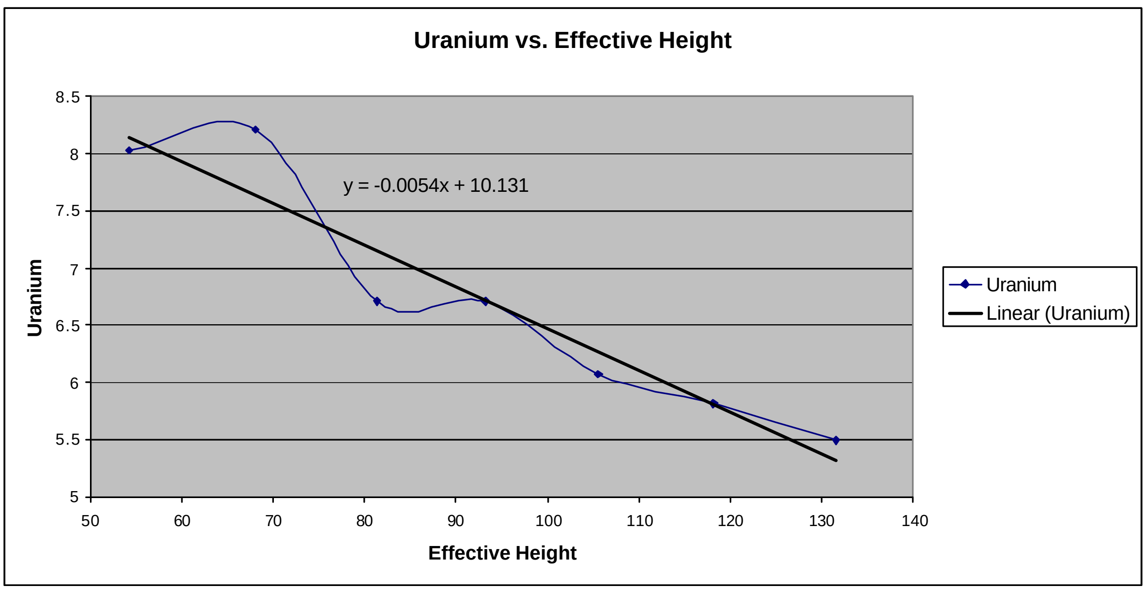
TESTS AND CALIBRATIONS

ALTITUDE ATTENUATION TESTS

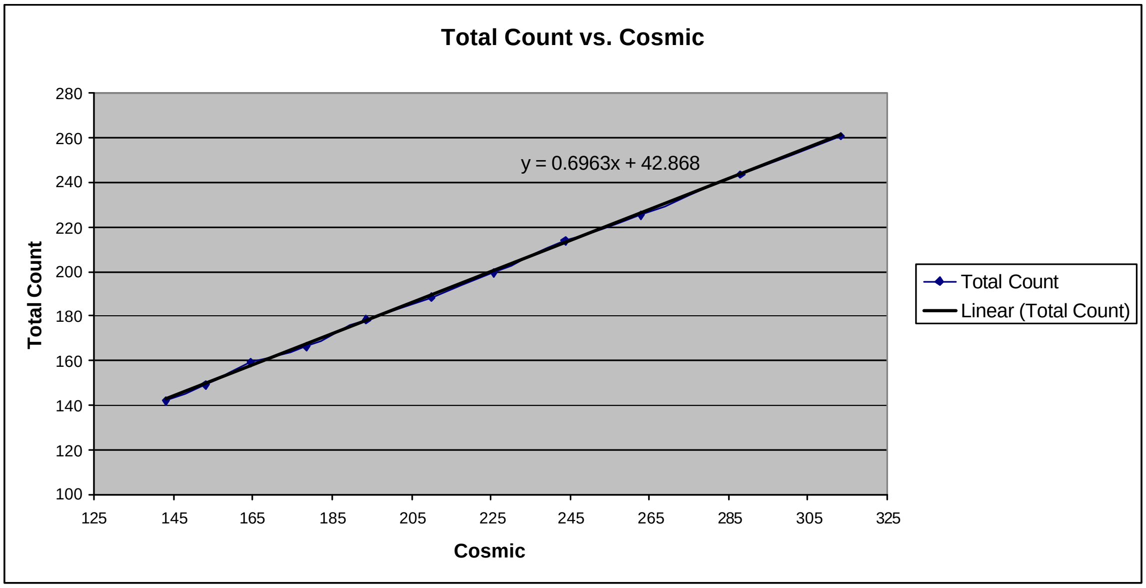


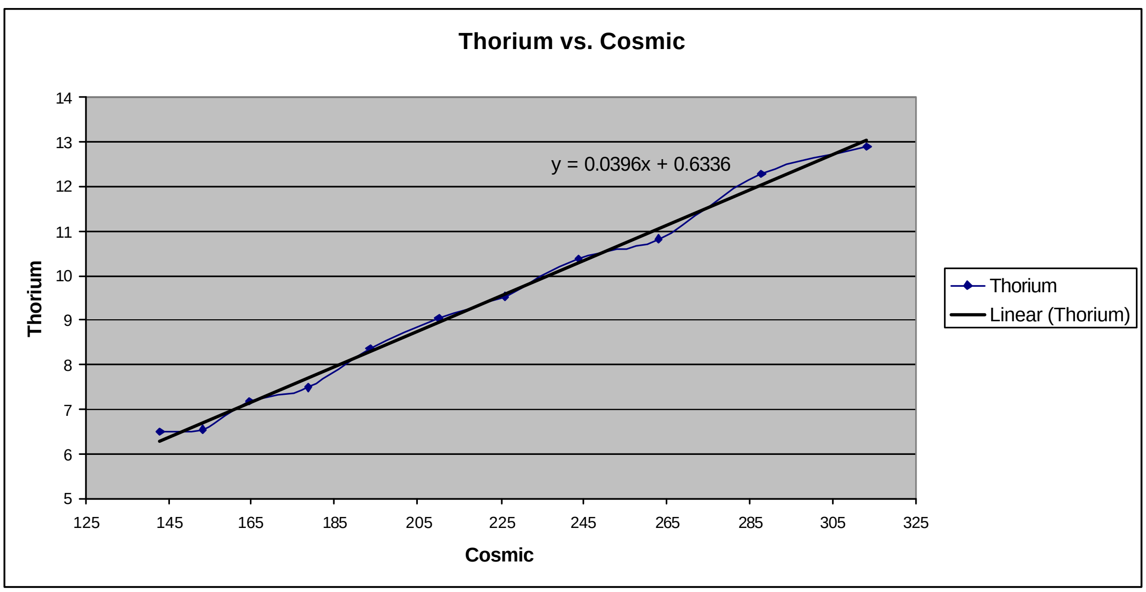


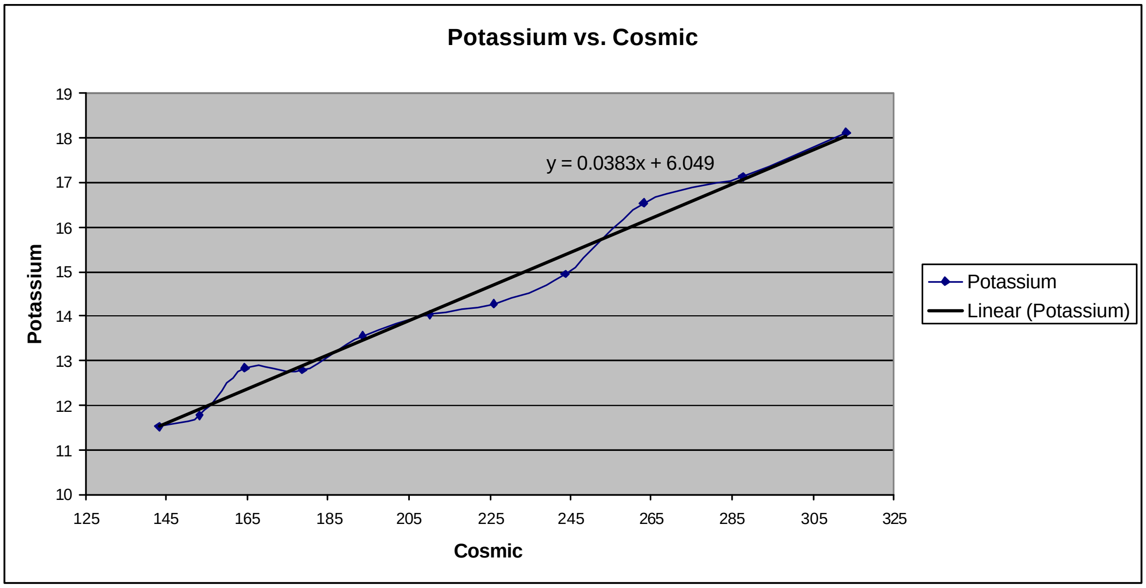

Thorium vs. Effective Height
12
11
10
9
8
7
6
5
Thorium
50
60
70
80
90
100
110
120
130
140
Effective Height
y = -0.0076x + 14.03
Thorium
Linear (Thorium)

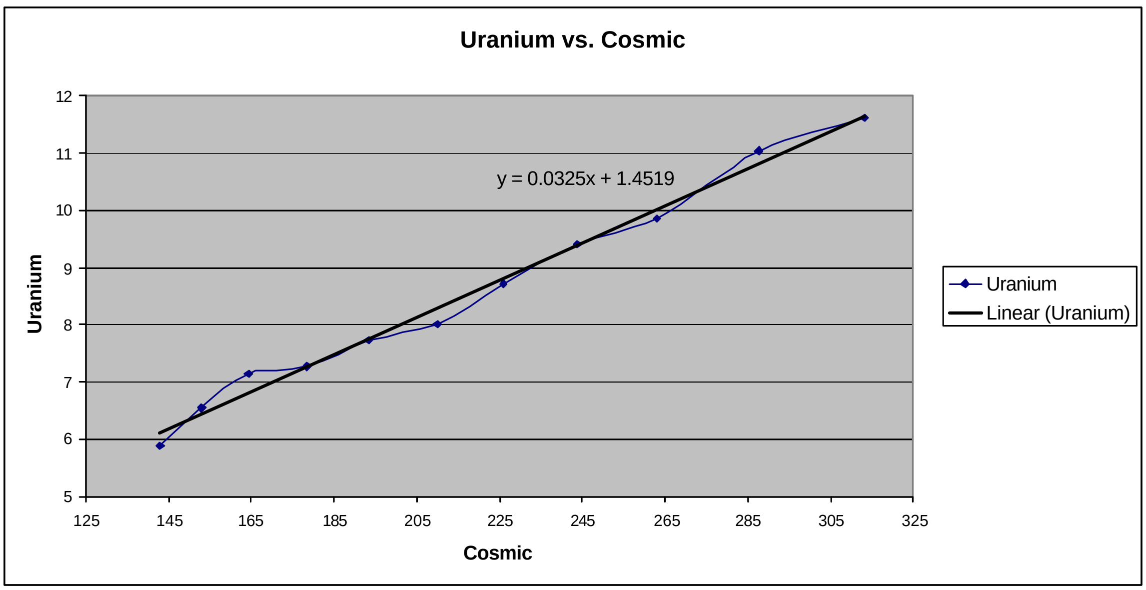

Uranium vs. Effective Height
8.5
8
7.5
7
6.5
6
5.5
5
Uranium
50
60
70
80
90
100
110
120
130
140
Effective Height
y = -0.0054x + 10.131
Uranium
Linear (Uranium)

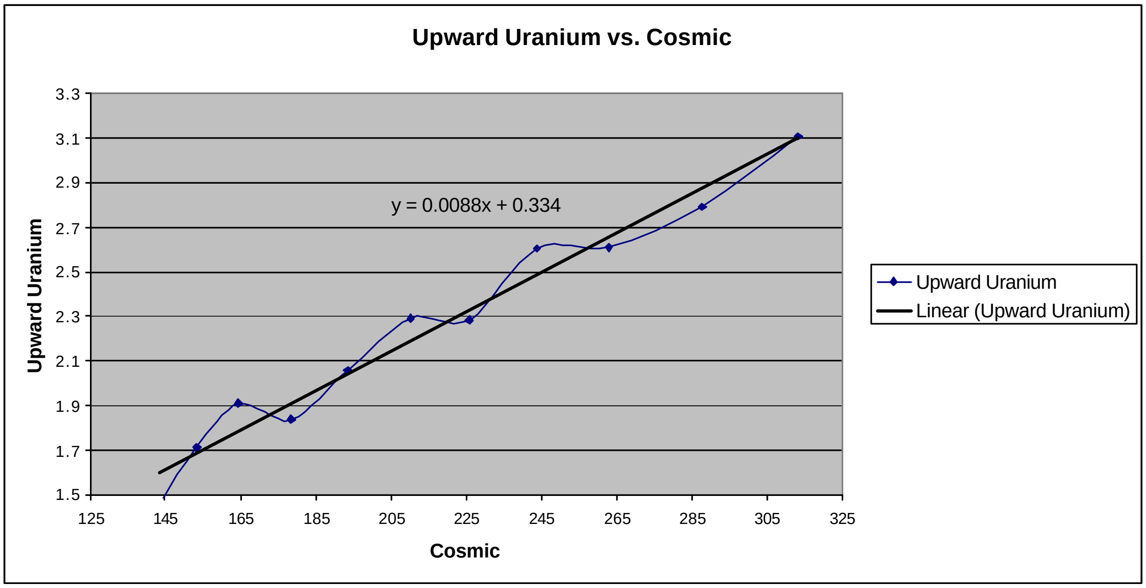
COSMIC TESTS






Potassium vs. Cosmic
y = 0.0383x + 6.049
Potassium
Cosmic
19
18
17
16
15
14
13
12
11
10
125
145
165
185
205
225
245
265
285
305
325
Potassium
Linear (Potassium)


Uranium vs. Cosmic
y = 0.0325x + 1.4519
Uranium
Cosmic
12
11
10
9
8
7
6
5
125
145
165
185
205
225
245
265
285
305
325
Uranium
Linear (Uranium)



Upward Uranium vs. Cosmic
y = 0.0088x + 0.334
Upward Uranium
Cosmic
3.3
3.1
2.9
2.7
2.5
2.3
2.1
1.9
1.7
1.5
125
145
165
185
205
225
245
265
285
305
325
Upward Uranium
Linear (Upward Uranium)

APPENDIX G

RADIOMETRIC PROCESSING CONTROL FILE

APPENDIX G

RADIOMETRIC PROCESSING
CONTROL FILE

```
///////////////////////////////////////////////////
// Atlas Control/Workspace File
// # or // for commment
///////////////////////////////////////////////////

CONTROL_BEGIN

  PROGRAM  = AGSCorrection
  VERSION  = 1.4.0

   ### Process or Calibration? ###
       WhatToDo = Process Survey Line

   ### Corrections to apply ###
       CorrectionType = Yes  Filtering
       CorrectionType = Yes  LiveTimeCorrection
       CorrectionType = Yes  CosmicAircraftBGRemove
       CorrectionType = Yes  CalcEffectiveHeight
       CorrectionType = Yes  RadonBGRemove
       CorrectionType = Yes  ComptonStripping
       CorrectionType = Yes  HeightCorrection
       CorrectionType = No   ConvertToConcentration


   ### Main I/O settings ###
       MainChannelIO|TC       = GR820_TC_DOWN --> TC_R
       MainChannelIO|K        = GR820_K_DOWN --> K_R
       MainChannelIO|U        = GR820_U_DOWN --> U_R
       MainChannelIO|Th       = GR820_TH_DOWN --> TH_R
       MainChannelIO|UpU      = GR820_U_UP --> U_UP_R
       MainChannelIO|Cosmic   = GR820_COSMIC --> COSMIC_R
       MainChannelIO|Spectrum = GR820_DOWN --> DOWN_COR

   ### Control Channel I/O settings ###
       ControlChannel|RadarAltimeter     = ALTR_M      [metres]
       ControlChannel|Pressure/Barometer = KPA         [kPa]
       ControlChannel|Temperature        = TEMP_EXT


   ### Input for correction ###
       InputForCorrection    = ROIs


   ### Pre-filtering settings ###
       Filtering|TC      = 0
       Filtering|K       = 0
       Filtering|U       = 0
       Filtering|Th      = 0
       Filtering|UpU     = 0
       Filtering|Cosmic  = 9
       Filtering|RadarAltimeter     = 3
       Filtering|Pressure/Barometer = 3
       Filtering|Temperature        = 3
```

- Appendix G.2 -

```
### Live-time correction settings ###
    LiveTimeChannel             = GR820_LIVE_TIME
    LiveTimeUnits               = milli-seconds
    ApplyLiveTimeCorrToUpU      = Yes

### Cosmic correction settings ###
    CosmicCorrParam|TC      = 0.696350,  42.868000
    CosmicCorrParam|K       = 0.038285,  3.049010
    CosmicCorrParam|U       = 0.032501,  0.251860
    CosmicCorrParam|Th      = 0.039573,  0.133575
    CosmicCorrParam|UpU     = 0.008828,  0.133958
    CosmicCorrParam|SpectrumBackgroundFile    =

### Effective-Height settings ###
    EffectiveHeightOutputChannel = EffectiveHeight
    EffectiveHeightOutputUnits   = metres

### Radon correction settings ###
    RadonCorrMethod                         = UpU
    RadonCorrParam_FilterWidth              = 71
    RadonCorrParam_UseRadonMeanForFewData   = Yes
    RadonOutputChannel                      = Radon
    RadonCorrParam_UgInUpU(A1) = 0.020000
    RadonCorrParam_ThInUpU(A2) = 0.100000
    RadonCorrParam|TC      = 14.000000,  0.000000
    RadonCorrParam|K       = 0.930000,  0.000000
    RadonCorrParam|Th      = 0.070000,  0.000000
    RadonCorrParam|UpU     = 0.280000,  0.000000

### Special Stripping (Compton Stripping) ###
    ComptonCorrParam_Stripping_Alpha     = 0.224000
    ComptonCorrParam_Stripping_Beta      = 0.393000
    ComptonCorrParam_Stripping_Gamma     = 0.717000
    ComptonCorrParam_AlphaPerMetre       = 0.000490
    ComptonCorrParam_BetaPerMetre        = 0.000650
    ComptonCorrParam_GammaPerMetre       = 0.000690
    ComptonCorrParam_GrastyBackscatter_a = 0.051000
    ComptonCorrParam_GrastyBackscatter_b = 0.004000
    ComptonCorrParam_GrastyBackscatter_g = 0.001000

### Height Correction settings ###
    SurveyHeightDatum     = 60.000000
    AttenuationCorrControl = 0
    AttenuationForNegROIs  = Yes
    HeightCorrParam|TC      = -0.007341, 300.000000
    HeightCorrParam|K       = -0.010257, 300.000000
    HeightCorrParam|U       = -0.005414, 300.000000
    HeightCorrParam|Th      = -0.007608, 300.000000

### Concentration settings ###
   ConcentrationParam|K       = Concentration_K,  0.000000
   ConcentrationParam|U       = Concentration_U,  0.000000
   ConcentrationParam|Th      = Concentration_Th,  0.000000
   AirAbsorbedDoseRateParam   = DoseRate,  0.000000
```

```
      NaturalAirAbsorbedDoseRateParam = NaturalDoseRate,  0.000000, 0.000000,
0.000000
```

CONTROL_END

APPENDIX H

GLOSSARY

APPENDIX H

GLOSSARY OF AIRBORNE GEOPHYSICAL TERMS

Note: The definitions given in this glossary refer to the common terminology as used in airborne geophysics.

altitude attenuation: the absorption of gamma rays by the atmosphere between the earth and the detector. The number of gamma rays detected by a system decreases as the altitude increases.

apparent- : the ***physical parameters*** of the earth measured by a geophysical system are normally expressed as apparent, as in "apparent ***resistivity*"**. This means that the measurement is limited by assumptions made about the geology in calculating the response measured by the geophysical system. Apparent resistivity calculated with ***HEM***, for example, generally assumes that the earth is a ***homogeneous half-space*** – not layered.

amplitude: The strength of the total electromagnetic field. In ***frequency domain*** it is most often the sum of the squares of ***in-phase*** and ***quadrature*** components. In multi-component electromagnetic surveys it is generally the sum of the squares of all three directional components.

analytic signal: The total amplitude of all the directions of magnetic ***gradient***. Calculated as the sum of the squares.

anisotropy: Having different ***physical parameters*** in different directions. This can be caused by layering or fabric in the geology. Note that a unit can be anisotropic, but still **homogeneous**.

anomaly: A localized change in the geophysical data characteristic of a discrete source, such as a conductive or magnetic body: something locally different from the **background**.

B-field: In time-domain **electromagnetic** surveys, the magnetic field component of the (electromagnetic) **field**. This can be measured directly, although more commonly it is calculated by integrating the time rate of change of the magnetic field **dB/dt**, as measured with a receiver coil.

background: The "normal" response in the geophysical data – that response observed over most of the survey area. **Anomalies** are usually measured relative to the background. In airborne gamma-ray spectrometric surveys the term defines the **cosmic**, radon, and aircraft responses in the absence of a signal from the ground.

base-level: The measured values in a geophysical system in the absence of any outside signal. All geophysical data are measured relative to the system base level.

base frequency: The frequency of the pulse repetition for a ***time-domain electromagnetic*** system. Measured between subsequent positive pulses.

bird: A common name for the pod towed beneath or behind an aircraft, carrying the geophysical sensor array.

bucking: The process of removing the strong ***signal*** from the ***primary field*** at the ***receiver*** from the data, to measure the ***secondary field***. It can be done electronically or mathematically. This is done in ***frequency-domain EM***, and to measure ***on-time*** in ***time-domain EM***.

calibration coil: A wire coil of known size and dipole moment, which is used to generate a field of known ***amplitude*** and ***phase*** in the receiver, for system calibration. Calibration coils can be external, or internal to the system. Internal coils may be called Q-coils.

coaxial coils: **[CX]** Coaxial coils in an HEM system are in the vertical plane, with their axes horizontal and collinear in the flight direction. These are most sensitive to vertical conductive objects in the ground, such as thin, steeply dipping conductors perpendicular to the flight direction. Coaxial coils generally give the sharpest anomalies over localized conductors. (See also ***coplanar coils***)

coil: A multi-turn wire loop used to transmit or detect electromagnetic fields. Time varying ***electromagnetic*** fields through a coil induce a voltage proportional to the strength of the field and the rate of change over time.

compensation: Correction of airborne geophysical data for the changing effect of the aircraft. This process is generally used to correct data in ***fixed-wing time-domain electromagnetic*** surveys (where the transmitter is on the aircraft and the receiver is moving), and magnetic surveys (where the sensor is on the aircraft, turning in the earth's magnetic field.

component: In ***frequency domain electromagnetic*** surveys this is one of the two **phase** measurements – ***in-phase or quadrature***. In "multi-component" electromagnetic surveys it is also used to define the measurement in one geometric direction (vertical, horizontal in-line and horizontal transverse – the Z, X and Y components).

Compton scattering: gamma ray photons will bounce off electrons as they pass through the earth and atmosphere, reducing their energy and then being detected by ***radiometric*** sensors at lower energy levels. See also ***stripping***.

conductance: See ***conductivity thickness***

conductivity: [s] The facility with which the earth or a geological formation conducts electricity. Conductivity is usually measured in milli-Siemens per metre (mS/m). It is the reciprocal of ***resistivity***.

conductivity-depth imaging: see ***conductivity-depth transform***.

conductivity-depth transform: A process for converting electromagnetic measurements to an approximation of the conductivity distribution vertically in the earth, assuming a ***layered earth***. (Macnae and Lamontagne, 1987; Wolfgram and Karlik, 1995)

conductivity thickness: [s**t**] The product of the ***conductivity***, and thickness of a large, tabular body. (It is also called the "conductivity-thickness product") In electromagnetic geophysics, the response of a thin plate-like conductor is proportional to the conductivity multiplied by thickness. For example a 10 metre thickness of 20 Siemens/m mineralization will be equivalent to 5 metres of 40 S/m; both have 200 S conductivity thickness. Sometimes referred to as conductance.

conductor: Used to describe anything in the ground more conductive than the surrounding geology. Conductors are most often clays or graphite, or hopefully some type of mineralization, but may also be man-made objects, such as fences or pipelines.

coplanar coils: **[CP]** In HEM, the coplanar coils lie in the horizontal plane with their axes vertical, and parallel. These coils are most sensitive to massive conductive bodies, horizontal layers, and the ***halfspace***.

cosmic ray: High energy sub-atomic particles from outer space that collide with the earth's atmosphere to produce a shower of gamma rays (and other particles) at high energies.

counts (per second): The number of ***gamma-rays*** detected by a gamma-ray ***spectrometer*. ** The rate depends on the geology, but also on the size and sensitivity of the detector.

culture: A term commonly used to denote any man-made object that creates a geophysical anomaly. Includes, but not limited to, power lines, pipelines, fences, and buildings.

current channelling: See current gathering.

current gathering: The tendency of electrical currents in the ground to channel into a conductive formation. This is particularly noticeable at higher frequencies or early time channels when the formation is long and parallel to the direction of current flow. This tends to enhance anomalies relative to inductive currents (see also ***induction***). Also known as current channelling.

daughter products: The radioactive natural sources of gamma-rays decay from the original "parent" element (commonly potassium, uranium, and thorium) to one or more lower-energy "daughter" elements. Some of these lower energy elements are also radioactive and decay further. ***Gamma-ray spectrometry*** surveys may measure the gamma rays given off by the original element or by the decay of the daughter products.

dB/dt: As the ***secondary electromagnetic field*** changes with time, the magnetic field [**B**] component induces a voltage in the receiving ***coil***, which is proportional to the rate of change of the magnetic field over time.

decay: In ***time-domain electromagnetic*** theory, the weakening over time of the ***eddy currents*** in the ground, and hence the ***secondary field*** after the ***primary field*** electromagnetic pulse is turned off. In ***gamma-ray spectrometry***, the radioactive breakdown of an element, generally potassium, uranium, thorium, or one of their ***daughter*** products.

decay constant: see time constant.

decay series: In ***gamma-ray spectrometry***, a series of progressively lower energy ***daughter products*** produced by the radioactive breakdown of uranium or thorium.

depth of exploration: The maximum depth at which the geophysical system can detect the target. The depth of exploration depends very strongly on the type and size of the target, the contrast of the target with the surrounding geology, the homogeneity of the surrounding geology, and the type of geophysical system. One measure of the maximum depth of exploration for an electromagnetic system is the depth at which it can detect the strongest conductive target – generally a highly conductive horizontal layer.

differential resistivity: A process of transforming ***apparent resistivity*** to an approximation of layer resistivity at each depth. The method uses multi-frequency HEM data and approximates the effect of shallow layer ***conductance*** determined from higher frequencies to estimate the deeper conductivities (Huang and Fraser, 1996)

dipole moment: [NIA] For a transmitter, the product of the area of a ***coil***, the number of turns of wire, and the current flowing in the coil. At a distance significantly larger than the size of the coil, the magnetic field from a coil will be the same if the dipole moment product is the same. For a receiver coil, this is the product of the area and the number of turns. The sensitivity to a magnetic field (assuming the source is far away) will be the same if the dipole moment is the same.

diurnal: The daily variation in a natural field, normally used to describe the natural fluctuations (over hours and days) of the earth's magnetic field.

dielectric permittivity: **[**e**]** The capacity of a material to store electrical charge, this is most often measured as the relative permittivity [ε_r], or ratio of the material dielectric to that of free space. The effect of high permittivity may be seen in HEM data at high frequencies over highly resistive geology as a reduced or negative ***in-phase***, and higher ***quadrature*** data.

drape: To fly a survey following the terrain contours, maintaining a constant altitude above the local ground surface. Also applied to re-processing data collected at varying altitudes above ground to simulate a survey flown at constant altitude.

drift: Long-time variations in the base-level or calibration of an instrument.

eddy currents: The electrical currents induced in the ground, or other conductors, by a time-varying ***electromagnetic field*** (usually the ***primary field***). Eddy currents are also induced in the aircraft's metal frame and skin; a source of ***noise*** in EM surveys.

electromagnetic: **[EM]** Comprised of a time-varying electrical and magnetic field. Radio waves are common electromagnetic fields. In geophysics, an electromagnetic system is one which transmits a time-varying ***primary field*** to induce ***eddy currents*** in the ground, and then measures the ***secondary field*** emitted by those eddy currents.

energy window: A broad spectrum of ***gamma-ray*** energies measured by a spectrometric survey. The energy of each gamma-ray is measured and divided up into numerous discrete energy levels, called windows.

equivalent (thorium or uranium): The amount of radioelement calculated to be present, based on the gamma-rays measured from a **daughter** element. This assumes that the ***decay series*** is in equilibrium – progressing normally.

exposure rate: in radiometric surveys, a calculation of the total exposure rate due to gamma rays at the ground surface. It is used as a measurement of the concentration of all the **radioelements** at the surface. See also: **natural exposure rate**.

fiducial, or fid: Timing mark on a survey record. Originally these were timing marks on a profile or film; now the term is generally used to describe 1-second interval timing records in digital data, and on maps or profiles.

Figure of Merit: **(FOM)** A sum of the 12 distinct magnetic noise variations measured by each of four flight directions, and executing three aircraft attitude variations (yaw, pitch, and roll) for each direction. The flight directions are generally parallel and perpendicular to planned survey flight directions. The FOM is used as a measure of the **manoeuvre noise** before and after **compensation.**

fixed-wing: Aircraft with wings, as opposed to "rotary wing" helicopters.

footprint: This is a measure of the area of sensitivity under the aircraft of an airborne geophysical system. The footprint of an ***electromagnetic*** system is dependent on the altitude of the system, the orientation of the transmitter and receiver and the separation between the receiver and transmitter, and the conductivity of the ground. The footprint of a ***gamma-ray spectrometer*** depends mostly on the altitude. For all geophysical systems, the footprint also depends on the strength of the contrasting ***anomaly***.

frequency domain: An ***electromagnetic*** system which transmits a ***primary field*** that oscillates smoothly over time (sinusoidal), inducing a similarly varying electrical current in the ground. These systems generally measure the changes in the ***amplitude*** and ***phase*** of the ***secondary field*** from the ground at different frequencies by measuring the **in-phase** and **quadrature** phase components. See also ***time-domain***.

full-stream data: Data collected and recorded continuously at the highest possible sampling rate. Normal data are stacked (see ***stacking***) over some time interval before recording.

gamma-ray: A very high-energy photon, emitted from the nucleus of an atom as it undergoes a change in energy levels.

gamma-ray spectrometry: Measurement of the number and energy of natural (and sometimes man-made) gamma-rays across a range of photon energies.

gradient: In magnetic surveys, the gradient is the change of the magnetic field over a distance, either vertically or horizontally in either of two directions. Gradient data is often measured, or calculated from the total magnetic field data because it changes more quickly over distance than the ***total magnetic field***, and so may provide a more precise measure of the location of a source. See also ***analytic signal***.

ground effect: The response from the earth. A common calibration procedure in many geophysical surveys is to fly to altitude high enough to be beyond any measurable response from the ground, and there establish ***base levels*** or ***backgrounds***.

half-space: A mathematical model used to describe the earth – as infinite in width, length, and depth below the surface. The most common halfspace models are ***homogeneous*** and ***layered earth***.

heading error: A slight change in the magnetic field measured when flying in opposite directions.

HEM: Helicopter ElectroMagnetic, This designation is most commonly used for helicopter-borne, ***frequency-domain*** electromagnetic systems. At present, the transmitter and receivers are normally mounted in a ***bird*** carried on a sling line beneath the helicopter.

herringbone pattern: A pattern created in geophysical data by an asymmetric system, where the **anomaly** may be extended to either side of the source, in the direction of flight. Appears like fish bones, or like the teeth of a comb, extending either side of centre, each tooth an alternate flight line.

homogeneous: This is a geological unit that has the same ***physical parameters*** throughout its volume. This unit will create the same response to an HEM system anywhere, and the HEM system will measure the same apparent ***resistivity*** anywhere. The response may change with system direction (see ***anisotropy***).

HTEM: Helicopter Time-domain ElectroMagnetic, This designation is used for the new generation of helicopter-borne, ***time-domain*** electromagnetic systems.

in-phase: the component of the measured ***secondary field*** that has the same phase as the transmitter and the ***primary field***. The in-phase component is stronger than the ***quadrature*** phase over relatively higher ***conductivity***.

induction: Any time-varying electromagnetic field will induce (cause) electrical currents to flow in any object with non-zero ***conductivity***. (see ***eddy currents***)

induction number: also called the “response parameter”, this number combines many of the most significant parameters affecting the ***EM*** response into one parameter against which to compare responses. For a ***layered earth*** the response parameter is mws**h**^{2} and for a large, flat, ***conductor*** it is mws**th**, where m is the ***magnetic permeability***, w is the angular ***frequency***, s is the **conductivity**, t is the thickness (for the flat conductor) and h is the height of the system above the conductor.

inductive limit: When the frequency of an EM system is very high, or the **conductivity** of the target is very high, the response measured will be entirely **in-phase** with no **quadrature** (**phase** angle =0). The in-phase response will remain constant with further increase in conductivity or frequency. The system can no longer detect changes in conductivity of the target.

infinite: In geophysical terms, an “infinite’ dimension is one much greater than the ***footprint*** of the system, so that the system does not detect changes at the edges of the object.

International Geomagnetic Reference Field: **[IGRF]** An approximation of the smooth magnetic field of the earth, in the absence of variations due to local geology. Once the IGRF is subtracted from the measured magnetic total field data, any remaining variations are assumed to be due to local geology. The IGRF also predicts the slow changes of the field up to five years in the future.

inversion, or **inverse modeling**: A process of converting geophysical data to an earth model, which compares theoretical models of the response of the earth to the data measured, and refines the model until the response closely fits the measured data (Huang and Palacky, 1991)

layered earth: A common geophysical model which assumes that the earth is horizontally layered – the ***physical parameters*** are constant to ***infinite*** distance horizontally, but change vertically.
magnetic permeability: **[m]** This is defined as the ratio of magnetic induction to the inducing magnetic field. The relative magnetic permeability [μ_r] is often quoted, which is the ratio of the rock permeability to the permeability of free space. In geology and geophysics, the ***magnetic susceptibility*** is more commonly used to describe rocks.

magnetic susceptibility: **[k]** A measure of the degree to which a body is magnetized. In SI units this is related to relative ***magnetic permeability*** by $k=\mu_r-1$, and is a dimensionless unit. For most geological material, susceptibility is influenced primarily by the percentage of magnetite. It is most often quoted in units of 10^{-6}. In HEM data this is most often apparent as a negative ***in-phase*** component over high susceptibility, high ***resistivity*** geology such as diabase dikes.

manoeuvre noise: variations in the magnetic field measured caused by changes in the relative positions of the magnetic sensor and magnetic objects or electrical currents in the aircraft. This type of noise is generally corrected by magnetic **compensation**.

model: Geophysical theory and applications generally have to assume that the geology of the earth has a form that can be easily defined mathematically, called the model. For example steeply dipping **conductor**s are generally modeled as being **infinite** in horizontal and depth extent, and very thin. The earth is generally modeled as horizontally layered, each layer infinite in extent and uniform in characteristic. These models make the mathematics to describe the response of the (normally very complex) earth practical. As theory advances, and computers become more powerful, the useful models can become more complex.

natural exposure rate: in radiometric surveys, a calculation of the total exposure rate due to natural-source gamma rays at the ground surface. It is used as a measurement of the concentration of all the natural **radioelements** at the surface. See also: **exposure rate**.

noise: That part of a geophysical measurement that the user does not want. Typically this includes electronic interference from the system, the atmosphere (***sferics***), and man-made sources. This can be a subjective judgment, as it may include the response from geology other than the target of interest. Commonly the term is used to refer to high frequency (short period) interference. See also ***drift***.

Occam's inversion: an ***inversion*** process that matches the measured ***electromagnetic*** data to a theoretical model of many, thin layers with constant thickness and varying resistivity (Constable et al, 1987).

off-time: In a ***time-domain electromagnetic*** survey, the time after the end of the ***primary field pulse***, and before the start of the next pulse.

on-time: In a ***time-domain electromagnetic*** survey, the time during the ***primary field pulse***.

overburden: In engineering and mineral exploration terms, this most often means the soil on top of the unweathered bedrock. It may be sand, glacial till, or weathered rock.

Phase, phase angle: The angular difference in time between a measured sinusoidal electromagnetic field and a reference – normally the primary field. The phase is calculated from $\tan^{-1}$(***in-phase / quadrature***).

physical parameters: These are the characteristics of a geological unit. For electromagnetic surveys, the important parameters are ***conductivity, magnetic permeability*** (or ***susceptibility***) and ***dielectric permittivity***; for magnetic surveys the parameter is magnetic susceptibility, and for gamma ray spectrometric surveys it is the concentration of the major radioactive elements: potassium, uranium, and thorium.

permittivity: see ***dielectric permittivity***.

permeability: see ***magnetic permeability***.

primary field: the EM field emitted by a transmitter. This field induces ***eddy currents*** in (energizes) the conductors in the ground, which then create their own ***secondary* fields**.

pulse: In time-domain EM surveys, the short period of intense ***primary*** field transmission. Most measurements (the ***off-time***) are measured after the pulse. **On-time** measurements may be made during the pulse.

quadrature: that component of the measured ***secondary field*** that is phase-shifted 90° from the ***primary field***. The quadrature component tends to be stronger than the ***in-phase*** over relatively weaker ***conductivity***.

Q-coils: see ***calibration coil***.

radioelements: This normally refers to the common, naturally-occurring radioactive elements: potassium (K), uranium (U), and thorium (Th). It can also refer to man-made radioelements, most often cobalt (Co) and cesium (Cs)

radiometric: Commonly used to refer to ***gamma ray*** spectrometry.

radon: A radioactive daughter product of uranium and thorium, radon is a gas which can leak into the atmosphere, adding to the non-geological background of a gamma-ray spectrometric survey.

receiver: the ***signal*** detector of a geophysical system. This term is most often used in active geophysical systems – systems that transmit some kind of signal. In airborne ***electromagnetic*** surveys it is most often a ***coil***. (see also, ***transmitter***)

resistivity: **[**ρ**]** The strength with which the earth or a geological formation resists the flow of electricity, typically the flow induced by the ***primary field*** of the electromagnetic transmitter. Normally expressed in ohm-metres, it is the reciprocal of ***conductivity***.

resistivity-depth transforms: similar to ***conductivity depth transforms***, but the calculated ***conductivity*** has been converted to ***resistivity***.

resistivity section: an approximate vertical section of the resistivity of the layers in the earth. The resistivities can be derived from the ***apparent resistivity***, the ***differential resistivities***, ***resistivity-depth transforms***, or ***inversions***.

Response parameter: another name for the **induction number**.

secondary field: The field created by conductors in the ground, as a result of electrical currents induced by the ***primary field*** from the ***electromagnetic*** transmitter. Airborne ***electromagnetic*** systems are designed to create and measure a secondary field.

Sengpiel section: a ***resistivity section*** derived using the ***apparent resistivity*** and an approximation of the depth of maximum sensitivity for each frequency.

sferic: Lightning, or the ***electromagnetic*** signal from lightning, it is an abbreviation of "atmospheric discharge". These appear to magnetic and electromagnetic sensors as sharp "spikes" in the data. Under some conditions lightning storms can be detected from hundreds of kilometres away. (see ***noise***)

signal: That component of a measurement that the user wants to see – the response from the targets, from the earth, etc. (See also ***noise***)

skin depth: A measure of the depth of penetration of an electromagnetic field into a material. It is defined as the depth at which the primary field decreases to 1/e of the field at the surface. It is calculated by approximately 503 x √(resistivity/frequency). Note that depth of penetration is greater at higher ***resistivity*** and/or lower ***frequency***.

spectrometry: Measurement across a range of energies, where ***amplitude*** and energy are defined for each measurement. In gamma-ray spectrometry, the number of gamma rays are measured for each energy ***window***, to define the ***spectrum***.

spectrum: In ***gamma ray spectrometry***, the continuous range of energy over which gamma rays are measured. In ***time-domain electromagnetic*** surveys, the spectrum is the energy of the **pulse** distributed across an equivalent, continuous range of frequencies.

spheric: see ***sferic***.

stacking: Summing repeat measurements over time to enhance the repeating ***signal***, and minimize the random ***noise***.

stripping: Estimation and correction for the gamma ray photons of higher and lower energy that are observed in a particular ***energy window***. See also ***Compton scattering***.

susceptibility: See ***magnetic susceptibility***.

tau: [t] Often used as a name for the ***time constant***.

TDEM: ***time domain electromagnetic***.

thin sheet: A standard model for electromagnetic geophysical theory. It is usually defined as a thin, flat-lying conductive sheet, ***infinite*** in both horizontal directions. (see also ***vertical plate***)

tie-line: A survey line flown across most of the ***traverse lines***, generally perpendicular to them, to assist in measuring ***drift*** and ***diurnal*** variation. In the short time required to fly a tie-line it is assumed that the drift and/or diurnal will be minimal, or at least changing at a constant rate.

time constant: The time required for an ***electromagnetic*** field to decay to a value of 1/e of the original value. In ***time-domain*** electromagnetic data, the time constant is proportional to the size and ***conductance*** of a tabular conductive body. Also called the decay constant.

Time channel: In ***time-domain electromagnetic*** surveys the decaying ***secondary field*** is measured over a period of time, and the divided up into a series of consecutive discrete measurements over that time.

time-domain: ***Electromagnetic*** system which transmits a pulsed, or stepped ***electromagnetic*** field. These systems induce an electrical current (***eddy current***) in the ground that persists after the ***primary field*** is turned off, and measure the change over time of the ***secondary field*** created as the currents ***decay***. See also ***frequency-domain***.

total energy envelope: The sum of the squares of the three ***components*** of the ***time-domain electromagnetic secondary field***. Equivalent to the ***amplitude*** of the secondary field.

transient: Time-varying. Usually used to describe a very short period pulse of ***electromagnetic*** field.

transmitter: The source of the ***signa***l to be measured in a geophysical survey. In airborne ***EM*** it is most often a **coil** carrying a time-varying electrical current, transmitting the ***primary field***. (see also ***receiver***)

traverse line: A normal geophysical survey line. Normally parallel traverse lines are flown across the property in spacing of 50 m to 500 m, and generally perpendicular to the target geology.

vertical plate: A standard model for electromagnetic geophysical theory. It is usually defined as thin conductive sheet, ***infinite*** in horizontal dimension and depth extent. (see also ***thin shee***t)

waveform: The shape of the ***electromagnetic pulse*** from a ***time-domain*** electromagnetic transmitter.

window: A discrete portion of a ***gamma-ray spectrum*** or ***time-domain electromagnetic decay***. The continuous energy spectrum or ***full-stream*** data are grouped into windows to reduce the number of samples, and reduce ***noise***.

Version 1.5, November 29, 2005
Greg Hodges,
Chief Geophysicist
Fugro Airborne Surveys, Toronto

Common Symbols and Acronyms

k Magnetic susceptibility
e Dielectric permittivity
m, m_r Magnetic permeability, relative permeability
r, r_a Resistivity, apparent resistivity
s, s_a Conductivity, apparent conductivity
s**t** Conductivity thickness
t Tau, or time constant
W**m** ohm-metres, units of resistivity
AGS Airborne gamma ray spectrometry.
CDT Conductivity-depth transform, conductivity-depth imaging (Macnae and Lamontagne, 1987; Wolfgram and Karlik, 1995)
CPI, CPQ Coplanar in-phase, quadrature
CPS Counts per second
CTP Conductivity thickness product
CXI, CXQ Coaxial, in-phase, quadrature
FOM Figure of Merit
fT femtoteslas, normal unit for measurement of B-Field
EM Electromagnetic
keV kilo electron volts – a measure of gamma-ray energy
MeV mega electron volts – a measure of gamma-ray energy 1MeV = 1000keV
NIA dipole moment: turns x current x Area
nT nanotesla, a measure of the strength of a magnetic field
nG/h nanoGreys/hour – gamma ray dose rate at ground level
ppm parts per million – a measure of secondary field or noise relative to the primary or radioelement concentration.
pT/s picoteslas per second: Units of decay of secondary field, dB/dt
S siemens – a unit of conductance
x: the horizontal component of an EM field parallel to the direction of flight.
y: the horizontal component of an EM field perpendicular to the direction of flight.
z: the vertical component of an EM field.

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APPENDIX IV

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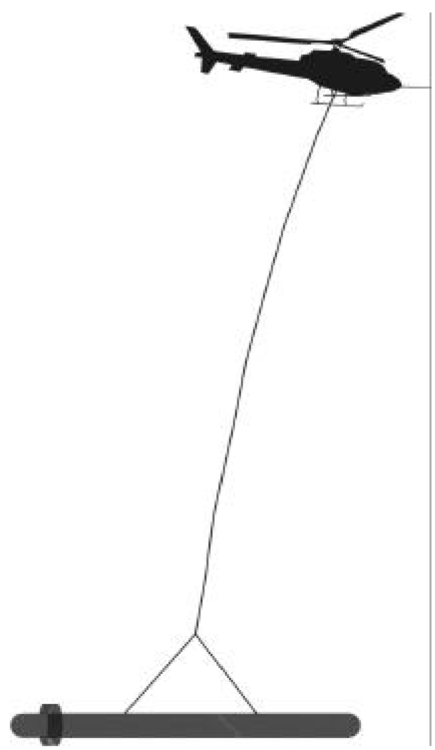
Report # 06041-4,5,6

DIGHEM SURVEY
FOR
HATHOR EXPLORATION LIMITED
ESKAY AREA BLOCKS 4, 5, 6 (2006-2007)
NORTHWESTERN BRITISH COLUMBIA

NTS: 104B/ 7,8,10,11,14, 15



Fugro Airborne Surveys Corp.
Mississauga, Ontario

February 19, 2008

SUMMARY

This report describes the logistics, data acquisition, processing and presentation of results of a DIGHEM airborne geophysical survey carried out for Hathor Exploration Limited, over a property located near Eskay Creek, British Columbia during the summer of 2006 and 2007. Only partial coverage was obtained in 2006 before the survey was disrupted by inclement weather.

The 2006 coverage for portions of Blocks 4, 5, and 6 amounted to 4196 km, or 71% of the 5916 km originally proposed for these areas. The first phase of the survey was flown from July 5th to October 12th, 2006. The balance of the flying was resumed in July, 2007. The second phase of the survey, from July 19th to September 5th, 2007, acquired 1515 km of data over the remaining portions of Blocks 4,5, and 6. . The total coverage for both phases amounted to 5611 km, which excludes the areas of overlapping coverage and repeat tie lines.

The purpose of the survey was to locate areas of potassic alteration, to detect skarn deposits and zones of conductive mineralization, and to provide information that could be used to map the geology and structure of the survey areas. This was accomplished by using a DIGHEM multi-coil, multi-frequency electromagnetic system, supplemented by a high sensitivity cesium magnetometer, and a 256-channel spectrometer. The information from these sensors was processed to produce maps that display the magnetic, radiometric, and conductive properties of the survey areas. A GPS electronic navigation

system ensured accurate positioning of the geophysical data with respect to the base maps.

The survey data were processed and compiled in the Fugro Airborne Surveys Toronto office. Map products and digital data were provided in accordance with the scales and formats specified in the Survey Agreement.

The survey properties contain several anomalous features, many of which are considered to be of moderate to high priority as exploration targets. Most of the inferred bedrock conductors and other anomalous zones appear to warrant further investigation using appropriate surface exploration techniques. Areas of interest may be assigned priorities on the basis of supporting geophysical, geochemical and/or geological information. After initial investigations have been carried out, it may be necessary to re-evaluate the remaining anomalies based on information acquired from the follow-up program.

CONTENTS

APPENDICES

1. INTRODUCTION

A DIGHEM electromagnetic/resistivity/magnetic/radiometric survey was flown for Hathor Exploration Limited during two phases. The first phase of survey was flown from July 5th to October 12th, 2006 and the second phase was flown from July 19th to September 5th, 2007. The survey blocks were located near Eskay Creek, northwestern British Columbia. The survey areas can be located on NTS map sheets 104 B/7,8,10,11,14,15 (Figure 2).

Total survey coverage consisted of approximately 5611 line-km, including 541 km of tie lines. Flight lines were flown in an azimuthal direction of 90°/270°, with a line separation of 150 metres. Tie lines were flown orthogonal to the traverse lines with a line separation of 1500 meters.

Traverse Lines Flown in 2006

North Block	Lines 40010-51200
Central Block	Lines 51650-52030
South Block	Lines 52040-53340
Southeast Block	Lines 63100-63170

Traverse Lines Flown in 2007

Central Block	233.7 km: Lines 51320-51640
South Block	56.5 km: Lines 52050-52210 19.2 km: Lines 52760-52790 28.0 km: Lines 52940-53000 30.3 km: Lines 49090-49140
Southeast Block	1146.8 km: Lines 62860-64040

The survey employed the DIGHEM electromagnetic system. Ancillary equipment consisted of a magnetometer, radar and barometric altimeters, a video camera, a digital recorder, a 256-channel spectrometer and an electronic navigation system. The instrumentation was installed in AS350B3 turbine helicopters (Registration C-FYZF for the 2006 phase, Registration C-FQDA for the 2007 phase) that were provided by Great Slave Helicopters Ltd. The helicopters flew at an average airspeed of 90 km/h with an EM sensor height of approximately 30 metres. The spectrometer crystal package was housed within the helicopter, with a nominal terrain clearance of 58 metres.

In some portions of the survey areas, the steep topography forced the pilot to exceed normal terrain clearance for safety reasons. It is possible that some weak conductors may have escaped detection in areas where the bird height exceeded 120 m. In difficult areas where near-vertical climbs were necessary, the forward speed of the helicopter was reduced to a level that permitted excessive bird swinging. This problem, combined with the severe stresses to which the bird was subjected, gave rise to aerodynamic noise levels that are slightly higher than normal on some lines. Where warranted, reflights were carried out to minimize these adverse effects.

Figure 1: Fugro Airborne Surveys DIGHEM V EM bird with AS350-B3

2. SURVEY OPERATIONS

The base of operations for the survey was established at Bell II Lodge, British Columbia.

Table 2-1 lists the corner coordinates of the portions of Blocks 4, 5 and 6 that were flown in 2006. The coordinates are in NAD83, UTM Zone 9 North, central meridian 129° West.

Table 2-1

Nad83 Utm Zone 9

Block	Corners	X-UTM (E)	Y-UTM (N)
06041-5	1	375251	6293886
North 1	2	380099	6293755
	3	380170	6296354
	4	384268	6296243
	5	384178	6292901
	6	378569	6293053
	7	378410	6287185
	8	375072	6287276
	9	375102	6288388
	10	376113	6288361
	11	376159	6290610
	12	375163	6290637
North 2	1	375072	6287276
	2	378410	6287185
	3	382024	6287088
	4	382182	6292955
	5	384178	6292901
	6	384156	6292094
	7	386105	6292042
	8	386035	6289443
	9	394832	6289204
	10	394768	6286855

	11	397567	6286780
	12	397512	6284730
	13	401310	6284628
	14	401165	6279267
	15	397903	6279356
	16	397862	6277868
	17	392661	6278009
	18	392666	6278208
	19	384559	6278411
	20	384611	6280309
	21	379488	6280416
	22	379597	6284415
	23	374998	6284539
Centre	1	386061	6271585
	2	399689	6271216
	3	399624	6268795
	4	395695	6268902
	5	395674	6268174
	6	394860	6268196
	7	394787	6265497
	8	392255	6265566
	9	392257	6265639
	10	387823	6265759
	11	387842	6266435
	12	385923	6266487
South1	1	390129	6256093
	2	395120	6255958
	3	395157	6257332
	4	395934	6257311
	5	395997	6259642
	6	393297	6259715
	7	393363	6262164
	8	392846	6262178
	9	392865	6262878
	10	398186	6262734
	11	398259	6265452
	12	403775	6265303

	13	403682	6261834
	14	406170	6261766
	15	406041	6257017
	16	412029	6256855
	17	412019	6256477
	18	411050	6256504
	19	411010	6255004
	20	411978	6254978
	21	411958	6254228
	22	407141	6254359
	23	407125	6253759
	24	411942	6253628
	25	411909	6252429
	26	404776	6252622
	27	404782	6252871
	28	402004	6252946
	29	401807	6245689
	30	394847	6245877
	31	394944	6249460
	32	392222	6249534
	33	392242	6250260
	34	390902	6250297
	35	390907	6250597
	36	393954	6250514
	37	393995	6252013
	38	390021	6252121
	39	390054	6253321
	40	392704	6253249
	41	392713	6253549
	42	390062	6253620
South2	1	404686	6249323
	2	413080	6249096
	3	413052	6248062
	4	418401	6247918
	5	418396	6247752
	6	404654	6248124

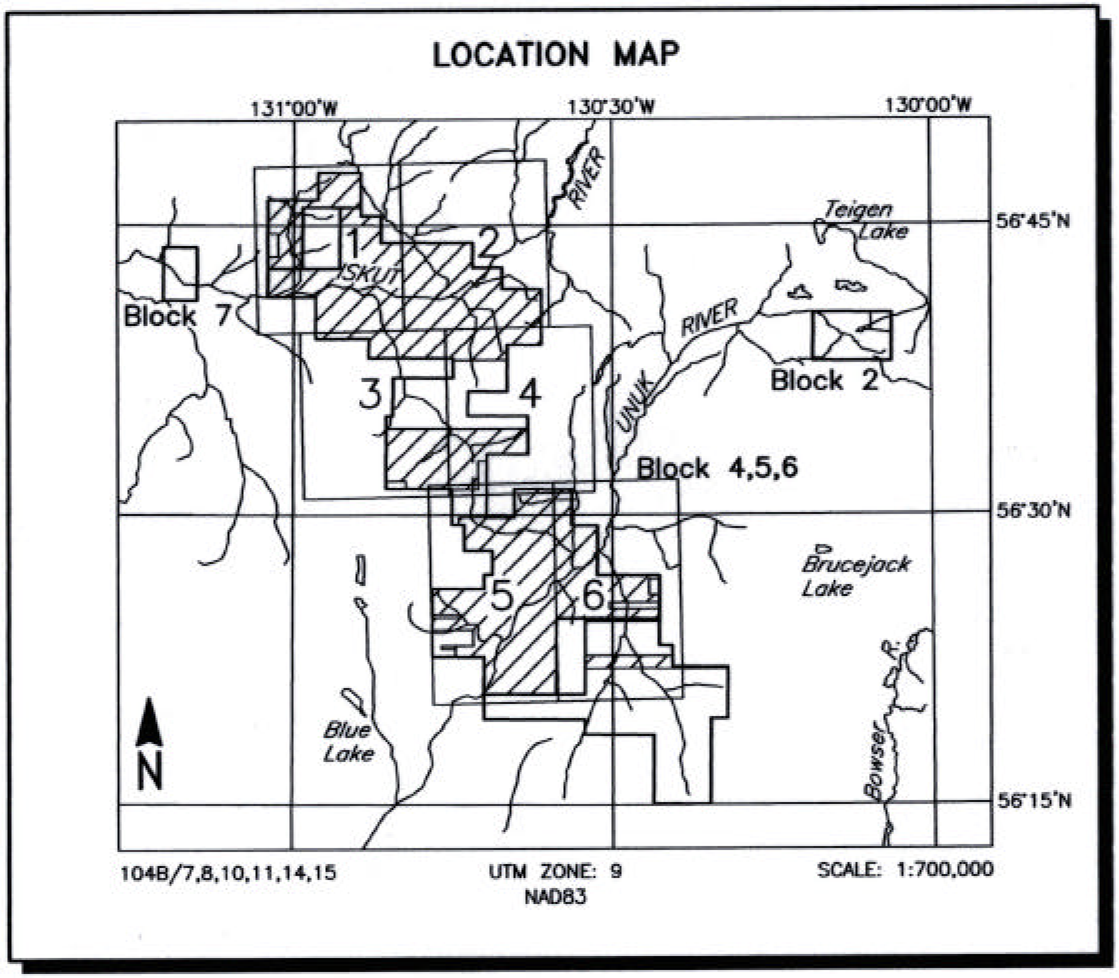


Figure 2a
Location Map and Sheet Layout
Eskay Claims Survey Area
2006 Coverage
Blocks 4,5 and 6
Job # 06041-4,5,6.

Table 2-2 lists the corner coordinates of the portions of Blocks 4, 5 and 6 that were flown in 2007. The coordinates are in NAD83, UTM Zone 9 North, central meridian 129° West.

Table 2-2

06041-5	1	375072	6287276
Blocks	2	382024	6287088
4,5,6 Centre	3	382182	6292955
	4	384178	6292901
	5	384156	6292094
	6	386105	6292042
	7	386035	6289443
	8	394832	6289204
	9	394768	6286855
	10	397567	6286780
	11	397512	6284730
	12	401310	6284628
	13	401165	6279267
	14	397903	6279356
	15	397781	6274861
	16	394012	6274963
	17	393948	6272624
	18	399723	6272467
	19	399624	6268795
	20	395695	6268902
	21	395518	6262806
	22	398186	6262734
	23	398259	6265452
	24	403775	6265303
	25	403682	6261834
	26	406170	6261766
	27	406041	6257017
	28	412029	6256855
	29	411916	6252678
	30	402004	6252946
	31	401807	6245689
	32	394847	6245877
	33	394944	6249460

	34	389953	6249595
	35	390129	6256093
	36	395120	6255958
	37	395157	6257332
	38	395934	6257311
	39	395997	6259642
	40	393297	6259715
	41	393363	6262164
	42	392164	6262197
	43	392257	6265639
	44	385905	6265811
	45	386094	6272812
	46	386749	6272794
	47	386848	6276452
	48	392614	6276296
	49	392666	6278208
	50	384559	6278411
	51	384611	6280309
	52	379488	6280416
	53	379597	6284415
	54	374998	6284539
06041-6	1	394847	6245877
Blocks	2	404586	6245614
4,5,6 South	3	404782	6252871
	4	411916	6252678
	5	411847	6250118
	6	413107	6250084
	7	413052	6248062
	8	418401	6247918
	9	418267	6242978
	10	416660	6243021
	11	416438	6234804
	12	410929	6234953
	13	411107	6241549
	14	404449	6241729
	15	404489	6243206
	16	394782	6243468

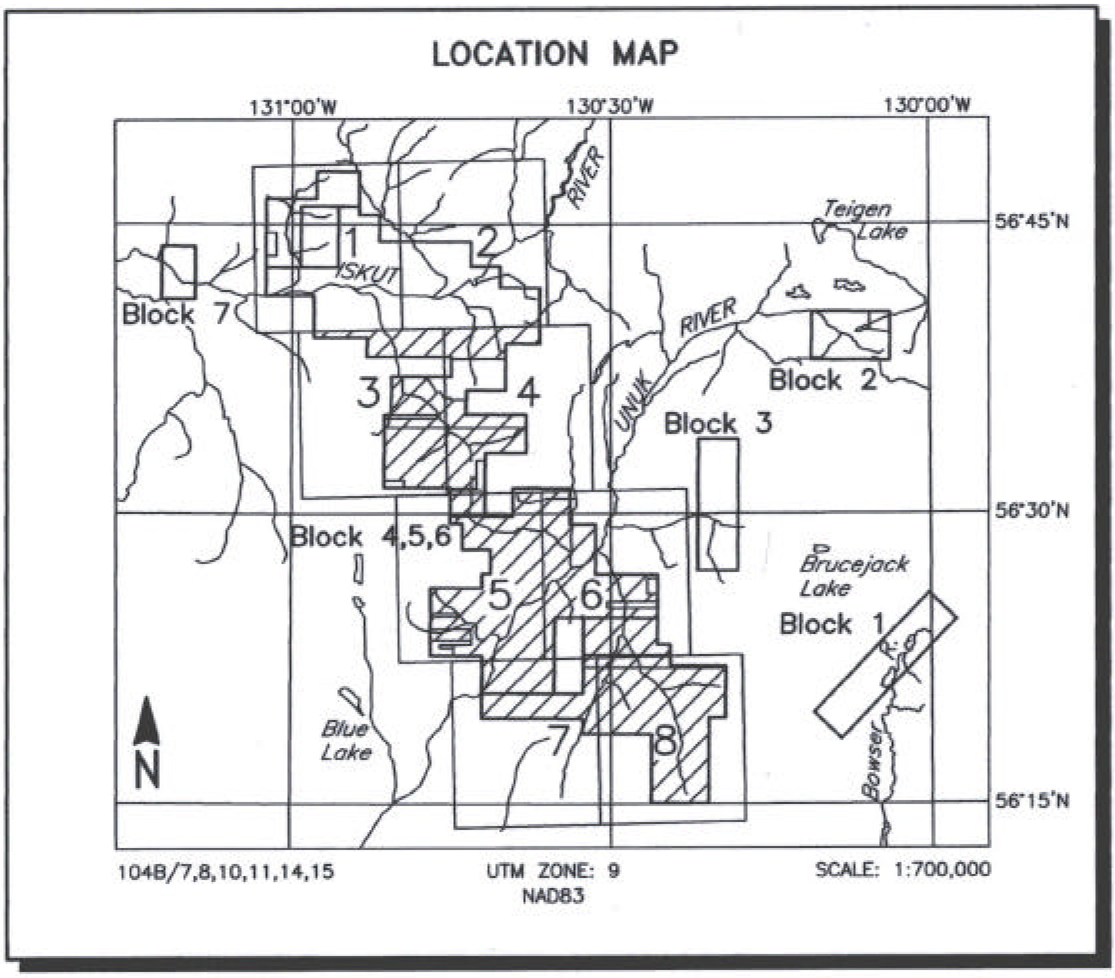


Figure 2b
Location Map and Sheet Layout
Eskay Claims Survey Area
2007 Coverage
Blocks 4,5 and 6
Job # 06041-4,5,6.

The survey specifications were as follows:

Parameter	Specifications
Traverse line direction	90°/270°,
Traverse line spacing	150 m
Tie line direction	0°/180°
Tie line spacing	1500 m
Sample interval	10 Hz, 3.3 m @ 120 km/h
Aircraft mean terrain clearance	58 m
Spectrometer Crystal Package	58 m
EM sensor mean terrain clearance	30 m
Mag sensor mean terrain clearance	30 m
Average speed	90 km/h
Navigation (guidance)	±5 m, Real-time GPS
Post-survey flight path	±2 m, Differential GPS

3. SURVEY EQUIPMENT

This section provides a brief description of the geophysical instruments used to acquire the survey data and the calibration procedures employed. The geophysical equipment was installed in an AS350B3 helicopter. This aircraft provides a safe and efficient platform for surveys of this type.

Electromagnetic System

2006 Phase

Model: DIGHEM V BKS52

Type: Towed bird, symmetric dipole configuration operated at a nominal survey altitude of 30 metres. Coil separation is 8 metres for 900 Hz, 1000 Hz, 5500 Hz and 7200 Hz, and 6.3 metres for the 56,000 Hz coil-pair.

Coil orientations, frequencies and dipole moments

Atm^2	orientation	nominal	actual
211	coaxial /	1000 Hz	1116 Hz
211	coplanar /	900 Hz	872 Hz
67	coaxial /	5500 Hz	5666 Hz
56	coplanar /	7200 Hz	7233 Hz
15	coplanar /	56,000 Hz	55,460 Hz

Channels recorded:
5 in-phase channels
5 quadrature channels
2 monitor channels

Sensitivity:
0.06 ppm at 1000 Hz Cx
0.12 ppm at 900 Hz Cp
0.12 ppm at 5,500 Hz Cx
0.24 ppm at 7,200 Hz Cp
0.60 ppm at 56,000 Hz Cp

Sample rate: 10 per second, equivalent to 1 sample every 3.3 m, at a survey speed of 120 km/h.

2007 Phase

Model: DIGHEM V BKS54

Type: Towed bird, symmetric dipole configuration operated at a nominal survey altitude of 30 metres. Coil separation is 8 metres for 900 Hz, 1000 Hz, 5500 Hz and 7200 Hz, and 6.3 metres for the 56,000 Hz coil-pair.

Coil orientations, frequencies and dipole moments

Atm^2	orientation		nominal	actual
211	coaxial	/	1000 Hz	1125 Hz
211	coplanar	/	900 Hz	875 Hz
67	coaxial	/	5500 Hz	5462 Hz
56	coplanar	/	7200 Hz	7233 Hz
15	coplanar	/	56,000 Hz	56,400 Hz

Channels recorded: 5 in-phase channels
5 quadrature channels
2 monitor channels

Sensitivity:
0.06 ppm at 1000 Hz Cx
0.12 ppm at 900 Hz Cp
0.12 ppm at 5,500 Hz Cx
0.24 ppm at 7,200 Hz Cp
0.60 ppm at 56,000 Hz Cp

Sample rate: 10 per second, equivalent to 1 sample every 3.3 m, at a survey speed of 120 km/h.

The electromagnetic system utilizes a multi-coil coaxial/coplanar technique to energize conductors in different directions. The coaxial coils are vertical with their axes in the flight direction. The coplanar coils are horizontal. The secondary fields are sensed simultaneously by means of receiver coils that are maximum coupled to their respective transmitter coils. The system yields an in-phase and a quadrature channel from each transmitter-receiver coil-pair.

In-Flight EM System Calibration

Calibration of the system during the survey uses the Fugro AutoCal automatic, internal calibration process. At the beginning and end of each flight, and at intervals during the flight, the system is flown up to high altitude to remove it from any "ground effect" (response from the earth). Any remaining signal from the receiver coils (base level) is measured as the zero level, and is removed from the data collected until the time of the next calibration. Following the zero level setting, internal calibration coils, for which the response phase and amplitude have been determined at the factory, are automatically triggered – one for each frequency. The on-time of the coils is sufficient to determine an accurate response through any ambient noise. The receiver response to each calibration coil "event" is compared to the expected response (from the factory calibration) for both phase angle and amplitude, and any phase and gain corrections are automatically applied to bring the data to the correct value.

In addition, the outputs of the transmitter coils are continuously monitored during the survey, and the gains are adjusted to correct for any change in transmitter output.

Because the internal calibration coils are calibrated at the factory (on a resistive halfspace) ground calibrations using external calibration coils on-site are not necessary for system calibration. A check calibration may be carried out on-site to ensure all systems are working correctly. All system calibrations will be carried out in the air, at sufficient altitude that there will be no measurable response from the ground.

The internal calibration coils are rigidly positioned and mounted in the system relative to the transmitter and receiver coils. In addition, when the internal calibration coils are calibrated at the factory, a rigid jig is employed to ensure accurate response from the external coils.

Using real time Fast Fourier Transforms and the calibration procedures outlined above, the data are processed in real time, from measured total field at a high sampling rate, to in-phase and quadrature values at 10 samples per second.

Airborne Magnetometer

2006 and 2007

Model:	Fugro D1344 processor with Scintrex CS2 sensor
Type:	Optically pumped cesium vapour
Sensitivity:	0.01 nT
Sample rate:	10 per second

The magnetometer sensor was mounted on the tail of the EM bird, 28 m below the helicopter.

Magnetic Base Station

Primary

Model: Fugro CF1 base station with timing provided by integrated GPS

Sensor type (2006): Geometrics G822A
Sensor type (2007): Scintrex CS3

Counter specifications:
- Accuracy: ±0.1 nT
- Resolution: 0.01 nT
- Sample rate 1 Hz

GPS specifications:
- Model: Marconi Allstar
- Type: Code and carrier tracking of L1 band, 12-channel, C/A code at 1575.42 MHz
- Sensitivity: -90 dBm, 1.0 second update
- Accuracy: Manufacturer's stated accuracy for differential corrected GPS is 2 metres

Environmental Monitor specifications:

Temperature:
- Accuracy: ±1.5ºC max
- Resolution: 0.0305ºC
- Sample rate: 1 Hz
- Range: -40ºC to +75ºC

Barometric pressure:
- Model: Motorola MPXA4115A
- Accuracy: ±3.0º kPa max (-20ºC to 105ºC temp. ranges)
- Resolution: 0.013 kPa
- Sample rate: 1 Hz
- Range: 55 kPa to 108 kPa

Backup

Model:	GEM Systems GSM-19T
Type:	Digital recording proton precession
Sensitivity:	0.10 nT
Sample rate:	3 second intervals

A digital recorder is operated in conjunction with the base station magnetometer to record the diurnal variations of the earth's magnetic field. The clock of the base station is synchronized with that of the airborne system, using GPS time, to permit subsequent removal of diurnal drift.

For the 2006 phase of the survey, a Fugro CF1 was the primary magnetic base station. It was located at Iskut River, at latitude 56°46’38.70927” N, longitude 130°34’59.06892” W, at an elevation of 292.2 metres above the ellipsoid. The CF1 was later moved to Bell II Lodge, latitude 56°44’41.56093” N, longitude 129°47’45.88900” W, at an elevation of 553.0 metres above the ellipsoid. The back-up GEM Systems GSM-19T was set up at the same location. During the second phase of the survey, in 2007, the Fugro CF1 was again used as the primary magnetic base station, at the same Bell II Lodge location

Navigation (Global Positioning System)

Airborne Receiver for Real-time Navigation & Guidance

Model:	Novatel OEM IV.
Type:	Code and carrier tracking of L1-C/A code at 1575.42 MHz and L2-P code at 1227.0 MHz. Dual frequency, 24-channel.
Sample rate:	10 Hz update.
Accuracy:	Better than 1 metre in differential mode.
Antenna:	Aero AT1675. Mounted on tail of aircraft

Primary Base Station for Post-Survey Differential Correction

Model:	Novatel OEM IV
Type:	Code and carrier tracking of L1-C/A code at 1575.42 MHz and L2-P code at 1227.0 MHz. Dual frequency, 24-channel.
Sample rate:	10 Hz update.
Accuracy:	Better than 1 metre in differential mode.

Secondary GPS Base Station

Model:	Marconi Allstar OEM, CMT-1200
Type:	Code and carrier tracking of L1 band, 12-channel, C/A code at 1575.42 MHz
Sensitivity:	-90 dBm, 1.0 second update
Accuracy:	Manufacturer’s stated accuracy for differential corrected GPS is 2 metres.

The Novatel OEM IV is a line of sight, satellite navigation system that utilizes time-coded signals from at least four of forty-eight available satellites. Both Russian GLONASS and American NAVSTAR satellite constellations are used to calculate the position and to provide real time guidance to the helicopter. A similar system was used as the primary base station receiver. The mobile and base station raw XYZ data were recorded, thereby permitting post-survey differential corrections for theoretical accuracies of better than 2 metres. A Marconi Allstar GPS unit, part of the CF-1, was used as a secondary (back-up) base station.

Each base station receiver is able to calculate its own latitude and longitude. For the 2006 phase of the survey, the primary GPS station was located at Iskut River, latitude 56°46'38.70927" N, longitude 130°34'59.06892" W, at an elevation of 292.2 metres above the ellipsoid. On July 4, the base station was moved to Bell II Lodge, latitude 56°44'41.56093" N, longitude 129°47'45.88900" W, at an elevation of elevation 553.0 metres above the ellipsoid. For the 2007 phase of the survey, the primary GPS station was re-established at the same Bell II Lodge location.

The GPS records data relative to the WGS84 ellipsoid, which is the basis of the revised North American Datum (NAD83). Conversion software is used to transform the WGS84 coordinates to the NAD83 UTM system displayed on the maps.

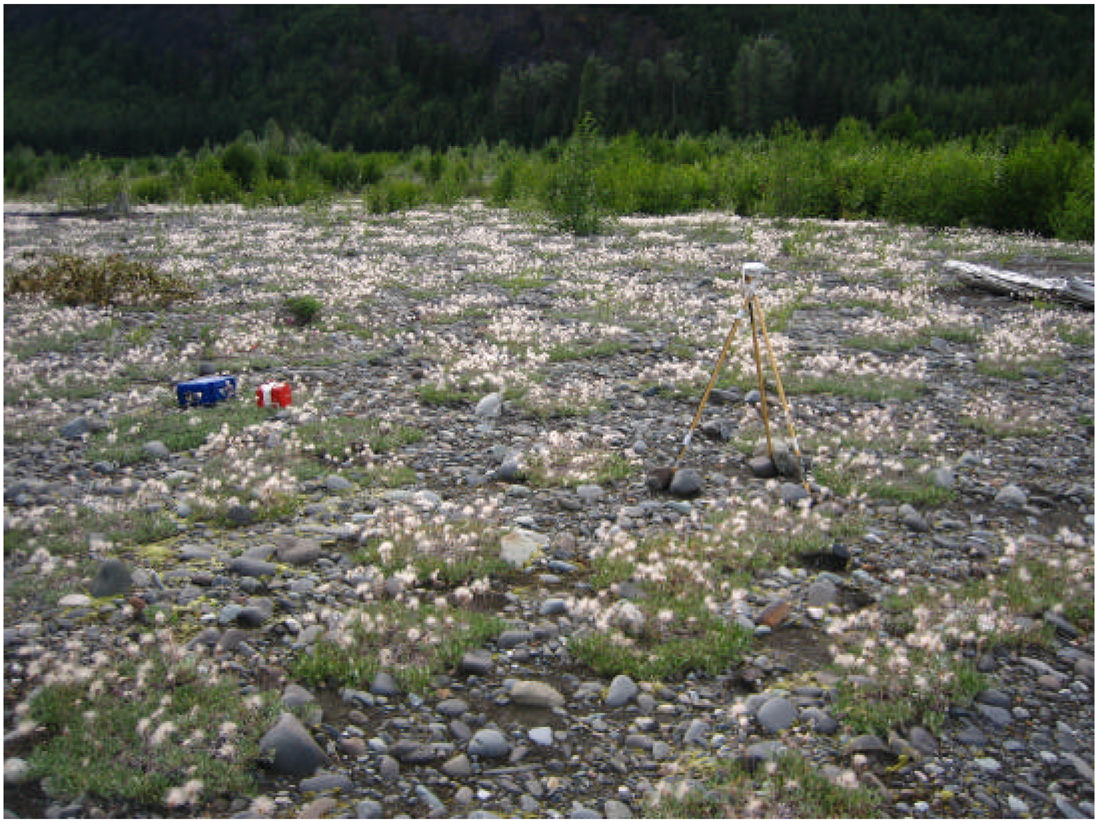


Figure 3-1: Fugro Primary GPS base station

Radar Altimeter

Manufacturer:	Sperry
Model:	RT220
Type:	Short pulse modulation, 4.3 GHz
Sensitivity:	0.3 m
Sample rate:	2 per second

The radar altimeter measures the vertical distance between the helicopter and the ground. This information is used in the processing algorithm that determines conductor depth.

Barometric Pressure and Temperature Sensors

Model:	DIGHEM D 1300	
Type:	Motorola MPX4115AP analog pressure sensor AD592AN high-impedance remote temperature sensors	
Sensitivity:	Pressure: Temperature:	150 mV/kPa 100 mV/°C or 10 mV/°C (selectable)
Sample rate:	10 per second	

The D1300 circuit is used in conjunction with one barometric sensor and up to three temperature sensors. Two sensors (baro and temp) are installed in the EM console in the aircraft, to monitor pressure (KPA) and internal (TEMP_INT) operating temperature. A third sensor is located in the bird to monitor the external (TEMP_EXT) operating temperature.

Digital Data Acquisition System

Manufacturer:	Fugro
Model:	HeliDAS

Recorder: Ultra II Compact Flash Memory Card

The stored data are downloaded to the field workstation PC at the survey base, for verification, backup and preparation of in-field products.

Video Flight Path Recording System

2006 Phase

Type: Panasonic WVCL322 Colour Video Camera

Recorder: Panasonic AG-720

Format: NTSC (VHS)

2007 Phase

Type: Panasonic WVCD322 Colour Video Camera

Recorder: Axis 241S Video Server and Tablet Computer

Format: Digital (*.BIN/*.BDX)

Fiducial numbers are recorded continuously and are displayed on the margin of each image. This procedure ensures accurate correlation of data with respect to visible features on the ground.

Spectrometer

Manufacturer:	Exploranium
Model:	GR-820
Type:	256 Multichannel, Potassium stabilized
Accuracy:	1 count/sec.
Update:	1 integrated sample/sec.

The GR-820 Airborne Spectrometer employs two downward looking crystals (1024 cu.in.- 16.8 L) and one upward looking crystal (256 cu.in.- 4.2 L). The downward crystal records the radiometric spectrum from 410 KeV to 3 MeV over 256 discrete energy windows, as well as a cosmic ray channel that detects photons with energy levels above 3.0 MeV. From these 256 channels, the standard Total Count, Potassium, Uranium and Thorium channels are extracted. The upward crystal is used to measure and correct for Radon.

The shock-protected Sodium Iodide (Thallium) crystal package is unheated, and is automatically stabilized with respect to the Potassium peak. The GR-820 provides raw or Compton stripped data that has been automatically corrected for gain, base level, ADC offset and dead time.

The system is calibrated before and after each flight using three accurately positioned hand-held sources. Additionally, fixed-site test lines are flown to determine if there are any differences in background. This procedure allows corrections to be applied to each survey flight, to eliminate any differences that might result from changes in temperature or humidity.

4. QUALITY CONTROL AND IN-FIELD PROCESSING

Digital data for each flight were transferred to the field workstation, in order to verify data quality and completeness. A database was created and updated using Geosoft Oasis Montaj and proprietary Fugro Atlas software. This allowed the field personnel to calculate, display and verify both the positional (flight path) and geophysical data on a screen or printer. Records were examined as a preliminary assessment of the data acquired for each flight.

In-field processing of Fugro survey data consists of differential corrections to the airborne GPS data, verification of EM calibrations, drift correction of the raw airborne EM data, spike rejection and filtering of all geophysical and ancillary data, verification of flight videos, calculation of preliminary resistivity data, diurnal correction, and preliminary leveling of magnetic data.

All data, including base station records, were checked on a daily basis, to ensure compliance with the survey contract specifications. Reflights were required if any of the following specifications were not met.

Navigation - Positional (x,y) accuracy of better than 10 m, with a CEP (circular error of probability) of 95%.

Flight Path	-	No lines to exceed ±25% departure from nominal line spacing over a continuous distance of more than 1 km, except for reasons of safety.
Clearance	-	Mean terrain sensor clearance of 30 m, ±10 m, except where precluded by safety considerations, e.g., restricted or populated areas, severe topography, obstructions, tree canopy, aerodynamic limitations, etc.
Airborne Mag	-	The non-normalized 4^{th} difference will not exceed 1.6 nT over a continuous distance of 1 kilometre excluding areas where this specification is exceeded due to natural anomalies.
Base Mag	-	Diurnal variations not to exceed 10 nT over a straight line time chord of 1 minute.
EM	-	Spheric pulses may occur having strong peaks but narrow widths. The EM data area considered acceptable when their occurrence is less than 10 spheric events exceeding the stated noise specification for a given frequency per 100 samples continuously over a distance of 2,000 metres.

Frequency	Coil Orientation	Peak to Peak Noise Envelope (ppm)
900 Hz	horizontal coplanar	10.0
1000 Hz	vertical coaxial	5.0
5500 Hz	vertical coaxial	10.0
7200 Hz	horizontal coplanar	20.0
56,000 Hz	horizontal coplanar	40.0

5. DATA PROCESSING

Flight Path Recovery

The raw range data from at least four satellites are simultaneously recorded by both the base and mobile GPS units. The geographic positions of both units, relative to the model ellipsoid, are calculated from this information. Differential corrections, which are obtained from the base station, are applied to the mobile unit data to provide a post-flight track of the aircraft, accurate to within 2 m. Speed checks of the flight path are also carried out to determine if there are any spikes or gaps in the data.

The corrected WGS84 latitude/longitude coordinates are transformed to the coordinate system used on the final maps. Images or plots are then created to provide a visual check of the flight path.

Electromagnetic Data

EM data are processed at the recorded sample rate of 10 samples/second. Spheric rejection median and Hanning filters are then applied to reduce noise to acceptable levels. EM test profiles are then created to allow the interpreter to select the most appropriate EM anomaly picking controls for a given survey area. The EM picking parameters depend on several factors but are primarily based on the dynamic range of the resistivities within the survey area, and the types and expected geophysical responses of the targets being sought.

Anomalous electromagnetic responses are selected and analysed by computer to provide a preliminary electromagnetic anomaly map. The automatic selection algorithm is intentionally oversensitive to assure that no meaningful responses are missed. Using the preliminary map in conjunction with the multi-parameter stacked profiles, the interpreter then classifies the anomalies according to their source and eliminates those that are not substantiated by the data. The final interpreted EM anomaly map includes bedrock, surficial and cultural conductors. A map containing only bedrock conductors can be generated, if desired.

Apparent Resistivity

The apparent resistivities in ohm-m are generated from the in-phase and quadrature EM components for all of the coplanar frequencies, using a pseudo-layer half-space model. The inputs to the resistivity algorithm are the in-phase and quadrature amplitudes of the secondary field. The algorithm calculates the apparent resistivity in ohm-m, and the apparent height of the bird above the conductive source. Any difference between the apparent height and the true height, as measured by the radar altimeter, is called the pseudo-layer and reflects the difference between the real geology and a homogeneous half-space. This difference is often attributed to the presence of a highly resistive upper layer. Any errors in the altimeter reading, caused by heavy tree cover, are included in the pseudo-layer and do not affect the resistivity calculation. The apparent depth estimates, however, will reflect the altimeter errors. Apparent resistivities calculated in this manner may differ from those calculated using other models.

In areas where the effects of magnetic permeability or dielectric permittivity have suppressed the in-phase responses, the calculated resistivities will be erroneously high. Various algorithms and inversion techniques can be used to partially correct for the effects of permeability and permittivity.

Apparent resistivity maps portray all of the information for a given frequency over the entire survey area. This full coverage contrasts with the electromagnetic anomaly map, which provides information only over interpreted conductors. The large dynamic range afforded by the multiple frequencies makes the apparent resistivity parameter an excellent mapping tool.

The preliminary apparent resistivity maps and images are carefully inspected to identify any lines or line segments that might require base level adjustments. Subtle changes between in-flight calibrations of the system can result in line-to-line differences that are more recognizable in resistive (low signal amplitude) areas. If required, manual level adjustments are carried out to eliminate or minimize resistivity differences that can be attributed, in part, to changes in operating temperatures. These leveling adjustments are usually very subtle, and do not result in the degradation of discrete anomalies.

After the manual leveling process is complete, revised resistivity grids are created. The resulting grids can be subjected to a microleveling technique in order to smooth the data for contouring. The coplanar resistivity parameter has a broad 'footprint' that requires very little filtering.--The calculated resistivities for the 900 Hz, 7200 Hz and 56000 Hz coplanar frequencies are included in the XYZ and grid archives. Values are in ohm-metres on all final products.

Dielectric Permittivity and Magnetic Permeability Corrections[1]

In resistive areas having magnetic rocks, the magnetic and dielectric effects will both generally be present in high-frequency EM data, whereas only the magnetic effect will exist in low-frequency data.

The magnetic permeability is first obtained from the EM data at the lowest frequency, because the ratio of the magnetic response to conductive response is maximized and because displacement currents are negligible. The homogeneous half-space model is used. The computed magnetic permeability is then used along with the in-phase and quadrature response at the highest frequency to obtain the relative dielectric permittivity, again using the homogeneous half-space model. The highest frequency is used because the ratio of dielectric response to conductive response is maximized. The resistivity can

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[1] Huang, H. and Fraser, D.C., 2001 Mapping of the Resistivity, Susceptibility, and Permittivity of the Earth Using a Helicopter-borne Electromagnetic System: Geophysics 106 pg 148-157.

then be determined from the measured in-phase and quadrature components of each frequency, given the relative magnetic permeability and relative dielectric permittivity.

Resistivity-depth Sections (optional)

The apparent resistivities for all frequencies can be displayed simultaneously as coloured resistivity-depth sections. Usually, only the coplanar data are displayed as the close frequency separation between the coplanar and adjacent coaxial data tends to distort the section. The sections can be plotted using the topographic elevation profile as the surface. The digital terrain values, in metres a.m.s.l., can be calculated from the GPS Z-value or barometric altimeter, minus the aircraft radar altimeter.

Resistivity-depth sections can be generated in three formats:

(1) Sengpiel resistivity sections, where the apparent resistivity for each frequency is plotted at the depth of the centroid of the in-phase current flow[2]; and,

(2) Differential resistivity sections, where the differential resistivity is plotted at the differential depth[3].

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2 Sengpiel, K.P., 1988, Approximate Inversion of Airborne EM Data from Multilayered Ground: Geophysical Prospecting 36, 446-459.

3 Huang, H. and Fraser, D.C., 1993, Differential Resistivity Method for Multi-frequency Airborne EM Sounding: presented at Intern. Airb. EM Workshop, Tucson, Ariz.

(3) Occam[4] or Multi-layer[5] inversion.

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[4] Constable et al, 1987, Occam's inversion: a practical algorithm for generating smooth models from electromagnetic sounding data: Geophysics, 52, 289-300.

[5] Huang H., and Palacky, G.J., 1991, Damped least-squares inversion of time domain airborne EM data based on singular value decomposition: Geophysical Prospecting, 39, 827-844.

Both the Sengpiel and differential methods are derived from the pseudo-layer half-space model. Both yield a coloured resistivity-depth section that attempts to portray a smoothed approximation of the true resistivity distribution with depth. Resistivity-depth sections are most useful in conductive layered situations, but may be unreliable in areas of moderate to high resistivity where signal amplitudes are weak. In areas where in-phase responses have been suppressed by the effects of magnetite, or adversely affected by cultural features, the computed resistivities shown on the sections may be unreliable.

Both the Occam and multi-layer inversions compute the layered earth resistivity model that would best match the measured EM data. The Occam inversion uses a series of thin, fixed layers (usually 20 x 5m and 10 x 10m layers) and computes resistivities to fit the EM data. The multi-layer inversion computes the resistivity and thickness for each of a defined number of layers (typically 3-5 layers) to best fit the data.

Total Magnetic Field

A fourth difference editing routine was applied to the magnetic data to remove any spikes. The aeromagnetic data were corrected for diurnal variation using the magnetic base station data. The results were then leveled using tie and traverse line intercepts. Manual adjustments were applied to any lines that required leveling, as indicated by shadowed images of the gridded magnetic data. The manually leveled data were then subjected to a microleveling filter.

Calculated Vertical Magnetic Gradient

The diurnally-corrected total magnetic field data were subjected to a processing algorithm that enhances the response of magnetic bodies in the upper 500 m and attenuates the response of deeper bodies. The resulting vertical gradient map provides better definition and resolution of near-surface magnetic units. It also identifies weak magnetic features that may not be evident on the total field map. However, regional magnetic variations and changes in lithology may be better defined on the total magnetic field map.

EM Magnetite (optional)

The apparent percent magnetite by weight is computed wherever magnetite produces a negative in-phase EM response. This calculation is more meaningful in resistive areas.

Magnetic Derivatives (optional)

The total magnetic field data can be subjected to a variety of filtering techniques to yield maps or images of the following:

enhanced magnetics

second vertical derivative

reduction to the pole/equator

magnetic susceptibility with reduction to the pole

upward/downward continuations

analytic signal

All of these filtering techniques improve the recognition of near-surface magnetic bodies, with the exception of upward continuation. Any of these parameters can be produced on request.

Digital Elevation (optional)

The radar altimeter values (ALTR – aircraft to ground clearance) are subtracted from the differentially corrected and de-spiked GPS-Z values to produce profiles of the height above the ellipsoid along the survey lines. These values are gridded to produce contour maps showing approximate elevations within the survey area. The calculated digital terrain data are then tie-line leveled and adjusted to mean sea level. Any remaining subtle line-to-line discrepancies are manually removed. After the manual corrections are applied, the digital terrain data are filtered with a microleveling algorithm.

The accuracy of the elevation calculation is directly dependent on the accuracy of the two input parameters, ALTR and GPS-Z. The ALTR value may be erroneous in areas of heavy tree cover, where the altimeter reflects the distance to the tree canopy rather than the ground. The GPS-Z value is primarily dependent on the number of available satellites. Although post-processing of GPS data will yield X and Y accuracies in the order of 1-2 metres, the accuracy of the Z value is usually much less, sometimes in the ±10 metre range. Further inaccuracies may be introduced during the interpolation and gridding process.

Because of the inherent inaccuracies of this method, no guarantee is made or implied that the information displayed is a true representation of the height above sea level. Although this product may be of some use as a general reference, THIS PRODUCT MUST NOT BE USED FOR NAVIGATION PURPOSES.

Contour, Colour and Shadow Map Displays

The geophysical data are interpolated onto a regular grid using a modified Akima spline technique. The resulting grid is suitable for image processing and generation of contour maps. The grid cell size is 20% of the line interval.

Colour maps are produced by interpolating the grid down to the pixel size. The parameter is then incremented with respect to specific amplitude ranges to provide colour "contour" maps.

Monochromatic shadow maps or images are generated by employing an artificial sun to cast shadows on a surface defined by the geophysical grid. There are many variations in the shadowing technique. These techniques can be applied to total field or enhanced magnetic data, magnetic derivatives, resistivity, etc. The shadowing technique is also used as a quality control method to detect subtle changes between lines.

Multi-channel Stacked Profiles

Distance-based profiles of the digitally recorded geophysical data are generated and plotted at an appropriate scale. These profiles also contain the calculated parameters that are used in the interpretation process. These are produced as worksheets prior to interpretation, and are also presented in the final corrected form after interpretation. The profiles display electromagnetic anomalies with their respective interpretive symbols. Table 5-1 shows the parameters and scales for the multi-channel stacked profiles.

In Table 5-1, the log resistivity scale of 0.06 decade/mm means that the resistivity changes by an order of magnitude in 16.6 mm. The resistivities at 0, 33 and 67 mm up from the bottom of the digital profile are respectively 1, 100 and 10,000 ohm-m.

Table 5-1. Multi-channel Stacked Profiles

Channel Name (Freq)	Observed Parameters	Scale Units/mm
MAGF	total magnetic field (fine)	5 nT
MAGF	total magnetic field (coarse)	50 nT
ALTBIRDM	EM sensor height above ground	6 m
TC	Total Counts	50 cps
K	Potassium counts	10 cps
TH	Thorium counts	2 cps
U	Uranium counts	2 cps
CXI1000	vertical coaxial coil-pair in-phase (1000 Hz)	2 ppm
CXQ1000	vertical coaxial coil-pair quadrature (1000 Hz)	2 ppm
CPI900	horizontal coplanar coil-pair in-phase (900 Hz)	4 ppm
CPQ900	horizontal coplanar coil-pair quadrature (900 Hz)	4 ppm
CXI5500	vertical coaxial coil-pair in-phase (5500 Hz)	4 ppm
CXQ5500	vertical coaxial coil-pair quadrature (5500 Hz)	4 ppm
CPI7200	horizontal coplanar coil-pair in-phase (7200 Hz)	10 ppm
CPQ7200	horizontal coplanar coil-pair quadrature (7200 Hz)	10 ppm
CPI56K	horizontal coplanar coil-pair in-phase (56,000 Hz)	10 ppm
CPQ56K	horizontal coplanar coil-pair quadrature (56,000 Hz)	10 ppm
CXSP	coaxial spherics monitor	
	Computed Parameters	
DIFI (mid freq.)	difference function in-phase from CXI and CPI	5 ppm
DIFQ (mid freq.)	difference function quadrature from CXQ and CPQ	5 ppm
RES900	log resistivity	.06 decade
RES7200	log resistivity	.06 decade
RES56K	log resistivity	.06 decade
DEP900	apparent depth	6 m
DEP7200	apparent depth	6 m
DEP56K	apparent depth	6 m

Radiometrics

All radiometric data reductions performed by Fugro rigorously follow the procedures described in the IAEA Technical Report[6].

All processing of radiometric data was undertaken at the natural sampling rate of the spectrometer, i.e., one second. The data were not interpolated to match the fundamental 0.1 second interval of the EM and magnetic data.

The following sections describe each step in the process.

Pre-filtering

The radar altimeter data were processed with a 15-point median filter to remove spikes.

Reduction to Standard Temperature and Pressure

The radar altimeter data were converted to effective height (h_e) in feet using the acquired temperature and pressure data, according to the following formula:

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[6] Exploranium, I.A.E.A. Report, Airborne Gamma-Ray Spectrometer Surveying, Technical Report No. 323, 1991.

$$h_e = h * \frac{273.15}{T + 273.15} * \frac{P}{1013.25}$$

where: *h* is the observed crystal to ground distance in feet

T is the measured air temperature in degrees Celsius

P is the barometric pressure in millibars

Live Time Correction

The spectrometer, an Exploranium GR-820, uses the notion of "live time" to express the relative period of time the instrument was able to register new pulses per sample interval. This is the opposite of the traditional "dead time", which is an expression of the relative period of time the system was unable to register new pulses per sample interval.

The GR-820 measures the live time electronically, and outputs the value in milliseconds. The live time correction is applied to the total count, potassium, uranium, thorium, upward uranium and cosmic channels. The formula used to apply the correction is as follows:

$$C_{lt} = C_{raw} * \frac{1000.0}{L}$$

where: C_{lt} is the live time corrected channel in counts per second

C_{raw} is the raw channel data in counts per second

L is the live time in milliseconds

Intermediate Filtering

Two parameters were filtered, but not returned to the database:

- Radar altimeter was smoothed with a 3-point Hanning filter (h_{ef}).
- The Cosmic window was smoothed with a 9-point Hanning filter (Cos_f).

Aircraft and Cosmic Background

Aircraft background and cosmic stripping corrections were applied to the total count, potassium, uranium, thorium and upward uranium channels using the following formula:

$$C_{ac} = C_{lt} - (a_c + b_c * \mathrm{Cos}_f)$$

where: C_{ac} is the background and cosmic corrected channel

C_{lt} is the live time corrected channel

a_c is the aircraft background for this channel

b_c is the cosmic stripping coefficient for this channel

Cos_f is the filtered Cosmic channel

Radon Background

The determination of calibration constants that enable the stripping of the effects of atmospheric radon from the downward-looking detectors through the use of an upward-looking detector is divided into two parts:

1) Determine the relationship between the upward- and downward-looking detector count rates for radiation originating from the ground.

2) Determine the relationship between the upward- and downward-looking detector count rates for radiation due to atmospheric radon.

The procedures to determine these calibration factors are documented in IAEA Report #323 on airborne gamma-ray surveying. The calibrations for the first part were determined as outlined in the report.

The latter case normally requires many over-water measurements where there is no contribution from the ground. Where this is not possible, it is standard procedure to establish a test line over which a series of repeat measurements are acquired. From these repeat flights, any change in the downward uranium window due to variations in radon background would be directly related to variations in the upward window and the other downward windows.

The validity of this technique rests on the assumption that the radiation from the ground is essentially constant from flight to flight. Inhomogeneities in the ground, coupled with deviations in the flight path between test runs, add to the inaccuracy of the accumulated results. Variations in flying heights and other environmental factors also contribute to the uncertainty.

The use of test lines is a common solution for a fixed-wing acquisition platform. The ability of rotary wing platforms to hover at a constant height over a fixed position eliminates a number of the variations which degrade the accuracy of the results required for this calibration.

A test site was established in or near the survey area. The tests were carried out at the start and end of each day, and at the end of each flight. Data were acquired over a four-minute period at the nominal survey altitude (60 m). The data were then corrected for live time, aircraft background and cosmic activity.

Once the survey was completed, the relationships between the counts in the downward uranium window and in the other four windows due to atmospheric radon were determined using linear regression for each of the hover sites. The following equations were used:

$$u_r = a_u Ur + b_u$$

$$K_r = a_K U_r + b_K$$

$$T_r = a_T U_r + b_T$$

$$I_r = a_I U_r + b_I$$

where: u_r is the radon component in the upward uranium window

K_r, U_r, T_r and I_r are the radon components in the various windows of the downward detectors

the various "a" and "b" coefficients are the required calibration constants

In practice, only the "a" constants were used in the final processing. The "b" constants, which are normally near zero for over-water calibrations, were of no value as they reflected the local distribution of the ground concentrations measured in the five windows.

Compton Stripping

Following the radon correction, the potassium, uranium and thorium are corrected for spectral overlap. First, α,β and γ the stripping ratios, are modified according to altitude. Then an adjustment factor based on a, the reversed stripping ratio, uranium into thorium, is calculated. (Note: the stripping ratio altitude correction constants are expressed in change per metre. A constant of 0.3048 is required to conform to the internal usage of height in feet):

$$a_h = a + h_{ef} * 0.00049$$

$$a_r = \frac{1.0}{1.0 - a * a_h}$$

$$b_h = b + h_{ef} * 0.00065$$

$$g_h = g + h_{ef} * 0.00069$$

where: α, β, γ are the Compton stripping coefficients

α_h, β_h, γ_h are the height corrected Compton stripping coefficients

h_{ef} is the height above ground in metres

α_r is the scaling factor correcting for back scatter

a is the reverse stripping ratio

The stripping corrections are then carried out using the following formulas:

$$Th_c = (Th_{rc} - a * U_{rc}) * a_r$$

$$K_c = K_{rc} - g_h * U_c - b_h * Th_c$$

$$U_c = (U_{rc} - a_h * Th_{rc}) * a_r$$

where: U_c, Th_c and K_c are corrected uranium, thorium and potassium

α_h,β_h,γ_h are the height corrected Compton stripping coefficients

U_{rc}, Th_{rc} and K_{rc} are radon-corrected uranium, thorium and potassium

α_r is the backscatter correction

Attenuation Corrections

The total count, potassium, uranium and thorium data are then corrected to a nominal survey altitude, in this case 200 feet. This is done according to the equation:

$$C_a = C * e^{m(h_{ef}-ho)}$$

where: C_a is the output altitude corrected channel

C is the input channel

e^{μ} is the attenuation correction for that channel

h_{ef} is the effective altitude

h_0 is the nominal survey altitude to correct to

6. PRODUCTS

This section lists the final maps and products that have been provided under the terms of the survey agreement. Other products can be prepared from the existing dataset, if requested. These include magnetic enhancements or derivatives, percent magnetite, resistivities corrected for magnetic permeability and/or dielectric permittivity, digital terrain, resistivity-depth sections, inversions, and overburden thickness. Most parameters can be displayed as contours, profiles, or in colour.

Base Maps

Base maps of the survey area were produced by scanning published topographic maps to a bitmap (.bmp) format. This process provides a relatively accurate, distortion-free base that facilitates correlation of the navigation data to the map coordinate system. The topographic files were combined with geophysical data for plotting the final maps. All maps were created using the following parameters:

Projection Description:

Datum:	NAD 83
Ellipsoid:	GRS80
Projection:	UTM (Zone: 9 North)
Central Meridian:	129 ° West
False Northing:	0
False Easting:	500000
Scale Factor:	0.9996
WGS84 to Local Conversion:	Molodensky
Datum Shifts:	DX: 0 DY: 0 DZ: 0

The following parameters are presented on 6 map sheets (2006) and 8 revised map sheets (2007), at a scale of 1:20000. All maps include flight lines and topography, unless otherwise indicated. Preliminary products are not listed.

Final Products

2006 Phase

	No. of Map Sets=2		
	Mylar	Blackline	Colour
EM Anomalies		2x6	
Total Magnetic Field			2x6
Calculated Vertical Magnetic Gradient			2x6
Apparent Resistivity 7200 Hz			2x6
Apparent Resistivity 56,000 Hz			2x6
Radiometrics - Total Count			2x6
- Potassium			2x6
- Uranium			2x6
- Thorium			2x6

Additional Products 2006

Digital Archive (see Archive Description)	1 CD-ROM
Survey Report	2 copies
Multi-channel Stacked Profiles	All 2006 lines
Flight Path Video (VHS)	20 cassettes

2007 Phase

	No. of Map Sets		
	Mylar	Blackline	Colour
EM Anomalies		2x6	
Total Magnetic Field			2x6
Calculated Vertical Magnetic Gradient			2x6
Apparent Resistivity 7200 Hz			2x6
Apparent Resistivity 56,000 Hz			2x6
Radiometrics - Total Count			2x6
- Potassium			2x6
- Uranium			2x6

- Thorium			2x6

Additional Products 2007

Digital Archive (see Archive Description)	1 DVD-ROM
Survey Report	2 copies
Multi-channel Stacked Profiles	All 2007 lines
Flight Path Video (*.BIN/*.BDX)	9 DVDs

7. SURVEY RESULTS

General Discussion

Tables 7-1 (2006) and 7-2 (2007) summarize the EM responses in the survey areas, with respect to conductance grade and interpretation. The apparent conductance and depth values shown in the EM Anomaly list appended to this report have been calculated from “local” in-phase and quadrature amplitudes of the Coaxial 5500 Hz frequency. The picking and interpretation procedure relies on several parameters and calculated functions. For this survey, the Coaxial 5500 Hz responses and the mid-frequency difference channels were used as two of the main picking criteria. The 7200 Hz coplanar results were also weighted to provide picks over wider or flat-dipping sources. The quadrature channels provided picks in areas where the in-phase responses might have been suppressed by magnetite.

The anomalies shown on the electromagnetic anomaly maps are based on a near-vertical, half plane model. This model best reflects "discrete" bedrock conductors. Wide bedrock conductors or flat-lying conductive units, whether from surficial or bedrock sources, may give rise to very broad anomalous responses on the EM profiles. These may not appear on the electromagnetic anomaly map if they have a regional character rather than a locally anomalous character.

TABLE 7-1 EM ANOMALY STATISTICS

ESKAY BLOCKS 4, 5, 6. (2006 Phase)

CONDUCTOR GRADE	CONDUCTANCE RANGE SIEMENS (MHOS)	NUMBER OF RESPONSES
7	>100	5
6	50 - 100	2
5	20 - 50	4
4	10 - 20	16
3	5 - 10	58
2	1 - 5	493
1	<1	396
*	INDETERMINATE	1051
TOTAL		2025

CONDUCTOR MODEL	MOST LIKELY SOURCE	NUMBER OF RESPONSES
D	DISCRETE BEDROCK CONDUCTOR	145
B	DISCRETE BEDROCK CONDUCTOR	308
S	CONDUCTIVE COVER	931
H	ROCK UNIT OR THICK COVER	560
E	EDGE OF WIDE CONDUCTOR	81
L	CULTURE	0
TOTAL		2025

(SEE EM MAP LEGEND FOR EXPLANATIONS)

TABLE 7-2 EM ANOMALY STATISTICS

ESKAY BLOCKS 4, 5, 6. (2007 Phase)

CONDUCTOR GRADE	CONDUCTANCE RANGE SIEMENS (MHOS)	NUMBER OF RESPONSES
7	>100	0
6	50 - 100	0
5	20 - 50	0
4	10 - 20	2
3	5 - 10	5
2	1 - 5	54
1	<1	207
*	INDETERMINATE	554
TOTAL		822

CONDUCTOR MODEL	MOST LIKELY SOURCE	NUMBER OF RESPONSES
D	DISCRETE BEDROCK CONDUCTOR	41
B	DISCRETE BEDROCK CONDUCTOR	35
S	CONDUCTIVE COVER	635
H	ROCK UNIT OR THICK COVER	100
E	EDGE OF WIDE CONDUCTOR	11
L	CULTURE	0
TOTAL		822

(SEE EM MAP LEGEND FOR EXPLANATIONS)

These broad conductors, which more closely approximate a half-space model, will be maximum coupled to the horizontal (coplanar) coil-pair and should be more evident on the resistivity parameter. Resistivity maps, therefore, may be more valuable than the electromagnetic anomaly maps, in areas where broad or flat-lying conductors are considered to be of importance. Contoured resistivity maps, based on the 7200 Hz and 56000 Hz coplanar data are included with this report.

Excellent resolution and discrimination of conductors was accomplished by using a fast sampling rate of 0.1 sec and by employing a “common” frequency (5500/7200 Hz) on two orthogonal coil-pairs (coaxial and coplanar). The resulting difference channel parameters often permit differentiation of bedrock and surficial conductors, even though they may exhibit similar conductance values.

Anomalies that occur near the ends of the survey lines (i.e., outside the survey area), and those that occur in areas of steep topography, should be viewed with caution. Some of the weaker anomalies could be due to aerodynamic noise, i.e., bird bending, which is created by abnormal stresses to which the bird is subjected during the climb and turn of the aircraft between lines. Such aerodynamic noise is usually manifested by an anomaly on the coaxial in-phase channel only, although severe stresses can affect the coplanar in-phase channels as well.

Magnetics

A Fugro CF-1 cesium vapour magnetometer was operated at the survey base to record diurnal variations of the earth's magnetic field. The clock of the base station was synchronized with that of the airborne system to permit subsequent removal of diurnal drift. A GEM Systems GSM-19T proton precession magnetometer was also operated as a backup unit.

The total magnetic field data have been presented as contours on the base map(s) using a contour interval of 5 nT where gradients permit. The maps show the magnetic properties of the rock units underlying the survey areas.

The total magnetic field data have been subjected to a processing algorithm to produce maps of the calculated vertical gradient. This procedure enhances near-surface magnetic units and suppresses regional gradients. It also provides better definition and resolution of magnetic units and displays weak magnetic features that may not be clearly evident on the total field maps.

There is some evidence on the magnetic maps that suggests that the survey areas have been subjected to deformation and/or alteration. These structural complexities are evident on the contour maps as variations in magnetic intensity, irregular patterns, and as offsets or changes in strike direction.

If a specific magnetic intensity can be assigned to the rock type that is believed to host the target mineralization, it may be possible to select areas of higher priority on the basis of the total field magnetic data. This is based on the assumption that the magnetite content of the host rocks will give rise to a limited range of contour values that will permit differentiation of various lithological units.

The magnetic results, in conjunction with the other geophysical parameters, have provided valuable information that can be used to effectively map the geology and structure in the survey areas.

Apparent Resistivity

Apparent resistivity maps, which display the conductive properties of the survey areas, were produced from the 7200 Hz and 56,000 Hz coplanar data. The maximum resistivity values, which are calculated for each frequency, are 8,000 and 20,000 ohm-m respectively. These cut-offs eliminate the erratic higher resistivities that would result from unstable ratios of very small EM amplitudes.

In general, the resistivity patterns show moderately good agreement with the magnetic trends. Most of the stronger conductive units are associated with zones of relatively low susceptibility. This suggests that many of the weaker resistivity lows could be related to conductive overburden rather than bedrock features. There are some areas, however, where obvious bedrock conductors correlate with magnetic highs.

Most of the major river valleys are conductive, particularly at the higher frequencies. However, there are a few broad conductive zones that extend beyond the valleys or occur on high ground. Some of these are quite extensive and probably reflect conductive sedimentary units or "formational" conductors that may be of minor interest as direct exploration targets. However, attention may be focused on areas where these zones appear to be faulted or folded or where anomaly characteristics differ along strike.

Electromagnetic Anomalies

The EM anomalies resulting from this survey appear to fall within one of three general categories. The first type consists of discrete, well-defined anomalies that yield marked inflections on the difference channels. These anomalies are usually attributed to conductive sulphides or graphite and are generally given a "B", "T" or "D" interpretive symbol, denoting a bedrock source.

The second class of anomalies comprises moderately broad responses that exhibit the characteristics of a half-space and do not yield well-defined inflections on the difference channels. Anomalies in this category are usually given an "S" or "H" interpretive symbol. The lack of a difference channel response usually implies a broad or flat-lying conductive source such as overburden. Some of these anomalies could reflect conductive rock units, zones of deep weathering, the weathered tops of plugs or pipes, or broad alteration zones, all of which can yield “non-discrete” signatures.

The effects of conductive overburden are evident over portions of the survey areas, primarily in the major river valleys. Although the difference channels (DIFI and DIFQ) are extremely valuable in detecting bedrock conductors that are partially masked by conductive overburden, sharp undulations in the bedrock/overburden interface can yield anomalies in the difference channels which may be interpreted as possible bedrock conductors. Such anomalies usually fall into the "S?" or "B?" classification but may also be given an "E" interpretive symbol, denoting a resistivity contrast at the edge of a conductive unit.

The "?" symbol does not question the validity of an anomaly, but instead indicates some degree of uncertainty as to which is the most appropriate EM source model. This ambiguity results from the combination of effects from two or more conductive sources, such as overburden and bedrock, gradational changes, or moderately shallow dips. The presence of a conductive upper layer has a tendency to mask or alter the characteristics of bedrock conductors, making interpretation difficult. This problem is further exacerbated in the presence of magnetite.

The third anomaly category includes responses that are associated with magnetite. Magnetite can cause suppression or polarity reversals of the in-phase components, particularly at the lower frequencies in resistive areas. The effects of magnetite-rich rock units are usually evident on the multi-parameter geophysical data profiles as negative excursions of the lower frequency in-phase channels.

In areas where EM responses are evident primarily on the quadrature components, zones of poor conductivity are indicated. Where these responses are coincident with magnetic anomalies, it is possible that the in-phase component amplitudes have been suppressed by the effects of magnetite. Poorly conductive magnetic features can give rise to resistivity anomalies that are only slightly below or slightly above background. If it is expected that poorly conductive economic mineralization could be associated with magnetite-rich units, most of these weakly anomalous features will be of interest. In areas where magnetite causes the in-phase components to become negative, the apparent conductance and depth of EM anomalies will be unreliable. Magnetite effects usually give rise to overstated (higher) resistivity values and understated (shallow) depth calculations.

As potential targets within the area may be associated with massive to weakly disseminated sulphides, which may or may not be hosted by magnetite-rich rocks, it is impractical to assess the relative merits of EM anomalies on the basis of conductance. It is recommended that an attempt be made to compile a suite of geophysical "signatures" over any known areas of interest. Anomaly characteristics are clearly defined on the multi-parameter geophysical data profiles that are supplied as one of the survey products.

Potential Targets in the Survey Area

The electromagnetic anomaly maps show the anomaly locations with the interpreted conductor type, dip, conductance and depth being indicated by symbols. Direct magnetic correlation is also shown if it exists. The strike direction and length of the conductors are indicated only where anomalies can be correlated from line to line with a reasonable degree of confidence.

In areas where several conductors or conductive trends appear to be related to a common geological unit, these have been outlined as "zones" on the 2006 EM anomaly maps. The zone outlines usually approximate the limits of conductive units defined by the resistivity contours, but may also be related to distinct rock units that can be inferred from the magnetic data.

Phase 2006

The conductors from the 2006 flying have been described in the previous report, with the low resistivity zones and the EM conductor axes being shown on the 2006 EM Maps only. The following section (up to and including page 7.25) is a duplicate of the 2006 anomaly description.

North Area (Lines 40010-51190)

The 7200 Hz and 56 kHz resistivity data show a broad resistivity low that strikes east, along the Iskut River valley. Although this zone has been attributed to conductive alluvium, the 900 Hz frequency defines several pods or bands of more conductive material within this trend, that could be due to bedrock sources at depth.

The magnetic data show a moderately strong, similarly broad anomaly that follows the same valley. This magnetic unit, however, is divided by a prominent non-magnetic curvilinear core, which roughly follows the central axis of the valley. This magnetic low is intruded or offset by at least six cross-cutting features that are clearly evident on the vertical gradient maps.

The western portion of the valley, west of tie line 49080, is more conductive than the eastern portion, although there are smaller conductive zones near 50820F and 50840D. East of tie line 49130, the more conductive zones occur north and south of the main valley, and exhibit north to NNW trends, in addition to the NE trend that parallels the valley. The narrow magnetic low that follows the valley exhibits an abrupt change in strike to the SE, near 50730F, and then north and northeast at 50750I and 50710F. This narrow magnetic low becomes a broad unit of low magnetic susceptibility, with an obvious contact that strikes NNW through 50660F and 50601C. A highly conductive unit, centered near 50660G, strikes north along tie line 49140, north of the valley.

A larger, stronger, conductive zone occurs in the area south of the valley, extending south from the magnetic contact at 50721K to 50871D. Anomaly 50770P is part of this broad conductive zone, but appears to be due to a separate, south-trending, east-dipping narrow source with a strike extent of more than 1.5 km. This conductive trend remains open to the north.

The EM anomalies that are associated with the Iskut River valley are often poorly defined, because the conductive zones are nearly parallel to the survey lines and are poorly coupled to the coaxial channels. Better definition of discrete sources should be evident on the tie lines that transect the main axis of the broad resistivity low. However, the tie lines tend to confirm the presence of a broad, highly conductive unit buried at a depth of more than 60 m. The north and south edges of this zone are generally more conductive, and are coincident with magnetic highs or gradients that define contacts. The area between 49033A and 49033C suggests a broad (>500 m) flat-dipping source, with a slight increase in depth towards the north. The 56 kHz frequency suggests that this broad, deep unit is overlain by at least 50 m of more resistive cover. The source between 49070A and 49070B is wider (~1.5 km) and deeper (60 m-90 m). A strong, deeply-buried source is also evident at 49100B.

Responses on the eastern half of the valley are generally of lower amplitude and less conductive, except for the strong flanking conductors at 49140F, 49153E and 49164C. Most of these conductive zones are associated with units of moderately low magnetic susceptibility.

In addition to the conductors associated with the valley, and the cross-cutting resistivity lows near tie lines 49140, 49153 and 49164, there are a few other moderately strong conductors on Sheets 1 and 2 that are considered to be of interest. A few of the stronger responses are listed in the following table:

Anomaly	Type	Mag	Comments
40400A 40430A 40470A 40500A	B D D D	- - 16 -	These anomalies are part of a moderately large resistivity low at the western ends of lines 40400-40500. This incomplete conductor occurs on an east-facing slope, and occurs near the western contact of a south-trending magnetic anomaly. Anomalies 40430A, 40470A and 40500A all reflect thin sources. They may all be part of a continuous south-trending conductor, but some lines did not extend far enough to the west to confirm this. On other lines, excessive flying heights precluded the development of anomalous responses. Anomaly 40500A is at least 550 m SW of the contact at 40470A, and is probably due to a different causative source. This conductor is also open to the NW.
49070F 50340C	B? B	- -	Tie line anomaly 49070F is associated with a prominent SE-trending magnetic low. This weak conductor strikes towards 50340C, an isolated response near the western contact of a magnetic unit. The isolated resistivity anomaly at 50340C, and the different magnetic responses, suggest that 50340C and 49070F are probably not related to the same horizon. Anomaly 49070F is associated with a weak potassium high, but there is a stronger anomaly to the NW, near 50280A.
50460F 50460G	D D	37 13	Two thin conductors are associated with a weak magnetic high. The two conductors are separated by about 120 m, but yield a single resistivity low that is open to the north. Additional work will be required to check the extent and the causative sources of these two thin conductors. Anomaly 50940E is part of an adjacent SE-trending weak resistivity low that follows a creek, and is likely due to conductive alluvium.
50460H 50480C	D D	- -	A small resistivity low hosts 50460H, a moderately wide conductor of probable bedrock origin that is associated with a weak magnetic low. This conductor is open to the

Anomaly	Type	Mag	Comments
			north. Anomaly 50480C, at its southern end, suggests a thin, west-dipping source. It is located north of the inferred northern contact of the moderately magnetic unit in the northeastern quadrant of the survey block.
50460I 50460J 50460K	D B? B	- - -	A strong, incomplete resistivity low, at the northern limit of the survey, hosts three or more strong conductors. This attractive zone is also open to the north and occurs within the magnetic low that flanks the northern contact of the large magnetic unit in the northeastern corner of the property. Additional work is recommended to check the sources and extents of these interesting conductors.
50470M 50490F	B B?	17 -	This weak conductor strikes north, from 50490F through 50470M, and beyond the northern survey limit. Resistivity values are the same on all three frequencies, suggesting a probable conductive half-space. Anomaly 50470M, however, may be due to a thin, west-dipping source. This conductive zone is located near the northern contact of the previously described magnetic unit.
50470O 50470P	B? B	- -	These two anomalies give rise to a moderate resistivity low in the extreme NE corner of the block. This zone could continue north and south but high flying precluded an anomalous response on line 50480.
50540C 50560E	B? B?	- -	Anomalies 50540C and 50560E are both very weak, poorly-defined responses of possible bedrock origin.
50580F	D	-	Anomaly 50580F reflects a thin, west-dipping, non-magnetic conductor. Although this conductor exhibits a relatively short strike length, it is considered to be an attractive target that warrants further investigation.
50601C 50601D 50601E	B D B	- - -	Anomaly 50601C is extremely weak, but it is located in close proximity to a magnetic contact. Anomalies 50601D and 50601E, about 500 m to the east, are more conductive, and give rise to a moderate resistivity low.
50620F 50620G 50620H 50620I 50671E	B B B B B	- - - - 24	Anomalies 50620F-I are due to four closely-spaced conductors that form a strong resistivity low that extends south to 50671E. This multi-conductor zone is open to the north. The very attractive resistivity low at 50671E could be due to a combination of two or more conductors, rather than a single thick source. This latter conductor occurs at an estimated depth of about 60 m. The lower resistivities on the low frequency indicate an increase in conductance at depth. This anomaly yields weak magnetic correlation, but it is located in a

Anomaly	Type	Mag	Comments
			moderately flat magnetic area between an anomalous high to the west and a very strong magnetic low about 1 km to the east, in the Iskut River valley. It is recommended that additional work be carried out in order to determine the causative source of this attractive target. The northern extent of the multi-conductor zone should also be determined.
50671F	D	-	Anomaly 50671F reflects a thin source with a probable dip to the east. It is located near the western contact of the strong magnetic low that is associated with the Iskut River.
50721D 50770A 50770G 50770I 50820F	H H H H H	12 - - - 33	These anomalies are typical of the broad parallel responses that are observed over the deep, flat-lying conductive unit that underlies the western portion of the Iskut River valley. Three of these correlate with magnetic highs, while 50770G coincides with a relative magnetic low. Anomalies 50770E and 50770F occur on the flanks of a magnetite-rich unit that yields a resistivity high. Anomaly 50820F reflects a more conductive zone in the centre of the valley.
50760P 50820I	B D	13 13	This weakly magnetic thin source is part of a moderate resistivity low that strikes SE, through 50820I. The resistivity low is part of a discontinuous 4 km-long trend that crosses the Iskut River valley.
50770K	B	-	Anomaly 50770K occurs at the north end of a south-trending conductor with a strike length of about 750 m. At least two of the anomalies comprising this trend suggest a non-magnetic, thin, east-dipping source. Anomaly 50770K is the most conductive portion and it occurs in close proximity to a probable NE-trending faulted contact that can be inferred from the magnetic data.
50760R 50780T 50830L 50851E	H B B H	- - 30 -	The anomalies in this group reflect the more conductive portions of a prominent resistivity low that is open to the north. This multi-conductor zone hosts at least six separate sources on line 50820, most of which indicate thin conductors with probable dips to the east. Resistivities of less than 2 ohm-m are observed at 50830L, which yields a magnetic correlation of 30 nT. Pyrrhotite is considered to be a likely contributing factor, although similar results could result from placer magnetite over conductive (graphitic) shales. Anomaly 50750P, at the northern end of the open resistivity low,

Anomaly	Type	Mag	Comments
			may be associated with a SE-trending fault that can be inferred from the magnetic data.
50902A 50902B	H B	- -	Both of these anomalies give rise to moderate resistivity lows of limited dimensions. Anomaly 50902A is probably due to a surficial source. However, anomaly 50902B, although of low amplitude, yields a much stronger resistivity low. The coaxial peak offset suggests a probable dip to the east. This small conductor is associated with a SSE-trending magnetic low.
51042E	H	-	This very low amplitude response could be due to surficial material, but the 900 Hz suggests a probable increase in conductivity with depth.
51131A	B?	-	This anomaly yields a moderate resistivity low near the southeastern contact of a magnetic unit.

Central Area (Lines 51600-52030)

Magnetic units strike SSE from fiducials 4160, 4190 and 3965 on line 51850. The latter zone exhibits a change in strike at line 51750, where it swings ENE to tie line 49135, and then SE and east, parallel to line 51760. At tie line 49165 the zone bifurcates, with one limb trending SSE and the other NE. A separate magnetic high is observed near the eastern end of lines 51690 to 51770.

The main arcuate east-west magnetic trend is flanked on the north by a prominent magnetic low that extends from fiducial 3945 to fiducial 3600 on line 51650.

With the exception of a weak east-west trending resistivity low through 51750E, there is very little correlation between magnetic patterns and resistivity patterns. The two main resistivity lows in this block strike roughly south, and are associated with units of relatively low magnetic susceptibility.

The main resistivity low extends south from an inferred SW-trending break at 51790C to 51960A, at the northwestern edge of an ice field. A single discrete bedrock conductor, 51950D, is evident at the southeastern edge of the ice field. However, on line 51960, the 900 Hz resistivity indicates a flat-dipping source at a depth of more than 120 m that continues beneath the ice field.

This multi-conductor zone hosts at least six separate sources on line 51920. Both magnetic and non-magnetic units occur within this large resistivity low, as evidenced by the sharp dipolar feature between 51920B and 51920D.

The second resistivity low on this block is a south-trending feature that extends from 51800F to 52030D, a distance of more than 3.3 km. Most of the anomalous responses comprising this trend suggest a moderately conductive source near surface. However, there are a few anomalies that yield direct magnetic correlation and at least four others that suggest the presence of a discrete source within this moderately wide unit.

Anomaly 51830E, for example, is probably due to surficial cover, but it yields a large amplitude response at the high frequency. Anomalies 51930F and 51940E are weakly magnetic and both indicate a possible thin source.

Gaps in resistivity coverage are evident between tie lines 49125 and 49135, from line 51810 to 51920. Severe topography also precluded data acquisition on the western half of line 52010 and the central segments of lines 52020 and 52030.

<u>South Areas (Lines 52040-63170)</u>

The Unuk River diagonally bisects this survey area from the southwest corner to the eastern end of line 52440, where it bifurcates into north- and SSE-trending limbs. A prominent resistivity low follows the main valley, with other more subtle lows evident on some of the tributaries and feeder creeks. Most of these lows are attributed to conductive alluvium, although some of the thin sources could be due to fault zones within the creeks and valleys.

In addition to the valley-hosted conductive zones, there are several others that are due to bedrock sources. Some of these occur on higher ground. The following table lists anomalous responses that are contained within some of the stronger resistivity lows and which are considered to be due to probable bedrock sources.

Anomaly	Type	Mag	Comments
52040C 52040D 52070H 52110F 52160B	D B D D D	- - 20 18 -	Anomalies 52040C and 52040D are part of a south-trending resistivity low on the western flank of a magnetic unit. The thin source at 52070H yields an apparent magnetic correlation, but actually appears to be associated with a weak non-magnetic core within the magnetic unit to the east. Anomalies 52110F and 52160B both indicate thin sources that are parts of the two (magnetic and non-magnetic) resistivity lows.

Anomaly	Type	Mag	Comments
52240E 52240F 52240G 52240H 52280C	H H B D H	- - - - -	Anomalies 52240G and H reflect thin, west-dipping conductors about 180 m apart. They are part of a common resistivity low, and are located between two weak, plug-like magnetic highs. The western magnetic anomaly is also quite conductive, as evidenced by the broad anomaly at 52280C. Anomaly 52240E also reflects a broad source near the northern portion of the magnetic high, while 52240F suggests the presence of a broad, buried conductive unit that connects 52240E and 52240G.
52250A	B?	-	The weak resistivity low at the western end of lines 52220 to 52250 could be due to surficial cover. However, anomaly 52250A suggests a discrete, thin source near a magnetic contact.
52290B 50300B	D B	- -	A thin, west-dipping bedrock conductor, with a strike extent of about 200 m, gives rise to a strong oblate resistivity low that straddles King Creek. The magnetic signatures associated with these two anomalies are quite different. Anomaly 52290B, in King Creek, is relatively non-magnetic, while 52300B is associated with a sharp magnetic low, south of the creek. The magnetic low is located near the eastern end of a prominent low that flanks the strong magnetic high that strikes WNW along the northern edge of King Creek. This magnetic unit yields a high of more than 59,860 nT on line 52300 at tie line 49165. This conductor is considered to be a very attractive target, even though it appears to be due to a thin source. The 900 Hz resistivity on line 52300 suggests that this west-dipping source exhibits an increase in conductance with depth.
52320C 52380D 52420H 52500M	B B H H	- - - -	Anomaly 52320C reflects a thin source with a probable dip to the east. It is part of a large conductive zone that strikes SSW across King Creek to 52580F, where it approaches the western edge of a similar, sub-parallel resistivity low that strikes SW, along the western side of the Iskut River valley. This formational unit does not host any prominent magnetic anomalies, although there is a weak, south-trending magnetic unit near 52391D. Slight increases in conductivity at 52420H and at 52500M are both associated with topographic lows.
52410A 52410E 52440C	D D D	32 21 -	Strong resistivity lows occur on the west, south and east flanks of a ridge of high ground centered near fiducial 3870 on line 52450. These multi-conductor zones

Anomaly	Type	Mag	Comments
52440D 52450B 52490C 52500E 52560C 52580E 52600D	D D B D D H B	124 23 75 - - 78 132	extend south to line 52643 past Fewright Creek which strikes east through 52620D. Line 52500 indicates the presence of at least nine separate conductors from the western to the eastern flank of the topographic high, between 52500C and 52500K. The topographic ridge is generally magnetic, although sharp, narrow gradients are observed on the flanks. Most conductors reflect thin sources. The magnetic correlation varies along strike, suggesting that the conductors are not all related to a common causative source. Dips also vary. Conductors on the western flank generally reflect westerly dips, while those on the east, such as 52410E, 52480F and 52510G indicate probable dips to the east. Most of the highly conductive, magnetic zones (52440D and 52600D) are likely due to pyrrhotite, while a few non-magnetic conductors (52440C and 52560C) could be due to graphitic sources. The numerous conductors comprising this complex, U-shaped resistivity low should be investigated in order to determine their causative sources. The most conductive portions are in the vicinity of 52500E and 52580E. The latter is a moderately wide source near a magnetic contact. A large (2.5km X 3.7km) ring-like structure can be inferred from the vertical gradient data. This feature could reflect the presence of a large oval-shaped intrusive.
52580A 52590A 52600A 52670A	S? B D B?	39 - - -	Anomaly 52580A is a quadrature only response located on the western contact of a strong magnetic high, with an estimated magnetite content of more than 11.5%. This anomaly, and 52590A and 52600A to the south, all indicate a thin, weakly conductive source. Anomaly 52670A is a stronger response, about 900 m to the south, that appears to be related to the same magnetic contact.
52470O 52500O 52611D	B? B? H	19 - -	These conductors are part of a SW-trending resistivity low, with a strike length of more than 3 km. They are associated with two separate SSW and SSE-trending magnetic lows. Most of the anomalies comprising this 3km-long SSW-trending conductive zone reflect moderately broad, buried sources. This formational unit merges with a similar feature near line 52600, near the northern edge of the Unuk River valley.
52580I 52620J	B D	- -	A moderately strong conductor, with a strike length of about 700 m, strikes SW from 52580I to 52620J. The

Anomaly	Type	Mag	Comments
			magnetic correlation is variable along strike. Anomaly 52580I correlates with the eastern edge of a magnetic high. The northern extent of the conductor may be truncated by a prominent linear magnetic low that strikes NNW from fiducial 4200 on this line. At 52600L, the conductor is associated with a circular magnetic low on the south flank of the magnetic unit at 52590J. The relatively low amplitudes, but apparent lower resistivities on the 900 Hz, suggest that this zone might be more conductive at depth.
52590I	D	94	The strong, small, circular resistivity low at 52590I has been attributed to a short, thin magnetic conductor with considerable depth extent. Although this source is probably less than 200 m in length, it is still considered to be a moderately attractive target. Pyrrhotite is considered to be a contributing factor.
52600M	B	-	A short, strong conductor, at a depth of about 50 m, occurs at 52600M. This thin, west-dipping source occurs on the western flank of a SSE-trending magnetic unit.
52580J 52680C 52710I 52800G 52850D	D D B D B?	1499 - - 124 -	Anomaly 52580J defines the north end of a very strong, thin conductor that is open to the north. This strong SSE-trending zone extends south to 52710I, about 500 m west of the South Unuk River. The anomalies comprising this >2.2 km-long conductor generally reflect east-dipping sources. The strong magnetic correlation at 52580J is likely due to pyrrhotite, but definitely warrants further investigation to determine its cause and its northern extent. A second parallel source is indicated on some lines, in close proximity to the eastern contact of the magnetic unit. The zone becomes much less conductive south of line 52611, but reappears as a strong, clearly-defined thin conductor from 52650D to 52680C. Anomaly 52710I is a probable southward continuation of the same conductor. It is also possible that the magnetic anomalies at 52800G and 52810C, and perhaps 52850D, could be associated with the same structure, as they also occur on a similarly sharp magnetic gradient.
52611L 52643O	B D	- -	A highly conductive unit, which is open to the north, strikes SSE from 52580M to 52661H. This broad, multi-conductor unit occurs on the west-facing slope of Mount Madge, east of the South Unuk River valley. This unit is

Anomaly	Type	Mag	Comments
			non-magnetic, but occurs near the western contact of a moderately strong magnetic high. The magnetic unit and the north-flanking conductive zone appear to be truncated by a SW-trending break that is associated with a (fault-controlled?) creek. The 300 m-wide resistivity low on line 52590 might actually comprise two or more conductors, although the patterns tend to suggest a single broad source with moderately conductive edges. The estimated depths are generally in the order of 30 m or more. On line 52643, four distinct conductors are indicated on the 5500 coaxial channel within a distance of 300 m. Three of the four are non-magnetic, with 52643O yielding a low frequency resistivity of less than 10 ohm-m, at a relatively shallow depth of about 12 m. Additional work is recommended in this area, although graphite is considered to be a likely cause.
52580O 52600S	D D	- 21	This thin, poorly conductive source does not yield a resistivity low, except at the highest frequency. Only three lines extended far enough to the east to detect this conductor, and it remains open to the north and south. This weak source is not within a valley, but is associated with a very weak magnetic gradient, and is possibly due to a poorly conductive faulted contact.
52611M 52611N	H D	31 -	A thin, west-dipping conductor coincides with a very sharp magnetic low at 52611N. The small coincident resistivity low extends west, to include 52611M. This anomaly could be due to a separate deeper source, but it is possibly a down-dip continuation of 52611N. There is a moderately strong potassium high to the south, near the eastern end of line 52620 and 52643.
52720F 52730D 52740F	E H B	- - 1252	These three anomalies combine to form a very attractive oblate resistivity low that coincides closely with the northwestern contact of a strong dipolar magnetic anomaly. The effects of magnetite are evident at the contact-related 52720F. Resistivities of less than 50 ohm-m are evident at 52730D, while even stronger conductivity is seen on the 900 Hz at 52740F. The latter suggests a possible west-dipping source, but the anomaly shapes have been affected by excessive flying heights on all three lines. Although this zone yields an apparent strike length of about 300 m, it is possible that it continues farther south (through the resistivity gap)

Anomaly	Type	Mag	Comments
			beyond line 52750. Although this is in an area of moderately steep terrain, it is considered to be a very attractive target that should be subjected to further investigation. The conductor is located on the eastern side of a steep SSE-trending ravine.
52740B 52780C	D B?	37 -	The weak resistivity low that is sub-parallel to tie line 49150, between lines 52661 and 52950, hosts a few discrete EM responses along its 4.5 km strike length that suggest thin bedrock sources. The main axis of this conductive feature correlates with a SSE-trending contact that crosses the tie line at a very shallow angle. The thin source at 52740B yields magnetic correlation while the stronger response at 52780C does not. There is a very subtle potassium high near 52740B.
52780E 52790E 52860C 52900D 52930D 52980A	H H H H H H	27 - - 12 - 69	These anomalies are all part of the broad resistivity low that is associated with the SW-trending Unuk River valley. While most of the anomalies comprising this conductive zone reflect a broad, flat-lying unit, there are a few that suggest possible discrete sources or concentrations of more conductive material. Anomaly 52780E, for example, shows a marked increase in conductivity at depth. Anomaly 52860C exhibits a similar increase in conductivity at depth, but suggests a flat, east-dipping source. Anomalies 52900D and 52930D are also more conductive at the deeper 900 Hz frequency, while the latter correlates with a strong magnetic low. Anomaly 52980A is much broader and deeper, but overlies a highly complex magnetic unit that strikes southwest from this point.
52830F 52880H 52900E	B D D	- - -	The anomalies in this group form part of a SW-trending resistivity low that is evident along the eastern flank of a SSW-trending magnetic unit. The anomalies occur on a west-facing slope and have been attributed to bedrock sources, rather than surficial cover. The overall length of the conductive unit is about 1.5 km. On line 52820 the magnetic unit exhibits a magnetite content of about 5.4% at fiducial 3600. Anomaly 52830F suggests a thin source with weaker conductors to the east and west. Anomalies 52870G and 52880H also reflect thin sources with a probable dip to the east. Anomalies 52900E and 52900F are separated by about 100 m, and 52900E is located in close proximity to the eastern contact of the strong magnetic unit. This is the most conductive portion

Anomaly	Type	Mag	Comments
			of the low resistivity zone. The strong plug-like magnetic high near fiducial 1750 on line 52950 is non-conductive.
53030B	D	-	Anomaly 53030B gives rise to a moderately strong, SW-trending resistivity low that correlates with a weak potassium high. The conductive zone follows an arcuate magnetic low that merges with the eastern portion of a sinusoidal magnetic low that surrounds the large, complex magnetic unit in the southwestern quadrant of sheet 5. Any conductors that are associated with this zone of structural deformation are considered to be of interest. Anomaly 53030B is located on the western side of a small creek valley. The low amplitude anomaly on the adjacent line at 53020B is probably due to excessive flying height over the valley. Anomaly 53030B suggests a thin, non-magnetic source with a near-vertical dip that should be subjected to further investigation.
53090A 53190A	H H	611 -	A strong, broad resistivity low follows a 2.2 km-long segment of Third Canyon, along the eastern side of the Unuk River valley. Anomalies 53090A and 53190A are typical of the responses that comprise this moderately deep conductive zone. North of line 53200, most anomalies yield direct magnetic correlation, while those to the south are non-magnetic. The calculated depths to the top of this buried conductive zone vary considerably. At 53090A, a depth of 75 m is indicated, with resistivity values of less than 4 ohm-m at the low frequency. Similar results are evident towards 53200A, beyond which the zone becomes non-magnetic and closer to surface. The differences between 53200A and 53210A may be indicative of a facies change or a completely different underlying lithology. It is considered unlikely that the highly conductive and magnetic responses such as that observed at 53090A could be due to non-bedrock sources. Therefore, it is recommenced that further investigation be carried out to determine the causative source of this very large conductive zone. Graphite could be a contributing factor to the high conductivity, but the coincident magnetic anomaly indicates the presence of magnetic material, such as pyrrhotite.
53180D 53240B 53240C	B D D	- - -	A discontinuous resistivity low extends in a SSE direction from 53160B to 53260C, with an apparent strike extent of about 1.8 km. The vertical gradient map

Anomaly	Type	Mag	Comments
53250C 53250D 53260C	D D B	- - -	suggests the presence of a SSE-trending linear break along the central axis of this discontinuous conductive trend. EM anomaly characteristics differ along strike. Anomaly 53180D, associated with the eastern contact of a magnetic unit, suggests a probable thin source, as does 53220E. Anomalies 53240B and 53240C reflect two thin sources separated by less than 50 m These are also in close proximity to the eastern contact of the magnetic unit. Three possible sources are suggested on line 53250. These occur at an apparent depth of about 60 m, and are contained within a relatively non-magnetic unit. A weak resistivity low on the 56 kHz map extends WSW from 53260C, along a linear magnetic low towards Boulder Creek.
63100D 63170F	D B?	22 -	An incomplete resistivity low that is open to the north, east and south is evident near the eastern ends of lines 63100-63160. Most of these responses indicate a weakly conductive half-space that is associated with a SSE-trending magnetic low. Anomaly 63100D, however, suggests a poorly conductive thin source, with a probable dip to the west. Anomaly 63160E yields a distinct resistivity low of unknown dimensions.
63110C	B?	-	A weak resistivity low strikes SSE through 63110C. This trend is coincident with a similar SSE-trending magnetic low, and is located about 1.2 km east of the South Unuk River. Most of the anomalies comprising this weakly conductive zone suggest a moderately broad source quite close to surface.
63130A 63130B	S S?	37 108	Two weak resistivity lows strike south and SSE, through 63130A and 63130B, respectively. These are both associated with creeks (Gracey Creek and South Unuk River) and are likely due to conductive alluvium. However, both conductive trends yield partial magnetic correlation along strike, indicating a possible bedrock component.

In addition to the conductive zones described in the foregoing pages, there are several other highly conductive to weak or poorly defined responses that might be of interest.

There are several areas where negative in-phase responses indicate increases in magnetite content. In some cases, these correlate with positive quadrature responses, denoting subtle increases in conductance. Some of these negative in-phase/positive quadrature anomalies could reflect weakly mineralized skarns. A few anomalies in this category would include 53290D,F,G, and H, 51970A, 51720E, 51710B, 51670C, 51180B, 51130B, 51060B, 51042A,B and C, 51020D, 50470E, 50330A, 50250B, 50240C, 40550A, 40340A, 40321B, 40200A, 40200C, and 40070A.

Phase 2007

The maps that accompany this report include all of the data from the combined 2006-2007 flying. Although the EM anomaly maps contain all the 2006 and 2007 anomalies, they only show the conductor axes that were defined in 2007. The following text describes some of the more attractive geophysical responses from the recent 2007 flying.

Map Sheets 3 & 4

Lines 51320 to 51641 were flown in 2007. This area hosts two main zones of moderately low resistivity, both of which are associated with Snippaker Creek.

The anomalies comprising the north zone, from 51320 A to 51360 A, indicate a moderately broad half-space, buried at a depth of up to 60 m. This conductive unit is associated with the same strong magnetic trend that follows the creek, and also hosts a second conductive zone from 51530 B through 51641 A. Most of the anomalies in the northern zone appear to be associated with the eastern contact of the sinuous magnetic unit while those in the south yield direct magnetic correlation.

In addition to these two main valley-hosted resistivity lows, there are at least three other weaker conductors of possibly bedrock origin. Anomaly 51370 B could be surficial, but it occurs on relatively high ground and is associated with a strong local magnetic high on the western flank of a prominent, south-trending linear magnetic low.

Anomalies 51550 A and 51550 B also correlate with sharp magnetic highs, with the former yielding an estimated magnetite content of about 13 %. Both occur on high ground. Anomaly 51550 B is on, or in close proximity to, a SSE trending magnetic contact that continues to the south over a distance of more than 5 km.

Map Sheets 5 & 6

The 2007 flying in the central area included lines 52051 to 52211 and 52941 to 53001 on Sheet 5, and lines 52762 to 52792 and 62861 to 63090 on Sheet 6.

Several strong discrete bedrock conductors are evident in the western portion of the first block. Anomalies 52071 A to 52121 A occur at the west end of the survey lines and their responses are not completely resolved. However, most anomalies suggest a moderately thin, west-dipping source of high conductance that is associated with an extremely weak south-trending magnetic anomaly. This attractive conductor remains open to the north and west.

The resistivity low that hosts this conductor continues south, where it hosts up to four separate conductors on line 52181. The southern portion of this multi-conductor unit is associated with a unit of relatively low magnetic susceptibility. Although the general strike in the area appears to be SSE, the vertical gradient maps suggests the presence of two possible parallel faults that strike southwest, near 52161 B and 52181 A. The complex structure in this area precludes correlation of anomalies between lines 52151 and 52211, but tends to increase the significance of the conductors in this area.

A moderately strong resistivity low, centered near 52111 E, hosts a probable thin east-dipping conductor with a strike length of about 500 m. The central, more conductive portion of this feature exhibits weak magnetic correlation, but the main conductor axis appears to lie in close proximity to a south trending contact, with a prominent low on the eastern flank of a broad weak magnetic unit. Additional work is recommended to check the causative source of the conductor near 52111 E.

The 7- line block from 52941 to 53001 hosts a weak arcuate resistivity low that follows the Canyon Creek valley. This valley may have incised the S to SSE-trending magnetic units, as they appear to terminate at Canyon Creek. However there is a lobe of magnetic material that follows the valley, ENE from 52920 A, which might be indicative of fracture filling. Anomalies 52941 A, 52951 A, 52961 A and 52961 B, all suggest a broad weak poorly-defined conductive layer near surface. All yield magnetic correlation, with the exception of 52961 B, but this could be coincidental, rather than direct.

Anomalies 52971 B and 52981 B follow a crest of high ground that is magnetic. Both magnetite-hosted anomalies are extremely weak. The lack of a resistivity low is attributed to the increased magnetite content, estimated to be about 6.0% at 52971 B.

The 2007 infill area on Sheet 6, between lines 62861 and 63090, hosts five distinct resistivity lows, four of which contain one or more bedrock conductors.

Anomaly 62861 B consists of a moderately strong, isolated anomaly, that indicates a thin, short bedrock conductor with a probably dip to the west. This conductor is associated with a subtle, S-trending magnetic anomaly and yields a magnetic correlation of 17 nT. Additional investigation is recommended, although this conductor appears to be of limited strike extent.

The main resistivity low that follows the South Unuk River shows an increase in conductivity near anomaly 62871 D. This broad source appears to be close to surface (alluvial cover?) but the effects of magnetite may have yielded erroneous depth estimates. This anomaly suggests a slight increase in conductivity beneath the river.

Anomaly 62890C is a very weak magnetite-hosted response that is associated with the eastern contact of a linear magnetic trend, which strikes SSE onto Sheet 8.

Anomaly 62890 A reflects a thin, contact-related conductor with a probable steep dip to the west. This is part of a 650m–long conductive trend that parallels the topographic elevation contours along a west-facing slope. The conductor follows a strong, moderately narrow magnetic unit that strikes south to line 63040, where it is folded or offset to the east before continuing SSE onto Sheet 8. The magnetic band also appears to be interrupted or offset by a NE trending break near fiducial 3270 on line 62940.

There is another SSE-trending resistivity low to the east, through 63000 E. Most of the anomalies comprising this zone suggest probable surficial conductivity. However, anomaly 63000 E exhibits a magnetic correlation of 391 nT.

In the southeastern corner of Sheet 6, there is a moderately attractive resistivity low that hosts anomalies 63060 I and 63060 J. These two parallel thin sources are separated by about 170 m. The former, 63060 I, occurs near the centre of a prominent magnetic low, and is part of the same unit that hosts 63050 H. The latter conductor, 63050 J, occurs near the eastern contact of the magnetic low, and is probably a southward continuation of 63040 G, which has also been attributed to a weakly conductive thin source along the same contact.

South Area – Sheets 7 & 8

The 2007 flying detected only three additional bedrock conductors on Sheet 7 and six or seven zones on Sheet 8.

Anomaly 63360 E is associated with a sharp magnetic high and is part of an extremely weak series of anomalies that strike SSW. Most anomalies comprising this trend suggest possible surficial sources. However, many yield direct magnetic correlation and they do not appear to be associated with creeks or alluvial filled valleys. This 1.5 km–long trend is located on an east-facing slope, parallel to the topographic contours. Because of the magnetite association, a weak resistivity low is evident on the high frequency (56,000 Hz) resistivity map only. This very weak conductor is near the western contact of the broad magnetic low that follows the Gracey Creek valley. Anomaly 63360 D suggests a thin, east-dipping, magnetite-hosted source with a direct magnetic correlation of 332 nT.

Anomaly 63380 C occurs on the southern edge of an ENE-trending resistivity low that follows Boulder Creek. This thin, north-dipping source is associated with a well-defined non-magnetic unit. The 900 Hz resistivity suggests an increase in conductivity with depth in the down-dip (north) direction. Other anomalies in the general area have been given an “H” interpretive symbol, denoting a broad, buried, conductive unit. The apparent width of these anomalies may be partially due to the shallow angle of the intersection with the survey lines.

Anomaly 63480 D is located on a ridge of high ground, just east of the South Unuk River valley. This single-line response is non-magnetic, near the eastern contact of a moderately strong, SSW- trending magnetic unit along the east side of the valley. The conductor gives rise to a moderately strong, isolated resistivity low, and appears to reflect a probable thin, east-dipping source. This is considered to be a moderately attractive conductor although it appears to be of limited strike length.

A prominent resistivity low follows the South Unuk River valley to line 63780. Although there are several anomalous zones along this trend, most of the anomalies reflect broad surficial or buried half-space type responses. However, many of these responses yield direct magnetic correlation within what appears to be a relatively non-magnetic host. In addition to these, there are several zones that appear to be due to more discrete anomalies of possible bedrock origin.

Anomalies 63220 B and 63230 B, for example, both yield magnetic correlation. This weak magnetite-associated conductor suggests a probable dip to the southwest, but resides within or beneath the South Unuk River.

The resistivity low bifurcates in the vicinity of line 63650, where as many as three possible bedrock sources are evident from 63650 A to 63650 C and 60660 A. Anomalies 63650 A to 63650 C are very weak, but 60550 B indicates a moderately, strong, thin, east-dipping conductor near the western contact of weak narrow magnetic unit. Anomaly 63660 A appears to be associated with the same contact, but is magnetite-hosted, and suggests a dip towards the west, opposite to the east dip indicated by 63650 B. These two anomalies could be offset portions of the same conductor, although the resistivity contours tend to suggest two distinctive lows.

Anomalies 63750 A, 63760 C and 63770 A, are located about 1.8 km SSW, along the same river valley. These three anomalies give rise to a moderately strong resistivity low. Two of the three yield weak magnetic correlation. The strongest response is at 63760 C, where a resistivity low of less than 65 ohm-m is observed on the low frequency. This moderately thick conductor is associated with a small, but distinct magnetic gradient, although the anomaly itself is non-magnetic. This response is located in the South Iskut River valley, but is considered to be a potential area for further work, in order to determine its source.

In the north-central portion of Sheet 8, between 63190C and 63260E, there is a strong SE-trending resistivity low that correlates closely with a similarly shaped magnetic low. This attractive resistivity low appears to terminate at the central axis of the east-trending Divelbliss Creek valley, but the magnetic patterns suggest a possible continuation towards the southeast, along the southwestern flank of an icefield.

This resistivity low hosts one or two parallel, thin sources, which generally indicate dips to the southwest. All anomalies are non-magnetic with the possible exception of 63190 D. Additional work is recommended in order to determine the causative source of the thin SW-dipping bedrock conductors near 63210 C and 63220 G, and near the inferred break at 60250 G.

Anomaly 63370 K is a short, weak, quadrature response in a south-trending magnetic low. This very weak response does not appear to be associated with a creek or alluvial cover, and could reflect a weakly conductive thin source of limited strike length.

In the western portion of line 63560, there are two thin conductors. Anomaly 63560 C yields a moderate resistivity low near the northern contact of a prominent ESE-trending magnetic low. This anomaly suggests a probable NE dip. Anomaly 63560 D, about 1 km to the east, consists of an extremely weak quadrature response that is associated with a moderately strong magnetic unit. This anomaly does not yield a resistivity low because of the magnetite suppression. The poorly defined quadrature response makes this a relatively low priority target.

Anomalies 63970 C and 64020 D are weak, single-line responses that suggest possible thin sources in the southeastern corner of the survey block. Both are non-magnetic. A subtle SW-trending break can be inferred from the magnetic data in the vicinity of 63970 C. The weak resistivity low at 64010 B has been attributed to a possible surficial source, but it too is magnetite-hosted.

8. CONCLUSIONS AND RECOMMENDATIONS

This report provides a very brief description of the survey results and describes the equipment, data processing procedures and logistics of the 2006 and 2007 surveys over Blocks 4, 5 and 6 in the Eskay Creek area.

There are more than 530 anomalies in the survey blocks that are typical of graphitic or massive sulphide responses. The survey was also successful in locating several moderately weak or broad conductors that may also warrant additional work. The various maps included with this report display the magnetic, radiometric, and conductive properties of the survey areas. It is recommended that a complete assessment and detailed evaluation of the survey results be carried out, in conjunction with all available geophysical, geological and geochemical information. Particular reference should be made to the multi-parameter data profiles that clearly define the characteristics of the individual anomalies.

Anomalies in the area vary from strong to moderately weak or poorly defined. Many of these have been attributed to conductive overburden, buried conductive layers, or deep weathering. Others coincide with magnetite-rich rock units and could be due to skarn-type mineralization. A few of the more discrete sources appear to be in close proximity to magnetic gradients that could reflect contacts, faults or shears. Such structural breaks are considered to be of particular interest as they may have influenced mineral deposition within the survey areas.

The results of the radiometric survey show several anomalous areas. Although most of these have been attributed to changes in rock types, there are others that could be at least partially caused by variations in survey height. It is recommended that radiometric ratio calculations be carried out in order to minimize any amplitude changes due to sensor heights, or changes in the overburden thickness or moisture content. Radioelement ratio maps should help to map near surface lithology and also locate zones of potassic alteration.

The interpreted bedrock conductors and anomalous targets defined by the survey should be subjected to further investigation, using appropriate surface exploration techniques. Anomalies that are currently considered to be of moderately low priority may require upgrading if follow-up results are favourable.

It is also recommended that additional processing of existing geophysical data be considered, in order to extract the maximum amount of information from the survey results. Current software and imaging techniques often provide valuable information on structure and lithology, which may not be clearly evident on the contour and colour maps. These techniques can yield images that define subtle, but significant, structural details.

Respectfully submitted,

FUGRO AIRBORNE SURVEYS CORP.

APPENDIX A

LIST OF PERSONNEL (2006)

The following personnel were involved in the acquisition, processing, interpretation and presentation of data, relating to a DIGHEM airborne geophysical survey carried out for Hathor Exploration Ltd., in the Eskay Creek Area, northwestern British Columbia.

David Miles	Manager, Helicopter Operations
Emily Farquhar	Manager, Data Processing and Interpretation
Andy Semple	Geophysical Operator
Anton Bogatyrov	Geophysical Operator
Delvin Masilamani	Geophysical Operator
John Douglas	Geophysical Operator
Amir Soltanzadeh	Field Geophysicist
Jeff Flemmng	Field Geophysicist
Amanda Heydorn	Field Geophysicist
Greg Charbonneau	Helicopter Pilot
Glen Charbonneau	Helicopter Pilot
Tom McMahon	Helicopter Pilot
Jeremy Chambers	Helicopter Mechanic
J.J. Holmstrom	Helicopter Mechanic
Igor Sram	Geophysical Data Processor
Paul Smith	Interpretation Supervisor
Lyn Vanderstarren	Drafting Supervisor
Susan Pothiah	Word Processing Operator
Albina Tonello	Secretary/Expeditor

The survey consisted of 4295 km of coverage, flown from July 5th to October 12th, 2006.

All personnel are employees of Fugro Airborne Surveys, except for the pilots and engineers who are employees of Great Slave Helicopters Ltd.

- Appendix A.2 -

LIST OF PERSONNEL (2007)

The following personnel were involved in the acquisition, processing, interpretation and presentation of data, relating to a DIGHEM airborne geophysical survey carried out for Hathor Exploration Ltd., in the Eskay Creek Area, northwestern British Columbia.

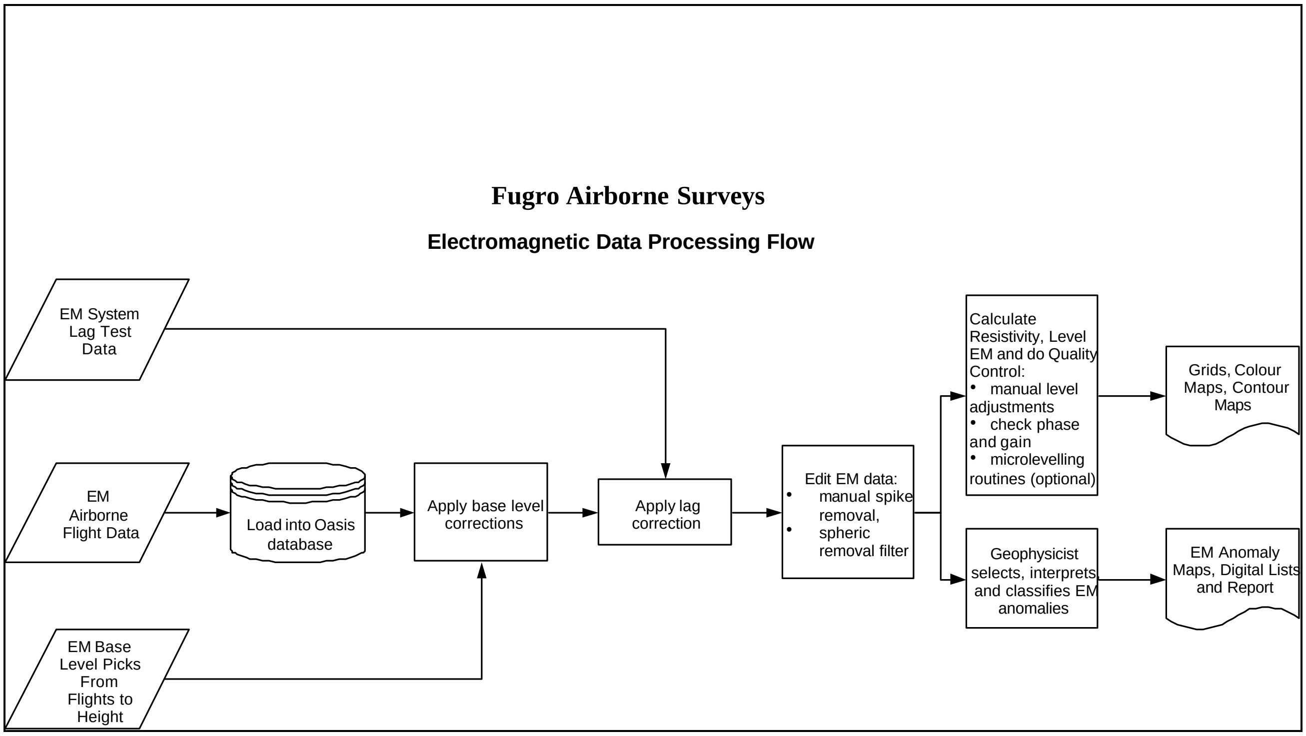
David Miles	Manager, Helicopter Operations
Emily Farquhar	Manager, Data Processing and Interpretation
Delvin Masilamani	Geophysical Operator
Lendl Mendes	Geophysical Operator
Darcy McGill	Field Geophysicist
Dima Amine	Field Geophysicist
Greg Charbonneau	Helicopter Pilot
Al Sweet	Helicopter Pilot
Scott McRae	Helicopter Mechanic
Igor Sram	Geophysical Data Processor/ Interpreter
Paul Smith	Geophysicist/ Interpreter
Lyn Vanderstarren	Drafting Supervisor
Susan Pothiah	Word Processing Operator
Albina Tonello	Secretary/Expeditor

The survey consisted of 1515 km of coverage, flown from July 19th to September 5th, 2007.

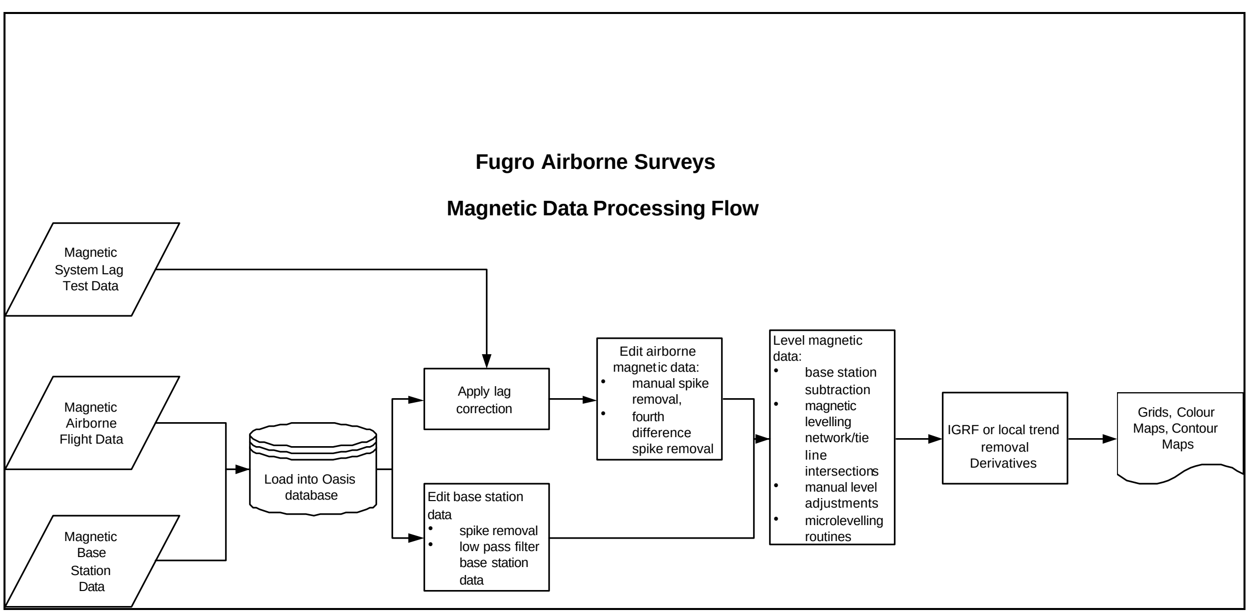
All personnel are employees of Fugro Airborne Surveys, except for the pilots and engineer, who are employees of Great Slave Helicopters Ltd.

APPENDIX B

Processing Flow Chart - Electromagnetic Data



Processing Flow Chart - Magnetic Data



APPENDIX C

BACKGROUND INFORMATION

BACKGROUND INFORMATION

Electromagnetics

Fugro electromagnetic responses fall into two general classes, discrete and broad. The discrete class consists of sharp, well-defined anomalies from discrete conductors such as sulphide lenses and steeply dipping sheets of graphite and sulphides. The broad class consists of wide anomalies from conductors having a large horizontal surface such as flatly dipping graphite or sulphide sheets, saline water-saturated sedimentary formations, conductive overburden and rock, kimberlite pipes and geothermal zones. A vertical conductive slab with a width of 200 m would straddle these two classes.

The vertical sheet (half plane) is the most common model used for the analysis of discrete conductors. All anomalies plotted on the geophysical maps are analyzed according to this model. The following section entitled **Discrete Conductor Analysis** describes this model in detail, including the effect of using it on anomalies caused by broad conductors such as conductive overburden.

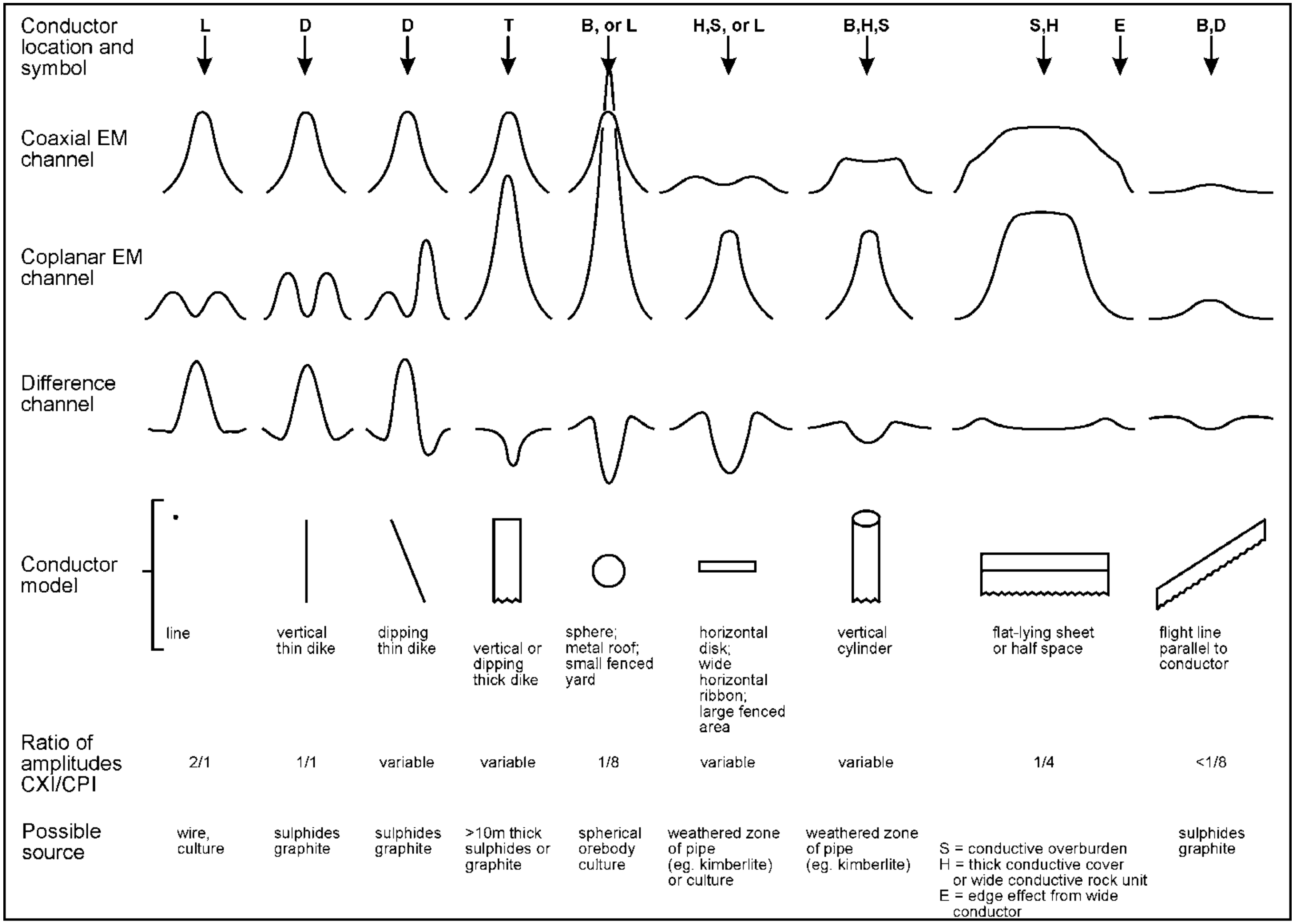
The conductive earth (half-space) model is suitable for broad conductors. Resistivity contour maps result from the use of this model. A later section entitled **Resistivity Mapping** describes the method further, including the effect of using it on anomalies caused by discrete conductors such as sulphide bodies.

Geometric Interpretation

The geophysical interpreter attempts to determine the geometric shape and dip of the conductor. Figure C-1 shows typical HEM anomaly shapes which are used to guide the geometric interpretation.

Discrete Conductor Analysis

The EM anomalies appearing on the electromagnetic map are analyzed by computer to give the conductance (i.e., conductivity-thickness product) in siemens (mhos) of a vertical sheet model. This is done regardless of the interpreted geometric shape of the conductor. This is not an unreasonable procedure, because the computed conductance increases as the electrical quality of the conductor increases, regardless of its true shape. DIGHEM anomalies are divided into seven grades of conductance, as shown in Table C-1. The conductance in siemens (mhos) is the reciprocal of resistance in ohms.



Typical HEM anomaly shapes

Figure C-1

The conductance value is a geological parameter because it is a characteristic of the conductor alone. It generally is independent of frequency, flying height or depth of burial, apart from the averaging over a greater portion of the conductor as height increases. Small anomalies from deeply buried strong conductors are not confused with small anomalies from shallow weak conductors because the former will have larger conductance values.

Table C-1. EM Anomaly Grades

Anomaly Grade	Siemens
7	> 100
6	50 - 100
5	20 - 50
4	10 - 20
3	5 - 10
2	1 - 5
1	< 1

Conductive overburden generally produces broad EM responses which may not be shown as anomalies on the geophysical maps. However, patchy conductive overburden in otherwise resistive areas can yield discrete anomalies with a conductance grade (cf. Table C-1) of 1, 2 or even 3 for conducting clays which have resistivities as low as 50 ohm-m. In areas where ground resistivities are below 10 ohm-m, anomalies caused by weathering variations and similar causes can have any conductance grade. The anomaly shapes from the multiple coils often allow such conductors to be recognized, and these are indicated by the letters S, H, and sometimes E on the geophysical maps (see EM legend on maps).

For bedrock conductors, the higher anomaly grades indicate increasingly higher conductances. Examples: the New Insco copper discovery (Noranda, Canada) yielded a grade 5 anomaly, as did the neighbouring copper-zinc Magusi River ore body; Mattabi (copper-zinc, Sturgeon Lake, Canada) and Whistle (nickel, Sudbury, Canada) gave grade 6; and the Montcalm nickel-copper discovery (Timmins, Canada) yielded a grade 7 anomaly. Graphite and sulphides can span all grades but, in any particular survey area, field work may show that the different grades indicate different types of conductors.

Strong conductors (i.e., grades 6 and 7) are characteristic of massive sulphides or graphite. Moderate conductors (grades 4 and 5) typically reflect graphite or sulphides of a less massive character, while weak bedrock conductors (grades 1 to 3) can signify poorly connected graphite or heavily disseminated sulphides. Grades 1 and 2 conductors may not respond to ground EM equipment using frequencies less than 2000 Hz.

The presence of sphalerite or gangue can result in ore deposits having weak to moderate conductances. As an example, the three million ton lead-zinc deposit of Restigouche Mining Corporation near Bathurst, Canada, yielded a well-defined grade 2 conductor. The 10 percent by volume of sphalerite occurs as a coating around the fine grained massive pyrite, thereby inhibiting electrical conduction. Faults, fractures and shear zones may produce anomalies that typically have low conductances (e.g., grades 1 to 3). Conductive rock formations can yield anomalies of any conductance grade. The conductive materials in such rock formations can be salt water, weathered products such as clays, original depositional clays, and carbonaceous material.

For each interpreted electromagnetic anomaly on the geophysical maps, a letter identifier and an interpretive symbol are plotted beside the EM grade symbol. The horizontal rows of dots, under the interpretive symbol, indicate the anomaly amplitude on the flight record. The vertical column of dots, under the anomaly letter, gives the estimated depth. In areas where anomalies are crowded, the letter identifiers, interpretive symbols and dots may be obliterated. The EM grade symbols, however, will always be discernible, and the obliterated information can be obtained from the anomaly listing appended to this report.

The purpose of indicating the anomaly amplitude by dots is to provide an estimate of the reliability of the conductance calculation. Thus, a conductance value obtained from a large ppm anomaly (3 or 4 dots) will tend to be accurate whereas one obtained from a small ppm anomaly (no dots) could be quite inaccurate. The absence of amplitude dots indicates that the anomaly from the coaxial coil-pair is 5 ppm or less on both the in-phase and quadrature channels. Such small anomalies could reflect a weak conductor at the surface or a stronger conductor at depth. The conductance grade and depth estimate illustrates which of these possibilities fits the recorded data best.

The conductance measurement is considered more reliable than the depth estimate. There are a number of factors that can produce an error in the depth estimate, including the averaging of topographic variations by the altimeter, overlying conductive overburden, and the location and attitude of the conductor relative to the flight line. Conductor location and attitude can provide an erroneous depth estimate because the stronger part of the conductor may be deeper or to one side of the flight line, or because it has a shallow dip. A heavy tree cover can also produce errors in depth estimates. This is because the depth estimate is computed as the distance of bird from conductor, minus the altimeter reading. The altimeter can lock onto the top of a dense forest canopy. This situation yields an erroneously large depth estimate but does not affect the conductance estimate.

Dip symbols are used to indicate the direction of dip of conductors. These symbols are used only when the anomaly shapes are unambiguous, which usually requires a fairly resistive environment.

A further interpretation is presented on the EM map by means of the line-to-line correlation of bedrock anomalies, which is based on a comparison of anomaly shapes on adjacent lines. This provides conductor axes that may define the geological structure over portions of the survey area. The absence of conductor axes in an area implies that anomalies could not be correlated from line to line with reasonable confidence.

The electromagnetic anomalies are designed to provide a correct impression of conductor quality by means of the conductance grade symbols. The symbols can stand alone with geology when planning a follow-up program. The actual conductance values are printed in the attached anomaly list for those who wish quantitative data. The anomaly ppm and depth are indicated by inconspicuous dots which should not distract from the conductor patterns, while being helpful to those who wish this information. The map provides an interpretation of conductors in terms of length, strike and dip, geometric shape, conductance, depth, and thickness. The accuracy is comparable to an interpretation from a high quality ground EM survey having the same line spacing.

The appended EM anomaly list provides a tabulation of anomalies in ppm, conductance, and depth for the vertical sheet model. No conductance or depth estimates are shown for weak anomalous responses that are not of sufficient amplitude to yield reliable calculations.

Since discrete bodies normally are the targets of EM surveys, local base (or zero) levels are used to compute local anomaly amplitudes. This contrasts with the use of true zero levels which are used to compute true EM amplitudes. Local anomaly amplitudes are shown in the EM anomaly list and these are used to compute the vertical sheet parameters of conductance and depth.

Questionable Anomalies

The EM maps may contain anomalous responses that are displayed as asterisks (*). These responses denote weak anomalies of indeterminate conductance, which may reflect one of the following: a weak conductor near the surface, a strong conductor at depth (e.g., 100 to 120 m below surface) or to one side of the flight line, or aerodynamic noise. Those responses that have the appearance of valid bedrock anomalies on the flight profiles are indicated by appropriate interpretive symbols (see EM legend on maps). The others probably do not warrant further investigation unless their locations are of considerable geological interest.

The Thickness Parameter

A comparison of coaxial and coplanar shapes can provide an indication of the thickness of a steeply dipping conductor. The amplitude of the coplanar anomaly (e.g., CPI channel) increases relative to the coaxial anomaly (e.g., CXI) as the apparent thickness increases, i.e., the thickness in the horizontal plane. (The thickness is equal to the conductor width if the conductor dips at 90 degrees and strikes at right angles to the flight line.) This report refers to a conductor as <u>thin</u> when the thickness is likely to be less than 3 m, and <u>thick</u> when in excess of 10 m. Thick conductors are indicated on the EM map by parentheses "(

)". For base metal exploration in steeply dipping geology, thick conductors can be high priority targets because many massive sulphide ore bodies are thick. The system cannot sense the thickness when the strike of the conductor is subparallel to the flight line, when the conductor has a shallow dip, when the anomaly amplitudes are small, or when the resistivity of the environment is below 100 ohm-m.

Resistivity Mapping

Resistivity mapping is useful in areas where broad or flat lying conductive units are of interest. One example of this is the clay alteration which is associated with Carlin-type deposits in the south west United States. The resistivity parameter was able to identify the clay alteration zone over the Cove deposit. The alteration zone appeared as a strong resistivity low on the 900 Hz resistivity parameter. The 7,200 Hz and 56,000 Hz resistivities showed more detail in the covering sediments, and delineated a range front fault. This is typical in many areas of the south west United States, where conductive near surface sediments, which may sometimes be alkalic, attenuate the higher frequencies.

Resistivity mapping has proven successful for locating diatremes in diamond exploration. Weathering products from relatively soft kimberlite pipes produce a resistivity contrast with the unaltered host rock. In many cases weathered kimberlite pipes were associated with thick conductive layers that contrasted with overlying or adjacent relatively thin layers of lake bottom sediments or overburden.

Areas of widespread conductivity are commonly encountered during surveys. These conductive zones may reflect alteration zones, shallow-dipping sulphide or graphite-rich units, saline ground water, or conductive overburden. In such areas, EM amplitude changes can be generated by decreases of only 5 m in survey altitude, as well as by increases in conductivity. The typical flight record in conductive areas is characterized by in-phase and quadrature channels that are continuously active. Local EM peaks reflect either increases in conductivity of the earth or decreases in survey altitude. For such conductive areas, apparent resistivity profiles and contour maps are necessary for the correct interpretation of the airborne data. The advantage of the resistivity parameter is that anomalies caused by altitude changes are virtually eliminated, so the resistivity data reflect only those anomalies caused by conductivity changes. The resistivity analysis also helps the interpreter to differentiate between conductive bedrock and conductive overburden. For example, discrete conductors will generally appear as narrow lows on the contour map and broad conductors (e.g., overburden) will appear as wide lows.

The apparent resistivity is calculated using the pseudo-layer (or buried) half-space model defined by Fraser (1978)[7]. This model consists of a resistive layer overlying a conductive

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[7] Resistivity mapping with an airborne multicoil electromagnetic system: Geophysics, v. 43, p.144-172

half-space. The depth channels give the apparent depth below surface of the conductive material. The apparent depth is simply the apparent thickness of the overlying resistive layer. The apparent depth (or thickness) parameter will be positive when the upper layer is more resistive than the underlying material, in which case the apparent depth may be quite close to the true depth.

The apparent depth will be negative when the upper layer is more conductive than the underlying material, and will be zero when a homogeneous half-space exists. The apparent depth parameter must be interpreted cautiously because it will contain any errors that might exist in the measured altitude of the EM bird (e.g., as caused by a dense tree cover). The inputs to the resistivity algorithm are the in-phase and quadrature components of the coplanar coil-pair. The outputs are the apparent resistivity of the conductive half-space (the source) and the sensor-source distance. The flying height is not an input variable, and the output resistivity and sensor-source distance are independent of the flying height when the conductivity of the measured material is sufficient to yield significant in-phase as well as quadrature responses. The apparent depth, discussed above, is simply the sensor-source distance minus the measured altitude or flying height. Consequently, errors in the measured altitude will affect the apparent depth parameter but not the apparent resistivity parameter.

The apparent depth parameter is a useful indicator of simple layering in areas lacking a heavy tree cover. Depth information has been used for permafrost mapping, where positive apparent depths were used as a measure of permafrost thickness. However, little quantitative use has been made of negative apparent depths because the absolute value of the negative depth is not a measure of the thickness of the conductive upper layer and, therefore, is not meaningful physically. Qualitatively, a negative apparent depth estimate usually shows that the EM anomaly is caused by conductive overburden. Consequently, the apparent depth channel can be of significant help in distinguishing between overburden and bedrock conductors.

Interpretation in Conductive Environments

Environments having low background resistivities (e.g., below 30 ohm-m for a 900 Hz system) yield very large responses from the conductive ground. This usually prohibits the recognition of discrete bedrock conductors. However, Fugro data processing techniques produce three parameters that contribute significantly to the recognition of bedrock conductors in conductive environments. These are the in-phase and quadrature difference channels (DIFI and DIFQ, which are available only on systems with "common" frequencies on orthogonal coil pairs), and the resistivity and depth channels (RES and DEP) for each coplanar frequency.

The EM difference channels (DIFI and DIFQ) eliminate most of the responses from conductive ground, leaving responses from bedrock conductors, cultural features (e.g., telephone lines, fences, etc.) and edge effects. Edge effects often occur near the perimeter of broad conductive zones. This can be a source of geologic noise. While edge effects yield anomalies on the EM difference channels, they do not produce resistivity anomalies. Consequently, the resistivity channel aids in eliminating anomalies due to edge effects. On the other hand, resistivity anomalies will coincide with the most highly conductive sections of conductive ground, and this is another source of geologic noise. The recognition of a bedrock conductor in a conductive environment therefore is based on the anomalous responses of the two difference channels (DIFI and DIFQ) and the resistivity channels (RES). The most favourable situation is where anomalies coincide on all channels.

The DEP channels, which give the apparent depth to the conductive material, also help to determine whether a conductive response arises from surficial material or from a conductive zone in the bedrock. When these channels ride above the zero level on the depth profiles (i.e., depth is negative), it implies that the EM and resistivity profiles are responding primarily to a conductive upper layer, i.e., conductive overburden. If the DEP channels are below the zero level, it indicates that a resistive upper layer exists, and this usually implies the existence of a bedrock conductor. If the low frequency DEP channel is below the zero level and the high frequency DEP is above, this suggests that a bedrock conductor occurs beneath conductive cover.

Reduction of Geologic Noise

Geologic noise refers to unwanted geophysical responses. For purposes of airborne EM surveying, geologic noise refers to EM responses caused by conductive overburden and magnetic permeability. It was mentioned previously that the EM difference channels (i.e., channel DIFI for in-phase and DIFQ for quadrature) tend to eliminate the response of conductive overburden.

Magnetite produces a form of geological noise on the in-phase channels. Rocks containing less than 1% magnetite can yield negative in-phase anomalies caused by magnetic permeability. When magnetite is widely distributed throughout a survey area, the in-phase EM channels may continuously rise and fall, reflecting variations in the magnetite percentage, flying height, and overburden thickness. This can lead to difficulties in recognizing deeply buried bedrock conductors, particularly if conductive overburden also exists. However, the response of broadly distributed magnetite generally vanishes on the in-phase difference channel DIFI. This feature can be a significant aid in the recognition of conductors that occur in rocks containing accessory magnetite.

EM Magnetite Mapping

The information content of HEM data consists of a combination of conductive eddy current responses and magnetic permeability responses. The secondary field resulting from conductive eddy current flow is frequency-dependent and consists of both in-phase and quadrature components, which are positive in sign. On the other hand, the secondary field resulting from magnetic permeability is independent of frequency and consists of only an in-phase component which is negative in sign. When magnetic permeability manifests itself by decreasing the measured amount of positive in-phase, its presence may be difficult to recognize. However, when it manifests itself by yielding a negative in-phase anomaly (e.g., in the absence of eddy current flow), its presence is assured. In this latter case, the negative component can be used to estimate the percent magnetite content.

A magnetite mapping technique, based on the low frequency coplanar data, can be complementary to magnetometer mapping in certain cases. Compared to magnetometry, it is far less sensitive but is more able to resolve closely spaced magnetite zones, as well as providing an estimate of the amount of magnetite in the rock. The method is sensitive to 1/4% magnetite by weight when the EM sensor is at a height of 30 m above a magnetitic half-space. It can individually resolve steep dipping narrow magnetite-rich bands which are separated by 60 m. Unlike magnetometry, the EM magnetite method is unaffected by remanent magnetism or magnetic latitude.

The EM magnetite mapping technique provides estimates of magnetite content which are usually correct within a factor of 2 when the magnetite is fairly uniformly distributed. EM magnetite maps can be generated when magnetic permeability is evident as negative in-phase responses on the data profiles.

Like magnetometry, the EM magnetite method maps only bedrock features, provided that the overburden is characterized by a general lack of magnetite. This contrasts with resistivity mapping which portrays the combined effect of bedrock and overburden.

The Susceptibility Effect

When the host rock is conductive, the positive conductivity response will usually dominate the secondary field, and the susceptibility effect[8] will appear as a reduction in the in-phase, rather than as a negative value. The in-phase response will be lower than would be predicted by a model using zero susceptibility. At higher frequencies the in-phase conductivity response also gets larger, so a negative magnetite effect observed on the low frequency might not be observable on the higher frequencies, over the same body. The susceptibility effect is most obvious over discrete magnetite-rich zones, but also occurs over uniform geology such as a homogeneous half-space.

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[8] Magnetic susceptibility and permeability are two measures of the same physical property. Permeability is generally given as relative permeability, μ_r, which is the permeability of the substance divided by the permeability of free space ($4\ \pi \times 10^{-7}$). Magnetic susceptibility k is related to permeability by $k=\mu^r-1$. Susceptibility is a unitless measurement, and is usually reported in units of 10^{-6}. The typical range of susceptibilities is –1 for quartz, 130 for pyrite, and up to 5×10^5 for magnetite, in 10^{-6} units (Telford et al, 1986).

High magnetic susceptibility will affect the calculated apparent resistivity, if only conductivity is considered. Standard apparent resistivity algorithms use a homogeneous half-space model, with zero susceptibility. For these algorithms, the reduced in-phase response will, in most cases, make the apparent resistivity higher than it should be. It is important to note that there is nothing wrong with the data, nor is there anything wrong with the processing algorithms. The apparent difference results from the fact that the simple geological model used in processing does not match the complex geology.

Measuring and Correcting the Magnetite Effect

Theoretically, it is possible to calculate (forward model) the combined effect of electrical conductivity and magnetic susceptibility on an EM response in all environments. The difficulty lies, however, in separating out the susceptibility effect from other geological effects when deriving resistivity and susceptibility from EM data.

Over a homogeneous half-space, there is a precise relationship between in-phase, quadrature, and altitude. These are often resolved as phase angle, amplitude, and altitude. Within a reasonable range, any two of these three parameters can be used to calculate the half space resistivity. If the rock has a positive magnetic susceptibility, the in-phase component will be reduced and this departure can be recognized by comparison to the other parameters.

The algorithm used to calculate apparent susceptibility and apparent resistivity from HEM data, uses a homogeneous half-space geological model. Non half-space geology, such as horizontal layers or dipping sources, can also distort the perfect half-space relationship of the three data parameters. While it may be possible to use more complex models to calculate both rock parameters, this procedure becomes very complex and time-consuming. For basic HEM data processing, it is most practical to stick to the simplest geological model.

Magnetite reversals (reversed in-phase anomalies) have been used for many years to calculate an “FeO” or magnetite response from HEM data (Fraser, 1981). However, this technique could only be applied to data where the in-phase was observed to be negative, which happens when susceptibility is high and conductivity is low.

Applying Susceptibility Corrections

Resistivity calculations done with susceptibility correction may change the apparent resistivity. High-susceptibility conductors, that were previously masked by the susceptibility effect in standard resistivity algorithms, may become evident. In this case the susceptibility corrected apparent resistivity is a better measure of the actual resistivity of the earth. However, other geological variations, such as a deep resistive layer, can also reduce the in-phase by the same amount. In this case, susceptibility correction would not be the best method. Different geological models can apply in different areas of the same data set. The effects of susceptibility, and other effects that can create a similar response, must be considered when selecting the resistivity algorithm.

Susceptibility from EM vs Magnetic Field Data

The response of the EM system to magnetite may not match that from a magnetometer survey. First, HEM-derived susceptibility is a rock property measurement, like resistivity. Magnetic data show the total magnetic field, a measure of the potential field, not the rock property. Secondly, the shape of an anomaly depends on the shape and direction of the source magnetic field. The electromagnetic field of HEM is much different in shape from the earth's magnetic field. Total field magnetic anomalies are different at different magnetic latitudes; HEM susceptibility anomalies have the same shape regardless of their location on the earth.

In far northern latitudes, where the magnetic field is nearly vertical, the total magnetic field measurement over a thin vertical dike is very similar in shape to the anomaly from the HEM-derived susceptibility (a sharp peak over the body). The same vertical dike at the magnetic equator would yield a negative magnetic anomaly, but the HEM susceptibility anomaly would show a positive susceptibility peak.

Effects of Permeability and Dielectric Permittivity

Resistivity algorithms that assume free-space magnetic permeability and dielectric permittivity, do not yield reliable values in highly magnetic or highly resistive areas. Both magnetic polarization and displacement currents cause a decrease in the in-phase component, often resulting in negative values that yield erroneously high apparent resistivities. The effects of magnetite occur at all frequencies, but are most evident at the lowest frequency. Conversely, the negative effects of dielectric permittivity are most evident at the higher frequencies, in resistive areas.

The table below shows the effects of varying permittivity over a resistive (10,000 ohm-m) half space, at frequencies of 56,000 Hz (DIGHEM^V) and 102,000 Hz (RESOLVE).

Apparent Resistivity Calculations

Effects of Permittivity on In-phase/Quadrature/Resistivity

Freq (Hz)	Coil	Sep (m)	Thres (ppm)	Alt (m)	In Phase	Quad Phase	App Res	App Depth (m)	Permittivity
56,000	CP	6.3	0.1	30	7.3	35.3	10118	-1.0	1 Air
56,000	CP	6.3	0.1	30	3.6	36.6	19838	-13.2	5 Quartz

56,000	CP	6.3	0.1	30	-1.1	38.3	81832	-25.7	10 Epidote
56,000	CP	6.3	0.1	30	-10.4	42.3	76620	-25.8	20 Granite
56,000	CP	6.3	0.1	30	-19.7	46.9	71550	-26.0	30 Diabase
56,000	CP	6.3	0.1	30	-28.7	52.0	66787	-26.1	40 Gabbro
102,000	CP	7.86	0.1	30	32.5	117.2	9409	-0.3	1 Air
102,000	CP	7.86	0.1	30	11.7	127.2	25956	-16.8	5 Quartz
102,000	CP	7.86	0.1	30	-14.0	141.6	97064	-26.5	10 Epidote
102,000	CP	7.86	0.1	30	-62.9	176.0	83995	-26.8	20 Granite
102,000	CP	7.86	0.1	30	-107.5	215.8	73320	-27.0	30 Diabase
102,000	CP	7.86	0.1	30	-147.1	259.2	64875	-27.2	40 Gabbro

Methods have been developed (Huang and Fraser, 2000, 2001) to correct apparent resistivities for the effects of permittivity and permeability. The corrected resistivities yield more credible values than if the effects of permittivity and permeability are disregarded.

Recognition of Culture

Cultural responses include all EM anomalies caused by man-made metallic objects. Such anomalies may be caused by inductive coupling or current gathering. The concern of the interpreter is to recognize when an EM response is due to culture. Points of consideration used by the interpreter, when coaxial and coplanar coil-pairs are operated at a common frequency, are as follows:

1. Channels CXPL and CPPL monitor 60 Hz radiation. An anomaly on these channels shows that the conductor is radiating power. Such an indication is normally a guarantee that the conductor is cultural. However, care must be taken to ensure that the conductor is not a geologic body that strikes across a power line, carrying leakage currents.

2. A flight that crosses a "line" (e.g., fence, telephone line, etc.) yields a centre-peaked coaxial anomaly and an m-shaped coplanar anomaly.[9] When the flight crosses the cultural line at a high angle of intersection, the amplitude ratio of coaxial/coplanar response is 2. Such an EM anomaly can only be caused by a line. The geologic body that yields anomalies most closely resembling a line is the vertically dipping thin dike. Such a body, however, yields an amplitude ratio of 1 rather than 2. Consequently, an m-shaped coplanar anomaly with a CXI/CPI amplitude ratio of 2 is virtually a guarantee that the source is a cultural line.

3. A flight that crosses a sphere or horizontal disk yields centre-peaked coaxial and coplanar anomalies with a CXI/CPI amplitude ratio (i.e., coaxial/coplanar) of 1/8. In the absence of geologic bodies of this geometry, the most likely conductor is a

[9] See Figure C-1 presented earlier.

metal roof or small fenced yard.[10] Anomalies of this type are virtually certain to be cultural if they occur in an area of culture.

4. A flight that crosses a horizontal rectangular body or wide ribbon yields an m-shaped coaxial anomaly and a centre-peaked coplanar anomaly. In the absence of geologic bodies of this geometry, the most likely conductor is a large fenced area.[5] Anomalies of this type are virtually certain to be cultural if they occur in an area of culture.
5. EM anomalies that coincide with culture, as seen on the camera film or video display, are usually caused by culture. However, care is taken with such coincidences because a geologic conductor could occur beneath a fence, for example. In this example, the fence would be expected to yield an m-shaped coplanar anomaly as in case #2 above. If, instead, a centre-peaked coplanar anomaly occurred, there would be concern that a thick geologic conductor coincided with the cultural line.

6. The above description of anomaly shapes is valid when the culture is not conductively coupled to the environment. In this case, the anomalies arise from inductive coupling to the EM transmitter. However, when the environment is quite conductive (e.g., less than 100 ohm-m at 900 Hz), the cultural conductor may be conductively coupled to the environment. In this latter case, the anomaly shapes tend to be governed by current gathering. Current gathering can completely distort the anomaly shapes, thereby complicating the identification of cultural anomalies. In such circumstances, the interpreter can only rely on the radiation channels and on the camera film or video records.

Magnetic Responses

The measured total magnetic field provides information on the magnetic properties of the earth materials in the survey area. The information can be used to locate magnetic bodies of direct interest for exploration, and for structural and lithological mapping.

The total magnetic field response reflects the abundance of magnetic material in the source. Magnetite is the most common magnetic mineral. Other minerals such as ilmenite, pyrrhotite, franklinite, chromite, hematite, arsenopyrite, limonite and pyrite are also magnetic, but to a lesser extent than magnetite on average.

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[10] It is a characteristic of EM that geometrically similar anomalies are obtained from: (1) a planar conductor, and (2) a wire which forms a loop having dimensions identical to the perimeter of the equivalent planar conductor.

In some geological environments, an EM anomaly with magnetic correlation has a greater likelihood of being produced by sulphides than one which is non-magnetic. However, sulphide ore bodies may be non-magnetic (e.g., the Kidd Creek deposit near Timmins, Canada) as well as magnetic (e.g., the Mattabi deposit near Sturgeon Lake, Canada).

Iron ore deposits will be anomalously magnetic in comparison to surrounding rock due to the concentration of iron minerals such as magnetite, ilmenite and hematite.

Changes in magnetic susceptibility often allow rock units to be differentiated based on the total field magnetic response. Geophysical classifications may differ from geological classifications if various magnetite levels exist within one general geological classification. Geometric considerations of the source such as shape, dip and depth, inclination of the earth's field and remanent magnetization will complicate such an analysis.

In general, mafic lithologies contain more magnetite and are therefore more magnetic than many sediments which tend to be weakly magnetic. Metamorphism and alteration can also increase or decrease the magnetization of a rock unit.

Textural differences on a total field magnetic contour, colour or shadow map due to the frequency of activity of the magnetic parameter resulting from inhomogeneities in the distribution of magnetite within the rock, may define certain lithologies. For example, near surface volcanics may display highly complex contour patterns with little line-to-line correlation.

Rock units may be differentiated based on the plan shapes of their total field magnetic responses. Mafic intrusive plugs can appear as isolated "bulls-eye" anomalies. Granitic intrusives appear as sub-circular zones, and may have contrasting rings due to contact metamorphism. Generally, granitic terrain will lack a pronounced strike direction, although granite gneiss may display strike.

Linear north-south units are theoretically not well-defined on total field magnetic maps in equatorial regions due to the low inclination of the earth's magnetic field. However, most stratigraphic units will have variations in composition along strike that will cause the units to appear as a series of alternating magnetic highs and lows.

Faults and shear zones may be characterized by alteration that causes destruction of magnetite (e.g., weathering) that produces a contrast with surrounding rock. Structural breaks may be filled by magnetite-rich, fracture filling material as is the case with diabase dikes, or by non-magnetic felsic material.

Faulting can also be identified by patterns in the magnetic total field contours or colours. Faults and dikes tend to appear as lineaments and often have strike lengths of several kilometres. Offsets in narrow, magnetic, stratigraphic trends also delineate structure. Sharp contrasts in magnetic lithologies may arise due to large displacements along strike-slip or dip-slip faults.

Gamma Ray Spectrometry

Radioelement concentrations are measures of the abundance of radioactive elements in the rock. The original abundance of the radioelements in any rock can be altered by the subsequent processes of metamorphism and weathering.

Gamma radiation in the range that is measured in the thorium, potassium, uranium and total count windows is strongly attenuated by rock, overburden and water. Almost all of the total radiation measured from rock and overburden originates in the upper .5 metres. Moisture in soil and bodies of water will mask the radioactivity from underlying rock. Weathered rock materials that have been displaced by glacial, water or wind action will not reflect the general composition of the underlying bedrock. Where residual soils exist, they may reflect the composition of underlying rock except where equilibrium does not exist between the original radioelement and the products in its decay series.

Radioelement counts (expressed as counts per second) are the rates of detection of the gamma radiation from specific decaying particles corresponding to products in each radioelements decay series. The radiation source for uranium is bismuth (Bi-214), for thorium it is thallium (Tl-208) and for potassium it is potassium (K-40).

The uranium and thorium radioelement concentrations are dependent on a state of equilibrium between the parent and daughter products in the decay series. Some daughter products in the uranium decay are long lived and could be removed by processes such as leaching. One product in the series, radon (Rn-222), is a gas which can easily escape. Both of these factors can affect the degree to which the calculated uranium concentrations reflect the actual composition of the source rock. Because the daughter products of thorium are relatively short lived, there is more likelihood that the thorium decay series is in equilibrium.

Lithological discrimination can be based on the measured relative concentrations and total, combined, radioactivity of the radioelements. Feldspar and mica contain potassium. Zircon, sphene and apatite are accessory minerals in igneous rocks that are sources of uranium and thorium. Monazite, thorianite, thorite, uraninite and uranothorite are also sources of uranium and thorium which are found in granites and pegmatites.

In general, the abundance of uranium, thorium and potassium in igneous rock increases with acidity. Pegmatites commonly have elevated concentrations of uranium relative to thorium. Sedimentary rocks derived from igneous rocks may have characteristic signatures that are influenced by their parent rocks, but these will have been altered by subsequent weathering and alteration.

Metamorphism and alteration will cause variations in the abundance of certain radioelements relative to each other. For example, alterative processes may cause uranium enrichment to the extent that a rock will be of economic interest. Uranium anomalies are more likely to be economically significant if they consist of an increase in the uranium relative to thorium and potassium, rather than a sympathetic increase in all three radioelements.

Faults can exhibit radioactive highs due to increased permeability which allows radon migration, or as lows due to structural control of drainage and fluvial sediments which attenuate gamma radiation from the underlying rocks. Faults can also be recognized by sharp contrasts in radiometric lithologies due to large strike-slip or dip-slip displacements. Changes in relative radioelement concentrations due to alteration will also define faults.

Similar to magnetics, certain rock types can be identified by their plan shapes if they also produce a radiometric contrast with surrounding rock. For example, granite intrusions will appear as sub-circular bodies, and may display concentric zonations. They will tend to lack a prominent strike direction. Offsets of narrow, continuous, stratigraphic units with contrasting radiometric signatures can identify faulting, and folding of stratigraphic trends will also be apparent.

APPENDIX D

DATA ARCHIVE DESCRIPTION

APPENDIX D

ARCHIVE DESCRIPTION

Phase 2006

Reference: CCD02499
Disc 1 of 1
Archive Date: January 29, 2007

This archive contains FINAL DATA ARCHIVES of an airborne geophysical survey conducted by FUGRO AIRBORNE SURVEYS CORP. over the Eskay Creek Areas 4,5 and 6, British Columbia, on behalf of Hathor Exploration Ltd., during July 5 to October 12, 2006.

Job # 06041-4,5,6.

******* Disc 1 of 1 *******

```
\README.TXT          - this file

GRIDS\
NOTE: _# indicates block number.(456)

            Grids in Geosoft binary (float) format

      RES900_#.GRD    - Apparent Resistivity 900 Hz coplanar
      RES7200_#.GRD   - Apparent Resistivity 7200 Hz coplanar
      RES56K_#.GRD    - Apparent Resistivity 56000 Hz coplanar
      MAG_#.GRD       - Total Magnetic Intensity nT
      CVG_#.GRD       - Calculated Vertical gradient from TMI grid nT/m
      K_#.GRD         - Potassium Counts (cps)
      U_#.GRD         - Uranium Counts (cps)
      TH_#.GRD        - Thorium Counts (cps)
      TC_#.GRD        - Total Counts (cps)



XYZ\

      Block#.XYZ     - ASCII line data archive in Geosoft XYZ format
      AnBlock#.XYZ   - Geosoft Anomaly ASCII data archive
```

All EM data in the archive is presented in the standard normalization convention for the coplanar coils. The ratio of coplanar to coaxial amplitudes for the same frequency is 4:1 over a layered earth.

Resistivity is calculated using a proprietary pseudo-layer half-space algorithm.

Phase 2007

Reference: CDVD00275
Disc 1 of 1
Archive Date: February 19, 2008

This archive contains FINAL DATA ARCHIVES of an airborne geophysical survey conducted by FUGRO AIRBORNE SURVEYS CORP. over the Eskay Creek Areas, British Columbia on behalf of Hathor Exploration Ltd. during July 19 to September 5, 2007.

Job # 06041-4,5,6

```
******* Disc 1 of 1 *******

\README.TXT          - this file

GRIDS\
NOTE: _# indicates block number.

            Grids in Geosoft binary (float) format

      RES900_456.GRD  - Apparent Resistivity 900 Hz coplanar
      RES7200_456.GRD - Apparent Resistivity 7200 Hz coplanar
      RES56K_456.GRD  - Apparent Resistivity 56000 Hz coplanar
      MAG_456.GRD     - Total Magnetic Intensity nT
      CVG_456.GRD     - Calculated Vertical gradient from TMI grid nT/m
      K_456.GRD   - Potasium Counts (cps)
      U_456.GRD   - Uranium Counts (cps)
      TH_456.GRD  - Thorium Counts (cps)
      TC_456.GRD  - Total Counts (cps)



XYZ\

      Block456.XYZ        - ASCII line data archive in Geosoft XYZ format
      anBlock456.XYZ      - Geosoft Anomaly ASCII data archive
```

- Appendix D.3 -

ArchiveSummary.txt - Summary of Channel Names in the ASCII line data archive

MAPS\

Block 456 Maps - Map Sheet 1

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aem_block456_sh1.pdf        - Electromagnetic Anomalies map
cvg_block456_sh1.pdf        - Calculated Vertical Gradient map
mag_block456_sh1.pdf        - Total Magnetic Field map
res56K_block456_sh1.pdf     - Apparent Resistivity Map 56 KHz
res7200_block456_sh1.pdf    - Apparent Resistivity Map 7200 Hz
res900_block456_sh1.pdf     - Apparent Resistivity Map 900 Hz
tc_block456_sh1.pdf         - Radiometric Total Count map
th_block456_sh1.pdf         - Radiometric Thorium counts map
k_block456_sh1.pdf          - Radiometric Potassium counts map
u_block456_sh1.pdf          - Radiometric Uranium counts map
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Block 456 Maps - Map Sheet 2

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aem_block456_sh2.pdf        - Electromagnetic Anomalies map
cvg_block456_sh2.pdf        - Calculated Vertical Gradient map
mag_block456_sh2.pdf        - Total Magnetic Field map
res56K_block456_sh2.pdf     - Apparent Resistivity Map 56 KHz
res7200_block456_sh2.pdf    - Apparent Resistivity Map 7200 Hz
res900_block456_sh2.pdf     - Apparent Resistivity Map 900 Hz
tc_block456_sh2.pdf         - Radiometric Total Count map
th_block456_sh2.pdf         - Radiometric Thorium counts map
k_block456_sh2.pdf          - Radiometric Potassium counts map
u_block456_sh2.pdf          - Radiometric Uranium counts map
```

Block 456 Maps - Map Sheet 3

```
aem_block456_sh3.pdf        - Electromagnetic Anomalies map
cvg_block456_sh3.pdf        - Calculated Vertical Gradient map
mag_block456_sh3.pdf        - Total Magnetic Field map
res56K_block456_sh3.pdf     - Apparent Resistivity Map 56 KHz
res7200_block456_sh3.pdf    - Apparent Resistivity Map 7200 Hz
res900_block456_sh3.pdf     - Apparent Resistivity Map 900 Hz
tc_block456_sh3.pdf         - Radiometric Total Count map
th_block456_sh3.pdf         - Radiometric Thorium counts map
k_block456_sh3.pdf          - Radiometric Potassium counts map
u_block456_sh3.pdf          - Radiometric Uranium counts map
```

Block 456 Maps - Map Sheet 4

```
aem_block456_sh4.pdf        - Electromagnetic Anomalies map
cvg_block456_sh4.pdf        - Calculated Vertical Gradient map
mag_block456_sh4.pdf        - Total Magnetic Field map
res56K_block456_sh4.pdf     - Apparent Resistivity Map 56 KHz
res7200_block456_sh4.pdf    - Apparent Resistivity Map 7200 Hz
res900_block456_sh4.pdf     - Apparent Resistivity Map 900 Hz
tc_block456_sh4.pdf         - Radiometric Total Count map
th_block456_sh4.pdf         - Radiometric Thorium counts map
k_block456_sh4.pdf          - Radiometric Potassium counts map
u_block456_sh4.pdf          - Radiometric Uranium counts map


     Block 456 Maps - Map Sheet 5

aem_block456_sh5.pdf        - Electromagnetic Anomalies map
cvg_block456_sh5.pdf        - Calculated Vertical Gradient map
mag_block456_sh5.pdf        - Total Magnetic Field map
res56K_block456_sh5.pdf     - Apparent Resistivity Map 56 KHz
res7200_block456_sh5.pdf    - Apparent Resistivity Map 7200 Hz
res900_block456_sh5.pdf     - Apparent Resistivity Map 900 Hz
tc_block456_sh5.pdf         - Radiometric Total Count map
th_block456_sh5.pdf         - Radiometric Thorium counts map
k_block456_sh5.pdf          - Radiometric Potassium counts map
u_block456_sh5.pdf          - Radiometric Uranium counts map


     Block 456 Maps - Map Sheet 6

aem_block456_sh6.pdf        - Electromagnetic Anomalies map
cvg_block456_sh6.pdf        - Calculated Vertical Gradient map
mag_block456_sh6.pdf        - Total Magnetic Field map
res56K_block456_sh6.pdf     - Apparent Resistivity Map 56 KHz
res7200_block456_sh6.pdf    - Apparent Resistivity Map 7200 Hz
res900_block456_sh6.pdf     - Apparent Resistivity Map 900 Hz
tc_block456_sh6.pdf         - Radiometric Total Count map
th_block456_sh6.pdf         - Radiometric Thorium counts map
k_block456_sh6.pdf          - Radiometric Potassium counts map
u_block456_sh6.pdf          - Radiometric Uranium counts map


     Block 456 Maps - Map Sheet 7

aem_block456_sh7.pdf        - Electromagnetic Anomalies map
cvg_block456_sh7.pdf        - Calculated Vertical Gradient map
mag_block456_sh7.pdf        - Total Magnetic Field map
res56K_block456_sh7.pdf     - Apparent Resistivity Map 56 KHz
res7200_block456_sh7.pdf    - Apparent Resistivity Map 7200 Hz
```

```
res900_block456_sh7.pdf     - Apparent Resistivity Map 900 Hz
tc_block456_sh7.pdf         - Radiometric Total Count map
th_block456_sh7.pdf         - Radiometric Thorium counts map
k_block456_sh7.pdf          - Radiometric Potassium counts map
u_block456_sh7.pdf          - Radiometric Uranium counts map
```

Block 456 Maps - Map Sheet 8

```
aem_block456_sh8.pdf        - Electromagnetic Anomalies map
cvg_block456_sh8.pdf        - Calculated Vertical Gradient map
mag_block456_sh8.pdf        - Total Magnetic Field map
res56K_block456_sh8.pdf     - Apparent Resistivity Map 56 KHz
res7200_block456_sh8.pdf    - Apparent Resistivity Map 7200 Hz
res900_block456_sh8.pdf     - Apparent Resistivity Map 900 Hz
tc_block456_sh8.pdf         - Radiometric Total Count map
th_block456_sh8.pdf         - Radiometric Thorium counts map
k_block456_sh8.pdf          - Radiometric Potassium counts map
u_block456_sh8.pdf          - Radiometric Uranium counts map
```

REPORT\

```
R06041_Block1-3.PDF         - Logistics and interpretation report
R06041_Block456.PDF         - Logistics and interpretation report
```

All EM data in the archive is presented in the standard normalization convention for the coplanar coils. The ratio of coplanar to coaxial amplitudes for the same frequency is 4:1 over a layered earth.

Resistivity is calculated using a proprietary pseudo-layer half-space algorithm.

The coordinate system for all grids and XYZ files is projected as follows

Datum	NAD 83
Spheroid	WGS84 (GRS1980)
Projection	UTM
Central meridian	129 West
False easting	500000
False northing	0
Scale factor	0.9996
Northern parallel	N/A
Base parallel	N/A

```
WGS84 to local conversion method    Molodensky
Delta X shift                       +0
Delta Y shift                       +0
Delta Z shift                       +0

--------------------------------------------------------------------------------
If you have any problems with this archive please contact
```


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E-mail toronto@fugroairborne.com

- Appendix D.7 -

Geosoft XYZ ARCHIVE SUMMARY

JOB TITLE: 06041-4,5,6

TYPE OF SURVEY :Fugro DIGHEM V EM, Magnetics, Resistivity, Radiometrics
AREA :Eskay Creek Areas, Blocks 4,5,6, British Columbia
CLIENT :Hathor Exploration Ltd.

****

NUMBER OF DATA FIELDS : 43

#	CHANNAME	TIME	UNITS	/ DESCRIPTION
1	X	0.1	m	UTME-NAD83 (ZONE-9N)
2	Y	0.1	m	UTMN-NAD83 (ZONE-9N)
3	LAT	0.1	deg.m	Latitude NAD83
4	LON	0.1	deg.m	Longitude NAD83
5	ALTBIRDM	0.1	m	Bird height above ground
6	ALTHELIM	0.1	m	Heli height above ground
7	FID	0.1	s	Fiducial
8	DIURNAL	0.1	nT	Diurnal correction
9	MAGR	0.1	nT	Lagged and diurnal corrected Total Magnetic Field
10	MAGF	0.1	nT	Final Total Magnetic Field
11	CPI900	0.1	ppm	INPHASE-COPLANAR 872 HZ
12	CPQ900	0.1	ppm	QUADRATURE- COPLANAR 872 HZ
13	CXI1000	0.1	ppm	INPHASE-COAXIAL 1116 HZ
14	CXQ1000	0.1	ppm	QUAD- COAXIAL 1116 HZ
15	CXI5500	0.1	ppm	INPHASE -COAXIAL 5666 HZ
16	CXQ5500	0.1	ppm	QUAD -COAXIAL 5666 HZ
17	CPI7200	0.1	ppm	INPHASE -COPLANAR 7233 HZ
18	CPQ7200	0.1	ppm	QUAD -COPLANAR 7233 HZ
19	CPI56K	0.1	ppm	INPHASE-COPLANAR 55460 HZ
20	CPQ56K	0.1	ppm	QUAD-COPLANAR 55460 HZ
21	RES900	0.1	ohm-m	APPARENT RESISTIVITY - 872 Hz
22	RES7200	0.1	ohm-m	APPARENT RESISTIVITY - 7233 Hz
23	RES56K	0.1	ohm-m	APPARENT RESISTIVITY - 55460 Hz
24	DEP900	0.1	m	APPARENT DEPTH - 872 Hz
25	DEP7200	0.1	m	APPARENT DEPTH - 7233 Hz
26	DEP56K	0.1	m	APPARENT DEPTH - 55460 Hz
27	COSMIC	1.0	counts/s	Cosmic counts
28	LIVE_TIME	1.0	ms	Spectrometer live time
29	URANUP	1.0	counts/s	Upward Uranium window
30	TC_RAW	1.0	counts/s	Total Count window - raw
31	TH_RAW	1.0	counts/s	Thorium window - raw
32	U_RAW	1.0	counts/s	Uranium window - raw
33	K_RAW	1.0	counts/s	Potassium window - raw
34	TC	1.0	counts/s	Total Count window - corrected
35	TH	1.0	counts/s	Thorium window - corrected
36	U	1.0	counts/s	Uranium window - corrected
37	K	1.0	counts/s	Potassium window - corrected
38	PRESSURE	0.1	kpa	Air pressure

```
 39 TEMPERATURE 0.1    Celsius     Outside air temperature
 40 Z           0.1    m           Height above mean sea level
 41 DTM         0.1    m           Digital Terrain Model
 42 FLT         0.1                Survey flight number
 43 DATE        0.1    Y/M/D       Date of the survey line
*****************************************************************************

ISSUE DATE         :February 15, 2007 (2006 Phase)
                   :February 19, 2008 (2007 Phase)
FOR WHOM           :Hathor Exploration Ltd.
BY  WHOM           :FUGRO AIRBORNE SURVEYS
                    2270 ARGENTIA ROAD, UNIT 2
                    MISSISSAUGA, ONTARIO,
                    CANADA  L5N 6A6
                    TEL. (905) 812-0212
                    FAX (905) 812-1504
```

APPENDIX E

EM ANOMALY LIST

EM Anomaly List (2006 Phase)

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 40030			FLIGHT 103										
A	577.4	S	381252	6295943	2.0	1.8	4.0	11.8	0.9	2.1	---	---	0
LINE 40040			FLIGHT 103										
A	861.7	S	381209	6295820	1.2	3.2	4.6	19.2	1.3	2.7	---	---	0
LINE 40050			FLIGHT 103										
A	1027.6	S?	382286	6295617	2.2	2.6	10.2	12.3	10.1	1.8	---	---	22
LINE 40070			FLIGHT 103										
A	1940.5	S?	381693	6295341	1.5	1.0	0.0	6.9	1.3	1.3	---	---	0
B	2020.0	S?	383348	6295275	0.0	0.4	13.4	4.7	14.3	1.2	---	---	91
LINE 40080			FLIGHT 104										
A	372.0	S?	381797	6295195	1.8	1.6	20.6	7.5	6.7	1.1	---	---	148
B	347.5	S	382395	6295154	4.2	1.4	24.3	2.6	27.9	0.7	---	---	0
C	287.2	S?	383361	6295144	0.0	1.9	0.3	4.7	3.7	0.8	---	---	0
LINE 40110			FLIGHT 142										
A	585.5	S	381824	6294740	3.1	1.5	4.2	7.9	3.1	2.2	---	---	0
LINE 40180			FLIGHT 142										
A	2869.6	S	375705	6293837	2.7	3.8	38.4	46.2	7.6	12.0	0.6	32	0

CX = COAXIAL
CP = COPLANAR

Note:EM values shown above are local amplitudes

*Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 40190			FLIGHT 147										
A	7991.7	S	375829	6293697	0.0	0.1	8.0	8.0	1.6	2.6	---	---	39
B	7947.1	S	377145	6293640	2.3	1.7	3.4	7.2	1.0	1.8	---	---	0
LINE 40200			FLIGHT 147										
A	8116.4	S?	376267	6293535	0.5	2.2	0.3	17.1	0.0	2.8	---	---	104
B	8148.7	S	377216	6293500	1.1	1.9	3.9	7.6	1.1	2.1	---	---	0
C	8366.6	S?	381914	6293386	11.8	3.9	48.1	25.3	56.0	3.5	---	---	0
LINE 40210			FLIGHT 147										
A	8730.0	S	380224	6293256	0.6	0.4	3.7	6.3	3.0	1.4	---	---	0
LINE 40220			FLIGHT 147										
A	10200.7	S	377330	6293208	3.2	2.1	4.2	11.1	0.7	2.6	---	---	0
B	10388.7	S	382044	6293078	2.0	1.3	14.9	10.1	14.9	2.3	---	---	0
C	10395.5	S?	382254	6293073	2.8	3.6	16.3	24.3	19.8	3.2	---	---	48
D	10410.6	S?	382650	6293074	0.0	1.6	0.0	3.3	6.6	1.4	---	---	14
LINE 40230			FLIGHT 147										
A	9093.4	S	376528	6293069	3.0	1.5	5.1	9.3	1.8	2.0	---	---	0
LINE 40240			FLIGHT 147										
A	9309.1	H	377718	6292884	2.9	2.3	6.3	10.8	1.3	2.7	---	---	0

CX = COAXIAL
CP = COPLANAR

Note:EM values shown above are local amplitudes

*Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 40290			FLIGHT 169										
A	4190.0	S?	375556	6292165	1.1	1.8	6.5	9.5	4.5	2.6	---	---	0
B	4136.0	S	375834	6292186	1.2	1.0	1.1	4.5	1.7	1.0	---	---	103
C	4031.0	H	377283	6292136	1.7	1.4	6.8	10.8	1.6	1.9	---	---	137
LINE 40301			FLIGHT 169										
A	4435.3	H	377358	6291986	0.7	0.2	3.9	14.7	1.7	1.7	---	---	128
LINE 40310			FLIGHT 169										
A	4688.5	S?	375464	6291906	4.6	8.6	17.7	23.8	14.3	3.9	---	---	0
B	4680.9	S	375605	6291898	0.6	0.6	24.0	3.6	30.2	0.5	0.5	94	0
C	4591.7	S	377394	6291845	0.4	2.3	7.1	18.5	0.8	3.9	---	---	90
LINE 40321			FLIGHT 169										
A	5237.9	S	375550	6291760	1.5	0.9	15.1	10.6	12.6	1.6	1.4	85	0
B	5201.1	S?	376162	6291720	2.6	5.1	10.9	17.8	14.0	2.9	---	---	114
C	5185.2	S?	376395	6291715	7.3	6.2	16.0	16.9	18.7	3.6	---	---	156
D	5141.9	S?	377366	6291707	2.9	1.2	5.9	16.6	1.5	3.6	---	---	0
LINE 40330			FLIGHT 169										
A	5397.0	S	377363	6291550	1.2	2.6	5.6	14.0	1.2	2.7	---	---	0
LINE 40340			FLIGHT 169										
A	5732.5	S?	375377	6291447	6.1	1.7	56.9	9.7	67.9	2.8	---	---	186

CX = COAXIAL
CP = COPLANAR

Note:EM values shown above are local amplitudes

*Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 40340			FLIGHT 169										
B	5713.8	S?	375600	6291473	5.5	0.2	21.7	14.3	24.1	2.1	---	---	0
C	5624.1	S?	377342	6291399	2.8	2.3	5.1	14.6	1.9	2.9	---	---	0
LINE 40350			FLIGHT 169										
A	5880.7	S?	377308	6291243	1.7	5.2	12.8	24.9	2.0	4.3	---	---	41
LINE 40360			FLIGHT 169										
A	6194.9	S	375498	6291153	3.8	1.8	24.9	1.8	29.6	0.3	---	---	54
B	6169.2	S?	375835	6291118	7.6	5.4	27.3	19.8	30.9	3.8	1.8	22	0
C	6116.4	S?	376471	6291124	2.3	0.8	15.7	12.6	6.8	5.6	2.9	86	0
D	6071.7	S?	377332	6291109	2.7	2.9	8.3	20.1	2.0	5.1	---	---	56
LINE 40370			FLIGHT 169										
A	6359.0	S	377226	6290956	2.0	2.8	6.5	16.3	4.0	3.0	---	---	0
LINE 40380			FLIGHT 169										
A	6843.7	S?	375614	6290833	0.4	6.7	15.2	9.7	0.4	2.6	---	---	84
B	6714.0	S	377175	6290779	2.5	4.9	4.9	12.1	1.7	2.2	---	---	21
LINE 40390			FLIGHT 169										
A	7096.0	S	377354	6290647	1.7	0.7	3.2	12.2	3.1	2.3	---	---	0
LINE 40400			FLIGHT 169										
A	7348.3	B	376207	6290536	5.8	6.1	45.0	42.5	8.1	18.9	1.0	19	0

CX = COAXIAL
CP = COPLANAR

Note:EM values shown above are local amplitudes

*Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 40420			FLIGHT 169										
A	7690.5	S?	376099	6290220	1.5	15.1	4.3	16.7	3.0	2.7	0.1	0	0
B	7605.6	S?	376962	6290214	4.5	1.6	5.5	8.8	4.5	2.3	---	---	0
LINE 40430			FLIGHT 169										
A	8016.5	D	376290	6290091	10.8	9.2	14.9	34.0	1.1	5.1	1.6	19	0
B	7934.3	S	377002	6290065	3.3	2.4	3.7	8.9	2.5	1.7	---	---	0
LINE 40450			FLIGHT 169										
A	8345.6	S?	376425	6289792	0.3	1.8	14.1	26.2	1.8	7.3	0.1	7	0
B	8336.3	S?	376521	6289789	6.3	6.6	0.2	18.3	0.9	3.6	1.0	19	33
LINE 40470			FLIGHT 169										
A	8681.6	D	376357	6289496	11.5	10.7	23.8	35.6	4.8	7.9	1.5	13	16
LINE 40500			FLIGHT 169										
A	9355.7	D	375965	6289030	39.0	21.3	103.9	60.7	26.3	43.8	4.3	8	0
LINE 40540			FLIGHT 170										
A	2414.7	S	377573	6288407	3.2	1.7	3.8	9.0	1.2	2.2	---	---	0
LINE 40550			FLIGHT 170										
A	1546.0	S?	375074	6288295	0.0	7.0	15.2	3.2	20.5	4.6	---	---	278
B	1558.0	S?	375261	6288288	5.4	2.2	69.4	10.1	85.5	2.4	---	---	0

CX = COAXIAL
CP = COPLANAR

Note:EM values shown above are local amplitudes

*Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 40550		FLIGHT 170											
C	1703.9	S?	377463	6288262	3.3	2.7	15.5	22.5	0.3	4.3	1.1	23	14
LINE 40560		FLIGHT 170											
A	1273.0	S?	377475	6288102	3.1	5.5	9.2	17.2	2.1	4.1	---	---	60
LINE 40570		FLIGHT 170											
A	1164.0	S	377467	6287967	1.1	0.7	1.1	2.9	1.1	0.5	---	---	15
LINE 40590		FLIGHT 169											
A	3066.4	S	375383	6287668	2.5	3.9	13.3	17.1	11.1	2.8	---	---	0
LINE 40600		FLIGHT 169											
A	2724.0	S	375182	6287571	0.8	1.3	7.0	6.3	6.5	1.4	---	---	0
LINE 49013		FLIGHT 147											
A	4279.1	H	375535	6284198	4.9	2.7	30.2	17.7	34.5	11.5	2.1	24	127
B	4299.7	H	375554	6284861	13.6	6.1	105.8	43.1	71.5	46.0	3.9	25	0
C	4441.4	S	375640	6287772	2.7	1.8	7.6	5.2	2.3	1.1	---	---	0
D	4490.7	B?	375869	6289082	4.6	4.4	12.8	13.7	5.8	7.1	1.1	21	0
E	4577.9	S	375731	6291006	5.3	0.5	11.9	10.0	6.6	1.4	---	---	0
F	4587.8	S?	375723	6291218	4.7	5.5	26.8	11.6	26.1	2.8	---	---	0
G	4603.0	S?	375718	6291566	2.8	2.4	5.8	17.1	0.0	2.4	---	---	224
H	4708.5	S	375845	6293838	3.5	3.6	15.6	27.3	2.4	5.1	0.9	13	0

CX = COAXIAL
CP = COPLANAR

Note:EM values shown above are local amplitudes

*Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 49020		FLIGHT 43											
A	1020.3	H	377062	6284811	2.1	0.4	25.7	13.3	16.0	9.2	6.9	57	0
B	995.4	H	377043	6285560	3.7	2.1	21.8	1.8	16.9	8.5	1.9	49	77
C	862.7	H?	377149	6288336	2.0	3.2	6.3	2.1	1.6	1.8	---	---	0
D	775.7	S?	377206	6290668	7.6	4.1	4.2	38.3	6.0	4.5	2.5	25	148
E	760.0	S?	377221	6291138	4.1	4.1	2.8	7.4	3.0	0.5	---	---	0
LINE 49033		FLIGHT 147											
A	5227.3	B	378550	6284730	22.1	14.3	130.9	102.3	48.1	63.8	2.8	7	149
B	5224.3	H	378552	6284819	8.4	6.3	130.9	102.3	48.1	63.8	1.7	34	43
C	5205.0	H	378565	6285445	1.0	3.9	10.2	22.8	8.2	3.6	---	---	0
D	5037.7	H	378697	6290256	1.1	0.3	3.0	7.1	5.3	1.3	---	---	0
E	4954.0	S	378744	6292170	0.8	1.0	3.3	3.9	1.1	0.7	---	---	0
F	4929.7	S?	378769	6292732	2.6	0.6	4.2	5.2	1.9	2.0	---	---	0
LINE 49040		FLIGHT 83											
A	4697.7	S?	379910	6281081	7.2	16.4	10.6	37.9	0.7	5.6	0.5	5	0
B	4600.0	H	379989	6281859	1.5	0.2	9.0	8.6	1.3	0.6	---	---	0
LINE 49041		FLIGHT 147											
A	5406.2	B	380040	6284624	10.8	6.0	44.1	37.2	16.0	17.9	2.7	0	189
B	5411.6	H	380054	6284821	2.2	1.6	44.1	15.0	19.9	17.9	1.1	73	73
C	5438.1	H	380053	6285744	0.7	0.5	22.5	0.6	19.6	9.3	0.9	115	0
D	5717.1	S	380230	6291770	3.9	0.3	2.7	6.5	1.7	1.1	---	---	11

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 49050			FLIGHT 83										
A	5157.1	S	381437	6281426	8.8	3.9	8.8	15.8	1.4	2.7	3.4	27	0
LINE 49053			FLIGHT 147										
A	6897.7	E	381522	6284367	2.1	2.3	16.8	14.4	8.7	6.1	---	---	441
B	6927.5	H	381559	6285291	1.2	0.5	26.8	5.2	19.3	9.2	2.0	108	0
C	6975.0	S	381593	6286822	1.1	1.6	4.5	7.6	3.8	1.3	---	---	0
D	7269.0	S	381759	6292290	1.9	4.0	5.6	19.9	1.2	3.7	---	---	119
E	7294.4	S?	381759	6292944	4.5	0.2	7.0	2.1	7.7	0.8	---	---	313
F	7308.1	S	381772	6293296	3.2	0.4	38.9	4.1	18.8	0.1	---	---	0
G	7355.3	S	381801	6294646	3.7	1.0	16.0	3.1	19.0	1.7	---	---	0
LINE 49063			FLIGHT 147										
A	6685.2	S?	382947	6280622	1.0	2.8	5.3	13.2	10.5	1.2	---	---	0
B	6525.8	H	383008	6283997	1.5	0.6	14.2	9.4	17.2	10.7	1.9	81	85
C	6506.8	H	383014	6284606	5.6	5.2	57.9	58.2	16.3	22.9	1.2	15	0
D	6503.4	B	383022	6284714	9.2	5.7	57.9	59.0	15.9	22.9	2.2	21	0
E	6427.5	S?	383107	6287084	2.6	1.0	5.5	8.1	0.4	1.8	---	---	0
F	6331.3	S?	383162	6289290	4.7	2.6	25.3	41.1	28.3	6.2	---	---	0
G	6314.9	S?	383181	6289745	5.7	1.1	32.5	6.6	35.6	1.0	---	---	0
H	6288.8	S?	383200	6290431	5.2	6.3	4.5	18.0	5.2	2.6	---	---	0
I	6248.1	S	383241	6291484	0.9	1.7	7.6	10.8	10.7	1.6	---	---	0
J	6227.5	H	383242	6292112	1.2	1.1	7.7	1.4	5.6	0.4	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 49070			FLIGHT 83										
A	1853.3	H	384524	6283956	1.2	0.8	13.7	9.4	9.4	4.1	---	---	0
B	1819.3	H	384541	6284970	2.8	2.8	25.2	14.8	25.9	12.3	---	---	414
C	1688.0	S	384624	6287704	2.3	1.3	3.9	5.2	10.3	1.1	---	---	109
D	1577.3	S?	384663	6289379	14.1	1.6	47.2	12.6	55.8	2.3	---	---	64
E	1525.9	S	384685	6290425	1.5	1.2	30.5	6.3	32.6	1.0	---	---	144
F	1469.5	B?	384733	6291550	6.0	4.6	16.8	18.2	7.8	4.5	---	---	0
LINE 49080			FLIGHT 74										
A	1099.0	H	385963	6280834	2.9	3.8	11.9	6.4	2.6	3.1	---	---	0
B	1027.7	S	386002	6282385	2.7	0.8	4.1	4.2	3.8	1.1	---	---	0
C	982.0	H	386030	6283541	1.4	2.4	9.3	6.0	3.3	3.1	---	---	0
D	953.9	H	386036	6284342	3.9	3.1	18.3	17.1	1.5	7.6	---	---	508
LINE 49090			FLIGHT 74										
A	1449.8	S	387418	6279722	6.4	3.2	2.3	8.1	2.8	1.8	---	---	0
B	1522.7	S?	387457	6280892	8.2	3.8	1.7	11.7	1.9	2.1	---	---	334
C	1541.3	S?	387450	6281274	1.7	2.4	15.5	11.1	12.7	2.2	---	---	0
D	1560.0	S?	387454	6281575	3.9	2.3	11.2	5.2	13.1	1.3	---	---	261
E	1695.0	H	387524	6283626	2.0	1.1	4.7	1.4	1.7	1.8	---	---	452
F	1976.7	S	387636	6288027	0.9	1.6	7.3	4.4	7.1	0.6	---	---	0
LINE 49095			FLIGHT 181										
A	4486.0	S	387064	6268252	1.3	2.4	3.7	15.1	1.1	2.9	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 49100			FLIGHT 74										
A	2673.9	S	388910	6279831	2.0	4.1	7.2	8.4	9.0	0.7	---	---	0
B	2477.7	H	389031	6283663	3.7	3.6	10.5	8.1	8.3	4.6	1.0	38	503
C	2273.3	S?	389129	6287141	2.9	1.6	17.0	9.2	15.3	0.7	---	---	0
D	2184.2	H	389174	6288917	1.1	1.1	12.3	5.5	2.3	4.2	---	---	0
E	2171.3	H	389192	6289310	4.6	2.8	9.7	3.2	5.2	3.8	---	---	0
LINE 49105			FLIGHT 181										
A	3859.2	S?	388624	6268698	2.0	4.5	4.7	19.2	2.2	2.7	---	---	0
LINE 49111			FLIGHT 75										
A	408.3	S?	390473	6281529	3.5	7.4	16.7	28.6	1.7	5.2	---	---	0
B	426.1	S?	390475	6281907	8.1	6.9	16.4	26.7	2.0	6.0	1.5	21	0
C	478.1	H	390506	6283112	2.4	2.6	13.1	6.8	4.3	7.9	---	---	0
D	742.0	S	390625	6287555	1.6	3.1	4.2	8.5	2.9	1.3	---	---	20
LINE 49120			FLIGHT 75										
A	1318.7	H	392034	6283644	3.4	2.1	2.4	10.2	3.0	2.6	---	---	684
B	1102.1	S?	392122	6287263	16.1	3.3	10.5	4.4	20.2	1.7	---	---	0
C	1028.6	S	392167	6288522	4.3	2.2	40.5	1.7	48.9	1.5	---	---	0
D	996.1	S?	392191	6289125	27.8	3.7	35.5	7.5	25.0	8.2	29.1	25	0
E	987.9	D	392193	6289298	59.6	28.8	375.8	191.3	133.2	148.4	5.8	0	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 49125			FLIGHT 181										
A	5764.0	S?	391611	6267879	1.5	0.9	9.4	17.2	0.4	3.0	---	---	0
B	5790.7	S	391600	6268216	3.6	7.4	2.9	23.3	1.4	4.0	---	---	0
C	5946.3	S?	391654	6271708	4.4	2.6	21.7	24.3	1.3	8.4	1.9	33	0
LINE 49126			FLIGHT 221										
A	7003.8	S?	391118	6249969	2.0	3.8	10.9	38.8	2.0	4.8	---	---	0
LINE 49130			FLIGHT 75										
A	1909.1	S?	393361	6277325	5.6	3.8	6.9	1.9	7.1	0.5	---	---	0
B	1932.2	S?	393372	6277833	3.2	2.0	14.7	8.2	21.4	1.2	---	---	0
C	1966.5	E	393396	6278715	13.2	27.4	62.2	126.0	2.8	21.7	0.7	0	0
D	1970.5	B	393400	6278834	12.2	23.0	102.2	126.0	8.5	33.3	0.7	7	0
E	1974.5	B	393407	6278954	9.2	1.0	102.2	91.5	8.5	33.3	24.9	42	0
F	1979.2	B	393414	6279096	7.1	4.7	90.3	97.7	9.7	36.4	1.9	34	0
G	1983.2	E	393418	6279217	14.4	7.0	91.7	97.7	0.4	12.0	3.6	23	0
H	2041.9	S	393446	6280787	6.3	1.3	4.4	6.7	2.4	0.9	---	---	0
I	2130.7	H	393494	6282956	4.2	2.4	14.0	14.8	1.0	4.0	---	---	0
J	2187.1	S?	393529	6284667	2.7	1.4	6.6	1.5	6.7	1.8	---	---	0
K	2340.0	S	393619	6287554	3.2	3.1	6.0	5.4	2.4	0.7	---	---	0
L	2383.9	S	393659	6288341	5.5	0.5	3.2	5.0	1.6	0.5	---	---	0
LINE 49135			FLIGHT 181										
A	3267.2	S?	392982	6263304	0.6	1.9	10.0	25.5	1.1	4.7	---	---	0

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EM Anomaly List

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LINE 49135			FLIGHT 181										
B	2997.0	H	393159	6270285	1.4	0.5	1.5	0.7	1.8	1.2	---	---	0
LINE 49136			FLIGHT 221										
A	7174.0	S	392640	6250521	1.9	0.8	7.3	1.8	8.8	1.2	---	---	0
B	7269.3	S	392668	6252486	2.3	0.5	2.9	3.7	1.0	0.9	---	---	709
LINE 49140			FLIGHT 75										
A	3111.1	S	394812	6275509	0.5	2.4	2.2	2.2	1.0	0.4	---	---	0
B	3009.4	S	394900	6278470	7.0	3.2	3.0	0.3	4.7	1.7	---	---	0
C	2953.5	S	394918	6279883	4.4	1.3	6.1	20.2	2.7	3.2	---	---	32
D	2727.5	H	395085	6285066	2.0	0.6	6.9	6.1	2.0	1.9	---	---	0
E	2676.6	D	395085	6285965	8.8	6.3	34.6	11.8	21.8	13.0	1.9	12	0
F	2640.3	D	395128	6286762	21.6	8.5	53.2	14.8	36.1	22.7	5.4	18	34
LINE 49147			FLIGHT 181										
A	2331.0	S	394437	6261992	1.5	2.7	8.2	24.7	2.2	4.5	---	---	26
B	2561.0	S?	394568	6267001	5.2	7.5	5.6	15.8	1.3	1.8	0.7	21	0
C	2643.2	H	394644	6269581	1.7	0.3	6.9	0.6	0.6	0.6	---	---	1877
D	2683.5	B?	394665	6270239	3.7	3.5	17.2	26.5	0.6	5.6	1.0	30	0
LINE 49148			FLIGHT 227										
A	5932.2	S?	394276	6250065	2.0	0.7	7.0	3.8	1.7	1.8	---	---	0
B	5884.2	S	394255	6251123	0.5	0.2	2.8	6.5	0.9	0.6	---	---	0

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LINE 49150			FLIGHT 173										
A	8431.3	S?	395413	6243347	1.5	1.4	3.0	8.5	3.9	1.1	---	---	0
B	8546.7	S?	395512	6246232	0.8	1.9	2.6	6.8	0.1	1.3	---	---	18
C	8604.8	H	395548	6247920	1.7	1.5	23.1	5.3	16.0	9.4	0.9	44	0
D	8622.0	H	395566	6248496	2.1	2.8	11.4	16.4	1.9	3.6	---	---	0
E	8740.0	S	395664	6251756	1.3	0.7	1.1	4.6	0.9	1.2	---	---	0
F	8884.4	S?	395729	6254278	1.2	3.6	14.7	37.5	1.8	6.5	0.2	17	0
G	9039.9	S?	395853	6257697	1.8	0.0	6.0	2.7	7.9	0.5	---	---	0
LINE 49153			FLIGHT 148										
A	2479.0	S?	396324	6276742	1.5	1.2	7.7	2.6	9.7	0.9	---	---	0
B	2418.1	S	396354	6278247	2.9	1.1	19.2	1.2	19.8	0.4	---	---	0
C	2372.7	S?	396412	6279043	2.7	2.0	13.5	6.8	16.8	1.5	---	---	32
D	2270.3	S?	396460	6281625	2.6	1.2	3.6	7.2	4.0	1.6	---	---	12
E	2221.3	H	396514	6283054	3.7	2.1	12.7	7.3	7.3	5.9	---	---	0
F	2195.0	H	396530	6283591	0.3	1.4	1.0	1.5	2.2	0.8	---	---	0
G	2045.5	H	396562	6285540	0.7	1.6	9.4	2.0	13.1	1.6	---	---	0
H	2002.1	S	396632	6286844	6.2	0.7	23.3	5.2	26.5	0.3	---	---	0
LINE 49154			FLIGHT 148										
A	2745.5	H	396139	6269674	2.2	0.3	25.1	0.0	3.7	5.6	---	---	1764
B	2739.5	H	396140	6269916	3.2	7.7	33.2	49.5	1.1	13.2	0.4	8	0

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LINE 49163			FLIGHT 148										
A	3022.6	S?	397663	6270053	8.4	20.2	43.4	117.6	12.4	24.0	0.5	0	1482
LINE 49164			FLIGHT 148										
A	1772.9	B	397997	6283128	15.3	10.9	81.9	70.8	18.0	26.3	2.2	3	0
B	1776.4	D	398000	6283233	19.6	18.1	81.9	70.8	11.3	26.3	1.8	10	0
C	1794.4	B	398019	6283692	25.4	16.0	86.7	76.8	14.8	35.7	3.1	12	0
D	1806.0	B	398023	6283897	8.2	4.5	17.1	14.2	5.8	7.9	2.5	19	0
E	1851.5	D	398047	6284690	13.6	6.6	22.2	15.1	7.0	8.2	3.5	10	0
LINE 49165			FLIGHT 181										
A	7125.8	S?	397033	6246687	0.0	1.5	2.9	6.5	1.7	3.0	---	---	0
B	7067.0	S?	397024	6247402	7.6	1.5	8.2	2.0	8.8	1.8	---	---	0
C	6944.0	S?	397127	6250182	1.3	1.9	9.3	0.8	5.4	2.5	---	---	0
D	6890.3	H	397152	6251409	1.3	2.9	11.3	6.9	5.4	5.9	---	---	357
E	6866.5	H	397178	6252168	2.1	3.1	26.4	20.0	11.2	9.6	0.5	25	0
F	6624.8	B	397350	6257480	10.8	9.8	79.9	40.6	38.0	35.6	1.5	0	0
G	6617.2	D	397363	6257617	26.6	13.0	92.9	46.0	41.3	43.1	4.4	0	0
H	6578.8	B	397339	6258327	92.8	22.9	268.3	145.0	73.8	115.2	17.0	0	0
I	6571.5	D	397339	6258481	27.8	53.5	246.2	146.2	65.6	94.5	0.9	0	0
J	6569.3	B	397339	6258530	26.1	53.5	246.2	146.2	65.6	94.5	0.9	0	0
K	6567.7	D	397340	6258567	26.1	11.1	246.2	146.2	66.8	94.5	5.2	7	0
L	6559.1	D	397350	6258782	38.0	30.0	37.2	25.0	9.0	15.6	2.7	0	49
M	6552.7	D	397365	6258960	15.1	14.4	86.6	71.1	12.3	20.4	1.6	10	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 49165			FLIGHT 181										
N	6542.9	S	397373	6259251	8.8	7.9	34.9	82.9	3.9	15.7	1.4	21	40
O	6527.1	E	397374	6259692	0.5	12.3	14.2	81.5	3.3	13.7	0.1	0	50
P	6343.2	S	397472	6263054	1.3	1.5	1.0	9.6	0.6	1.4	---	---	0
LINE 49170			FLIGHT 227										
A	6359.1	S	398489	6246098	0.8	1.7	1.1	8.6	0.7	0.9	---	---	0
B	6517.5	S?	398582	6249318	2.1	1.3	9.6	5.3	2.4	1.8	---	---	0
C	6660.4	H	398734	6254077	1.4	5.1	71.6	76.0	16.2	13.1	0.2	7	18
D	6771.0	H?	398790	6256284	0.0	0.3	20.4	33.5	2.1	6.8	---	---	0
E	6815.0	H	398812	6257109	1.1	0.7	3.2	1.6	0.8	1.3	---	---	0
F	6848.3	H	398826	6257556	6.7	5.0	37.7	33.9	5.3	13.1	1.6	6	0
G	6863.7	B	398837	6257891	9.0	4.8	58.5	52.4	8.9	19.7	2.7	19	0
H	6873.1	H	398847	6258125	2.6	3.5	46.1	8.9	22.3	19.2	0.6	26	13
I	6876.6	B	398848	6258209	4.5	2.9	46.1	8.9	22.3	19.2	1.7	37	31
J	6881.5	H	398851	6258324	5.7	6.4	66.1	59.2	14.9	22.3	0.9	16	0
K	6897.4	H	398862	6258751	1.1	2.1	34.7	45.4	12.3	12.7	0.3	38	0
L	6903.8	E	398873	6258952	4.1	6.7	34.8	39.0	5.3	3.2	0.6	0	0
M	6919.1	S?	398883	6259458	0.9	1.6	5.0	3.1	5.0	0.6	---	---	0
N	6986.0	S?	398910	6260819	1.7	1.8	8.8	16.5	1.0	2.9	---	---	0
O	7035.4	S?	398938	6262108	0.6	0.1	4.0	7.6	1.4	1.8	---	---	0
P	7168.2	S?	399014	6263857	2.8	2.3	9.2	15.2	1.2	3.4	---	---	0
LINE 49173			FLIGHT 147										
A	2956.2	S	399465	6280853	0.6	0.7	1.5	5.6	1.1	1.3	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 49173			FLIGHT 147										
B	3115.4	S?	399516	6283389	0.6	0.4	2.8	14.5	1.9	2.3	---	---	0
LINE 49174			FLIGHT 148										
A	3357.8	E	399137	6269512	0.4	7.6	12.0	50.1	13.0	6.5	---	---	0
B	3345.5	S?	399141	6269821	2.2	3.8	21.6	40.5	15.4	6.6	0.4	33	0
C	3333.9	S?	399147	6270166	0.2	0.4	16.6	10.1	17.9	1.4	0.2	112	0
D	3321.0	S?	399164	6270529	3.5	1.4	19.1	22.5	13.2	4.3	3.0	68	0
E	3312.2	S?	399167	6270783	5.0	6.7	23.3	107.9	11.9	15.5	0.7	26	0
F	3281.2	S	399173	6271430	1.2	0.9	18.4	69.7	4.5	11.5	1.0	93	415
LINE 49180			FLIGHT 78										
A	508.2	S?	400738	6279962	4.4	3.2	15.9	27.3	4.9	4.7	---	---	0
B	569.0	S	401011	6281384	2.5	1.1	1.2	10.1	1.1	1.3	---	---	89
C	754.7	S?	401042	6284370	2.9	6.3	10.9	31.4	6.9	5.3	---	---	284
LINE 49181			FLIGHT 233										
A	4698.0	S	400026	6246650	2.0	2.3	33.4	4.2	43.3	1.1	0.7	19	0
B	4730.7	S?	400026	6246973	3.0	3.7	18.6	7.2	17.7	2.0	0.7	33	0
C	4761.5	S	400034	6247360	1.8	0.8	11.5	3.2	12.0	1.0	---	---	0
D	5048.3	H	400261	6254760	3.4	4.2	31.3	34.8	7.2	11.4	0.7	0	68
E	5370.0	H	400442	6261684	1.5	0.9	2.0	6.1	0.7	1.6	---	---	0
F	5389.9	H	400441	6262051	0.0	1.1	42.6	36.8	3.2	13.0	0.1	12	0
G	5404.7	B	400444	6262268	6.1	6.2	21.5	38.2	0.7	5.9	1.1	24	0
H	5536.7	S?	400489	6263905	2.3	0.0	15.2	21.5	0.8	5.9	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 49181			FLIGHT 233										
I	5565.4	S	400510	6264481	1.6	5.9	24.2	78.7	1.0	10.6	0.2	0	0
J	5583.7	S?	400514	6264691	2.3	9.4	24.2	65.4	0.6	11.8	---	---	0
K	5596.9	S	400515	6264874	1.2	12.8	27.7	89.8	1.1	14.4	0.1	0	0
LINE 49190			FLIGHT 173										
A	7836.7	E	401633	6252255	5.0	2.2	71.6	48.8	10.4	25.9	---	---	0
B	7830.9	H	401645	6252446	4.8	6.0	71.6	48.8	10.4	25.9	0.8	6	0
C	7798.2	S?	401724	6253324	7.6	2.5	45.2	5.3	51.3	0.4	4.8	36	0
D	7635.8	H	401758	6255370	1.4	2.4	22.6	25.0	3.2	7.0	0.4	48	0
E	7606.4	S?	401772	6256393	1.9	8.0	31.3	74.6	0.6	13.8	0.2	0	0
F	7562.7	H	401823	6257863	4.1	3.9	32.0	38.6	3.9	12.4	1.0	37	0
G	7542.6	H	401856	6258417	4.1	4.3	23.1	14.0	2.2	10.3	0.9	25	0
H	7536.8	S?	401862	6258573	2.7	1.0	23.1	11.0	7.2	10.3	2.9	34	0
I	7440.1	B	401880	6260406	7.6	4.8	42.3	35.1	6.5	17.5	2.1	16	0
J	7308.0	S?	401979	6263284	2.8	9.8	10.7	52.6	1.0	8.5	---	---	0
K	7239.7	H	402014	6265108	2.6	3.2	27.5	18.7	14.5	7.8	0.7	31	0
L	7228.4	H	402011	6265502	12.3	8.9	79.1	40.0	22.9	35.1	2.1	1	0
LINE 49191			FLIGHT 233										
A	4003.7	S	401485	6245201	1.3	0.7	4.1	7.2	3.8	1.8	---	---	11
LINE 49200			FLIGHT 173										
A	6694.7	H	403269	6255002	1.8	0.6	12.3	5.9	7.7	4.8	---	---	0
B	6764.3	S?	403306	6257195	2.8	4.1	26.5	59.3	3.7	11.4	0.6	27	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 49200			FLIGHT 173										
C	6776.0	H	403311	6257542	1.5	0.4	3.6	0.0	3.5	2.0	---	---	0
D	6798.3	S	403343	6258245	0.3	3.8	8.9	47.7	0.8	6.0	---	---	0
E	6928.0	H	403420	6262066	0.4	1.5	4.4	5.9	0.2	1.5	---	---	0
F	7029.7	H	403512	6265071	0.5	1.3	9.4	8.7	2.5	3.2	---	---	0
LINE 49201			FLIGHT 233										
A	3819.3	S	402996	6245321	1.8	0.6	2.9	6.6	0.9	1.6	---	---	0
LINE 49210			FLIGHT 173										
A	6319.0	H	404831	6258008	0.7	0.9	6.0	6.5	2.2	5.8	---	---	0
B	6191.3	S?	404920	6261435	0.5	1.1	4.0	4.4	0.5	1.0	---	---	0
LINE 49211			FLIGHT 233										
A	3562.7	S	404438	6243404	2.4	3.3	12.9	14.3	3.3	2.3	---	---	0
LINE 49222			FLIGHT 173										
A	3626.7	S	405993	6245537	2.5	1.2	9.0	6.2	9.0	1.2	---	---	0
B	3721.2	S?	406029	6247222	0.6	0.6	4.5	5.0	4.1	0.9	---	---	0
C	3892.0	S?	406171	6251675	1.9	2.4	7.9	14.3	8.5	2.4	---	---	0
D	4086.1	B	406326	6256824	4.6	4.9	18.0	29.4	0.9	6.5	0.9	29	0
LINE 49230			FLIGHT 173										
A	2438.7	H	407630	6250192	0.9	1.4	7.1	9.7	1.3	3.0	---	---	120
B	2305.3	S?	407676	6253879	0.1	2.1	12.7	23.8	3.0	4.1	0.1	0	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 49230		FLIGHT 173											
C	2231.9	B	407763	6255428	5.8	5.1	36.0	32.6	6.9	16.2	1.2	18	0
D	2177.0	S	407811	6257225	1.4	1.6	5.0	9.5	0.0	2.3	---	---	0
LINE 49231		FLIGHT 173											
A	2746.6	S?	407430	6244191	1.6	3.7	9.0	0.6	11.1	0.7	---	---	0
LINE 49240		FLIGHT 173											
A	4784.2	S?	408961	6244479	1.2	0.3	4.4	22.7	1.4	2.9	---	---	363
B	4756.6	S?	408988	6245300	4.5	1.6	20.3	25.0	27.4	3.3	---	---	0
C	4742.0	B?	408995	6245739	1.6	7.9	12.7	22.1	8.5	5.1	---	---	428
D	4547.1	S	409131	6249810	2.0	0.9	1.9	2.3	0.3	0.9	---	---	0
E	4485.0	S	409172	6251782	0.8	1.9	4.6	10.1	2.2	2.1	---	---	0
F	4415.7	H	409218	6253954	0.7	0.4	5.1	3.5	0.7	1.2	---	---	0
G	4344.5	B?	409277	6256341	1.6	1.5	12.6	12.3	7.5	5.5	---	---	0
H	4334.1	H	409294	6256587	0.4	1.4	10.8	3.4	8.3	4.1	---	---	0
LINE 49250		FLIGHT 173											
A	5221.0	S?	410436	6243439	2.6	2.3	21.3	10.1	22.7	2.3	---	---	0
B	5388.1	H	410533	6247215	3.3	3.3	34.6	25.7	2.7	10.7	0.9	0	187
C	5565.8	S?	410621	6250548	4.0	4.2	21.6	52.0	2.8	9.7	0.9	16	46
D	5813.7	S	410770	6255557	0.9	3.9	4.0	20.2	0.8	2.6	---	---	0
E	5841.8	H	410788	6256447	2.6	1.6	8.1	3.2	2.3	2.7	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 49260			FLIGHT 225										
A	2411.1	S?	412040	6246046	1.9	3.9	27.9	29.7	0.9	8.2	0.4	9	0
LINE 49270			FLIGHT 225										
A	3132.4	D	413327	6239138	19.9	13.4	55.2	44.7	15.7	21.1	2.6	14	0
LINE 49271			FLIGHT 233										
A	2755.1	H	413426	6243212	0.8	2.1	11.7	25.4	0.8	4.4	---	---	0
LINE 49272			FLIGHT 225										
A	3509.5	D	413551	6247371	8.7	7.8	36.2	33.5	13.7	15.8	1.4	9	0
LINE 49280			FLIGHT 225										
A	4362.3	S	414733	6234857	3.1	6.3	12.3	26.4	10.7	3.1	---	---	0
B	4040.0	S?	414898	6241852	1.0	1.5	2.5	11.1	3.2	1.6	---	---	71
C	3839.0	S?	415044	6246214	0.8	1.0	4.9	3.8	0.9	1.8	---	---	0
LINE 49290			FLIGHT 225										
A	4473.3	S?	416183	6235294	0.8	3.0	1.0	8.6	0.1	1.9	---	---	0
B	4489.2	S?	416201	6235504	2.8	1.2	13.0	7.2	15.3	1.6	---	---	0
C	4757.1	S?	416353	6241069	0.6	0.7	0.0	5.2	0.0	0.9	---	---	142
D	4958.7	S?	416496	6246182	3.5	0.6	8.4	13.9	4.3	3.2	---	---	49

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 49300			FLIGHT 221										
A	9177.7	S	418006	6246057	2.1	1.7	13.2	11.8	6.1	2.8	---	---	0
LINE 50230			FLIGHT 82										
A	9393.0	S	382127	6292975	0.7	0.6	9.4	7.9	12.3	0.9	---	---	0
B	9421.7	S?	382644	6292907	4.0	1.0	53.4	7.7	61.9	1.6	---	---	221
C	9433.4	S?	382847	6292879	7.1	4.1	26.1	18.7	30.8	2.3	---	---	25
D	9492.0	S?	383688	6292884	1.2	2.5	2.7	18.4	1.4	2.3	---	---	107
LINE 50240			FLIGHT 82										
A	9290.0	S?	383210	6292706	3.5	2.8	9.8	12.0	11.7	1.9	---	---	55
B	9245.0	S	383568	6292736	1.8	2.7	30.8	14.2	18.5	1.9	---	---	0
C	9219.3	S?	383903	6292715	6.3	0.7	8.2	10.5	9.8	1.9	---	---	18
D	9206.1	S	384039	6292699	6.1	0.2	33.7	20.7	38.6	2.7	---	---	0
LINE 50250			FLIGHT 82										
A	9034.2	S	382245	6292584	5.3	1.8	21.1	8.7	24.7	1.0	---	---	0
B	9083.0	S?	383146	6292605	1.0	2.2	4.0	20.6	4.7	2.3	---	---	122
LINE 50260			FLIGHT 82										
A	8933.0	S?	383204	6292447	2.6	1.5	13.7	18.4	15.4	2.9	---	---	60
B	8904.2	S?	383522	6292429	2.4	2.9	12.2	16.0	15.9	2.5	0.6	39	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50270			FLIGHT 82										
A	8793.0	S	383839	6292275	0.4	9.0	5.8	38.0	2.0	5.8	---	---	0
LINE 50280			FLIGHT 82										
A	8538.7	S	384009	6292145	1.2	2.6	13.2	29.2	3.7	4.8	---	---	23
LINE 50290			FLIGHT 82										
A	8295.0	S	384057	6291963	2.2	2.4	12.5	28.5	3.2	4.2	---	---	0
LINE 50300			FLIGHT 82										
A	7946.0	S	384513	6291804	1.2	3.7	8.9	25.5	6.2	3.8	---	---	0
LINE 50310			FLIGHT 82										
A	7733.3	S	384602	6291667	1.9	5.5	3.0	29.9	0.1	5.4	---	---	0
B	7771.0	S	385384	6291636	7.3	5.8	6.9	32.5	1.8	4.1	---	---	0
LINE 50320			FLIGHT 82										
A	7315.4	S	383345	6291551	3.1	2.7	64.3	15.4	76.2	0.9	---	---	0
B	7309.8	E	383435	6291544	7.1	2.0	64.2	15.4	76.2	2.2	---	---	0
C	7286.7	S?	383908	6291512	3.6	3.0	23.9	13.4	24.0	2.4	---	---	0
D	7253.4	S?	384690	6291490	8.2	3.3	32.7	17.7	32.3	6.8	---	---	0
E	7229.1	S	385232	6291484	1.5	2.1	11.4	23.1	16.3	3.4	---	---	104

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50330			FLIGHT 82										
A	6981.7	S?	383935	6291354	0.8	6.1	7.6	30.7	0.0	4.9	---	---	0
B	7042.0	S	385094	6291345	0.6	1.3	4.2	12.6	2.4	0.9	---	---	0
LINE 50340			FLIGHT 82										
A	6671.3	S	383287	6291229	1.2	0.3	16.1	3.7	19.7	1.0	---	---	0
B	6652.5	S	383639	6291224	3.5	2.3	9.5	18.3	11.2	2.2	---	---	0
C	6570.2	B?	385537	6291198	3.3	3.4	13.7	19.6	3.4	6.5	---	---	0
LINE 50350			FLIGHT 82										
A	5668.0	S?	382188	6291101	0.3	0.6	0.3	4.4	2.3	0.8	---	---	327
B	5751.1	S	383402	6291056	5.7	2.4	24.6	11.1	27.3	1.7	3.1	43	0
C	5761.2	S?	383589	6291055	2.6	2.7	7.3	11.1	10.4	1.6	---	---	0
LINE 50360			FLIGHT 82										
A	5501.3	S?	383456	6290934	1.8	2.3	8.5	6.6	5.9	1.4	---	---	0
LINE 50370			FLIGHT 82										
A	5176.8	S	383453	6290786	1.8	6.1	53.8	10.5	61.6	1.6	---	---	0
B	5218.2	S?	384226	6290770	10.3	2.6	31.1	3.8	36.5	1.0	---	---	0
C	5230.4	E	384436	6290767	11.8	1.4	40.6	19.5	47.3	3.0	---	---	0
D	5273.0	S	385187	6290742	2.0	2.3	21.3	5.7	26.2	1.4	---	---	0
E	5286.8	S?	385447	6290728	6.5	2.7	23.0	14.5	23.8	1.3	---	---	150

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50390			FLIGHT 82										
A	4553.3	S?	383363	6290491	3.4	0.1	8.7	9.0	10.6	1.2	---	---	22
B	4588.0	S	384059	6290459	0.7	0.0	2.2	11.7	4.4	1.3	---	---	0
LINE 50400			FLIGHT 82										
A	4274.8	S?	383759	6290321	5.2	0.7	29.2	1.6	33.3	0.6	---	---	130
B	4262.1	S	384038	6290312	1.3	0.6	10.3	2.7	12.1	0.6	---	---	0
LINE 50410			FLIGHT 82										
A	4014.5	S?	383582	6290170	2.0	2.5	8.2	13.6	23.6	1.9	---	---	0
LINE 50420			FLIGHT 82										
A	3680.0	S?	383542	6290033	2.4	4.6	12.3	33.1	8.1	5.0	---	---	0
LINE 50430			FLIGHT 82										
A	3332.7	S?	383497	6289881	3.1	1.8	3.5	5.8	2.7	1.6	---	---	0
B	3345.0	S?	383794	6289867	5.8	1.8	20.8	2.8	24.6	0.7	---	---	0
LINE 50440			FLIGHT 82										
A	3055.2	S	383356	6289724	1.7	3.1	7.1	19.1	3.3	1.9	---	---	0
LINE 50450			FLIGHT 82										
A	2787.0	S	383502	6289604	2.1	0.0	8.7	0.2	10.5	0.8	---	---	0
B	2841.0	S?	384812	6289556	5.4	0.5	31.3	7.4	35.9	1.9	---	---	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50460			FLIGHT 82										
A	9852.0	S	383014	6289460	7.1	1.9	66.1	6.1	75.0	1.2	---	---	0
B	9873.8	S?	383510	6289434	4.7	2.4	65.0	2.7	76.3	0.7	---	---	0
C	9889.4	S	383861	6289410	6.7	0.8	25.6	9.7	28.4	1.3	---	---	0
D	9918.1	S	384379	6289401	2.5	2.4	15.7	11.7	17.8	1.7	---	---	0
E	10035.1	S	386638	6289348	3.8	2.8	8.2	35.5	2.7	2.6	---	---	0
F	10174.0	D	389492	6289270	5.6	0.6	50.7	11.7	22.8	20.1	---	---	37
G	10180.0	D	389615	6289277	5.0	6.7	71.3	70.6	22.8	24.3	0.8	18	13
H	10308.9	B	391276	6289208	11.8	18.0	70.0	87.8	7.8	26.5	0.9	3	0
I	10339.6	D	391921	6289203	52.8	26.4	220.8	194.7	104.1	96.7	5.3	6	22
J	10344.1	B?	392034	6289203	14.1	4.8	225.7	96.6	121.8	92.1	5.8	23	0
K	10346.7	B	392101	6289204	34.4	23.5	225.7	96.6	121.8	92.1	3.1	2	0
L	10405.8	B?	393532	6289142	6.6	11.6	26.2	52.2	3.9	11.4	0.6	5	0
M	10480.0	H	394735	6289166	1.0	1.6	0.7	3.8	1.3	0.6	---	---	0
LINE 50470			FLIGHT 83										
A	1125.5	S	383143	6289284	3.9	2.6	40.9	15.3	35.5	2.3	---	---	0
B	1102.7	S	383739	6289276	6.7	1.3	29.9	13.6	34.7	2.6	---	---	0
C	1096.1	S	383864	6289273	11.8	1.8	7.9	18.8	13.6	2.9	---	---	114
D	1057.7	S	384745	6289249	9.4	0.6	31.4	4.5	40.2	1.4	---	---	0
E	1031.7	S?	385377	6289222	0.0	0.8	121.0	2.6	141.3	2.9	---	---	499
F	997.4	S?	386040	6289230	22.2	1.3	4.1	8.3	5.1	2.3	---	---	107
G	928.6	B?	387480	6289194	2.3	2.3	12.4	14.4	2.0	4.1	---	---	33
H	856.7	B?	389420	6289131	5.2	4.3	8.1	7.3	4.3	4.2	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50470			FLIGHT 83										
I	850.0	H	389619	6289122	1.3	1.5	9.1	6.1	6.4	5.1	---	---	47
J	758.9	B	391399	6289072	9.7	14.5	35.4	45.7	7.5	13.1	0.8	2	0
K	753.0	B?	391521	6289075	6.9	8.1	17.0	34.7	1.6	7.1	1.0	27	0
L	735.2	B	391853	6289071	8.9	4.9	31.0	22.5	21.4	5.1	2.6	16	0
M	666.8	B	393489	6289014	15.1	13.4	95.5	129.9	13.1	33.5	1.7	4	17
N	664.3	E	393561	6289016	13.9	21.1	95.5	129.9	13.1	33.5	0.9	1	21
O	543.5	B?	394674	6288993	2.5	4.4	19.6	26.7	1.7	4.9	---	---	0
P	531.0	B	394807	6288984	8.6	7.5	30.9	30.1	1.4	12.6	1.5	18	0
LINE 50480			FLIGHT 78										
A	5014.0	S	383164	6289144	3.0	3.0	4.7	19.9	2.3	3.2	---	---	0
B	5075.8	S	384505	6289114	4.1	2.4	17.9	2.0	18.7	1.2	---	---	0
C	5280.0	H	389335	6288963	2.4	1.3	7.2	6.1	3.6	3.0	---	---	23
D	5387.2	D	391412	6288931	9.2	4.2	28.9	23.1	6.7	11.0	3.3	0	0
E	5472.3	B?	393369	6288865	4.9	6.3	39.1	65.7	1.8	15.7	0.8	15	15
LINE 50490			FLIGHT 78										
A	4821.0	S?	383367	6288944	2.8	0.8	9.1	14.4	1.4	2.3	---	---	0
B	4747.7	S	384596	6288965	1.4	1.0	16.0	6.4	16.9	1.5	---	---	0
C	4641.6	S	386689	6288905	2.3	1.7	12.5	6.8	13.1	0.2	---	---	0
D	4619.2	S	387176	6288856	2.8	1.1	14.9	2.4	17.0	0.9	---	---	0
E	4510.1	H	389439	6288847	2.8	2.7	10.2	5.4	8.1	5.5	---	---	47
F	4267.7	B?	393463	6288722	3.1	3.8	16.3	33.2	3.5	7.2	0.7	39	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50500			FLIGHT 64										
A	2479.5	S?	383443	6288834	1.5	3.6	1.6	12.3	3.9	1.4	---	---	0
B	2334.0	S	386577	6288724	4.7	2.1	11.9	3.6	6.4	0.8	---	---	0
C	2210.3	H	389569	6288650	4.7	4.5	6.6	4.0	3.0	2.0	---	---	0
D	2049.7	S?	391882	6288620	1.2	0.5	0.2	8.6	0.1	0.5	---	---	147
E	1996.9	S	393008	6288576	3.2	1.4	16.7	4.1	18.6	1.0	---	---	0
F	1980.0	S?	393431	6288566	1.9	2.7	5.5	12.1	2.2	2.2	---	---	0
LINE 50510			FLIGHT 64										
A	1296.0	S	383405	6288693	1.7	1.1	12.0	7.0	5.4	1.3	---	---	0
B	1420.0	S	386539	6288627	1.8	1.6	5.0	3.1	4.9	1.3	---	---	0
C	1545.2	S?	389857	6288533	3.4	2.5	7.9	18.7	2.0	3.5	---	---	0
D	1737.3	S	393567	6288401	0.5	0.5	5.7	21.7	1.3	3.5	---	---	12
LINE 50521			FLIGHT 64										
A	688.0	S	389928	6288370	1.2	1.1	4.7	8.4	0.7	1.4	---	---	12
B	482.2	S?	393496	6288251	3.7	4.4	3.0	13.5	2.3	2.0	---	---	0
LINE 50522			FLIGHT 64										
A	960.2	S	385690	6288461	3.1	1.8	7.5	5.7	9.3	0.9	---	---	0
B	928.1	S	386518	6288436	1.0	0.8	4.5	10.6	4.9	1.9	---	---	0
LINE 50530			FLIGHT 63										
A	6094.1	S	390015	6288205	1.5	1.3	5.7	10.1	1.2	1.8	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50530			FLIGHT 63										
B	6251.0	S	393553	6288143	0.9	3.9	3.2	16.4	0.9	2.5	---	---	0
LINE 50540			FLIGHT 63										
A	5576.0	S	386543	6288127	4.5	2.7	4.4	11.8	2.7	2.0	---	---	0
B	5520.0	S	388029	6288114	3.2	0.3	3.9	1.5	6.1	0.8	---	---	0
C	5175.7	B?	394564	6287929	2.0	1.6	18.0	18.9	1.9	6.5	1.0	60	0
LINE 50550			FLIGHT 63										
A	4716.0	S	387624	6287969	2.2	3.6	12.4	8.6	12.1	1.8	---	---	0
B	4912.4	S?	391488	6287840	6.2	0.4	21.0	0.8	24.1	0.2	---	---	0
C	5046.1	S?	394512	6287814	2.1	2.6	6.0	11.4	1.2	2.9	---	---	0
LINE 50560			FLIGHT 63										
A	4263.7	S	386596	6287839	2.2	3.2	8.5	20.6	5.2	3.1	---	---	0
B	4183.4	S?	388009	6287799	33.0	0.8	197.7	7.2	225.5	0.6	---	---	289
C	4163.9	S?	388208	6287809	2.9	1.3	0.0	11.3	0.0	0.6	---	---	0
D	3816.0	S	393473	6287671	3.4	0.2	22.1	5.4	25.0	0.7	---	---	0
E	3751.6	B?	394680	6287608	2.1	10.6	3.6	22.8	0.2	4.0	0.2	0	0
LINE 50570			FLIGHT 63										
A	3175.0	S	385220	6287738	1.6	2.8	5.4	8.6	2.0	1.8	---	---	0
B	3280.5	S?	387754	6287692	3.0	0.1	37.8	0.7	42.9	1.5	---	---	0
C	3285.8	S?	387835	6287671	0.0	1.4	0.0	5.2	0.0	1.0	---	---	177
D	3559.5	D	393780	6287523	1.5	9.6	3.6	24.4	7.4	4.3	---	---	11

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50580			FLIGHT 63										
A	2858.3	S?	384977	6287601	0.8	4.1	0.8	18.0	0.2	3.1	---	---	0
B	2669.8	S	388453	6287483	0.0	1.9	115.5	10.1	1.5	1.4	---	---	162
C	2645.3	S?	388645	6287494	5.0	1.3	42.6	4.6	51.1	1.4	---	---	28
D	2487.1	S	390544	6287463	1.6	2.7	2.0	3.6	1.1	0.5	---	---	11
E	2318.4	E	393684	6287360	5.8	4.3	35.9	8.9	33.4	1.5	---	---	0
F	2304.9	D	394018	6287335	28.8	33.9	109.1	88.5	23.0	43.9	1.5	5	0
LINE 50590			FLIGHT 63										
A	1640.0	S?	384087	6287453	1.0	1.3	2.3	6.3	1.8	1.6	---	---	35
B	1708.0	S	386262	6287425	1.5	1.1	8.7	2.2	7.1	1.1	---	---	0
C	1806.9	S	388413	6287336	2.8	1.7	33.8	1.8	38.3	0.3	---	---	0
D	2032.9	S?	392569	6287240	1.9	2.3	17.1	5.8	20.1	0.8	---	---	0
E	2051.3	S?	393014	6287240	0.9	1.5	6.6	4.6	6.1	1.1	---	---	240
F	2091.9	B?	393928	6287218	0.4	3.7	11.1	11.6	13.1	2.3	---	---	0
G	2113.0	B	394414	6287205	0.8	3.1	16.6	26.3	3.9	8.5	---	---	0
LINE 50601			FLIGHT 63										
A	1214.7	S	385867	6287259	1.3	1.7	9.3	8.7	8.2	1.5	---	---	0
B	1008.0	S?	389236	6287191	2.5	3.5	9.8	11.0	9.5	1.6	---	---	48
C	723.0	B	393929	6287041	6.9	7.2	14.6	14.2	8.6	3.1	1.1	16	0
D	703.4	D	394399	6287034	11.4	14.2	35.2	46.7	3.8	13.7	1.1	9	0
E	698.2	B	394502	6287036	8.1	8.3	35.2	46.7	3.8	13.7	1.2	17	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50610		FLIGHT 52											
A	2902.5	S	385910	6287123	1.6	0.4	6.8	5.9	5.8	0.8	---	---	0
B	3017.6	S?	388543	6287055	0.4	2.1	18.2	9.0	22.3	1.0	---	---	0
C	3021.0	S?	388623	6287052	1.7	2.3	18.2	9.0	22.3	1.2	---	---	19
D	3260.0	B?	393974	6286912	4.4	3.5	6.5	5.6	6.1	1.5	---	---	0
LINE 50620		FLIGHT 52											
A	2302.3	S?	378227	6287171	1.1	2.6	1.2	2.5	0.4	0.7	---	---	0
B	2152.0	S	381874	6287081	0.3	1.9	6.1	3.1	5.2	0.6	---	---	0
C	2117.7	S?	382886	6287033	1.5	3.5	6.2	6.4	1.9	1.4	---	---	0
D	1994.1	S?	386173	6286938	1.8	0.9	5.4	4.1	2.5	0.9	---	---	0
E	1881.3	S?	388825	6286904	1.7	1.8	5.7	3.8	11.1	1.3	---	---	0
F	1555.2	B	395080	6286708	10.5	5.2	68.9	24.6	37.3	28.9	3.2	27	0
G	1543.7	B	395209	6286722	7.6	5.2	23.6	16.4	13.6	9.6	1.8	30	0
H	1534.9	B	395320	6286729	4.7	0.9	41.9	0.0	53.2	5.4	9.6	55	0
I	1525.4	B	395430	6286732	9.8	2.7	52.5	20.2	36.4	18.3	6.9	36	0
LINE 50630		FLIGHT 52											
A	600.7	S?	381769	6286915	1.7	1.9	3.8	6.8	0.9	0.7	---	---	0
B	760.0	S	386166	6286825	1.5	0.7	6.8	2.9	5.9	0.5	---	---	0
C	845.9	S?	388439	6286765	5.2	1.9	38.9	5.3	42.1	1.1	---	---	0
D	857.6	S?	388717	6286766	3.0	0.3	51.6	0.3	59.9	0.5	---	---	0
E	1148.7	B	394991	6286580	6.2	1.8	17.0	7.0	13.2	6.0	5.4	42	0
F	1158.0	B	395184	6286582	2.6	3.0	9.3	3.4	6.4	4.3	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50640			FLIGHT 48										
A	9553.3	S	381715	6286784	1.5	2.1	4.4	6.4	2.5	1.4	---	---	0
B	9816.8	S?	388680	6286620	1.6	1.7	10.2	9.6	12.0	1.9	---	---	55
C	10108.0	B?	394921	6286424	3.0	2.5	3.8	1.8	0.7	1.4	---	---	0
D	10120.7	B?	395151	6286432	2.2	2.1	8.0	4.7	4.7	3.5	---	---	0
LINE 50650			FLIGHT 20										
A	7608.4	B	394556	6286268	6.7	0.0	7.9	13.7	0.1	2.9	846.7	55	0
B	7603.1	B	394672	6286280	4.4	3.4	14.3	8.6	8.5	7.7	1.3	45	0
C	7596.7	B	394803	6286286	3.9	0.7	1.2	2.8	1.1	0.5	---	---	0
D	7590.1	B	394932	6286289	3.0	4.2	25.1	21.2	6.7	10.9	0.6	40	0
E	7582.4	B	395083	6286282	10.3	7.6	26.5	18.5	3.4	8.5	1.9	26	0
F	7577.5	B	395182	6286280	2.3	2.9	26.5	19.8	6.4	8.5	0.6	26	0
G	7573.5	B?	395265	6286276	8.6	8.0	17.6	19.8	8.1	7.7	1.3	25	0
H	7549.7	H	395612	6286274	4.7	1.9	0.9	7.1	2.0	1.3	3.1	59	0
I	7518.7	S?	396429	6286227	0.1	1.9	0.0	10.6	0.1	6.0	---	---	736
J	7499.2	S?	397012	6286227	5.7	0.0	17.3	6.8	21.3	5.2	---	---	765
LINE 50655			FLIGHT 147										
A	3582.7	S	389215	6286437	1.2	0.9	1.3	3.0	6.8	1.1	---	---	0
LINE 50660			FLIGHT 20										
A	6582.0	S?	379104	6286548	0.8	0.4	3.0	2.9	0.7	0.7	---	---	0
B	6635.0	S?	380699	6286500	3.3	1.6	2.2	4.0	0.9	1.3	---	---	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50660			FLIGHT 20										
C	6684.3	S?	382447	6286464	0.4	3.0	2.0	2.6	1.1	1.2	---	---	0
D	6906.3	S	389072	6286291	1.6	1.3	2.8	2.1	5.3	0.6	---	---	0
E	6928.9	S?	389714	6286264	0.1	1.0	9.8	1.7	11.5	2.0	---	---	79
F	7119.8	B	394627	6286122	5.3	3.6	11.4	18.5	1.5	7.1	1.6	26	0
G	7133.2	B	395014	6286145	4.4	2.8	11.2	2.6	6.8	3.6	---	---	0
H	7184.2	S?	396384	6286072	1.5	0.9	0.0	7.6	0.0	2.1	---	---	1003
LINE 50671			FLIGHT 20										
A	5978.5	H	382294	6286305	3.2	1.2	28.7	23.8	3.0	9.7	3.2	59	0
B	5700.0	S?	389683	6286103	0.0	1.5	0.0	3.9	0.0	11.6	---	---	202
C	5675.9	S?	390016	6286086	6.6	1.4	144.1	6.2	197.8	0.0	---	---	0
D	5412.7	B	394965	6285966	15.5	6.0	3.4	0.0	5.2	0.0	---	---	0
E	5408.3	B	395085	6285961	15.5	4.9	78.9	27.3	69.9	29.8	6.6	27	24
F	5379.2	D	395740	6285977	14.1	6.9	24.6	25.4	8.9	11.2	3.5	16	111
G	5371.7	B	395978	6285970	3.8	0.0	15.8	0.9	13.5	1.7	---	---	0
LINE 50680			FLIGHT 20										
A	4079.6	S?	380620	6286195	4.3	3.3	9.5	20.7	1.4	4.8	---	---	0
B	4122.3	H	382298	6286179	4.9	4.5	52.0	49.9	4.7	15.3	1.1	27	0
C	4578.8	H	395769	6285851	1.4	1.7	15.2	8.9	6.1	6.5	---	---	164
D	4615.9	H	397084	6285795	5.0	3.8	5.1	2.4	6.7	0.3	---	---	0
LINE 50690			FLIGHT 17										
A	9410.4	B?	380603	6286058	6.0	0.0	5.1	11.3	0.9	2.1	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50690			FLIGHT 17										
B	9426.7	S?	381145	6286021	3.0	2.4	6.2	15.5	2.1	4.1	---	---	10
C	9466.7	S?	382466	6286004	3.7	1.6	3.5	16.2	1.2	2.5	---	---	0
D	9732.0	S?	390142	6285810	0.0	3.2	29.8	2.3	37.7	5.7	---	---	236
E	9955.0	H	395662	6285695	3.1	6.0	9.7	7.2	3.4	3.2	---	---	0
F	9990.0	H	396853	6285628	0.8	1.5	3.3	1.2	4.4	0.7	---	---	280
LINE 50700			FLIGHT 17										
A	8098.5	H	395331	6285501	1.0	2.1	11.4	7.2	4.6	4.8	---	---	0
B	8048.4	B?	396809	6285470	2.6	0.9	2.1	2.1	3.5	1.8	---	---	0
LINE 50710			FLIGHT 17										
A	7282.4	H	378261	6285833	2.4	3.8	16.8	22.0	0.5	5.0	0.5	36	0
B	7332.3	H	380043	6285774	1.8	0.1	3.2	1.8	7.0	1.0	---	---	0
C	7337.7	B	380238	6285771	2.4	1.1	3.1	1.3	4.7	1.1	---	---	0
D	7387.1	S	381956	6285725	0.0	2.2	6.3	15.6	2.7	2.7	---	---	11
E	7833.5	H	394404	6285391	2.0	1.6	8.1	3.6	3.4	2.5	---	---	0
F	7855.3	H	395084	6285362	1.4	0.5	4.2	1.5	2.9	0.7	---	---	0
G	7889.0	H	396221	6285331	1.1	1.3	2.0	3.6	3.9	0.2	---	---	0
LINE 50721			FLIGHT 17										
A	6912.5	H	377462	6285709	2.5	0.0	18.6	4.9	17.9	9.1	---	---	0
B	6897.2	H	377977	6285692	1.6	0.3	3.1	0.7	5.5	1.1	---	---	0
C	6867.8	H	378941	6285630	1.0	2.5	8.2	12.8	11.6	2.8	0.3	16	141
D	6833.3	H	380109	6285639	0.6	2.2	0.0	1.1	0.8	0.6	---	---	12

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50721		FLIGHT 17											
E	6795.1	E	381345	6285570	2.3	1.8	23.1	9.9	12.9	9.1	1.1	62	0
F	6620.5	S	386491	6285438	2.7	1.0	5.2	3.3	4.4	1.2	---	---	0
G	6344.4	S?	392807	6285301	0.3	3.0	3.2	9.6	1.5	2.3	---	---	0
H	6280.7	H	394418	6285254	1.2	1.7	9.8	0.6	3.9	3.8	---	---	0
I	6258.7	H	395035	6285226	2.0	2.0	3.6	0.4	3.7	0.9	---	---	0
J	6238.8	H	395602	6285177	2.6	0.5	0.9	4.1	1.0	0.4	---	---	0
K	6180.4	H	397213	6285150	2.5	0.7	7.3	4.8	5.9	3.4	---	---	0
LINE 50730		FLIGHT 17											
A	5253.1	H	377068	6285543	0.0	1.5	10.5	0.6	11.5	3.5	---	---	128
B	5270.0	H	377647	6285535	1.4	0.6	3.7	4.7	3.0	1.7	---	---	17
C	5325.7	H	379478	6285494	0.3	2.3	3.0	0.0	2.7	3.1	---	---	0
D	5375.0	H	381141	6285427	1.9	0.2	7.0	3.1	6.2	2.1	---	---	0
E	5759.0	S?	392781	6285117	1.5	1.5	2.7	5.3	1.4	1.4	---	---	0
F	5806.0	H	394310	6285083	1.9	0.0	5.1	8.1	5.5	3.2	---	---	0
G	5820.7	H	394805	6285065	1.9	0.9	3.8	6.6	1.3	0.7	---	---	321
H	5843.0	H	395505	6285074	0.6	0.0	1.8	2.0	2.7	0.7	---	---	0
I	5889.9	H	397126	6285046	4.5	1.6	21.5	6.5	14.3	12.2	3.6	43	0
J	5893.4	H	397247	6285038	4.3	1.6	21.5	19.0	8.9	12.2	3.6	52	0
LINE 50740		FLIGHT 17											
A	4913.5	E	376378	6285439	5.2	2.6	35.8	21.0	10.4	14.5	---	---	0
B	4904.0	H	376681	6285404	3.7	1.9	32.7	19.8	15.4	14.2	2.1	48	94
C	4889.7	H	377123	6285378	1.8	1.3	0.2	0.1	0.0	0.6	---	---	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50740		FLIGHT 17											
D	4837.5	H	378706	6285351	1.6	1.5	7.0	23.3	5.7	5.2	---	---	0
E	4804.7	H	379702	6285328	5.3	4.2	19.1	38.3	7.3	8.2	1.4	24	0
F	4755.0	H	381187	6285291	1.7	3.3	23.2	22.1	14.5	9.1	0.4	24	0
G	4719.0	H	382294	6285262	2.0	0.7	4.5	2.4	8.4	1.7	---	---	0
H	4706.3	E	382683	6285240	7.5	1.5	37.0	15.5	17.0	17.7	10.2	41	0
I	4621.6	B	385007	6285186	7.7	8.2	47.1	56.5	8.1	23.5	1.1	14	0
J	4618.0	H	385108	6285180	5.8	6.4	47.1	56.5	9.6	23.5	1.0	23	0
K	4227.5	H	393955	6284950	0.5	2.1	7.0	0.7	5.7	1.7	---	---	0
L	4197.3	H	394821	6284925	2.0	0.8	6.3	5.3	2.9	1.8	---	---	158
M	4111.7	B	397399	6284858	6.2	1.4	38.8	14.5	20.2	16.7	7.7	39	0
LINE 50750		FLIGHT 20											
A	1329.4	H	376132	6285279	5.7	5.5	49.4	33.1	32.2	20.7	1.1	9	0
B	1326.5	B	376225	6285279	11.7	9.4	50.2	83.6	25.5	30.8	1.8	7	99
C	1321.1	H	376405	6285275	6.1	7.7	51.7	83.6	31.0	31.7	0.9	20	0
D	1303.3	H	376959	6285264	4.5	1.8	7.3	4.4	6.3	2.4	---	---	12
E	1254.0	H	378473	6285212	2.1	2.3	15.5	14.6	7.7	8.0	0.7	50	0
F	1218.8	H	379552	6285191	3.6	2.5	21.7	53.2	8.2	12.7	1.4	50	0
G	1144.3	H	381870	6285140	2.6	1.5	5.9	1.8	8.3	2.9	---	---	0
H	1128.0	H	382366	6285117	5.2	1.6	20.4	45.8	29.3	12.8	4.9	56	0
I	1048.2	H	384843	6285030	0.3	2.1	5.2	1.3	15.4	0.5	---	---	0
J	1035.8	H	385215	6285018	3.5	0.6	11.9	6.7	16.2	6.9	9.1	63	0
K	656.0	H	393901	6284790	0.0	3.2	1.7	7.5	4.3	1.2	---	---	949
L	625.0	H	394844	6284754	2.8	1.0	3.5	1.4	3.3	0.8	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50750		FLIGHT 20											
M	595.5	H	395739	6284753	2.1	1.8	11.2	3.3	7.9	4.2	---	---	0
N	587.0	B	396010	6284746	13.9	4.0	15.4	14.7	2.9	6.3	7.3	25	0
O	535.6	B	397458	6284718	15.6	3.4	48.8	28.0	26.8	20.8	11.0	21	0
P	532.9	H	397540	6284720	10.5	7.7	48.8	28.0	26.8	20.8	1.9	8	0
Q	511.8	H	398221	6284686	3.7	1.6	13.2	9.4	7.9	7.2	---	---	0
R	397.1	S	400707	6284620	1.6	1.8	11.0	1.8	16.4	0.2	0.6	52	0
LINE 50760		FLIGHT 20											
A	1609.2	H	376029	6285133	4.6	1.9	43.0	15.9	45.2	16.1	3.0	41	19
B	1618.6	B?	376385	6285130	3.4	3.5	39.2	60.3	23.2	18.3	0.9	35	0
C	1650.0	H	377542	6285090	5.2	2.7	7.1	15.7	4.7	3.3	---	---	0
D	1718.1	H	380072	6285021	2.8	3.3	14.1	22.6	6.6	6.2	---	---	0
E	1774.2	H	382217	6284976	0.0	0.8	2.0	1.0	2.0	0.8	---	---	0
F	1788.7	H	382768	6284934	4.8	2.7	60.7	45.5	20.1	27.9	2.0	28	0
G	1791.4	E	382872	6284924	10.2	4.6	60.7	45.5	21.7	27.9	3.5	14	49
H	1819.8	H	383929	6284905	3.3	2.1	37.9	14.2	26.6	11.8	1.5	31	0
I	1842.0	H	384813	6284903	1.3	1.0	9.7	3.4	9.0	1.6	---	---	0
J	1852.7	H	385241	6284891	2.6	2.5	8.9	5.7	15.1	2.3	---	---	0
K	1906.0	S	387217	6284794	0.7	1.5	1.8	2.2	4.3	1.4	---	---	0
L	2114.0	H	393584	6284665	1.4	1.1	4.1	2.5	5.4	1.8	---	---	0
M	2168.9	H	395636	6284603	0.7	0.9	29.8	25.0	6.4	11.5	0.5	93	0
N	2171.1	B	395711	6284600	7.9	3.0	29.8	25.0	4.6	11.5	4.0	41	0
O	2178.8	B?	395974	6284595	8.6	3.2	44.2	29.1	8.3	18.3	4.4	33	14
P	2181.0	B	396050	6284598	18.7	9.1	44.2	29.1	8.3	18.3	3.9	14	13

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50760		FLIGHT 20											
Q	2224.2	B	397471	6284568	11.7	2.6	29.7	13.1	19.2	12.7	10.2	13	0
R	2226.0	H	397535	6284564	0.0	3.3	29.7	13.1	19.2	12.7	---	---	0
S	2245.3	H	398204	6284561	4.1	1.9	47.1	21.9	30.3	17.7	2.4	39	0
T	2265.2	B	398867	6284553	9.0	5.3	39.4	30.1	12.9	15.2	2.4	21	0
LINE 50770		FLIGHT 20											
A	3579.2	H	375694	6284973	15.4	1.3	140.8	52.1	128.8	66.8	44.7	37	0
B	3491.9	H	378431	6284924	7.2	8.6	29.1	73.7	15.2	19.4	1.0	34	485
C	3454.3	H	379553	6284888	6.5	5.4	10.8	46.1	5.8	10.0	1.4	36	0
D	3366.0	H	382295	6284805	2.5	1.9	7.5	7.6	4.9	1.2	---	---	0
E	3343.7	E	382917	6284826	14.9	4.0	41.9	64.6	13.2	14.5	8.1	19	0
F	3326.7	E	383447	6284774	1.6	6.7	24.4	49.9	21.1	9.5	0.2	0	0
G	3311.0	H	383925	6284754	0.6	0.0	1.5	2.8	7.1	2.8	---	---	0
H	3283.8	H	384758	6284746	2.5	0.9	11.7	5.5	11.8	4.2	3.0	83	0
I	3264.3	H	385389	6284723	2.5	3.0	15.2	6.9	33.8	10.1	0.7	49	0
J	2988.0	H	393362	6284521	0.8	1.8	7.1	1.9	6.5	1.3	---	---	0
K	2925.3	B	395283	6284467	19.0	7.9	23.1	17.8	8.6	11.3	4.9	9	0
L	2921.8	B	395386	6284460	5.1	4.1	23.1	17.8	8.7	11.3	1.4	40	0
M	2901.2	H	396010	6284433	4.6	3.8	29.8	20.2	6.9	13.2	1.3	41	17
N	2854.5	D	397432	6284395	19.6	3.0	77.2	22.1	67.7	27.7	---	---	0
O	2847.2	B	397652	6284391	13.4	5.0	45.9	5.4	51.3	15.4	5.0	12	11
P	2827.4	B	398211	6284400	9.3	4.9	27.7	15.3	11.9	9.7	2.8	23	0
Q	2825.2	H	398278	6284398	8.3	4.2	27.7	15.3	11.9	9.7	2.8	17	0
R	2715.5	B?	400998	6284304	0.0	4.0	1.0	33.9	0.1	17.9	---	---	361

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50780			FLIGHT 21										
A	1312.4	B	375068	6284855	5.6	6.4	68.5	45.6	8.1	26.4	0.9	32	124
B	1297.3	H	375488	6284842	4.3	2.0	56.6	18.5	99.9	33.8	2.5	63	14
C	1289.6	H	375696	6284840	6.9	7.7	44.8	17.8	41.5	15.1	1.0	28	0
D	1255.2	H	376627	6284805	4.1	8.7	10.6	53.8	6.5	13.2	0.4	24	578
E	1238.8	H	377054	6284786	2.0	2.4	19.3	0.0	15.4	12.7	0.6	61	0
F	1227.1	H	377345	6284780	6.3	13.1	17.2	55.0	39.3	11.9	0.5	17	0
G	1206.4	H	377880	6284764	4.8	2.0	25.7	4.0	24.4	8.8	3.0	61	27
H	1182.9	B?	378502	6284772	10.6	5.3	52.6	25.5	0.2	35.2	3.1	37	152
I	1171.9	H	378800	6284759	4.9	5.2	45.8	32.0	16.2	38.6	0.9	39	41
J	1163.7	H	379023	6284743	3.9	1.4	25.7	6.5	10.8	5.6	---	---	24
K	1052.7	H	382162	6284645	2.6	0.0	1.9	1.1	1.6	1.7	---	---	60
L	1022.6	S?	383013	6284650	1.8	0.8	33.4	29.6	6.9	15.0	2.0	73	0
M	996.3	H	383765	6284613	1.3	1.7	0.6	2.0	2.0	0.2	---	---	0
N	961.5	H	384737	6284600	1.7	2.0	16.6	4.9	16.8	6.0	---	---	10
O	936.4	H	385427	6284579	3.2	1.7	14.5	6.6	24.8	13.1	2.0	73	88
P	909.0	S	386223	6284545	2.5	1.2	6.4	11.1	2.0	2.8	---	---	0
Q	617.1	H	393994	6284338	1.9	2.8	3.3	10.4	2.4	2.8	---	---	29
R	567.1	D	395337	6284313	14.4	7.3	21.3	24.1	4.1	8.1	3.4	21	0
S	488.5	D	397390	6284275	41.0	3.1	72.7	18.1	75.3	21.5	---	---	0
T	482.4	B	397555	6284263	5.4	1.4	42.6	7.8	39.9	7.5	---	---	0
U	478.8	E	397653	6284260	14.8	3.9	31.0	7.8	24.1	7.5	---	---	0
V	458.4	B	398202	6284242	13.7	2.4	22.9	9.5	13.2	11.0	---	---	0
W	337.0	S	400980	6284180	3.3	2.3	3.4	13.8	1.9	4.8	---	---	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50790			FLIGHT 49										
A	1600.2	H	375141	6284704	3.2	1.9	33.4	19.4	20.9	15.8	1.6	68	0
B	1553.7	H	376459	6284661	6.4	0.0	27.6	0.0	30.3	13.2	836.8	68	547
C	1540.8	H	376838	6284661	7.0	7.0	66.0	41.1	50.2	33.6	1.2	24	0
D	1505.8	H	377820	6284617	3.0	2.6	43.4	21.9	29.4	19.1	1.0	48	0
E	1502.0	B?	377943	6284608	4.4	3.4	43.4	47.9	28.9	19.1	1.4	38	0
F	1497.2	H	378105	6284611	1.7	2.0	50.7	14.9	42.5	22.2	0.6	42	526
G	1467.0	H	379068	6284614	4.1	0.9	65.5	23.0	47.8	40.2	7.3	63	88
H	1460.1	H	379286	6284613	8.0	3.4	43.9	25.7	30.2	10.2	3.6	33	0
I	1370.0	H	382140	6284516	1.8	2.5	4.8	2.5	2.5	1.7	---	---	0
J	1264.1	H	385359	6284427	3.5	4.9	10.8	11.9	17.8	7.9	0.6	33	99
K	1234.7	S?	386232	6284392	0.6	1.9	21.3	24.6	2.2	6.9	0.2	0	0
L	984.0	H	392876	6284238	0.0	1.3	5.4	2.5	2.4	1.9	---	---	0
M	941.7	H	394003	6284190	1.8	1.9	3.1	0.5	1.1	1.4	---	---	72
N	885.3	D	395359	6284171	5.4	2.4	8.5	10.0	2.9	3.8	2.8	35	0
O	859.0	B	396054	6284142	6.0	8.1	17.0	13.4	9.6	6.8	0.8	10	0
P	805.6	D	397382	6284115	15.3	1.1	44.0	5.1	38.7	15.9	55.8	14	0
Q	799.8	B	397541	6284107	6.1	3.4	42.4	14.3	38.7	14.4	2.3	22	0
R	774.7	B	398188	6284089	8.4	4.0	13.2	14.4	9.0	10.8	3.1	34	0
LINE 50800			FLIGHT 48										
A	1399.8	H	376241	6284522	3.1	2.6	60.9	23.3	38.6	27.4	1.1	45	0
B	1291.7	H	379209	6284478	7.1	3.5	101.9	10.9	83.2	45.1	2.8	28	0
C	1189.1	H	382207	6284371	1.4	1.4	6.3	7.0	4.0	3.4	---	---	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50800		FLIGHT 48											
D	1101.0	H	384976	6284285	1.4	0.9	6.2	3.0	5.6	2.1	---	---	0
E	777.5	H	393646	6284066	1.4	0.9	2.6	6.2	0.9	1.7	---	---	64
F	710.0	D	395311	6284027	7.1	2.5	10.5	8.0	5.0	2.2	4.3	14	0
G	675.7	B	396220	6284005	3.6	1.1	14.5	5.3	8.2	7.5	4.3	53	0
H	633.3	D	397351	6283981	26.9	10.2	66.5	21.4	41.8	26.5	6.1	13	0
I	626.5	B	397530	6283974	21.5	6.8	69.4	27.9	41.9	29.3	7.3	9	0
J	614.9	B	397820	6283964	6.5	2.9	21.5	11.6	5.7	7.6	3.1	15	0
K	608.1	B	397984	6283965	6.5	2.8	13.3	3.7	9.8	7.8	3.2	29	0
L	597.0	D	398248	6283950	8.1	3.0	19.8	15.2	7.4	8.4	4.2	14	0
M	566.0	S	398973	6283906	2.4	0.9	12.7	6.3	6.5	1.9	---	---	0
LINE 50810		FLIGHT 47											
A	3875.0	S	380898	6284248	0.3	1.9	5.2	12.0	0.9	1.7	---	---	0
B	3916.0	H	382213	6284212	1.7	0.6	6.6	6.1	5.1	2.4	---	---	0
C	4001.0	H	384882	6284132	0.4	0.2	5.2	0.5	4.9	1.5	---	---	71
D	4087.7	S	387781	6284053	1.2	0.0	7.1	14.4	1.5	2.5	---	---	0
E	4151.5	H	389831	6284016	4.4	0.7	3.7	3.2	2.1	1.7	---	---	33
F	4230.0	S	392360	6283970	1.2	0.3	6.2	2.0	3.3	2.0	---	---	0
G	4343.7	B	395255	6283860	3.7	2.9	4.0	4.7	2.2	3.3	1.2	27	0
H	4382.2	B	396200	6283829	12.5	7.7	65.9	40.7	13.1	25.7	2.5	22	0
I	4391.6	B	396459	6283848	2.9	0.6	30.0	6.9	17.5	13.4	7.8	67	0
J	4402.7	B	396793	6283860	3.0	2.8	27.2	23.1	5.1	8.6	---	---	0
K	4405.9	D	396881	6283860	6.5	4.1	27.2	23.1	5.1	8.6	2.0	31	0
L	4421.4	B	397333	6283826	11.5	4.1	58.6	8.2	35.3	21.3	5.1	12	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50810		FLIGHT 47											
M	4426.1	D	397485	6283816	23.6	9.1	58.1	27.2	35.3	21.3	5.7	12	0
N	4432.9	B	397677	6283807	11.3	6.0	40.8	17.1	5.0	18.2	2.9	19	0
O	4439.7	B	397819	6283806	7.5	3.5	40.8	18.8	5.0	18.2	3.1	27	0
P	4454.5	B	398105	6283794	3.1	4.5	64.8	37.8	22.2	27.4	0.6	19	0
LINE 50820		FLIGHT 47											
A	5484.0	S?	380454	6284118	1.5	3.9	9.5	19.1	4.5	2.9	---	---	0
B	5426.0	H	382288	6284064	1.1	1.3	6.0	4.7	5.4	3.3	---	---	0
C	5400.0	H	383107	6284048	0.5	2.5	20.4	12.5	13.0	9.7	---	---	50
D	5347.2	H	384884	6284004	2.0	1.0	9.0	0.3	5.8	4.0	---	---	68
E	5233.9	H	388490	6283948	5.1	5.1	43.7	61.4	4.6	15.1	1.0	26	0
F	5189.0	H	389985	6283835	2.4	1.7	45.4	8.4	32.6	18.9	1.2	21	0
G	5009.1	D	395249	6283710	4.7	4.0	13.0	10.1	0.5	5.0	1.2	29	0
H	4964.8	E	396342	6283679	9.0	2.9	41.4	23.2	13.1	18.2	5.3	29	0
I	4961.6	D	396431	6283680	11.9	7.1	41.4	23.2	16.7	18.2	2.5	16	13
J	4931.6	B	397216	6283663	22.6	4.1	89.7	23.6	58.2	38.7	16.5	15	0
K	4924.0	B	397430	6283651	15.2	3.7	5.6	11.8	4.4	3.1	9.5	14	0
L	4917.8	D	397601	6283639	25.9	19.5	71.5	54.8	5.9	31.1	2.5	10	0
M	4914.6	B	397683	6283635	31.9	12.8	71.5	54.8	26.7	31.1	6.0	7	0
N	4901.6	D	398004	6283621	14.2	10.0	76.8	64.2	13.8	32.1	2.2	13	0
O	4894.8	D	398175	6283615	20.0	7.6	80.1	57.7	16.1	31.8	5.5	2	0
LINE 50830		FLIGHT 47											
A	5586.0	S?	380376	6283967	1.5	2.2	12.4	21.7	2.1	3.6	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50830		FLIGHT 47											
B	5674.4	H	382922	6283903	1.1	0.0	2.1	2.0	4.2	1.0	---	---	0
C	5734.0	H	384874	6283850	0.8	0.5	12.3	1.9	10.8	4.2	---	---	16
D	5847.7	H	388763	6283742	0.5	1.2	4.1	2.7	1.9	1.4	---	---	0
E	5885.0	H	390057	6283698	0.1	0.4	5.3	0.5	12.2	3.9	---	---	0
F	6005.7	H	394218	6283608	0.7	1.0	8.4	8.1	1.0	3.7	---	---	253
G	6016.0	S	394555	6283593	0.4	0.6	3.2	5.1	1.2	1.4	---	---	0
H	6092.1	B	395830	6283573	3.2	2.2	9.2	6.6	4.4	3.7	---	---	0
I	6111.0	D	396386	6283546	6.8	4.2	13.3	13.5	5.4	5.9	2.0	20	0
J	6127.5	E	396797	6283554	0.0	1.5	0.2	3.2	0.5	0.0	---	---	0
K	6134.3	D	396997	6283536	43.9	14.3	209.8	61.5	137.3	78.7	8.9	7	0
L	6137.0	B	397079	6283527	14.5	8.5	209.8	61.5	137.3	78.7	2.8	11	30
M	6146.3	D	397368	6283514	10.0	3.9	23.7	23.4	0.0	11.1	4.3	9	0
N	6155.3	B	397659	6283526	12.1	2.7	76.5	19.7	48.0	33.7	10.3	16	0
O	6173.6	D	398191	6283488	18.1	8.1	83.6	46.2	28.9	38.4	4.3	15	0
LINE 50840		FLIGHT 48											
A	1706.7	S	380365	6283827	1.2	1.9	4.5	14.3	1.3	2.2	---	---	0
B	1802.0	H	382915	6283764	0.7	0.7	5.5	0.6	4.3	4.5	---	---	0
C	1862.2	H	384798	6283697	2.2	0.0	10.0	2.7	8.8	3.7	---	---	152
D	1981.0	H	388772	6283574	1.6	0.0	2.7	1.7	1.2	1.0	---	---	23
E	2018.8	H	390118	6283570	1.1	0.0	3.2	1.6	8.2	1.4	---	---	0
F	2062.0	H	391565	6283515	0.3	1.3	0.4	3.0	2.3	0.6	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50842		FLIGHT 47											
A	6579.9	D	397070	6283364	17.3	8.3	54.2	22.8	27.6	21.3	3.9	12	19
B	6571.8	D	397314	6283357	14.7	5.4	33.8	16.5	6.4	15.7	5.2	7	0
C	6563.5	B	397577	6283351	31.6	26.8	189.2	104.7	113.9	83.9	2.3	4	0
D	6560.5	B	397673	6283349	18.5	5.0	189.2	104.7	113.9	83.9	8.9	4	0
E	6549.0	H	398035	6283348	1.5	5.2	15.7	17.3	8.9	4.3	0.2	5	0
F	6542.7	B	398226	6283338	11.6	11.4	63.7	55.7	14.2	23.3	1.4	9	0
LINE 50850		FLIGHT 48											
A	2660.0	S?	379771	6283694	1.6	0.8	2.3	5.9	0.8	1.2	---	---	42
B	2557.7	H	382887	6283609	0.6	0.2	6.7	6.9	0.5	2.7	---	---	230
C	2496.5	H	384728	6283549	1.1	1.1	18.9	1.1	15.2	6.8	0.7	81	171
D	2371.7	H	388780	6283444	0.3	1.3	5.0	3.6	5.7	2.5	---	---	0
E	2327.4	H	390164	6283406	0.8	0.4	3.0	1.4	4.4	1.4	---	---	0
F	2283.7	H	391434	6283358	0.0	0.4	3.0	2.2	3.0	1.6	---	---	0
G	2265.2	H	391947	6283367	0.6	0.3	2.5	0.0	2.9	0.4	---	---	0
H	2207.5	S?	393510	6283299	1.5	0.5	1.3	11.9	2.2	2.2	---	---	719
LINE 50851		FLIGHT 47											
A	6854.0	S?	394259	6283313	0.9	0.9	9.4	15.1	3.1	3.1	---	---	381
B	6953.9	S?	395807	6283265	4.9	2.3	6.4	4.7	2.2	2.0	2.6	11	0
C	6989.1	H	396538	6283244	1.7	1.5	7.9	8.7	1.5	4.3	---	---	0
D	7037.0	B	397522	6283214	12.9	3.4	51.9	15.1	19.7	22.1	8.2	0	0
E	7043.2	H	397709	6283201	41.8	10.2	138.3	25.5	98.2	59.1	13.3	2	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50860			FLIGHT 48										
A	2950.1	S	379960	6283546	0.0	0.9	3.0	5.1	0.1	1.1	---	---	53
B	3045.0	S?	382872	6283467	1.1	1.1	1.4	1.3	1.5	0.5	---	---	0
C	3102.2	H	384794	6283377	0.3	1.1	5.8	2.2	2.7	2.6	---	---	326
D	3246.2	H	390051	6283274	1.9	0.0	0.8	3.3	2.5	1.1	---	---	147
E	3279.5	H	391314	6283241	1.2	0.8	1.4	1.2	2.0	0.5	---	---	0
LINE 50861			FLIGHT 47										
A	7550.0	S?	394193	6283167	1.0	0.8	5.3	7.7	1.8	2.0	---	---	146
B	7485.6	B?	395843	6283096	6.7	5.1	9.2	9.2	3.0	3.1	---	---	0
C	7454.7	D	396682	6283082	9.3	3.6	21.0	14.7	4.9	8.7	4.2	23	0
D	7435.9	B	397203	6283064	5.8	2.0	29.0	8.2	9.3	11.7	4.1	22	0
E	7421.9	B	397600	6283056	31.0	17.0	163.6	94.9	61.8	68.5	3.9	11	0
F	7418.7	D	397689	6283054	23.4	12.1	163.6	94.9	61.8	68.5	3.8	0	0
LINE 50870			FLIGHT 48										
A	3865.0	S	379696	6283394	1.8	0.5	3.8	7.5	1.0	1.4	---	---	0
B	3661.5	H	385641	6283219	1.4	0.9	6.1	5.3	1.2	2.7	---	---	0
C	3499.0	H	391127	6283074	0.6	0.0	1.3	0.3	2.4	0.7	---	---	61
LINE 50871			FLIGHT 47										
A	7710.0	S	393854	6283008	1.2	0.1	2.5	1.1	2.2	0.7	---	---	0
B	7813.3	B?	396486	6282910	2.6	2.2	13.6	9.8	2.9	4.1	1.0	27	0
C	7827.1	H	396880	6282910	8.2	7.3	40.4	19.6	13.1	16.9	1.4	12	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50871			FLIGHT 47										
D	7859.0	H	397681	6282947	3.1	0.4	17.5	6.8	10.1	7.7	15.8	12	0
LINE 50880			FLIGHT 48										
A	4054.1	S	379877	6283257	3.4	2.8	8.5	28.5	0.5	4.2	---	---	0
B	4211.7	S	384456	6283099	1.2	0.7	6.6	2.5	6.1	0.6	---	---	0
C	4248.1	S?	385718	6283062	1.3	0.0	0.7	1.6	0.6	0.9	---	---	278
D	4404.4	H	390946	6282931	1.3	1.2	1.3	0.5	5.9	0.3	---	---	0
E	4473.5	S?	393345	6282876	1.6	1.5	8.9	9.4	1.2	2.1	---	---	0
LINE 50881			FLIGHT 47										
A	8431.5	S?	394002	6282868	1.2	2.1	16.0	13.9	4.3	5.4	---	---	0
B	8147.0	S	400862	6282657	1.2	0.2	0.9	5.3	0.4	1.5	---	---	0
LINE 50891			FLIGHT 47										
A	8902.7	H	391007	6282795	1.9	0.8	5.0	3.9	1.7	2.6	---	---	24
B	8975.0	S?	393012	6282726	2.0	2.3	10.1	12.2	0.3	4.5	---	---	0
C	9009.5	H	394123	6282683	2.7	0.8	14.4	11.9	3.4	6.4	---	---	14
D	9060.6	B	395537	6282688	5.2	3.2	18.9	11.5	5.3	7.1	1.9	35	0
LINE 50893			FLIGHT 83										
A	4372.1	S	379627	6283100	0.5	2.5	4.8	16.1	1.3	2.5	---	---	0
B	4259.5	S?	383170	6282980	1.9	0.8	3.4	3.9	1.3	1.1	---	---	0
C	4174.0	S?	385560	6282925	0.8	0.5	2.0	1.4	1.6	0.7	---	---	1589

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50902		FLIGHT 47											
A	9806.0	H	394144	6282554	0.8	1.2	14.4	3.0	4.9	6.3	---	---	0
B	9754.1	B	395590	6282512	6.0	1.8	31.4	12.8	11.9	14.3	5.4	47	0
C	9520.0	S	400137	6282381	0.7	1.8	0.4	2.4	1.6	0.7	---	---	0
D	9456.6	S	400858	6282374	1.0	1.1	1.6	7.0	0.3	1.8	---	---	0
LINE 50904		FLIGHT 48											
A	5749.1	S	379559	6282938	0.2	1.8	4.1	4.5	0.8	1.8	---	---	0
B	5277.0	S	392902	6282585	1.0	1.4	11.1	6.3	1.2	2.6	---	---	0
LINE 50910		FLIGHT 48											
A	5847.5	S	379584	6282792	2.6	1.1	5.7	3.4	1.2	0.4	---	---	0
B	5977.7	S?	383215	6282718	1.2	0.6	1.6	3.3	0.8	1.0	---	---	0
C	6289.0	S	393009	6282439	1.8	0.0	5.5	4.4	0.5	1.9	---	---	0
LINE 50911		FLIGHT 47											
A	9986.4	H	393939	6282418	3.4	5.4	34.5	27.4	5.3	12.2	0.6	20	0
B	9994.1	H	394159	6282402	4.2	4.4	42.8	40.1	6.6	15.5	0.9	24	0
LINE 50920		FLIGHT 83											
A	5855.1	S?	379862	6282644	3.5	3.0	13.8	16.9	16.0	2.1	---	---	0
B	6089.5	S	386159	6282467	3.5	2.4	2.2	6.0	1.3	0.8	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50921			FLIGHT 84										
A	301.7	S	389643	6282372	2.7	0.6	4.1	4.6	1.2	1.2	---	---	0
B	392.7	S	392498	6282292	5.2	2.6	6.2	13.9	1.4	2.2	---	---	0
C	433.7	H	393834	6282252	1.4	1.8	9.2	5.1	3.3	3.3	---	---	0
D	744.4	S	399982	6282102	1.4	0.5	2.4	7.9	1.0	2.2	---	---	0
LINE 50930			FLIGHT 48										
A	6542.7	S?	389486	6282209	0.8	0.8	3.3	6.1	1.2	1.2	---	---	0
B	6450.2	S?	392392	6282151	1.3	1.0	2.1	3.7	0.9	1.0	---	---	0
LINE 50935			FLIGHT 147										
A	10860.0	S?	393727	6282115	1.5	0.3	5.0	8.9	0.9	2.3	---	---	19
B	11238.0	S	401235	6281901	1.7	1.7	1.5	21.3	1.0	2.9	---	---	0
LINE 50944			FLIGHT 85										
A	6028.5	S?	390513	6282062	1.1	2.5	4.8	8.1	2.7	2.2	---	---	0
B	5552.0	S?	400523	6281780	1.4	1.8	0.6	15.5	0.1	4.3	---	---	0
LINE 50950			FLIGHT 48										
A	7740.1	S?	390268	6281917	3.2	5.1	21.6	21.9	1.2	6.6	0.5	22	0
LINE 50960			FLIGHT 48										
A	8460.0	S?	390358	6281760	3.5	2.5	11.0	15.4	1.7	3.9	---	---	0
B	8433.7	S?	391088	6281728	1.4	0.3	8.1	10.9	1.1	2.7	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 50970			FLIGHT 60										
A	852.0	H	390615	6281568	2.2	1.6	13.9	14.7	1.8	4.6	---	---	68
B	639.0	S	395973	6281446	3.2	3.8	3.1	9.3	2.8	1.2	---	---	0
LINE 50971			FLIGHT 116										
A	1236.7	S?	398135	6281396	6.1	2.0	23.4	11.4	24.5	2.8	---	---	0
B	1408.0	S?	401024	6281312	1.4	5.4	7.4	42.9	6.1	6.3	---	---	68
LINE 50980			FLIGHT 60										
A	1454.0	S	380468	6281743	5.2	2.0	7.3	28.9	0.8	3.3	3.4	37	0
B	1922.7	H	390841	6281448	2.0	1.2	4.2	4.0	2.4	2.1	---	---	0
LINE 50990			FLIGHT 60										
A	2798.1	S	384074	6281465	0.0	1.6	0.4	3.6	1.8	0.9	---	---	41
B	2612.0	S	387560	6281358	0.8	1.6	8.7	5.2	1.5	1.1	---	---	0
C	2489.2	H	390754	6281282	3.3	1.3	5.9	9.4	1.7	2.4	---	---	0
LINE 50994			FLIGHT 83										
A	2440.8	S?	381543	6281527	4.2	6.7	12.8	26.2	1.8	5.3	0.6	15	0
LINE 51000			FLIGHT 60										
A	2992.3	S	382226	6281353	5.9	5.3	5.6	14.0	3.5	1.7	1.2	37	0
B	3248.8	S	387613	6281224	5.2	3.3	5.3	6.9	2.8	1.3	---	---	0
C	3368.6	S?	390822	6281133	4.0	2.0	4.2	5.9	0.5	1.5	---	---	32

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 51000			FLIGHT 60										
D	3409.7	S	391956	6281094	6.6	4.6	2.9	4.2	1.1	0.9	---	---	22
LINE 51002			FLIGHT 78										
A	2201.1	S?	401089	6280874	3.1	12.8	38.9	53.9	37.5	9.2	0.2	0	73
LINE 51004			FLIGHT 83										
A	2603.0	H	381605	6281397	1.2	0.9	6.4	9.7	1.0	2.4	---	---	10
LINE 51010			FLIGHT 60										
A	4027.7	S?	387582	6281068	2.8	0.6	6.8	6.2	4.3	1.9	---	---	0
B	3916.1	S?	390782	6281001	5.4	3.1	5.9	1.8	1.2	1.2	2.1	37	0
C	3911.1	H	390937	6280996	4.6	1.8	11.5	5.1	0.6	2.6	---	---	0
LINE 51011			FLIGHT 129										
A	4630.1	S	396753	6280820	4.6	1.8	3.8	3.0	0.8	1.1	---	---	0
B	4387.0	S	400240	6280727	4.8	4.1	7.3	20.8	1.3	4.4	---	---	0
LINE 51012			FLIGHT 85										
A	1650.2	S	381877	6281242	1.6	3.3	14.1	31.2	2.0	7.4	---	---	0
LINE 51020			FLIGHT 60										
A	4416.0	S	382037	6281072	10.5	7.1	13.1	20.9	0.9	4.0	2.1	10	0
B	4601.2	S	386257	6280974	1.5	3.7	2.9	7.9	0.6	1.2	---	---	0
C	4681.6	S	387172	6280921	3.5	2.3	24.7	3.8	11.7	0.8	---	---	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 51020			FLIGHT 60										
D	4709.5	S?	387645	6280947	0.1	9.2	40.3	27.2	0.0	3.8	---	---	1156
E	4716.7	S?	387866	6280932	4.2	5.1	42.2	9.5	47.9	1.6	---	---	0
F	4819.5	S?	390910	6280836	2.1	2.1	4.0	4.9	1.4	1.0	---	---	0
G	4850.7	S	391818	6280816	3.1	0.3	2.7	2.7	1.5	0.8	---	---	0
H	5006.7	B	395310	6280715	11.0	5.1	11.9	13.5	0.8	3.2	3.5	15	0
LINE 51021			FLIGHT 78										
A	1538.0	B?	395327	6280717	5.4	5.8	13.0	8.2	4.2	4.0	---	---	0
B	1447.5	S	396672	6280652	2.2	1.8	6.3	3.7	3.4	0.9	---	---	0
C	1382.7	S?	397533	6280645	3.2	1.9	2.7	16.3	3.0	2.4	---	---	49
LINE 51022			FLIGHT 85										
A	4220.0	S?	398966	6280645	2.8	3.5	4.6	21.2	3.7	3.5	---	---	0
B	4299.5	S	400244	6280598	1.1	1.0	6.9	3.8	4.7	1.3	---	---	0
LINE 51024			FLIGHT 83										
A	2757.3	S	380059	6281104	1.8	3.9	14.0	23.8	1.3	5.2	0.3	11	0
B	2784.5	S?	380566	6281115	3.4	0.3	25.8	18.8	33.5	2.7	---	---	0
C	2863.7	S?	381926	6281107	2.0	4.8	17.8	34.9	11.4	5.4	---	---	0
LINE 51030			FLIGHT 60										
A	5471.0	S?	387582	6280768	20.2	3.2	54.2	22.1	64.6	2.3	---	---	115
B	5468.2	B?	387644	6280767	0.0	11.0	54.2	22.1	64.6	4.3	---	---	850
C	5423.0	S	388843	6280737	4.4	2.8	3.9	8.0	4.8	1.9	---	---	54

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 51032			FLIGHT 77										
A	2566.3	S	396725	6280545	2.7	1.3	10.1	2.0	5.2	0.7	---	---	0
B	2795.2	H	400280	6280417	0.8	3.2	10.3	6.3	4.7	3.1	---	---	0
LINE 51040			FLIGHT 60										
A	5888.0	S	382228	6280767	8.5	2.7	3.4	9.8	0.4	1.2	---	---	0
B	5911.0	S	382740	6280756	6.6	4.4	2.9	10.4	1.3	1.4	---	---	0
C	6005.3	S	384718	6280682	3.9	3.2	5.1	6.6	0.3	0.9	1.2	46	0
D	6055.6	S	385745	6280664	2.4	3.5	6.8	10.5	1.6	2.3	---	---	120
E	6201.3	S?	387843	6280612	3.0	1.7	14.5	23.1	8.6	3.1	---	---	0
F	6501.8	D	395104	6280407	21.3	7.4	13.7	21.3	2.0	5.6	6.4	12	31
LINE 51042			FLIGHT 77										
A	2340.0	S?	395860	6280394	0.0	4.2	2.2	17.0	3.3	2.4	---	---	149
B	2218.1	S?	398101	6280354	30.5	1.9	38.9	12.1	40.3	1.9	---	---	0
C	2189.3	S	398571	6280348	3.3	1.9	25.7	12.8	28.4	1.5	---	---	0
D	2172.7	S?	398848	6280303	0.7	2.8	11.9	10.2	13.1	1.9	---	---	0
E	2086.6	H	400256	6280263	3.8	4.2	24.0	31.7	3.5	10.3	0.8	15	0
LINE 51044			FLIGHT 83										
A	3353.7	S?	382182	6280779	2.6	1.5	7.5	23.7	2.4	3.5	---	---	0
LINE 51050			FLIGHT 60										
A	7264.0	S?	382972	6280619	10.6	5.6	16.6	15.7	17.6	3.1	---	---	0

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LINE 51050			FLIGHT 60										
B	7137.7	S?	385589	6280527	3.0	2.3	5.8	11.0	1.2	2.1	---	---	303
C	7031.5	S?	387670	6280469	4.0	4.0	9.8	12.1	13.6	3.5	---	---	297
D	6772.0	S	394128	6280278	2.5	2.9	2.9	7.8	1.3	1.7	---	---	0
LINE 51052			FLIGHT 77										
A	1638.0	S	396834	6280235	3.9	1.5	5.4	6.8	3.9	1.7	---	---	0
B	1673.3	S?	397407	6280200	1.2	3.2	0.0	7.9	0.0	1.3	---	---	20
C	1826.1	B?	400292	6280139	8.0	11.0	19.9	37.8	2.4	6.9	0.8	4	0
LINE 51060			FLIGHT 60										
A	7465.1	S	382797	6280449	9.5	7.9	26.5	16.1	29.2	2.4	1.6	31	0
B	7472.7	S?	382941	6280438	0.0	11.0	0.0	15.9	0.0	1.3	---	---	359
C	7734.2	S?	387849	6280336	0.0	10.0	0.0	6.5	0.0	0.7	---	---	372
D	8052.8	S?	394999	6280105	4.4	9.9	2.5	16.5	2.4	2.2	0.4	6	0
LINE 51062			FLIGHT 77										
A	1331.0	S?	395742	6280106	2.2	3.2	16.9	6.3	19.2	1.3	---	---	73
B	1268.0	S	396829	6280063	1.6	0.3	7.4	3.0	2.4	1.3	---	---	0
C	1177.0	S?	398205	6280065	3.1	4.6	15.6	10.1	16.7	1.8	---	---	0
D	1069.0	S?	400096	6279971	2.8	4.7	7.8	12.9	1.3	3.5	---	---	30
E	1041.7	S	400615	6279944	2.8	6.1	5.5	12.1	1.6	2.2	---	---	0
LINE 51070			FLIGHT 76										
A	1448.3	S	385250	6280261	1.9	1.3	2.6	10.5	0.4	1.8	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 51070			FLIGHT 76										
B	1257.7	S?	388788	6280122	3.8	2.2	12.8	5.1	14.0	0.6	---	---	0
C	1213.5	S	389842	6280120	0.7	1.5	5.8	4.0	6.2	1.2	---	---	17
D	639.2	S	398939	6279883	5.7	4.4	3.0	7.7	1.6	1.7	---	---	0
E	551.6	S	400741	6279794	2.9	2.3	2.2	9.9	1.0	2.0	1.2	44	22
LINE 51080			FLIGHT 76										
A	1716.0	S	386620	6280044	2.2	0.7	4.1	2.6	2.6	0.9	---	---	0
B	1975.7	S	389724	6279950	3.2	2.7	7.9	8.6	4.8	1.0	---	---	0
C	2280.0	S	394869	6279835	4.6	3.5	2.6	5.8	0.6	0.7	---	---	12
D	2710.0	S?	400598	6279705	1.7	1.4	6.1	13.0	1.6	2.8	---	---	0
LINE 51090			FLIGHT 76										
A	3780.0	S?	386493	6279904	1.4	2.6	6.9	4.3	3.8	1.2	---	---	1429
B	3669.6	S?	388001	6279880	6.4	2.3	18.7	9.6	24.0	1.5	---	---	0
C	3630.0	S	388887	6279845	3.3	1.2	10.2	9.9	14.1	1.7	---	---	29
D	3607.7	S	389505	6279835	5.0	1.6	7.5	8.2	11.4	1.0	---	---	0
E	3571.2	S	390520	6279794	3.9	3.1	16.3	7.3	15.5	1.1	---	---	0
F	3126.4	S	397663	6279611	7.0	3.4	22.2	4.4	23.4	0.6	---	---	0
G	3115.0	S?	397859	6279598	4.0	4.4	9.2	12.0	9.7	2.1	---	---	170
LINE 51100			FLIGHT 76										
A	4157.0	H	386618	6279756	3.5	2.3	7.3	9.2	0.5	2.2	---	---	834
B	4234.3	S	387478	6279744	3.7	2.8	6.1	0.2	5.1	1.1	1.3	31	0
C	4285.8	S	387848	6279710	2.4	2.6	4.7	8.9	5.5	1.2	---	---	10

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 51100			FLIGHT 76										
D	4328.0	S	388594	6279713	2.6	0.8	18.6	5.4	19.6	1.3	---	---	0
E	4357.5	S?	389290	6279641	2.6	6.3	4.6	16.7	8.8	2.7	---	---	0
F	4408.3	S?	390521	6279630	2.8	4.9	16.9	27.2	20.1	3.6	---	---	96
LINE 51101			FLIGHT 77										
A	399.1	S?	394336	6279533	2.5	2.8	5.6	6.6	3.5	1.4	---	---	0
B	726.7	S?	398039	6279445	1.5	4.8	7.6	19.9	6.6	3.1	---	---	33
C	821.0	S	399895	6279400	2.1	2.9	2.8	13.4	0.8	2.3	---	---	0
LINE 51111			FLIGHT 85										
A	1309.0	S?	386595	6279575	1.1	0.9	7.3	8.7	0.1	3.2	---	---	1903
B	1221.6	S	387765	6279550	6.7	0.5	14.7	5.1	16.2	1.2	---	---	0
C	1172.5	S?	388455	6279538	2.1	4.3	3.5	16.2	5.6	3.3	---	---	34
D	1141.6	S	389098	6279529	1.9	2.1	11.8	8.0	14.9	1.2	---	---	0
E	1086.6	S	390502	6279505	3.4	4.2	19.5	27.9	18.1	4.0	---	---	0
F	1052.7	S?	390874	6279479	4.3	5.3	46.5	40.3	54.1	5.5	---	---	0
G	883.9	S?	393102	6279420	2.4	2.7	4.7	11.2	5.9	1.9	---	---	116
H	851.0	S	393469	6279403	0.6	3.5	3.9	5.5	2.8	1.2	---	---	0
LINE 51115			FLIGHT 129										
A	4928.0	S	394101	6279411	5.4	1.8	8.6	9.7	1.5	2.3	---	---	0
LINE 51120			FLIGHT 85										
A	2147.0	H	386728	6279468	2.1	2.6	8.6	8.2	0.6	2.5	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 51120			FLIGHT 85										
B	2309.2	S?	388330	6279414	4.1	2.4	1.8	5.2	1.5	1.4	---	---	0
C	2336.9	S	388917	6279379	3.9	1.9	15.3	3.8	18.0	0.3	---	---	0
D	2387.0	S	390289	6279337	1.5	10.0	6.5	42.5	0.3	6.8	---	---	48
LINE 51121			FLIGHT 129										
A	5636.3	S?	394107	6279242	2.6	1.2	8.6	5.3	0.9	2.9	---	---	0
LINE 51130			FLIGHT 85										
A	3194.0	S?	386562	6279304	2.3	2.0	4.1	6.5	0.9	1.9	---	---	1692
B	3076.2	S?	388395	6279249	11.1	2.4	31.6	7.8	34.9	4.4	---	---	261
C	3050.7	S	388770	6279228	6.0	4.1	36.3	7.3	41.0	1.3	---	---	0
D	2974.4	S	390234	6279194	3.3	5.1	4.7	31.1	3.0	4.8	---	---	0
E	2688.5	B	393376	6279130	7.8	13.3	49.4	40.9	6.4	20.5	0.7	0	0
LINE 51131			FLIGHT 129										
A	5783.5	B?	393399	6279110	6.2	3.9	13.3	17.8	3.0	6.3	1.9	0	0
B	5820.0	S?	394054	6279104	3.4	1.5	17.3	10.1	2.9	6.0	---	---	0
C	6088.5	S	397594	6279013	1.6	3.2	5.2	18.2	5.4	2.8	---	---	0
LINE 51140			FLIGHT 85										
A	3643.0	H	386687	6279152	2.1	2.3	5.0	6.7	1.3	1.8	---	---	1248
B	3797.7	S?	389002	6279084	6.3	0.9	0.1	7.3	0.9	1.9	---	---	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 51141			FLIGHT 129										
A	6663.5	S	390174	6279064	4.1	6.7	5.5	28.8	0.9	5.4	---	---	0
B	6571.1	S	391473	6279013	2.3	1.5	3.0	3.7	1.3	1.1	---	---	0
C	6517.0	S?	392317	6279000	0.0	0.6	2.2	5.3	4.8	1.0	---	---	231
D	6450.7	S?	393435	6278967	2.0	3.2	22.3	15.7	2.9	8.9	0.5	8	0
E	6417.7	S	394032	6278952	3.3	2.4	11.6	2.5	2.2	5.3	---	---	0
F	6202.2	S	397614	6278848	0.5	1.8	3.3	6.6	2.3	1.6	---	---	0
LINE 51150			FLIGHT 129										
A	7006.0	H	386553	6279007	1.6	1.7	5.3	5.8	2.0	1.3	---	---	0
B	7194.0	S	390161	6278876	2.4	2.3	4.6	2.0	2.6	1.4	---	---	0
C	7269.8	S	391512	6278890	4.4	2.0	2.9	6.6	1.0	0.9	---	---	89
D	7400.7	B	393490	6278821	4.6	4.7	2.8	9.1	0.9	2.0	1.0	0	0
E	7411.3	B?	393668	6278815	3.1	3.5	10.4	16.4	1.6	2.6	---	---	0
F	7420.0	H	393869	6278810	1.0	1.6	12.1	16.0	3.0	3.7	---	---	0
LINE 51160			FLIGHT 129										
A	8436.1	H	386688	6278842	1.8	2.0	5.7	8.8	2.2	1.9	---	---	0
B	8334.0	S?	388699	6278793	1.9	2.4	8.3	9.7	6.6	1.4	---	---	0
C	8319.0	S?	389010	6278785	1.0	3.4	2.9	13.0	0.0	2.2	---	---	215
D	8018.2	S?	393986	6278636	3.0	2.4	9.7	3.8	2.2	1.8	---	---	0
E	8011.2	B?	394137	6278630	5.5	3.9	9.8	27.1	3.2	5.7	---	---	60
F	7825.4	H	397054	6278570	3.3	0.6	5.0	1.2	2.1	0.8	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 51170			FLIGHT 129										
A	8846.0	H	386677	6278703	3.4	1.5	4.9	8.2	2.5	2.6	---	---	0
B	9249.5	S?	394155	6278502	2.9	1.3	6.3	5.5	1.1	1.6	---	---	40
LINE 51180			FLIGHT 130										
A	1263.0	H	386675	6278541	1.2	2.9	7.2	12.4	0.9	2.4	---	---	102
B	1070.9	S?	390579	6278449	5.5	3.9	29.2	16.9	32.6	2.8	---	---	0
C	610.0	S?	396608	6278268	4.8	9.1	10.0	30.3	0.7	4.9	0.5	0	17
LINE 51190			FLIGHT 130										
A	2240.0	S?	394191	6278204	5.4	2.4	5.4	6.1	2.5	2.2	---	---	0
B	2547.0	S?	396639	6278120	3.5	4.1	3.2	11.9	2.0	2.1	---	---	0
LINE 51200			FLIGHT 130										
A	2824.1	S?	396213	6277983	0.5	2.0	2.0	5.9	1.0	1.4	---	---	0
LINE 51650			FLIGHT 130										
A	4273.5	S	386032	6271507	2.9	4.6	9.0	26.9	0.8	3.7	---	---	0
B	3957.4	H	391849	6271365	3.2	2.1	20.4	22.2	1.9	8.8	---	---	0
C	3768.2	S	396323	6271242	3.2	2.4	4.4	14.9	0.1	2.8	---	---	0
D	3660.1	S	397725	6271176	2.2	0.0	6.7	15.2	1.6	3.1	---	---	0
E	3605.2	S?	398979	6271148	4.0	10.4	25.5	51.1	0.8	8.9	---	---	193
F	3576.3	S	399589	6271131	2.4	2.9	18.1	15.3	5.4	4.4	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 51660			FLIGHT 130										
A	4345.0	S	386152	6271351	3.0	2.0	4.6	10.8	1.0	1.5	---	---	0
B	4575.5	S	390373	6271247	2.4	3.2	4.2	15.1	3.5	2.5	---	---	0
C	4582.7	S	390530	6271236	3.5	0.0	34.4	4.7	27.7	0.6	---	---	0
D	4665.0	H	391947	6271215	4.5	5.5	15.5	25.3	4.0	9.7	0.8	14	0
E	4810.0	S	394813	6271104	2.3	4.5	9.1	35.5	0.8	5.6	---	---	0
F	4991.0	S	398839	6271010	6.4	8.7	33.1	57.6	1.5	10.8	0.8	0	247
G	5021.4	S	399434	6270999	2.1	0.0	18.0	58.4	12.6	9.8	---	---	0
LINE 51670			FLIGHT 130										
A	5523.2	H	391974	6271045	3.0	1.4	10.9	8.2	2.6	5.5	---	---	0
B	5387.3	S	395354	6270968	2.7	4.1	15.7	59.5	1.2	9.6	---	---	0
C	5329.0	S?	396778	6270897	0.0	0.5	17.5	14.8	18.1	2.1	---	---	0
D	5281.0	S	397664	6270893	0.4	0.9	8.4	8.1	0.2	2.2	---	---	0
E	5230.0	S	398846	6270866	2.3	4.9	31.1	71.0	0.6	12.1	0.4	13	0
F	5203.1	S	399414	6270857	3.1	9.9	13.1	49.7	6.1	8.4	---	---	0
LINE 51680			FLIGHT 130										
A	6170.0	H	391955	6270908	3.7	1.1	10.8	16.2	2.8	5.6	---	---	0
B	6251.9	S	393892	6270853	4.4	6.8	22.4	38.5	2.5	9.5	0.6	9	0
C	6277.0	S	394535	6270817	2.9	14.4	24.9	103.9	0.8	15.3	0.2	0	0
D	6389.4	S	397337	6270754	2.6	5.6	12.8	29.7	3.1	5.1	---	---	0
E	6440.9	S	398795	6270701	2.3	8.4	20.3	67.0	8.0	9.6	0.2	1	0
F	6466.5	S	399278	6270702	1.5	7.7	12.9	58.8	3.0	9.1	---	---	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 51690			FLIGHT 130										
A	6951.7	H	392079	6270730	1.0	0.6	8.1	9.2	2.2	4.2	---	---	0
B	6894.4	S	393634	6270704	1.5	1.7	16.8	21.0	1.2	4.5	---	---	0
LINE 51700			FLIGHT 130										
A	7659.0	S?	393955	6270545	3.1	3.6	21.1	25.5	1.0	6.4	0.7	23	0
LINE 51710			FLIGHT 130										
A	8313.5	H	393268	6270399	1.3	1.6	9.4	15.8	2.9	5.5	---	---	0
B	8216.3	S?	395682	6270330	6.1	4.2	23.0	25.3	11.5	5.8	1.7	10	0
C	8147.0	S	397646	6270303	5.6	4.4	13.7	24.3	1.1	4.6	1.4	23	0
D	8127.9	S	398124	6270299	4.3	1.8	14.2	14.8	20.7	2.5	---	---	0
LINE 51720			FLIGHT 130										
A	8680.0	S?	385978	6270479	0.7	22.4	14.0	121.8	0.4	18.3	---	---	0
B	8997.6	H	393542	6270245	1.6	1.8	23.7	30.0	3.0	8.3	0.6	35	0
C	9039.8	S	394690	6270233	0.4	5.3	17.8	39.8	1.5	6.9	0.1	0	0
D	9070.7	S	395705	6270209	0.9	1.0	8.2	14.3	2.2	3.2	---	---	0
E	9128.5	S?	397698	6270159	4.0	2.1	11.3	42.0	9.0	7.6	2.0	53	0
F	9139.5	S	398029	6270144	3.3	6.6	25.8	50.8	9.9	10.5	0.4	7	0
LINE 51730			FLIGHT 131										
A	1249.4	S	386248	6270294	2.9	5.8	8.2	34.5	0.8	5.6	---	---	0
B	878.7	H	392637	6270126	0.2	2.2	12.5	21.3	3.8	6.3	---	---	468

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 51730		FLIGHT 131											
C	854.1	S	393507	6270107	1.2	2.3	17.1	17.5	1.6	5.0	---	---	0
D	750.7	S	396194	6270043	4.5	8.3	16.1	35.7	1.2	6.9	0.5	10	0
E	722.5	S	397118	6270000	3.9	5.2	20.4	37.5	13.0	6.0	0.7	21	1468
F	702.4	S?	397781	6269989	2.2	3.6	52.8	41.9	16.2	9.9	0.5	22	0
LINE 51740		FLIGHT 131											
A	1500.1	S?	391028	6270027	2.4	2.5	14.4	28.0	0.9	4.7	---	---	0
B	1571.7	H	392719	6269986	1.9	1.8	18.5	6.5	5.2	7.6	0.8	55	0
C	1600.3	S	393641	6269951	0.3	1.5	5.8	9.1	1.3	1.3	---	---	0
D	1679.1	S	396035	6269910	6.5	4.5	23.8	39.0	2.2	8.4	1.7	9	0
E	1702.7	S	396862	6269868	5.0	5.6	27.4	34.3	1.6	8.2	0.9	11	0
F	1743.4	S?	397809	6269845	1.4	5.0	30.3	37.1	2.3	12.8	0.2	0	1091
G	1747.5	S?	397951	6269846	4.4	6.5	30.3	37.1	3.2	12.4	0.7	0	0
LINE 51750		FLIGHT 73											
A	6820.4	S?	391273	6269859	4.6	3.9	11.8	22.6	0.9	5.8	---	---	0
B	6969.6	S?	394628	6269779	3.3	5.8	20.9	37.3	0.5	8.2	0.5	18	0
C	6997.4	S?	395477	6269740	3.3	4.6	23.0	31.5	2.1	10.2	0.6	22	0
D	7021.8	S?	396183	6269738	4.3	5.1	30.7	40.4	2.6	10.7	0.8	0	0
E	7041.6	S	396778	6269717	5.3	7.1	54.9	63.0	1.8	18.8	0.8	16	951
F	7120.0	S	398009	6269657	1.5	1.4	7.4	9.4	1.1	2.8	---	---	0
LINE 51760		FLIGHT 73											
A	4881.5	S	386165	6269874	2.4	4.4	5.8	18.3	1.4	3.6	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 51760			FLIGHT 73										
B	5137.4	H	391209	6269742	4.9	2.8	30.7	31.5	3.9	10.3	1.9	45	0
C	5201.6	S?	392625	6269692	1.4	3.3	41.6	52.9	3.4	12.5	0.3	31	0
D	5275.4	S?	394384	6269621	3.5	5.3	31.4	43.4	1.6	9.4	0.6	25	0
E	5307.8	S?	395297	6269619	5.2	4.3	36.0	30.8	5.2	12.7	1.3	23	0
F	5335.6	S	396016	6269591	4.0	5.3	32.3	51.0	4.8	14.8	0.7	28	0
G	5358.9	S?	396645	6269563	3.3	3.6	40.5	48.3	4.6	17.1	0.8	31	97
LINE 51770			FLIGHT 73										
A	4699.6	S	386701	6269672	1.5	14.2	24.9	114.9	5.4	16.0	0.1	0	0
B	4483.5	H	391015	6269566	5.7	5.9	63.7	49.5	4.6	19.0	1.0	16	0
C	4450.2	H	392045	6269532	0.1	1.3	22.3	9.9	4.4	8.8	---	---	0
D	4168.2	S	398164	6269357	1.6	2.9	19.6	17.3	2.2	5.3	0.4	0	0
LINE 51780			FLIGHT 73										
A	6266.7	S	386658	6269540	3.0	21.3	40.8	153.9	3.3	21.1	0.2	0	0
B	6146.2	S?	389394	6269485	2.4	1.2	18.2	2.5	19.9	0.3	---	---	47
C	6131.3	S	389593	6269477	2.0	0.7	25.7	6.6	27.1	1.1	---	---	0
D	6073.1	H	390980	6269415	3.1	3.6	48.2	33.7	3.8	14.1	0.7	36	0
E	6040.5	H	391850	6269378	2.0	0.2	21.5	14.2	3.5	6.8	---	---	0
F	5721.8	S	398198	6269205	2.6	2.7	23.5	15.7	2.3	6.9	0.8	13	0
LINE 51790			FLIGHT 73										
A	3299.0	S	386805	6269395	0.0	2.3	5.3	11.6	0.6	2.0	---	---	0
B	3463.6	B?	390981	6269294	4.8	1.7	48.4	32.2	3.7	16.3	3.9	21	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 51790			FLIGHT 73										
C	3480.3	B?	391496	6269273	7.3	10.3	20.7	25.8	1.5	8.0	0.8	8	13
D	3490.5	D	391778	6269271	13.0	9.1	34.8	35.1	4.2	10.9	2.2	5	0
E	3531.0	S	392716	6269188	1.1	1.3	2.8	7.1	0.9	1.4	---	---	15
F	3621.1	S	394512	6269162	0.9	3.6	8.6	23.8	0.5	4.0	---	---	0
G	3788.0	S	398362	6269082	1.1	1.3	3.2	7.3	0.4	2.0	---	---	0
LINE 51800			FLIGHT 73										
A	7950.5	S	386713	6269220	1.7	1.9	6.1	25.1	1.8	4.1	---	---	0
B	7791.9	H	390820	6269122	7.3	4.2	65.5	66.2	9.1	23.2	2.3	38	0
C	7763.0	H	391473	6269081	2.2	3.6	9.0	11.7	4.5	5.5	---	---	21
D	7721.1	B?	392093	6269096	4.3	7.8	9.2	24.8	0.9	3.5	---	---	0
E	7649.0	S	392742	6269094	0.8	3.2	8.7	32.0	1.0	4.9	---	---	17
F	7556.3	H	394241	6269028	1.2	1.6	11.5	17.7	1.2	3.3	---	---	37
G	7366.8	S	398071	6268916	0.0	1.3	19.8	15.3	1.9	6.4	0.1	32	0
LINE 51810			FLIGHT 73										
A	8417.3	H	390692	6268968	3.7	5.6	68.2	72.4	7.9	20.4	0.6	31	0
B	8432.1	H	391081	6268971	4.2	6.8	15.9	17.4	0.9	2.0	0.6	27	0
C	8451.3	B?	391490	6268980	10.8	6.6	54.6	32.8	3.8	13.6	2.4	26	0
D	8463.3	E	391703	6268986	2.6	6.2	51.2	97.4	2.3	19.2	0.4	10	0
E	8665.6	H	394275	6268882	2.9	4.5	18.3	31.3	1.1	6.7	0.5	33	0
LINE 51820			FLIGHT 73										
A	9279.4	S	390243	6268818	2.4	6.6	36.4	42.7	1.9	9.3	0.3	6	88

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 51820			FLIGHT 73										
B	9261.1	B?	390574	6268804	5.8	5.9	23.7	50.8	3.4	9.1	1.1	8	0
C	9216.3	B?	391359	6268772	6.2	4.4	21.8	14.3	4.5	8.8	1.6	1	0
D	8984.8	S	394284	6268739	5.2	17.8	50.8	123.3	2.1	22.9	0.3	0	39
LINE 51830			FLIGHT 131										
A	2332.8	S	390037	6268692	5.1	10.3	66.3	96.4	3.1	21.9	0.5	11	0
B	2301.3	B	390922	6268666	10.8	12.8	64.6	51.6	10.6	23.2	1.1	0	35
C	2295.0	D	391032	6268657	11.4	16.1	64.6	51.6	10.6	23.2	0.9	0	0
D	2276.5	B?	391361	6268651	5.2	5.7	21.5	28.6	5.1	9.5	0.9	28	49
E	2092.5	B?	394331	6268590	31.8	83.7	204.2	488.6	3.4	88.6	0.8	0	0
LINE 51840			FLIGHT 131										
A	2568.1	S?	389885	6268570	4.2	3.5	50.5	42.9	6.0	13.5	1.2	34	0
B	2601.6	E	390769	6268540	12.8	7.7	106.5	42.6	33.0	44.8	2.6	0	0
C	2607.6	B	390826	6268541	7.3	6.3	106.5	35.1	33.0	44.7	1.4	3	35
D	2620.8	B?	390955	6268542	9.3	3.9	84.6	35.6	18.8	34.8	3.8	16	0
E	2645.3	B	391233	6268519	4.0	9.6	21.3	34.9	6.2	9.2	0.4	0	0
F	2650.7	D	391323	6268515	17.0	18.6	24.4	34.9	1.4	10.3	1.4	0	13
G	2805.6	S	394265	6268433	7.1	11.8	52.6	89.7	1.7	19.6	0.7	0	16
LINE 51850			FLIGHT 148										
A	4093.9	H	389669	6268405	1.6	4.3	44.3	57.5	5.5	12.6	0.3	18	0
B	4047.7	H	390814	6268358	1.5	1.1	15.9	6.1	5.4	6.2	---	---	27
C	4035.9	B	391073	6268368	1.8	2.7	20.1	6.5	12.4	8.7	0.5	0	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 51850			FLIGHT 148										
D	4024.2	E	391307	6268372	6.7	6.1	30.4	21.8	5.8	12.7	---	---	26
E	3789.7	S	394381	6268291	4.3	0.3	33.2	37.9	2.1	9.7	---	---	46
LINE 51860			FLIGHT 148										
A	4384.7	H	389592	6268270	4.3	10.0	53.5	68.6	3.2	15.4	0.4	12	0
B	4459.8	B	390997	6268237	9.3	10.2	61.4	87.1	29.5	23.0	1.1	13	0
C	4483.9	B?	391204	6268213	4.4	17.3	243.5	416.8	18.4	89.7	0.3	1	0
D	4493.9	E	391277	6268202	27.7	50.7	232.5	431.2	1.8	89.9	1.0	7	100
E	4526.2	S	391629	6268180	0.6	1.9	16.8	73.8	0.3	11.4	---	---	0
F	4659.9	S	394213	6268141	6.4	13.9	32.4	63.6	2.0	12.3	0.5	0	20
LINE 51870			FLIGHT 148										
A	4984.8	S	388880	6268134	6.4	28.6	51.0	234.4	3.3	33.9	0.3	0	0
B	4960.8	S?	389654	6268117	4.6	8.0	38.7	106.1	2.5	19.0	0.6	23	0
C	4902.2	B?	390904	6268082	4.6	9.4	67.9	70.1	7.7	20.8	0.5	0	0
D	4898.8	B	390969	6268081	5.1	7.8	67.9	70.1	12.0	20.8	0.6	7	0
E	4890.8	B	391122	6268077	3.7	6.7	98.7	123.4	12.0	30.8	0.5	16	0
F	4864.5	H	391578	6268049	1.9	5.1	18.8	58.3	3.4	7.8	---	---	0
G	4856.3	S	391702	6268046	0.8	5.6	17.4	93.1	2.0	12.6	---	---	0
H	4747.2	S	394219	6267994	6.7	16.6	48.2	93.0	2.1	17.9	0.5	0	17
LINE 51880			FLIGHT 148										
A	5263.8	S	388143	6268010	4.8	6.9	45.9	132.7	2.7	19.4	0.7	36	0
B	5282.9	S	388768	6267996	5.3	5.2	85.3	170.1	5.5	29.6	1.1	43	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 51880		FLIGHT 148											
C	5390.2	D	390998	6267911	17.8	21.7	93.6	81.2	20.8	35.9	1.3	0	0
D	5397.4	B	391096	6267907	42.3	61.4	241.1	434.2	7.8	79.8	1.4	1	77
E	5421.0	B?	391518	6267890	11.0	57.0	71.0	277.2	1.5	39.0	0.3	0	0
F	5428.2	S?	391626	6267883	7.0	28.3	32.3	140.1	0.2	20.5	0.3	0	0
G	5563.6	S	394256	6267835	6.0	15.0	48.9	69.7	0.9	15.4	0.5	0	18
LINE 51890		FLIGHT 148											
A	5894.3	E	387837	6267880	5.9	18.3	9.2	153.4	1.8	21.5	0.4	0	0
B	5886.4	S	388129	6267853	3.7	9.1	69.5	145.4	3.4	33.8	0.4	15	0
C	5869.1	S	388757	6267815	6.5	9.6	60.8	166.3	3.3	28.3	0.7	24	0
D	5794.0	B	390831	6267789	20.5	11.8	54.5	66.9	10.0	21.1	3.2	4	0
E	5787.3	D	390993	6267795	50.6	55.3	189.0	213.1	46.1	73.6	2.0	0	57
F	5783.6	E	391062	6267790	22.1	29.0	193.3	213.1	11.5	56.6	1.3	5	28
G	5764.9	H	391370	6267772	5.4	1.1	47.8	61.8	4.1	17.1	9.2	62	0
H	5760.6	S?	391464	6267759	11.0	46.8	51.5	183.9	4.0	30.2	0.4	0	124
I	5738.2	B	391907	6267719	4.0	4.8	95.5	46.4	45.9	37.2	0.8	0	20
J	5736.0	E	391971	6267719	15.3	11.1	95.5	46.4	45.9	37.2	2.2	0	19
K	5649.4	S?	394197	6267687	14.5	20.5	63.8	122.5	1.6	23.1	1.0	0	15
LINE 51900		FLIGHT 148											
A	6939.2	S	388154	6267720	8.1	33.1	110.4	365.8	3.8	61.2	0.3	0	0
B	6953.9	S	388627	6267710	7.4	10.6	74.5	97.0	3.8	22.5	0.8	25	0
C	7053.8	B	390815	6267618	60.3	66.2	223.5	229.9	37.5	89.8	2.1	0	0
D	7061.4	B	390979	6267608	29.8	16.0	214.9	136.6	34.5	17.9	4.0	7	15

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 51900		FLIGHT 148											
E	7081.5	B	391297	6267615	18.2	18.0	106.2	144.9	15.6	33.6	1.6	0	16
F	7086.2	B	391387	6267609	17.0	7.4	89.9	42.2	15.6	36.1	4.4	9	0
G	7091.7	E	391493	6267611	10.5	18.2	9.9	20.4	0.0	1.1	0.7	0	0
H	7115.0	H	391959	6267614	44.8	27.5	172.3	96.6	73.1	82.6	3.8	0	0
I	7117.1	B	392015	6267612	76.1	34.7	172.3	96.6	73.1	82.6	6.8	0	0
J	7231.7	S?	394204	6267556	19.5	27.5	69.9	151.7	1.7	26.7	1.1	0	23
LINE 51910		FLIGHT 148											
A	7573.6	S?	388549	6267554	3.4	14.3	81.6	223.3	2.8	38.2	0.2	3	13
B	7477.1	D	390871	6267467	69.2	71.9	288.9	272.8	51.6	119.4	2.4	0	0
C	7471.7	B	390982	6267468	44.7	65.5	288.9	272.8	51.6	119.4	1.4	1	139
D	7462.0	B?	391154	6267452	10.5	14.0	53.1	59.8	0.1	17.8	1.0	14	0
E	7456.2	B	391239	6267446	8.3	7.0	61.0	66.2	7.0	21.8	1.5	23	10
F	7446.7	B	391391	6267434	3.2	5.2	36.4	32.1	4.2	12.1	---	---	0
G	7431.1	B	391772	6267429	10.6	5.2	40.8	20.5	20.9	15.5	3.2	2	0
H	7426.4	B	391950	6267433	10.6	5.6	40.8	21.7	20.9	15.5	2.9	0	0
I	7326.0	S	394206	6267377	9.0	7.7	30.4	48.1	2.5	9.9	1.5	0	0
LINE 51920		FLIGHT 148											
A	7794.8	S?	388408	6267405	4.0	12.4	26.9	50.4	2.5	9.5	0.3	0	0
B	7897.3	D	390872	6267328	50.3	37.7	172.9	137.3	32.2	68.3	3.1	0	0
C	7900.6	D	390930	6267326	30.9	38.6	172.9	137.3	32.2	68.3	1.5	0	71
D	7909.6	D	391089	6267320	24.6	32.1	65.4	86.0	0.6	20.9	1.3	0	0
E	7913.0	B	391152	6267317	20.0	30.1	65.4	86.0	2.7	20.9	1.1	0	20

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 51920			FLIGHT 148										
F	7924.0	B	391381	6267310	7.1	18.7	53.7	59.1	12.7	23.2	0.5	0	0
G	7936.8	B	391787	6267298	16.0	9.0	72.0	37.7	24.3	28.3	3.1	3	0
H	7939.4	E	391895	6267299	19.3	8.8	72.0	37.7	24.3	28.3	4.3	0	0
I	8059.9	S	394215	6267246	11.4	12.3	33.2	71.9	3.2	12.6	1.3	0	0
LINE 51930			FLIGHT 148										
A	8282.9	D	390928	6267162	13.1	13.1	23.5	26.2	0.5	9.5	1.4	15	39
B	8267.2	B	391164	6267148	5.3	5.5	31.1	51.4	8.0	9.6	1.0	13	0
C	8257.1	B	391356	6267148	28.9	25.8	89.9	87.5	21.3	37.7	2.1	0	0
D	8245.6	H	391744	6267151	2.4	4.1	21.9	18.8	6.9	8.5	0.4	26	0
E	8188.4	S?	393154	6267111	1.6	2.3	5.9	9.1	9.4	0.9	---	---	0
F	8135.1	B?	394228	6267088	11.7	12.5	52.4	74.8	2.8	18.2	1.3	0	17
LINE 51940			FLIGHT 148										
A	8853.8	D	390916	6267029	10.0	18.2	26.6	56.3	0.1	12.5	0.7	8	0
B	8864.9	H	391125	6267032	9.0	8.2	28.8	89.1	13.4	10.1	1.4	8	0
C	8870.7	B	391254	6267028	38.9	32.8	194.4	116.6	39.4	79.3	2.5	0	0
D	8880.7	H	391612	6267016	1.1	2.3	22.3	17.7	10.0	8.7	---	---	0
E	8998.1	B?	394207	6266946	7.9	9.1	39.3	29.4	3.9	13.5	1.0	2	15
LINE 51950			FLIGHT 148										
A	9204.6	E	390968	6266868	6.1	8.1	6.9	0.0	1.7	0.4	0.8	7	0
B	9195.1	B	391185	6266866	12.7	12.8	60.3	75.2	12.1	22.4	1.4	0	0
C	9177.2	H	391857	6266852	2.1	0.7	16.0	2.8	12.3	5.9	---	---	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 51950		FLIGHT 148											
D	9165.9	B	392283	6266849	9.2	13.5	73.2	109.5	13.1	28.1	0.8	2	0
E	9077.2	H	394188	6266785	5.2	5.2	35.3	57.7	3.0	14.1	1.0	21	0
LINE 51960		FLIGHT 148											
A	9663.8	B	391087	6266737	8.3	5.8	18.3	20.9	6.7	6.1	1.9	15	0
B	9682.8	H	391777	6266706	6.8	2.8	37.8	16.6	27.8	10.4	3.4	41	0
C	9690.9	H	392026	6266681	3.3	5.1	30.9	48.2	15.1	14.0	0.6	13	0
D	9792.3	H	394163	6266627	2.2	5.5	25.8	34.7	3.5	11.0	0.3	0	0
LINE 51970		FLIGHT 149											
A	1092.0	S?	388142	6266661	0.0	2.2	3.3	13.0	144.2	4.1	---	---	938
B	1064.3	S	388844	6266635	2.4	1.1	2.9	0.3	0.8	0.7	---	---	10
C	945.9	H	391856	6266546	2.2	4.8	31.9	42.3	13.1	10.8	0.4	10	39
D	820.0	H	394123	6266482	4.2	4.6	33.1	42.1	3.0	13.3	0.9	30	0
LINE 51980		FLIGHT 149											
A	1327.5	S?	389057	6266501	2.5	4.1	2.8	30.3	0.3	4.1	---	---	25
B	1418.3	H	391659	6266421	4.9	7.0	21.4	23.1	4.6	6.9	0.7	0	28
C	1548.9	H	394121	6266328	4.0	0.6	32.5	26.3	4.7	12.1	11.7	36	0
LINE 51990		FLIGHT 149											
A	1771.2	H	391419	6266251	1.2	1.4	12.5	9.6	5.6	4.0	---	---	0
B	1639.0	H	394048	6266179	4.8	6.4	26.1	32.2	3.5	10.4	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52000			FLIGHT 149										
A	2103.0	S	389390	6266177	1.2	2.9	3.6	10.5	0.5	2.5	---	---	0
B	2169.0	H	391358	6266123	1.3	1.4	6.5	1.5	4.3	2.5	---	---	0
C	2305.6	B?	393773	6266056	9.6	7.3	17.1	15.7	2.2	6.0	1.8	3	0
D	2313.7	H	394041	6266040	4.7	6.7	36.6	28.6	3.5	12.5	0.7	14	0
LINE 52010			FLIGHT 149										
A	2409.1	S?	394074	6265878	5.2	4.4	17.1	16.4	2.1	7.0	---	---	0
LINE 52020			FLIGHT 149										
A	10470.4	H	394048	6265744	1.9	3.2	19.9	15.6	3.1	5.7	0.4	29	0
LINE 52030			FLIGHT 149										
A	10091.1	S	389579	6265696	1.2	4.5	3.4	26.4	0.1	3.5	---	---	0
B	10006.0	S?	392018	6265637	1.7	2.4	0.9	11.5	1.4	1.6	---	---	19
C	9938.0	S	393125	6265598	1.4	0.3	2.8	15.8	0.7	2.3	---	---	0
D	9901.7	S	394110	6265571	5.1	2.6	10.1	8.8	1.0	3.3	---	---	0
LINE 52040			FLIGHT 149										
A	2847.3	S	398533	6265329	2.0	8.0	10.7	34.8	4.4	4.1	---	---	0
B	2909.3	S?	400113	6265291	3.9	9.8	15.5	70.7	0.4	9.0	---	---	0
C	2975.5	D	401830	6265220	9.4	2.9	67.6	12.7	29.0	28.6	5.9	23	0
D	2979.9	B	401992	6265218	14.8	4.4	67.6	17.5	29.0	28.6	7.0	2	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52050			FLIGHT 149										
A	3245.5	S	400239	6265127	1.3	2.0	11.4	49.4	0.7	7.3	---	---	0
B	3185.8	B	401589	6265099	10.0	6.3	16.0	19.9	2.3	6.9	2.2	5	0
C	3178.8	B?	401801	6265103	7.0	4.2	39.4	4.9	16.9	18.3	---	---	39
D	3173.4	H	401986	6265088	8.7	4.0	63.2	22.6	17.6	23.2	3.2	5	0
E	3156.5	B?	402500	6265046	10.4	8.4	16.1	43.5	3.4	7.1	1.7	12	82
LINE 52060			FLIGHT 149										
A	3404.0	S?	398848	6264989	1.3	4.2	5.0	25.7	3.5	3.3	---	---	0
B	3413.0	S?	399107	6264977	1.8	4.3	3.1	19.6	0.9	2.2	---	---	0
C	3465.2	S?	400346	6264984	4.2	7.0	19.5	30.4	2.6	4.9	0.6	20	0
D	3506.8	E	401401	6264938	11.6	12.9	59.7	43.9	3.3	16.2	1.2	6	0
E	3511.3	B?	401547	6264928	9.4	5.9	59.7	19.7	1.5	16.2	2.2	15	0
F	3519.4	B	401806	6264920	10.8	5.3	80.9	38.6	15.3	29.9	3.2	23	0
G	3524.4	B	401973	6264914	14.3	9.7	80.9	38.6	15.3	29.9	2.3	0	0
H	3544.9	D	402453	6264915	13.0	8.0	21.7	49.2	0.5	7.0	2.5	1	46
LINE 52070			FLIGHT 149										
A	3768.0	S	398792	6264883	2.1	9.3	5.6	31.9	2.1	4.0	---	---	0
B	3696.3	S?	400428	6264808	2.4	23.3	25.4	134.9	1.3	20.7	0.1	0	0
C	3680.8	S?	400731	6264796	2.7	22.0	25.2	104.6	0.9	13.2	0.1	0	0
D	3666.5	H	401104	6264800	3.7	7.5	16.2	25.8	1.9	5.9	0.5	2	22
E	3640.8	B?	401874	6264784	6.3	3.3	109.5	52.4	23.2	44.2	2.5	7	0
F	3637.4	E	401972	6264778	20.5	9.1	109.5	52.4	23.2	44.2	4.5	0	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52070			FLIGHT 149										
G	3618.2	E	402402	6264763	6.9	6.7	28.9	65.3	6.0	9.0	1.2	18	83
H	3615.0	D	402488	6264756	11.2	17.1	28.9	65.3	3.2	9.0	0.9	1	20
LINE 52080			FLIGHT 149										
A	3855.7	S	398763	6264712	1.2	8.0	4.4	27.8	3.5	4.1	---	---	0
B	3940.0	S?	400773	6264665	6.5	12.3	44.1	53.9	2.3	12.8	0.6	0	0
C	3970.3	B?	401768	6264638	16.2	6.9	68.8	40.9	14.9	25.2	4.5	1	0
D	3993.9	S?	402457	6264630	6.3	7.1	12.2	26.0	0.2	3.6	1.0	10	23
LINE 52090			FLIGHT 149										
A	4301.2	S	398782	6264567	0.7	6.0	1.7	36.6	1.5	5.5	---	---	0
B	4210.8	B	400550	6264489	11.0	31.0	26.6	125.1	2.7	16.8	0.5	0	0
C	4202.0	H	400776	6264494	0.3	3.9	17.7	0.0	2.2	7.6	---	---	0
D	4166.5	B	401759	6264489	18.4	8.1	67.7	52.3	9.6	23.5	4.4	8	0
LINE 52100			FLIGHT 149										
A	4389.2	S	398642	6264400	1.0	1.7	2.3	24.8	1.4	3.3	---	---	0
B	4504.5	E	401719	6264345	13.0	11.2	75.3	52.4	8.2	24.9	1.7	10	0
C	4506.8	B	401788	6264342	10.8	6.9	75.3	52.4	8.2	24.9	2.3	17	0
D	4517.2	B	402069	6264332	9.3	7.0	26.7	27.3	2.8	8.6	1.8	15	0
LINE 52110			FLIGHT 149										
A	4792.5	E	399893	6264231	6.2	7.7	11.7	28.7	6.8	6.4	0.9	22	0
B	4787.6	S?	400017	6264232	1.8	4.2	25.9	47.5	2.8	9.7	0.3	17	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52110			FLIGHT 149										
C	4730.5	S?	401671	6264177	12.2	14.2	114.2	105.5	19.9	45.2	1.2	0	0
D	4727.4	S?	401774	6264179	8.2	13.2	114.2	105.5	19.9	45.2	0.7	0	0
E	4703.2	S?	402403	6264155	4.0	2.4	9.6	18.0	1.7	3.9	1.7	24	0
F	4690.9	D	402684	6264144	9.3	3.5	11.8	4.6	3.4	5.2	4.3	28	18
LINE 52120			FLIGHT 149										
A	4961.0	S	399368	6264082	2.7	16.5	13.1	126.0	3.7	17.0	---	---	0
B	4979.6	H	399947	6264083	4.7	2.2	53.6	26.7	7.3	13.7	2.6	40	0
C	5032.0	H	401680	6264037	0.1	0.9	29.8	55.4	8.4	13.0	0.1	12	0
D	5040.0	E	401918	6264032	6.3	6.2	14.9	31.0	1.9	5.2	1.1	5	0
E	5046.3	H	402086	6264029	1.1	2.9	0.0	2.7	0.6	0.0	---	---	0
F	5055.8	B?	402342	6264020	6.2	3.6	14.6	20.8	0.2	3.7	2.1	36	19
G	5067.5	D	402674	6264014	8.8	5.2	15.0	9.2	3.2	4.8	2.4	8	0
LINE 52130			FLIGHT 149										
A	5331.0	S	399423	6263941	2.2	10.7	22.9	78.4	3.3	12.5	0.2	0	0
B	5312.1	H	399979	6263927	6.5	9.8	72.3	83.9	9.1	21.0	0.7	18	0
C	5289.6	S?	400711	6263907	12.4	12.3	86.8	76.4	6.2	25.7	1.4	0	0
D	5278.1	S?	401083	6263889	6.6	11.6	31.0	55.6	2.4	9.7	0.6	9	0
E	5271.5	H	401287	6263893	0.0	2.5	31.0	2.9	1.8	1.6	0.1	22	0
F	5260.8	H	401614	6263884	4.4	5.0	32.3	32.6	3.6	11.1	0.9	22	13
LINE 52140			FLIGHT 149										
A	5510.6	H	400089	6263780	4.1	5.1	53.3	55.1	3.7	15.6	0.8	29	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52140			FLIGHT 149										
B	5554.4	B	401447	6263745	16.5	16.6	67.3	87.2	4.7	23.5	1.5	4	0
C	5578.0	S	402079	6263720	2.1	4.5	6.6	35.5	0.7	4.1	---	---	0
LINE 52150			FLIGHT 149										
A	5851.7	S	399079	6263674	1.6	1.9	9.0	17.0	1.4	4.4	---	---	0
B	5812.1	H	400162	6263617	5.0	7.7	19.4	30.6	1.4	5.6	0.6	11	0
C	5769.7	B?	401503	6263584	4.9	15.0	19.3	65.1	0.6	11.2	0.4	2	0
D	5756.8	D	401931	6263563	4.7	7.2	11.1	13.0	2.6	4.1	0.6	22	0
E	5726.1	S	402864	6263543	1.3	5.5	1.8	27.8	1.0	3.7	---	---	30
LINE 52160			FLIGHT 149										
A	7368.1	H	401694	6263431	1.8	5.4	20.7	13.9	1.6	4.0	---	---	0
B	7363.2	D	401832	6263427	4.1	10.4	20.7	40.2	3.2	5.8	0.4	7	0
LINE 52170			FLIGHT 149										
A	7230.0	S?	401807	6263271	11.0	12.8	77.1	102.9	2.9	23.2	1.1	0	0
B	7232.4	E	401874	6263267	11.3	14.5	77.1	102.9	2.9	23.2	1.0	9	0
LINE 52180			FLIGHT 149										
A	7008.2	S	398652	6263216	0.4	1.1	1.9	36.2	0.9	4.7	---	---	0
B	6880.6	S?	401756	6263131	6.4	10.9	58.0	107.3	2.7	21.7	0.6	11	0
C	6874.5	E	401867	6263122	8.1	12.5	64.1	107.3	2.3	21.7	0.8	3	0
D	6853.0	S	402325	6263110	3.3	11.7	2.5	28.3	1.4	2.9	0.3	5	0

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LINE 52190			FLIGHT 149										
A	6693.4	S	400432	6263005	3.0	4.2	16.9	27.4	0.7	6.7	0.6	17	0
B	6733.9	S?	401672	6262970	3.6	2.4	16.3	35.0	1.8	6.0	1.5	23	0
LINE 52200			FLIGHT 149										
A	6432.2	S?	400379	6262862	2.2	1.4	14.8	14.4	1.6	3.9	1.4	32	0
B	6404.1	S?	401190	6262834	5.6	5.7	6.9	22.3	0.4	3.9	1.1	27	0
C	6392.7	H	401544	6262833	0.1	0.7	8.0	4.6	1.5	3.4	---	---	0
LINE 52210			FLIGHT 149										
A	6177.5	S?	400363	6262691	6.0	6.3	20.2	23.3	1.8	7.6	1.0	0	0
B	6220.7	H	401601	6262682	1.8	1.3	21.1	15.3	3.7	6.3	1.0	55	0
LINE 52220			FLIGHT 170										
A	5879.3	S	394608	6262706	0.6	5.1	8.3	33.0	2.2	5.3	---	---	0
B	5983.3	S?	396102	6262680	2.6	1.8	5.2	5.3	0.2	2.0	---	---	0
C	6020.0	S	397038	6262632	0.8	1.8	2.6	17.1	1.8	2.1	---	---	0
D	6157.4	H	400384	6262581	5.7	3.2	12.8	4.2	2.9	4.2	2.2	2	0
E	6171.3	H	400793	6262570	2.6	4.9	29.0	28.7	3.1	11.0	---	---	0
F	6196.5	B?	401566	6262537	3.4	4.8	24.9	30.2	7.3	10.1	0.6	13	0
G	6259.0	H	402926	6262490	2.8	3.3	10.2	27.2	0.4	4.6	---	---	0
LINE 52230			FLIGHT 170										
A	5747.3	S?	393017	6262625	8.2	8.5	15.9	76.0	1.0	12.0	1.2	28	0

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LINE 52230			FLIGHT 170										
B	5672.7	S	393803	6262596	2.5	8.0	3.2	21.3	2.1	4.0	---	---	0
C	5554.4	S?	396229	6262500	1.8	2.0	5.9	5.4	0.6	1.9	---	---	0
D	5433.7	H	398788	6262443	6.4	3.1	10.2	12.7	1.3	2.4	2.8	9	0
E	5366.3	H	400424	6262402	4.9	1.9	21.7	7.8	6.4	7.5	---	---	0
F	5355.0	B	400725	6262420	16.1	13.6	50.6	61.3	5.3	18.9	1.8	0	14
G	5329.4	H	401290	6262377	4.0	3.6	9.2	4.2	1.8	2.5	1.1	0	0
H	5238.5	S?	403069	6262353	5.8	6.4	15.8	39.3	1.3	7.0	1.0	7	0
LINE 52240			FLIGHT 170										
A	4566.1	E	393080	6262487	4.5	10.1	6.6	12.4	1.2	2.9	0.5	0	0
B	4613.3	S?	394084	6262437	1.8	5.7	0.8	21.9	0.2	3.8	---	---	67
C	4626.7	S	394492	6262409	1.4	3.2	8.0	19.7	8.6	3.9	---	---	0
D	4724.0	S	396419	6262375	1.5	0.6	1.5	6.8	1.4	1.8	---	---	0
E	4888.3	H	400544	6262269	7.6	4.3	48.8	50.6	3.5	14.9	2.4	38	0
F	4902.2	H	401011	6262231	0.5	1.5	0.0	3.9	1.2	0.1	---	---	0
G	4920.1	B	401591	6262215	11.1	8.0	34.8	27.7	8.5	12.4	2.0	0	0
H	4934.7	D	401872	6262211	15.5	10.1	29.6	29.6	6.0	11.4	2.5	18	0
I	4972.1	H	402714	6262207	4.2	5.2	12.2	26.4	1.3	5.8	0.8	22	0
LINE 52250			FLIGHT 170										
A	4529.8	B?	392973	6262300	9.5	11.5	9.6	19.8	0.6	3.9	1.0	14	0
B	4492.0	B?	393226	6262303	5.3	12.7	23.4	63.6	1.7	11.7	0.5	12	0
C	4445.3	S?	394150	6262273	3.3	6.8	3.9	48.5	0.3	8.4	---	---	96
D	4186.9	S?	398931	6262142	3.5	1.1	4.5	3.2	0.7	1.1	---	---	0

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LINE 52250			FLIGHT 170										
E	4138.4	H	400392	6262103	5.4	6.6	40.4	30.8	7.6	15.5	0.8	22	0
F	4109.1	H	401202	6262079	5.1	7.0	7.9	34.9	2.4	5.0	0.7	28	0
G	4099.1	H	401455	6262076	2.4	0.5	9.8	1.8	3.8	4.7	---	---	0
H	4078.9	E	401924	6262083	7.2	4.6	11.7	8.9	5.2	4.0	2.0	18	0
I	4044.1	S?	402692	6262047	5.4	7.8	22.7	46.9	1.2	8.9	0.7	11	0
LINE 52260			FLIGHT 170										
A	3396.6	S	394198	6262113	2.5	5.7	19.4	52.6	3.6	9.1	0.4	19	10
B	3636.9	B	400346	6261972	5.1	3.0	27.7	22.6	3.3	8.3	1.9	37	10
C	3662.4	B	401095	6261970	7.5	2.0	38.0	41.2	2.9	12.9	6.4	29	0
D	3679.6	B	401598	6261927	5.3	3.3	21.8	26.3	3.3	6.2	1.9	32	0
E	3697.8	B	401961	6261920	5.1	4.1	9.1	9.1	0.0	1.9	1.3	37	0
F	3727.7	B	402726	6261926	18.9	9.4	49.4	54.6	2.6	16.5	3.8	8	0
LINE 52270			FLIGHT 108										
A	2938.9	S	394296	6261981	1.7	6.0	24.0	76.4	0.7	11.6	0.2	1	46
B	3114.7	H	400022	6261778	2.8	2.4	31.8	13.9	4.0	11.9	1.0	45	0
C	3150.2	B	401132	6261815	7.6	4.2	22.1	26.3	4.0	8.8	2.4	23	0
D	3168.5	H	401610	6261777	1.9	2.7	22.1	22.5	3.0	8.4	0.5	34	0
E	3185.0	B	402024	6261747	6.3	7.0	15.3	45.8	0.5	6.3	1.0	18	0
F	3209.0	D	402718	6261802	5.1	3.4	25.1	19.9	0.7	7.0	1.7	23	0
LINE 52280			FLIGHT 120										
A	2509.1	H	398956	6261690	1.1	0.4	7.7	7.5	2.5	4.4	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52280			FLIGHT 120										
B	2475.4	H	399959	6261661	4.6	3.2	31.2	18.7	4.5	10.9	1.6	32	0
C	2445.8	H	400783	6261638	3.2	1.0	24.0	9.0	7.4	9.3	3.9	27	0
D	2415.4	H	401591	6261618	3.8	4.0	32.8	22.2	5.8	13.0	0.9	9	0
E	2391.8	B	402074	6261623	6.7	4.4	6.8	7.9	3.7	3.1	1.8	14	0
F	2386.7	B?	402215	6261616	1.4	1.4	1.0	0.8	0.6	0.9	---	---	50
LINE 52290			FLIGHT 120										
A	2868.5	H	395874	6261633	1.6	2.9	13.0	19.0	3.1	4.6	---	---	0
B	2981.0	D	398902	6261544	18.2	6.9	55.9	43.0	16.8	23.7	5.4	0	0
C	3013.7	H	399969	6261520	2.1	3.2	10.6	12.3	2.3	3.2	---	---	0
D	3032.1	H	400539	6261484	0.8	1.1	0.1	0.0	5.2	0.2	---	---	0
E	3041.3	H	400826	6261492	4.7	3.7	33.6	13.1	11.0	13.9	1.4	16	0
F	3085.3	H	401694	6261490	1.9	2.7	35.5	15.4	7.6	13.6	0.5	16	0
G	3102.8	D	402098	6261491	6.8	3.8	9.1	14.3	1.1	3.5	2.3	23	0
H	3116.4	H	402473	6261478	0.3	1.3	15.1	14.3	2.5	5.0	0.1	22	0
LINE 52300			FLIGHT 120										
A	3901.8	H	396145	6261496	4.1	3.7	22.5	31.9	1.6	9.2	1.1	33	0
B	3776.9	B	399036	6261389	19.8	5.1	67.9	46.0	39.7	28.4	9.6	13	0
C	3718.7	H	400637	6261351	9.4	3.4	53.8	26.6	18.0	21.4	4.5	13	0
D	3700.7	H	401199	6261340	1.8	0.7	0.0	1.8	1.3	0.9	---	---	0
E	3663.0	H	402046	6261323	0.0	0.0	8.6	0.0	3.7	4.0	---	---	0
F	3656.2	B	402208	6261323	6.9	1.8	14.3	14.2	1.3	4.7	6.5	27	0
G	3470.0	S	406085	6261195	0.9	1.7	5.6	6.0	0.9	1.9	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52310			FLIGHT 120										
A	4162.0	H	395727	6261334	2.2	3.0	14.8	17.0	11.8	4.0	---	---	0
B	4226.2	S?	397798	6261293	3.1	2.6	20.1	23.0	1.7	4.9	1.0	6	0
C	4262.0	H	398864	6261279	2.2	4.1	3.7	6.6	3.8	2.2	---	---	0
D	4323.2	H	400819	6261199	3.0	1.5	26.1	18.6	6.6	9.8	2.0	26	0
E	4357.4	B	401868	6261169	5.5	2.8	5.1	16.0	0.5	3.3	2.4	28	0
F	4378.5	H	402401	6261168	3.9	4.6	15.5	19.2	1.9	3.9	0.8	26	0
LINE 52320			FLIGHT 120										
A	5149.9	H	400713	6261061	2.6	1.4	16.7	14.5	4.0	7.7	1.8	41	0
B	5121.7	B	401386	6261054	4.1	1.2	11.2	5.3	2.7	3.6	4.8	0	0
C	5103.7	B	401933	6261041	9.2	4.9	20.9	22.4	2.1	8.7	2.7	10	0
D	5094.0	H	402173	6261042	2.1	1.3	3.2	0.5	4.9	2.6	---	---	0
LINE 52330			FLIGHT 120										
A	5899.0	S?	400719	6260910	2.0	1.6	9.0	11.3	0.7	3.0	---	---	0
B	5928.8	B	401412	6260890	4.8	2.2	10.1	6.9	1.6	3.3	2.7	9	0
C	5944.8	B	401958	6260863	5.9	3.0	35.2	18.6	10.8	18.2	2.5	28	0
D	5954.5	H	402195	6260878	2.5	3.5	54.4	28.8	11.5	20.0	0.6	28	0
LINE 52340			FLIGHT 120										
A	6858.0	S	393541	6260944	2.3	5.4	4.7	12.0	0.7	2.3	---	---	0
B	6608.3	H	398636	6260806	2.2	2.9	20.4	28.5	1.2	6.6	0.6	26	0
C	6584.4	E	399083	6260792	3.1	6.5	0.2	4.6	0.4	0.7	0.4	11	24

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52340			FLIGHT 120										
D	6506.4	B?	400881	6260749	3.5	4.6	3.4	12.7	1.7	2.4	---	---	0
E	6481.0	B	401415	6260741	6.5	2.3	12.4	11.1	1.1	3.9	4.3	25	0
F	6454.6	H	402036	6260720	4.6	2.0	19.4	12.3	5.1	8.1	2.8	13	0
G	6423.7	S?	402750	6260718	5.4	8.6	16.8	26.1	1.2	5.2	0.6	7	0
LINE 52350			FLIGHT 120										
A	6963.3	S	393540	6260821	1.9	3.3	5.6	18.0	1.0	2.9	---	---	0
B	7159.5	S	397914	6260698	2.6	4.3	4.1	34.0	0.2	4.6	---	---	0
C	7192.1	S?	398781	6260692	2.2	11.9	10.0	52.1	1.5	5.5	---	---	0
D	7199.4	S?	398926	6260679	1.8	3.4	14.7	41.8	4.6	5.0	---	---	0
E	7327.1	H	401865	6260568	3.5	1.8	14.1	7.5	8.0	6.3	---	---	0
F	7361.2	S?	402712	6260581	5.5	4.5	16.0	26.0	1.0	4.7	1.3	28	0
G	7419.3	S	403912	6260536	1.1	2.5	5.0	11.2	4.3	2.5	---	---	0
LINE 52360			FLIGHT 120										
A	7945.4	S	398968	6260491	2.2	4.5	18.5	22.7	1.6	6.3	0.4	0	17
B	7823.2	D	401566	6260420	5.4	3.4	23.5	19.6	4.7	7.7	1.8	17	0
C	7813.5	D	401715	6260419	4.0	2.0	8.6	10.1	0.9	6.4	---	---	0
D	7808.3	H	401797	6260413	0.4	2.2	19.1	11.4	3.8	6.4	0.1	3	0
E	7769.0	S?	402709	6260420	1.4	3.5	11.1	8.6	1.1	2.6	---	---	0
F	7716.6	S	403894	6260372	3.8	2.9	5.6	10.3	3.1	2.2	---	---	0
LINE 52370			FLIGHT 120										
A	8624.7	H	399023	6260346	7.5	6.3	17.4	32.7	2.2	6.6	1.4	13	0

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LINE 52370			FLIGHT 120										
B	8733.5	H	401664	6260275	7.0	4.5	38.2	27.6	7.3	13.9	2.0	8	0
C	8770.0	S	402782	6260267	0.9	1.6	9.8	13.5	1.3	2.5	---	---	0
LINE 52380			FLIGHT 120										
A	9378.0	S?	397757	6260221	1.2	12.2	2.1	41.3	0.7	4.8	---	---	0
B	9315.2	H	399099	6260196	9.1	14.2	31.9	71.0	2.5	13.2	0.8	9	0
C	9212.1	B?	401065	6260143	3.9	4.3	19.9	27.0	1.7	6.6	0.9	23	0
D	9191.4	B	401630	6260130	7.4	2.9	38.4	13.6	11.5	15.6	3.8	25	0
E	9101.1	S	403821	6260080	5.1	4.2	8.9	8.8	5.9	1.6	---	---	0
LINE 52391			FLIGHT 120										
A	10027.3	S?	397570	6260097	0.8	4.7	8.1	23.9	1.1	3.8	---	---	0
B	10103.6	B?	399255	6260057	2.9	8.2	36.7	55.1	2.0	11.2	0.3	0	0
C	10210.5	H	401587	6259974	4.3	3.0	39.0	21.5	8.5	14.9	1.4	30	0
D	10285.8	H	403483	6259944	3.8	1.5	6.4	15.6	1.6	2.1	---	---	0
E	10367.7	H	405349	6259876	5.4	3.3	17.7	16.9	2.1	5.6	---	---	0
LINE 52400			FLIGHT 121										
A	1279.1	S?	397584	6259926	9.1	18.7	51.9	128.0	1.1	24.3	0.6	1	92
B	1201.1	H	399211	6259890	5.0	7.4	25.6	47.8	2.1	10.1	0.7	0	15
C	1196.8	D	399338	6259885	11.2	11.3	25.6	18.1	2.1	10.6	1.3	0	15
D	1022.2	H	401542	6259833	2.0	0.3	16.1	7.8	3.8	5.3	---	---	0
E	816.4	H	405414	6259742	5.7	5.1	17.8	14.8	3.7	5.8	---	---	0

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LINE 52410			FLIGHT 121										
A	1466.8	D	397516	6259804	26.9	31.4	136.5	286.6	7.8	64.7	1.5	8	32
B	1474.1	S?	397686	6259797	24.1	64.5	106.7	311.5	1.7	49.5	0.7	0	87
C	1488.6	S?	398054	6259783	8.2	12.8	41.9	106.6	1.1	17.5	0.8	7	0
D	1549.2	H	399225	6259754	1.3	8.3	31.8	42.6	2.2	12.0	0.1	0	27
E	1553.1	D	399323	6259753	26.7	25.1	73.8	80.3	17.3	35.3	1.9	1	21
F	1656.5	H	401431	6259672	1.5	2.1	38.7	21.5	10.0	15.4	0.5	35	0
G	1704.0	B?	402659	6259652	7.9	4.8	10.7	19.3	0.6	3.6	2.2	25	0
H	1745.7	S?	404206	6259606	1.7	1.3	10.8	12.0	6.1	2.3	---	---	0
I	1807.9	H	405562	6259591	5.2	2.2	13.5	11.0	0.7	3.9	---	---	0
LINE 52420			FLIGHT 121										
A	2418.4	H	397485	6259635	8.3	0.0	43.3	70.3	7.2	18.8	---	---	26
B	2415.3	B	397598	6259632	13.5	17.7	68.8	70.3	9.1	22.7	1.1	2	45
C	2411.3	B?	397742	6259631	16.4	16.9	68.8	60.0	9.1	22.7	1.5	0	0
D	2401.0	D	398103	6259623	17.9	25.5	46.8	77.1	3.1	17.0	1.1	0	17
E	2298.1	B	399168	6259595	5.7	7.6	37.8	66.2	1.8	15.5	0.8	11	14
F	2294.9	B	399244	6259589	4.2	8.4	37.8	66.2	3.9	15.5	0.5	16	32
G	2291.2	D	399348	6259582	12.2	15.8	34.5	66.2	3.9	13.8	1.0	5	32
H	2159.5	H	401469	6259538	1.5	4.2	46.0	23.2	12.6	18.7	---	---	0
I	2155.7	E	401593	6259536	9.7	4.0	46.0	23.2	12.6	18.7	3.9	8	0
J	2105.7	S?	402683	6259505	4.9	2.7	13.5	19.4	0.6	4.2	2.1	27	0
K	2081.1	S	403387	6259485	5.1	1.6	4.9	11.0	2.9	1.5	---	---	0
L	2053.0	S?	404293	6259476	2.4	4.5	9.9	14.7	4.2	2.5	---	---	0

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LINE 52420			FLIGHT 121										
M	1981.4	H	405676	6259413	5.2	3.9	8.7	11.3	0.3	1.9	---	---	0
LINE 52430			FLIGHT 121										
A	2573.9	E	397238	6259497	4.5	14.7	45.4	87.8	1.9	16.8	0.3	0	17
B	2582.3	S?	397470	6259495	3.2	20.6	15.8	170.8	8.9	10.1	0.2	0	85
C	2589.5	B	397649	6259501	31.1	48.8	443.7	537.8	37.5	164.6	1.2	4	0
D	2591.7	D	397699	6259502	81.8	85.2	443.7	537.8	37.5	164.6	2.5	0	33
E	2608.9	D	398096	6259486	38.9	46.6	138.6	228.9	5.7	51.1	1.7	1	20
F	2663.4	D	399130	6259455	10.7	16.6	49.8	54.4	4.2	14.7	0.8	0	0
G	2667.0	D	399222	6259456	7.4	12.7	49.8	54.4	4.1	14.7	0.7	1	0
H	2672.0	B?	399359	6259448	7.6	12.4	6.1	32.5	1.0	4.7	---	---	19
I	2769.2	H	401135	6259388	4.9	2.7	16.4	17.0	0.1	6.5	2.1	22	0
J	2810.8	H	402327	6259360	3.2	6.0	22.1	32.0	0.7	7.4	0.5	14	23
K	2845.4	S	403407	6259335	2.0	2.0	8.7	20.2	4.4	4.1	---	---	0
L	2878.0	S?	404328	6259319	3.2	3.4	8.0	14.0	2.2	1.8	---	---	0
M	2935.3	S?	405808	6259278	6.0	1.5	9.5	20.8	3.0	4.3	---	---	38
LINE 52440			FLIGHT 121										
A	3648.3	S?	397399	6259337	12.3	26.2	45.6	106.3	6.9	22.0	---	---	35
B	3642.5	B	397616	6259340	123.8	112.8	485.0	377.2	127.3	196.1	3.3	0	0
C	3640.2	D	397702	6259339	123.8	112.8	485.0	377.2	127.3	196.1	3.3	0	0
D	3635.0	D	397892	6259332	55.2	55.1	193.4	209.0	38.5	77.8	2.3	0	124
E	3629.2	B?	398108	6259325	14.8	30.7	74.6	115.8	10.2	26.8	0.7	0	0
F	3546.3	H	399143	6259293	4.8	4.9	20.8	18.9	3.3	6.1	1.0	0	0

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LINE 52440			FLIGHT 121										
G	3287.7	H	401227	6259252	5.4	3.9	15.8	14.4	2.5	6.2	1.5	9	0
H	3243.6	H	402291	6259214	1.6	2.6	38.1	13.7	5.4	14.5	0.4	40	0
I	3228.2	H	402565	6259205	5.2	4.4	23.4	29.5	1.3	7.1	1.3	37	0
J	3192.1	S?	403377	6259182	4.9	2.6	10.6	11.5	4.8	2.5	---	---	0
K	3158.3	S?	404256	6259169	2.2	4.6	11.3	20.9	1.4	3.2	---	---	0
L	3098.0	S	405925	6259114	4.8	8.0	25.7	59.1	7.4	12.9	---	---	0
LINE 52450			FLIGHT 121										
A	3806.0	S?	397369	6259210	15.5	25.6	67.4	101.8	14.4	24.4	0.9	0	0
B	3816.3	D	397623	6259199	179.5	174.8	1167.5	1088.0	183.4	445.2	3.5	0	23
C	3818.7	D	397676	6259201	130.5	133.4	1167.5	1088.0	183.4	445.2	3.0	0	14
D	3827.2	D	397855	6259200	72.3	104.6	275.9	373.7	41.7	107.9	1.7	0	55
E	3839.0	S?	398071	6259185	8.7	38.9	23.8	150.7	2.4	22.6	0.3	0	23
F	3899.2	S?	399158	6259161	9.4	12.2	42.5	48.9	5.1	16.1	1.0	0	16
G	3999.9	H	401211	6259086	10.9	4.9	37.2	35.8	4.7	11.8	3.6	2	0
H	4007.5	S?	401488	6259084	8.2	7.3	29.8	33.3	1.9	10.3	1.4	0	0
I	4032.0	H	402347	6259060	3.5	1.6	9.4	6.5	1.4	4.2	---	---	19
J	4116.0	S	404468	6259008	4.3	2.9	6.1	19.0	1.1	2.8	---	---	0
K	4160.0	S?	405894	6258979	3.7	5.8	16.4	36.4	1.1	6.7	---	---	0
LINE 52460			FLIGHT 121										
A	4768.1	S?	397475	6259049	34.7	69.4	174.5	259.0	18.2	62.7	1.0	0	111
B	4764.4	D	397615	6259043	9.8	11.3	43.9	259.0	22.3	20.3	1.1	12	0
C	4760.3	H	397759	6259033	22.9	25.8	51.7	54.7	13.6	18.9	1.5	0	34

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LINE 52460			FLIGHT 121										
D	4752.6	D	398025	6259020	32.6	56.9	114.5	218.0	10.6	47.1	1.1	0	28
E	4747.7	H	398194	6259018	1.2	5.1	12.0	7.7	4.0	2.2	---	---	0
F	4667.1	S?	399071	6258984	5.8	5.0	43.5	36.8	5.9	15.8	1.3	0	0
G	4504.4	S?	401264	6258933	7.5	14.2	85.8	129.0	7.8	33.0	0.6	0	0
H	4499.9	E	401415	6258932	15.8	20.4	85.8	129.0	7.7	33.0	1.1	0	0
I	4462.7	H	402494	6258897	3.7	1.8	69.5	59.8	7.1	26.0	---	---	0
J	4340.0	S?	406165	6258808	2.3	0.2	4.6	0.0	1.7	0.3	---	---	0
LINE 52470			FLIGHT 121										
A	4971.8	S?	397268	6258912	23.8	41.3	179.2	212.7	13.6	60.8	1.0	0	53
B	4979.3	B	397432	6258912	53.6	79.5	424.3	516.6	28.3	141.6	1.5	0	0
C	4982.3	D	397486	6258910	64.7	81.9	424.3	516.6	28.3	141.6	1.9	1	51
D	4988.1	D	397596	6258905	66.2	70.8	224.3	264.5	22.4	77.8	2.3	0	0
E	4993.3	B	397702	6258897	48.7	63.0	224.3	221.0	22.4	77.8	1.7	2	10
F	4998.0	D	397789	6258891	14.6	31.7	71.0	132.3	0.0	27.4	0.7	8	54
G	5004.5	H	397924	6258888	12.3	26.0	252.2	449.4	15.5	95.0	0.7	5	0
H	5007.8	D	398004	6258885	61.4	71.4	252.2	449.4	15.5	95.0	2.0	0	0
I	5059.3	B?	398987	6258844	11.6	11.5	61.6	36.4	11.6	22.5	1.4	0	0
J	5062.6	B?	399054	6258844	6.2	3.2	61.6	36.4	11.6	22.5	2.5	27	0
K	5066.5	H	399138	6258836	11.5	12.0	35.5	25.2	10.7	13.2	1.3	16	0
L	5153.7	H	400699	6258793	1.3	2.6	25.9	16.7	5.9	9.9	0.3	1	0
M	5172.7	S?	401209	6258788	7.5	15.2	117.0	166.3	9.6	42.7	0.6	0	0
N	5209.3	H	402415	6258755	4.7	8.4	67.7	45.2	9.0	25.3	0.6	9	17
O	5212.6	B?	402524	6258750	10.7	6.0	67.7	47.1	9.0	25.3	2.7	11	19

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52470		FLIGHT 121											
P	5232.0	H	403195	6258738	1.8	0.5	10.0	13.3	2.9	3.2	---	---	0
Q	5317.0	S	405863	6258687	2.1	3.8	18.7	39.0	4.5	5.7	0.4	23	0
LINE 52480		FLIGHT 121											
A	5919.7	H	397416	6258747	7.9	10.4	66.9	29.6	21.1	22.4	0.9	0	0
B	5916.6	B	397496	6258741	18.6	8.7	161.6	29.6	46.5	62.4	4.0	0	0
C	5912.1	D	397610	6258735	22.1	12.3	161.6	96.2	46.5	62.4	3.4	0	52
D	5905.1	H	397811	6258733	1.0	2.1	99.7	13.0	9.8	44.2	0.3	33	0
E	5899.6	D	397996	6258735	36.7	40.2	99.7	141.7	13.9	44.2	1.8	0	29
F	5831.5	D	399012	6258694	10.2	4.3	72.1	39.8	17.2	28.7	3.9	0	0
G	5825.5	E	399140	6258699	12.2	7.2	72.1	39.8	17.2	28.7	2.6	0	0
H	5696.4	H	400728	6258645	2.6	2.7	11.9	12.7	3.1	5.9	---	---	0
I	5671.2	S?	401284	6258634	8.2	6.3	41.2	53.7	5.5	15.0	1.6	9	0
J	5641.1	H	402017	6258637	4.7	2.9	52.3	31.2	13.2	21.7	1.8	30	15
K	5626.5	E	402466	6258598	11.7	7.8	48.9	44.3	9.5	20.7	2.2	14	25
L	5596.0	S?	403385	6258597	2.6	4.5	12.3	21.7	2.6	4.6	---	---	295
M	5544.4	S?	404947	6258535	5.4	9.8	56.3	92.7	0.9	19.3	0.6	15	0
N	5520.4	H	405862	6258520	2.6	6.6	20.0	49.1	1.4	8.2	0.3	0	19
LINE 52490		FLIGHT 121											
A	6153.7	B?	397129	6258597	8.3	11.8	65.8	62.4	10.1	23.6	0.8	3	0
B	6170.8	D	397413	6258610	37.0	54.9	384.5	415.2	73.8	144.9	1.3	3	14
C	6179.6	B	397552	6258608	208.1	145.7	1008.2	877.3	180.8	375.3	5.4	0	75
D	6184.8	E	397655	6258603	42.7	41.6	92.6	149.8	110.9	35.6	2.2	0	31

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52490			FLIGHT 121										
E	6193.8	H	397851	6258592	5.8	2.3	183.8	269.9	19.5	66.7	3.4	56	0
F	6198.7	B	397959	6258588	29.6	34.9	183.8	271.5	17.6	66.7	1.6	0	67
G	6218.7	B?	398422	6258574	4.9	21.2	4.6	50.5	3.3	6.6	0.3	1	33
H	6253.2	B	398974	6258557	25.5	8.3	116.1	68.4	26.9	45.8	7.5	0	36
I	6257.7	E	399074	6258556	20.4	13.3	116.1	30.1	26.9	45.8	2.7	0	0
J	6260.4	H	399139	6258551	8.6	8.0	42.3	40.9	13.2	15.2	1.3	10	0
K	6353.0	S?	401188	6258499	4.2	2.6	11.7	12.9	0.9	4.5	---	---	0
L	6383.1	H	401918	6258476	5.2	2.8	32.6	24.3	7.9	12.2	2.2	24	0
M	6396.9	H	402316	6258446	0.3	4.9	31.8	12.5	5.4	12.2	0.1	0	0
N	6480.5	S?	404912	6258415	4.6	9.3	49.2	77.3	1.8	18.0	0.5	0	0
LINE 52500			FLIGHT 121										
A	7130.7	E	397068	6258455	21.7	24.6	125.2	139.5	6.6	15.6	1.5	0	50
B	7124.7	B	397182	6258455	26.4	13.6	163.0	144.8	33.9	68.6	4.0	0	0
C	7120.8	D	397251	6258451	29.0	43.0	170.8	142.7	45.1	70.7	1.2	0	0
D	7116.5	D	397328	6258445	18.9	48.7	170.8	142.7	31.6	70.7	0.6	0	22
E	7107.8	D	397492	6258445	101.7	99.6	560.4	347.0	171.8	224.0	2.9	0	0
F	7100.5	D	397648	6258449	111.3	64.5	334.3	197.8	104.1	130.3	5.6	0	0
G	7091.3	D	397896	6258440	76.3	62.0	261.2	310.4	60.1	103.3	3.2	0	0
H	7082.7	H	398163	6258439	0.0	2.5	1.2	0.0	3.9	1.3	0.1	18	0
I	7074.4	B	398373	6258444	12.6	23.8	131.9	192.9	13.2	39.9	0.7	17	80
J	7070.7	D	398440	6258440	16.9	36.5	131.9	192.9	13.2	39.9	0.7	0	0
K	6995.0	B	398977	6258396	8.8	3.0	113.2	53.3	28.6	45.6	---	---	38
L	6989.0	E	399064	6258395	15.5	23.7	116.5	62.0	28.6	43.5	1.0	0	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52500			FLIGHT 121										
M	6861.5	H	400919	6258339	2.3	3.1	50.0	27.2	12.4	21.4	---	---	0
N	6815.8	H	401973	6258321	5.6	2.6	41.8	29.6	10.6	17.8	2.8	48	0
O	6809.2	B?	402172	6258312	8.9	3.7	30.0	22.8	9.6	11.7	3.7	18	0
P	6736.0	S?	404379	6258242	1.9	2.9	23.0	19.4	4.3	5.9	0.5	39	11
Q	6720.7	S	404887	6258235	1.7	3.4	16.2	33.6	0.7	6.3	0.4	23	0
R	6697.8	S?	405689	6258208	1.5	9.2	28.5	70.5	1.4	13.9	0.1	0	0
LINE 52510			FLIGHT 121										
A	7371.6	B	397230	6258303	5.6	1.5	60.2	33.3	37.9	25.4	5.8	24	0
B	7383.1	B	397324	6258302	7.0	3.7	117.7	64.7	29.1	52.9	2.5	24	22
C	7389.6	D	397400	6258317	18.4	7.6	73.8	76.5	41.2	34.1	4.9	17	0
D	7401.3	D	397629	6258314	47.7	43.5	327.4	190.1	117.0	126.9	2.4	0	0
E	7406.8	B	397781	6258291	51.5	27.7	222.9	131.0	43.3	95.9	4.8	0	0
F	7413.3	E	397984	6258280	10.2	11.0	58.2	33.7	13.6	20.3	1.2	6	20
G	7466.4	D	398949	6258246	19.1	12.6	120.7	86.3	32.5	49.3	2.6	0	85
H	7470.4	E	399043	6258251	20.4	21.9	120.7	86.3	32.5	49.3	1.5	0	0
I	7586.8	H	401958	6258151	4.7	3.0	23.8	19.3	4.2	9.3	1.7	15	0
J	7646.0	H	404176	6258125	4.4	3.0	12.5	9.5	1.7	2.5	---	---	20
LINE 52520			FLIGHT 121										
A	8257.0	B?	397046	6258147	4.2	2.4	25.5	7.4	13.9	11.6	1.9	0	0
B	8250.0	B	397164	6258141	13.2	3.7	0.0	0.7	19.8	0.0	7.3	0	27
C	8243.5	B	397262	6258140	11.6	3.8	40.3	24.4	20.8	16.0	5.7	0	0
D	8227.4	D	397479	6258136	15.4	10.9	40.6	26.1	2.3	18.3	2.3	4	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52520			FLIGHT 121										
E	8220.9	B	397579	6258137	16.3	15.3	93.4	120.8	17.9	36.6	1.6	10	27
F	8216.4	D	397662	6258140	12.9	22.3	19.4	93.7	16.5	5.7	0.8	0	0
G	8210.3	B	397808	6258140	69.6	58.0	399.6	358.3	56.9	158.4	3.1	0	50
H	8205.9	E	397928	6258136	38.7	59.1	399.6	358.3	54.2	158.4	1.3	0	46
I	8190.9	B?	398322	6258117	1.4	15.6	14.6	53.8	5.6	7.3	0.1	0	34
J	8158.6	D	398751	6258075	10.6	4.9	79.9	66.7	17.5	25.6	3.4	7	0
K	8146.6	D	398932	6258079	29.9	21.9	118.8	91.7	31.9	45.1	2.7	0	86
L	8142.3	E	399037	6258085	19.9	15.0	116.9	91.7	25.7	42.7	2.3	0	0
M	8061.3	S?	400605	6258046	2.8	0.6	17.2	7.6	3.2	6.1	6.9	0	0
N	8002.6	H	401787	6258043	5.3	2.1	24.4	6.8	5.7	10.2	3.3	14	30
O	7938.3	H	403956	6257966	2.5	4.5	14.7	12.3	1.3	5.4	0.4	36	0
P	7905.7	S?	405035	6257941	3.1	7.7	25.2	58.8	0.6	14.9	0.4	11	0
LINE 52530			FLIGHT 121										
A	8530.9	H	397225	6257981	0.1	2.5	46.8	20.3	30.4	18.7	0.1	0	0
B	8540.7	B	397339	6257995	16.0	8.7	34.1	38.9	8.0	11.4	3.2	1	0
C	8551.0	H	397446	6257998	0.0	1.9	24.6	4.9	13.8	9.9	0.1	3	0
D	8570.9	H	397675	6257999	5.6	12.8	6.3	14.7	40.1	65.5	0.5	8	0
E	8577.5	B	397840	6258000	58.6	54.3	207.5	201.8	40.1	79.7	2.6	0	99
F	8590.6	S?	398205	6257980	2.5	8.4	17.7	41.2	1.9	5.5	0.3	3	22
G	8621.0	H	398741	6257966	1.0	3.9	30.1	25.3	8.6	11.4	0.2	0	0
H	8627.4	H	398852	6257963	8.5	2.7	18.8	29.2	6.1	7.8	5.2	2	0
I	8632.3	B	398948	6257963	11.4	12.8	45.3	29.2	9.9	16.4	1.2	0	34
J	8705.1	H	400597	6257913	5.7	3.3	24.2	17.9	3.5	8.1	2.1	19	0

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LINE 52530			FLIGHT 121										
K	8751.0	H	401722	6257895	3.1	1.7	26.4	17.5	3.7	9.3	1.9	47	21
L	8757.8	E	401946	6257889	8.0	5.7	24.6	26.9	5.0	10.4	1.8	25	0
M	8797.5	S?	403329	6257842	6.9	2.6	7.7	16.1	1.6	4.0	4.0	17	0
N	8833.0	H	404669	6257815	3.2	5.0	27.2	45.9	0.4	14.3	0.6	30	0
LINE 52540			FLIGHT 121										
A	9427.5	S?	397127	6257835	3.1	2.1	43.6	5.5	19.0	18.5	1.4	0	0
B	9410.0	B?	397391	6257844	5.0	3.7	17.7	13.1	4.0	1.2	1.5	0	0
C	9400.3	H	397516	6257844	6.5	11.4	28.2	75.7	5.5	17.7	0.6	9	0
D	9388.7	D	397678	6257846	18.0	17.3	101.3	37.7	29.1	41.4	1.6	5	41
E	9383.3	D	397773	6257851	37.7	22.6	143.6	70.6	30.3	58.6	3.7	0	0
F	9332.9	H	398791	6257800	7.8	4.4	28.8	17.8	11.9	12.6	2.4	1	0
G	9283.1	H	399810	6257787	2.2	2.8	16.6	18.6	1.0	5.0	0.6	1	25
H	9241.6	H	400570	6257758	8.2	5.1	21.4	14.3	2.9	7.1	2.2	16	0
I	9188.2	H	401754	6257732	3.3	2.2	19.0	11.1	5.8	6.9	1.5	53	0
J	9156.5	H	402695	6257708	4.2	1.3	16.7	8.3	4.2	5.3	4.3	54	0
K	9130.1	H	403632	6257663	2.4	3.5	30.0	60.6	3.9	13.4	0.5	36	0
L	9106.1	S?	404527	6257642	6.4	9.6	39.2	92.0	5.2	16.7	0.7	19	0
M	9102.4	S?	404665	6257637	11.5	13.6	39.2	92.0	6.1	17.7	1.1	4	0
LINE 52550			FLIGHT 121										
A	9599.6	H	396182	6257729	7.2	0.0	19.4	2.9	25.1	0.9	---	---	0
B	9642.5	B	397242	6257693	7.7	6.7	131.4	32.0	46.9	55.5	1.4	0	23
C	9659.5	E	397413	6257683	6.2	4.7	101.7	67.4	25.1	40.2	1.5	14	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52550		FLIGHT 121											
D	9677.5	B	397700	6257688	25.1	12.4	73.7	34.0	27.3	30.6	4.2	0	0
E	9691.3	S?	398021	6257681	5.8	15.3	0.1	29.5	0.7	3.1	0.4	5	0
F	9719.8	H	398598	6257668	2.1	1.6	19.7	4.9	12.6	7.5	---	---	0
G	9730.2	E	398829	6257660	8.6	1.2	25.0	13.5	9.2	11.4	17.2	13	0
H	9842.7	H	401574	6257574	2.1	1.7	9.7	0.9	4.0	2.8	---	---	11
I	9872.3	H	402591	6257563	2.5	2.7	15.8	11.4	2.2	8.9	0.8	38	0
LINE 52560		FLIGHT 160											
A	2693.3	D	397459	6257565	24.6	19.2	69.1	73.3	13.5	27.1	2.3	4	0
B	2677.5	H	397866	6257542	1.1	1.9	2.4	1.4	0.4	0.4	---	---	41
C	2660.9	D	398200	6257515	75.2	77.3	323.1	325.8	58.3	119.2	2.5	0	0
D	2647.4	B	398466	6257509	11.0	11.1	21.5	26.0	31.4	10.5	1.3	0	0
E	2642.9	H	398568	6257509	0.1	0.4	21.5	0.0	31.4	10.5	0.1	46	11
F	2636.8	B?	398729	6257507	8.8	8.8	79.2	56.2	29.7	28.6	1.2	11	0
G	2632.7	E	398839	6257505	11.4	13.6	79.2	62.1	16.8	28.6	1.1	8	0
H	2554.7	B?	400485	6257470	6.1	3.5	17.6	17.2	2.4	6.2	2.1	29	0
I	2492.0	H	401583	6257454	2.9	3.6	8.3	13.8	4.2	5.7	---	---	26
J	2456.5	H	402663	6257386	3.2	1.0	32.2	13.5	7.5	14.1	3.8	75	0
K	2437.9	H	403233	6257364	1.8	2.1	34.0	26.4	6.8	14.3	0.6	62	0
LINE 52571		FLIGHT 160											
A	3083.3	H	397317	6257380	10.6	5.8	43.3	26.5	18.1	19.3	2.7	0	0
B	3088.5	D	397407	6257377	9.6	5.3	43.3	25.0	6.9	19.3	2.6	24	0
C	3093.4	H	397498	6257383	9.4	3.1	40.4	44.0	8.8	16.8	5.3	32	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52571			FLIGHT 160										
D	3119.2	B	398045	6257373	10.2	11.2	69.4	60.1	26.4	27.7	1.2	10	0
E	3132.6	H	398339	6257380	20.0	11.9	77.9	61.8	30.6	37.3	3.1	10	0
F	3142.4	H	398562	6257383	5.3	0.0	43.2	0.0	42.1	9.2	782.2	4	0
G	3151.9	B	398788	6257378	15.6	10.7	21.3	23.7	7.9	9.0	2.4	20	16
H	3221.0	H	400421	6257344	0.2	3.5	17.7	14.7	4.3	7.7	0.1	0	0
I	3277.4	S?	401484	6257285	4.0	2.0	20.8	30.1	2.9	6.6	2.2	14	17
J	3286.4	H	401717	6257261	0.8	0.3	0.7	0.6	2.8	1.1	---	---	0
K	3337.3	H	403152	6257239	3.1	5.7	56.0	81.2	7.2	22.6	0.5	22	0
LINE 52580			FLIGHT 160										
A	4688.2	S?	395379	6257280	5.9	4.0	18.6	27.0	54.0	5.5	1.8	52	39
B	4545.0	B	397491	6257258	21.1	18.6	76.0	67.3	21.0	34.7	1.9	4	11
C	4541.0	D	397603	6257253	22.2	11.9	73.2	67.3	21.0	34.7	3.6	4	0
D	4524.7	H	398053	6257216	26.2	15.3	125.7	63.0	42.1	52.2	3.4	14	0
E	4505.7	H	398499	6257212	18.1	1.7	154.5	19.3	140.0	40.9	40.7	8	78
F	4423.8	B?	400364	6257192	5.8	2.8	10.1	8.7	2.2	5.0	2.7	20	0
G	4376.2	H	401220	6257165	3.7	1.9	35.9	19.6	6.4	14.4	2.1	49	0
H	4315.9	H	403013	6257078	3.8	6.8	41.1	45.2	2.4	16.6	0.5	26	0
I	4209.3	B	405557	6257027	9.6	6.3	28.9	27.4	7.4	12.1	2.1	24	0
J	4089.2	D	407322	6257003	14.7	7.8	48.6	32.8	0.0	27.6	3.2	27	1499
K	4084.2	B	407418	6257000	4.0	2.0	48.6	32.8	13.9	27.6	2.2	54	0
L	4055.2	S?	408081	6256970	2.6	3.2	27.0	36.2	1.9	8.4	0.6	22	137
M	4020.0	H	409025	6256933	3.8	1.9	13.5	5.7	7.3	5.7	---	---	0
N	3911.1	S	411074	6256860	1.8	2.0	7.2	3.0	1.9	1.0	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52580			FLIGHT 160										
O	3872.2	D	411968	6256839	3.2	14.2	3.0	23.6	0.4	3.9	---	---	0
LINE 52590			FLIGHT 160										
A	4772.4	B	395339	6257144	4.2	10.7	3.8	15.9	3.7	1.9	---	---	0
B	4873.2	H	397560	6257077	6.9	8.2	13.6	20.5	2.9	5.6	0.9	22	0
C	4890.0	H	398018	6257053	30.5	27.2	182.3	109.5	57.2	70.2	2.1	5	0
D	4901.7	H	398324	6257061	28.7	5.7	189.3	28.3	167.4	51.3	16.0	11	0
E	4940.2	B?	399351	6257040	2.2	1.3	22.6	21.8	4.1	6.7	1.5	53	32
F	5002.0	S?	400772	6257015	16.3	10.9	46.7	46.3	8.8	18.4	2.5	20	18
G	5025.3	S	401310	6256974	11.5	8.8	50.0	56.7	4.1	16.3	1.9	0	46
H	5056.6	H	402253	6256965	2.5	7.3	21.5	72.5	1.8	12.6	0.3	8	0
I	5149.5	D	404624	6256901	3.5	1.8	10.7	1.8	9.9	2.0	2.0	61	94
J	5217.5	D	405440	6256893	4.1	3.9	29.0	32.5	7.1	12.7	1.0	34	0
K	5262.7	H	406294	6256814	3.8	4.2	29.0	37.4	2.9	10.8	0.8	42	0
L	5268.4	H	406430	6256812	1.3	2.1	22.8	27.6	3.5	8.7	0.4	36	0
M	5321.0	B?	407370	6256848	3.2	1.8	14.8	9.1	10.3	6.0	---	---	582
N	5325.3	B	407462	6256849	0.2	1.4	14.8	5.3	10.3	6.0	0.1	0	0
O	5355.5	S?	408163	6256821	2.5	4.4	22.4	30.0	0.9	9.2	0.4	0	0
P	5404.5	H	409184	6256760	4.8	1.3	48.3	12.7	28.3	19.5	5.6	64	0
Q	5415.5	D	409328	6256757	14.5	2.5	64.5	16.4	18.4	23.6	15.3	27	0
R	5599.6	D	411951	6256691	8.5	18.8	7.2	27.0	0.9	3.9	0.6	0	0
LINE 52600			FLIGHT 160										
A	7155.0	D	395286	6257017	2.2	8.6	7.1	29.2	11.3	4.4	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52600			FLIGHT 160										
B	7144.4	S?	395445	6257028	2.4	2.9	7.3	13.6	10.7	2.6	---	---	284
C	7006.5	H	398093	6256924	8.3	3.8	64.0	42.8	39.5	26.2	3.2	37	0
D	7000.6	B	398240	6256912	33.6	16.8	64.0	31.2	39.2	26.2	4.6	8	132
E	6986.0	H	398595	6256901	3.6	1.0	28.8	12.6	22.1	9.5	5.0	49	0
F	6961.4	H	399318	6256891	6.5	4.6	17.5	20.6	3.6	6.2	1.7	5	24
G	6924.6	S	400114	6256894	1.0	1.4	27.1	50.2	1.2	10.6	0.4	58	0
H	6885.2	H	400853	6256859	10.0	5.3	35.0	19.7	17.6	17.7	2.8	25	0
I	6868.0	H	401410	6256850	1.3	1.0	0.2	0.1	1.7	0.4	---	---	0
J	6847.4	S	402050	6256825	1.5	13.1	18.0	64.4	0.9	9.9	0.1	0	0
K	6818.9	S	402927	6256797	2.0	7.3	37.7	87.2	0.1	19.5	0.2	8	0
L	6710.3	B	405385	6256718	5.6	6.3	18.8	24.1	3.9	8.0	---	---	0
M	6648.3	B	406548	6256715	4.8	4.6	34.0	13.8	10.2	14.6	1.1	36	0
N	6596.6	D	407322	6256676	14.7	7.9	62.2	46.3	30.9	30.9	3.1	25	1390
O	6592.0	B	407398	6256671	6.7	5.6	62.2	46.1	30.9	30.9	1.4	30	0
P	6540.1	S?	408248	6256665	2.9	5.2	37.1	60.1	0.6	14.8	0.5	17	0
Q	6495.6	H	409326	6256632	0.9	0.4	26.4	2.8	18.2	10.0	1.8	72	0
R	6413.7	H	410898	6256579	3.0	1.9	10.7	1.4	3.4	4.1	---	---	0
S	6353.7	D	411958	6256557	7.0	15.8	3.6	19.5	0.9	2.6	0.5	3	21
LINE 52611			FLIGHT 160										
A	7918.9	H	398229	6256769	18.2	8.9	90.1	36.0	50.3	41.1	3.8	4	98
B	7933.4	H	398599	6256766	1.5	1.3	13.1	1.5	18.5	1.1	0.9	77	0
C	7958.9	H	399293	6256750	6.9	4.1	15.1	16.3	4.0	5.0	2.2	5	0
D	8026.8	H	400828	6256713	3.0	2.2	38.7	7.3	15.4	9.3	1.2	46	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52611		FLIGHT 160											
E	8037.0	B	401109	6256677	19.2	17.1	85.2	96.4	4.1	30.5	1.8	0	34
F	8054.1	H	401521	6256692	3.4	5.2	23.6	37.1	1.6	10.4	0.6	25	0
G	8102.0	S	402884	6256653	2.1	3.7	42.6	92.3	0.0	17.0	0.4	43	0
H	8218.5	B	405212	6256572	7.9	8.5	16.4	29.4	3.6	5.3	1.1	10	0
I	8344.9	B	407353	6256526	7.0	3.8	37.7	32.0	11.6	14.8	2.4	36	1083
J	8394.7	S?	408286	6256508	1.9	3.7	24.9	35.1	0.2	8.7	0.4	4	48
K	8435.1	H	409276	6256477	6.9	3.3	70.2	10.4	42.6	27.0	2.9	43	0
L	8448.5	B	409517	6256462	25.1	10.9	150.5	62.8	53.9	64.5	5.0	20	0
M	8534.5	H	410859	6256441	0.4	4.1	33.2	27.6	9.2	17.2	---	---	31
N	8544.9	D	411018	6256427	10.8	25.0	41.6	97.0	4.3	14.9	0.6	6	0
LINE 52620		FLIGHT 160											
A	9194.0	S	397042	6256676	2.0	0.9	6.2	10.3	0.9	2.1	---	---	0
B	9147.9	B	398317	6256614	15.7	9.8	41.6	30.7	17.8	17.0	2.7	7	0
C	9144.7	H	398418	6256612	1.7	9.9	41.6	21.6	17.5	17.0	0.2	0	0
D	9136.1	H	398681	6256611	20.1	7.2	37.7	16.8	14.6	18.8	6.0	0	0
E	9124.9	B?	398996	6256614	13.1	8.6	61.6	49.0	10.1	22.1	2.3	6	0
F	9107.1	B?	399438	6256620	10.0	13.1	35.1	37.2	5.3	12.3	1.0	1	0
G	9057.4	H	400795	6256569	0.1	1.5	30.4	13.4	11.2	12.0	0.1	6	0
H	9027.0	S	401696	6256533	4.7	12.7	45.7	156.9	6.6	26.6	0.4	2	0
I	8990.7	S	402807	6256499	5.0	10.8	44.5	80.5	2.4	20.5	0.5	6	0
J	8879.3	D	405154	6256428	6.0	4.6	6.3	10.3	0.7	3.1	1.5	16	0
K	8745.7	H	407418	6256393	0.3	1.5	10.3	14.7	2.2	4.4	---	---	472
L	8694.9	H	408348	6256366	1.7	4.6	33.1	59.6	0.5	12.2	0.3	8	91

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52620			FLIGHT 160										
M	8661.4	H	409260	6256324	5.6	2.9	27.0	14.4	12.9	10.6	2.4	28	0
N	8647.8	B	409519	6256300	7.6	3.4	53.6	20.2	19.6	23.7	3.2	27	0
LINE 52630			FLIGHT 184										
A	3228.0	S	396894	6256508	2.5	6.1	11.3	26.0	7.7	5.0	---	---	0
B	3171.2	H	398307	6256470	4.8	2.3	17.8	9.8	3.4	5.8	---	---	0
C	3156.4	B	398644	6256423	32.0	21.7	114.1	78.8	24.0	45.2	3.0	1	0
D	3137.4	B?	399065	6256428	8.0	4.5	13.3	12.1	3.5	7.6	2.4	38	0
E	3123.1	H	399336	6256448	6.3	9.1	20.4	24.5	2.6	7.3	0.8	15	39
F	3088.3	H	399614	6256467	1.7	3.6	15.3	38.0	1.5	8.2	0.3	34	0
G	3065.6	H	399927	6256418	2.2	2.6	25.6	17.8	4.9	9.7	0.6	21	0
H	3025.8	H	400786	6256421	2.3	6.1	36.1	19.3	10.8	15.3	0.3	9	0
I	2990.3	S	401706	6256371	2.9	12.5	40.9	141.2	4.5	25.8	0.2	0	14
J	2950.0	S	402813	6256353	7.3	18.6	76.4	204.9	1.2	38.1	0.5	0	0
K	2558.0	H	408383	6256200	4.8	2.3	27.0	29.3	1.2	6.3	2.6	25	49
L	2515.1	B?	409521	6256169	6.7	4.6	25.5	6.1	6.1	11.5	1.8	2	0
M	2509.2	H	409632	6256162	3.1	1.9	25.5	8.2	10.8	11.5	1.6	25	0
LINE 52643			FLIGHT 184										
A	3538.3	S?	395704	6256405	0.2	5.3	13.3	32.3	14.1	5.1	---	---	0
B	3581.9	S	396841	6256357	3.6	10.8	25.8	69.7	3.7	11.4	---	---	0
C	3636.0	S?	398261	6256323	5.4	10.8	18.1	51.5	3.3	9.0	---	---	0
D	3647.5	E	398585	6256318	15.2	21.6	54.9	87.5	1.7	17.9	1.0	8	15
E	3650.6	H	398663	6256317	6.9	16.9	54.9	87.5	1.7	17.9	0.5	3	0

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LINE 52643			FLIGHT 184										
F	3767.3	H	400606	6256265	4.4	3.6	26.9	25.9	7.0	8.9	1.3	18	0
G	3773.8	B	400760	6256261	4.4	4.4	28.3	17.2	5.6	12.2	1.0	7	0
H	3803.0	S	401599	6256236	2.3	4.1	28.9	85.2	4.3	14.8	0.4	35	0
I	3966.0	S?	404930	6256140	0.3	1.3	9.6	10.3	3.4	3.6	---	---	0
J	4138.0	S?	407663	6256059	2.8	2.2	0.6	3.2	0.8	1.1	---	---	0
K	4181.4	S?	408323	6256057	4.3	2.7	15.5	22.4	0.2	5.5	---	---	0
L	4227.3	D	409444	6256014	12.6	6.4	50.3	43.5	6.4	13.0	3.2	23	0
M	4232.1	D	409519	6256016	14.4	25.6	51.6	79.7	27.2	44.6	0.8	1	19
N	4239.6	D	409626	6256009	52.5	20.6	168.2	143.6	26.4	70.4	7.4	7	0
O	4244.7	D	409705	6256004	47.8	22.3	303.7	143.8	130.7	134.7	5.6	2	0
LINE 52650			FLIGHT 184										
A	5371.0	S?	396612	6256216	1.2	7.6	19.4	42.2	3.5	7.8	0.1	0	122
B	5151.2	H	400566	6256103	4.2	0.6	24.8	11.5	7.2	11.1	---	---	0
C	5119.2	H	401459	6256075	3.7	5.8	43.5	94.7	2.8	17.5	0.6	23	0
D	4785.4	D	407551	6255950	6.9	16.5	10.2	32.2	13.2	6.9	0.5	0	118
E	4737.0	H	408496	6255896	1.3	1.3	17.2	21.0	1.6	4.7	---	---	0
F	4688.0	H	409689	6255867	6.6	4.2	28.6	17.2	7.6	11.8	1.9	0	0
LINE 52661			FLIGHT 184										
A	5635.4	S?	395418	6256100	1.5	3.8	20.2	35.7	3.1	8.8	0.3	10	0
B	5654.3	S	396067	6256062	2.9	4.2	15.4	35.5	2.1	6.2	0.6	17	0
C	5669.1	S?	396528	6256065	4.2	8.2	19.2	43.6	4.5	6.4	0.5	20	0
D	5791.0	S?	399336	6255997	1.4	3.3	11.5	39.3	0.7	6.7	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52661			FLIGHT 184										
E	5858.0	H	400622	6255969	1.2	0.6	11.6	2.7	3.9	3.1	---	---	0
F	5883.8	H	401413	6255944	8.3	14.8	38.5	98.0	4.5	19.7	0.7	3	0
G	6209.0	H	407699	6255767	0.1	0.8	5.3	3.5	3.0	3.3	---	---	0
H	6303.2	H	409737	6255726	7.5	5.7	43.1	32.5	8.6	18.1	1.6	31	0
I	6390.0	S	410824	6255686	1.0	6.3	6.2	41.7	1.7	6.1	---	---	0
LINE 52670			FLIGHT 210										
A	2365.3	B?	395318	6255988	20.5	27.9	57.1	102.6	9.6	22.1	1.2	0	0
B	2115.0	H	400633	6255812	0.8	0.8	0.2	0.0	2.6	0.8	---	---	0
C	2092.5	H	401333	6255748	3.6	8.9	31.8	75.1	5.6	14.5	0.4	3	21
D	1768.6	D	407683	6255599	19.4	19.3	19.0	32.2	3.0	7.5	1.6	0	32
E	1752.0	B?	407871	6255596	2.8	2.6	7.4	5.1	2.4	1.8	---	---	0
LINE 52671			FLIGHT 210										
A	4063.2	D	407676	6255621	6.3	5.8	8.7	11.4	1.8	1.2	1.2	0	0
B	4010.6	H	408672	6255583	1.6	0.5	17.6	8.2	2.4	3.7	2.7	93	0
LINE 52680			FLIGHT 210										
A	3054.0	H	395556	6255804	4.3	10.0	10.7	19.2	1.4	5.7	---	---	0
B	3313.8	H	401321	6255651	4.1	4.3	24.3	45.2	4.2	10.0	0.9	15	10
C	3655.7	D	407705	6255471	10.3	6.5	33.4	29.3	7.2	15.3	2.3	8	0
D	3708.0	S?	408733	6255431	2.4	1.9	15.6	9.4	2.3	3.9	1.0	39	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52690			FLIGHT 211										
A	1538.0	S?	395609	6255662	2.1	9.9	10.4	18.8	14.8	2.5	---	---	0
B	1297.5	H	400049	6255508	0.1	1.0	21.9	16.2	3.9	6.8	---	---	0
C	1261.4	H	401140	6255463	2.3	2.2	19.9	43.8	3.8	8.0	0.8	47	0
D	1235.4	S?	401903	6255466	0.9	2.8	22.7	25.4	2.6	7.8	---	---	0
E	961.0	S	407292	6255316	0.8	4.4	2.9	17.0	2.6	1.7	---	---	148
LINE 52700			FLIGHT 211										
A	2182.7	S	391460	6255575	0.8	1.8	4.4	7.4	4.1	1.2	---	---	0
B	2504.0	S?	395704	6255476	1.1	0.9	14.5	2.5	8.0	0.6	---	---	0
C	2711.2	H	399920	6255398	0.9	1.6	26.9	22.2	3.2	9.0	---	---	0
D	2765.4	H	401328	6255359	3.1	17.8	39.1	131.6	5.7	21.7	0.2	0	0
E	2978.0	S	405193	6255248	3.1	3.3	10.8	19.7	11.6	2.4	---	---	0
F	3002.0	S	405716	6255227	3.8	8.4	16.8	24.6	16.4	4.0	---	---	0
G	3099.6	S?	407344	6255174	1.8	9.7	18.1	54.6	0.6	8.8	---	---	17
H	3181.7	H	408762	6255129	1.9	0.9	16.4	16.2	1.9	5.7	---	---	33
LINE 52710			FLIGHT 211										
A	4542.2	S?	393937	6255387	7.3	1.0	18.4	0.9	19.9	0.6	---	---	0
B	4434.2	S	395731	6255337	1.2	0.0	26.6	3.5	23.4	0.3	---	---	0
C	4194.5	H	400017	6255219	0.7	1.9	16.2	5.6	4.4	5.8	---	---	0
D	4171.9	H	400669	6255195	1.9	7.8	25.9	64.8	3.9	13.3	0.2	0	0
E	4155.1	H	401205	6255188	3.8	5.6	33.1	79.1	9.2	15.5	0.6	20	0
F	4077.4	H	403251	6255134	0.0	1.7	5.0	3.2	2.7	2.1	---	---	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52710		FLIGHT 211											
G	3984.9	S	405214	6255079	4.3	1.0	17.1	3.3	19.9	0.4	---	---	14
H	3818.6	B?	407896	6255020	19.3	25.4	45.8	91.2	2.5	17.8	1.2	0	0
I	3774.0	H	408721	6254986	1.7	1.3	15.3	18.5	0.4	5.5	---	---	0
LINE 52720		FLIGHT 211											
A	5224.2	S	395283	6255206	4.7	1.9	9.7	15.1	12.1	2.0	---	---	0
B	5241.0	S	395622	6255192	1.4	0.6	13.5	1.3	11.7	0.5	---	---	0
C	5465.2	H	400623	6255064	3.4	10.5	30.4	74.8	4.7	14.5	0.3	0	0
D	5488.4	H	401278	6255052	4.1	15.9	64.3	165.0	10.5	34.5	0.3	0	0
E	5588.7	H	403346	6254985	10.2	8.1	79.3	48.3	28.4	29.1	1.7	13	0
F	5596.6	E	403470	6254975	9.1	4.7	79.3	42.3	33.2	25.8	2.8	29	0
G	5705.3	S	405155	6254949	4.2	2.6	55.0	9.0	60.3	2.0	1.7	35	0
H	5898.0	H	408776	6254843	2.6	0.6	18.0	21.7	1.8	6.5	---	---	13
LINE 52730		FLIGHT 211											
A	7189.0	E	395718	6255029	2.5	0.8	25.5	14.5	21.2	2.4	3.8	77	0
B	6931.9	H	400488	6254906	5.3	15.6	46.8	120.8	7.4	24.7	0.4	0	0
C	6911.5	H	401110	6254890	6.7	17.1	77.7	218.5	0.6	41.3	0.5	9	0
D	6808.8	H	403470	6254836	3.7	2.0	21.2	5.9	16.6	9.8	2.0	10	0
E	6729.8	S	405155	6254794	3.4	0.9	9.4	17.8	11.7	2.8	---	---	0
LINE 52740		FLIGHT 211											
A	7675.0	S	391283	6255014	0.7	1.5	3.7	8.4	5.8	2.6	---	---	0
B	7873.2	D	395531	6254898	4.4	15.0	10.5	43.6	3.8	6.0	---	---	37

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52740		FLIGHT 211											
C	8066.2	H	399382	6254787	2.9	2.4	25.1	32.9	5.8	9.1	1.1	50	0
D	8100.6	H	400433	6254772	3.3	8.5	36.6	88.8	5.8	19.7	0.4	10	0
E	8113.9	H	400871	6254767	2.1	8.2	71.9	164.9	7.9	29.5	0.2	7	0
F	8219.3	B	403454	6254697	3.1	1.6	14.7	10.9	7.0	5.9	1.9	9	1252
LINE 52750		FLIGHT 221											
A	2486.5	S	395542	6254749	1.3	7.7	1.8	13.9	1.1	2.4	---	---	21
B	2258.5	H	399051	6254634	3.2	4.6	39.8	41.0	4.8	17.6	0.6	31	0
C	2232.9	H	399987	6254605	2.4	3.5	39.3	86.8	8.9	16.0	0.5	46	40
D	2217.0	H	400585	6254601	6.8	25.5	92.2	192.6	0.8	37.8	0.3	0	0
E	1823.6	S?	408945	6254388	2.9	2.1	23.9	19.7	1.7	9.1	1.3	10	0
LINE 52760		FLIGHT 221											
A	3069.3	S?	395445	6254603	2.4	9.6	0.2	36.7	0.0	3.4	---	---	0
B	3170.0	S	397477	6254548	2.1	0.8	3.2	3.8	0.4	1.2	---	---	0
C	3239.6	H	399117	6254515	4.0	3.8	52.4	65.1	12.9	23.5	1.0	35	0
D	3260.8	H	399956	6254491	3.0	6.3	63.6	101.5	12.1	20.8	0.4	17	52
E	3356.4	S	402621	6254403	1.7	0.2	2.7	6.5	0.6	0.9	---	---	0
F	3513.8	S	405417	6254325	1.1	0.3	8.4	9.5	8.0	1.5	---	---	0
LINE 52770		FLIGHT 221											
A	4830.7	S?	395511	6254450	5.6	10.2	11.7	34.7	3.9	4.3	---	---	0
B	4924.3	S	397421	6254395	1.3	1.2	3.2	5.4	1.7	1.1	---	---	0
C	4985.1	H	399050	6254365	0.8	2.8	95.8	162.4	14.0	39.5	0.2	26	10

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52770			FLIGHT 221										
D	5002.5	H	399739	6254350	1.0	3.4	84.0	94.3	14.6	35.8	0.2	18	0
E	5005.9	E	399875	6254345	9.3	10.8	84.0	98.5	14.6	35.8	1.1	7	52
F	5104.7	S	402575	6254270	1.5	0.8	2.5	5.4	2.4	0.7	---	---	0
LINE 52780			FLIGHT 221										
A	6114.7	S?	391405	6254424	1.5	0.9	13.4	1.8	16.0	1.1	---	---	0
B	5967.7	S	394936	6254315	1.7	2.5	4.5	13.5	1.8	2.5	---	---	0
C	5930.9	B?	395811	6254288	6.0	11.5	24.0	38.4	2.2	8.5	0.6	0	0
D	5776.7	H	398661	6254189	4.7	9.1	81.8	123.6	3.8	32.3	0.5	21	14
E	5749.8	H	399642	6254165	11.8	9.4	81.4	49.4	31.2	31.9	1.8	22	27
F	5745.0	E	399793	6254158	8.7	5.7	81.1	21.1	29.5	30.8	2.1	12	0
LINE 52790			FLIGHT 221										
A	7751.4	S?	391539	6254277	0.8	1.1	4.9	4.9	3.3	2.0	---	---	1026
B	7915.7	E	395627	6254156	1.3	8.6	6.0	37.6	4.0	4.3	---	---	0
C	7923.1	B?	395753	6254152	0.2	10.2	8.3	29.7	2.0	4.4	---	---	0
D	8039.7	H	398456	6254075	6.7	10.1	105.8	202.6	7.5	45.2	0.7	20	0
E	8063.6	H	399462	6254061	11.0	5.5	85.8	36.7	27.6	35.9	3.2	0	0
F	8242.1	S	403649	6253903	0.9	0.0	3.3	2.3	1.3	1.3	---	---	0
LINE 52800			FLIGHT 226										
A	1745.0	S?	391594	6254102	3.5	0.9	8.1	2.9	8.9	1.0	---	---	0
B	1568.0	S	395679	6254018	1.3	6.9	4.3	30.0	0.4	3.4	---	---	0
C	1418.4	E	398118	6253903	11.1	19.4	99.5	170.5	1.1	38.0	0.7	0	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52800			FLIGHT 226										
D	1411.3	H	398383	6253893	3.0	13.4	103.4	171.6	13.9	38.7	0.2	0	0
E	1383.8	H	399459	6253877	1.5	1.7	32.7	19.0	6.5	13.1	---	---	0
F	1094.8	S?	406026	6253696	3.8	1.0	0.7	8.8	0.4	1.8	---	---	0
G	986.2	D	407974	6253652	3.8	1.6	14.4	7.8	5.3	8.8	---	---	124
H	905.6	H	409020	6253616	1.6	1.0	15.2	12.2	0.9	4.4	---	---	0
LINE 52810			FLIGHT 226										
A	2580.0	H	398246	6253775	8.3	11.4	74.4	111.6	14.8	30.1	0.9	7	0
B	2587.2	H	398540	6253781	2.7	7.2	50.3	111.6	7.2	30.1	0.3	5	0
C	3073.3	B?	407965	6253509	1.4	2.9	13.2	12.6	3.4	6.9	---	---	305
D	3126.8	H	408919	6253489	1.3	2.4	19.6	20.0	1.8	7.0	0.3	14	0
LINE 52820			FLIGHT 185										
A	3250.3	S	395004	6253717	2.0	2.1	3.2	4.9	0.9	1.9	---	---	0
B	3297.4	S	395715	6253690	2.0	7.1	8.6	21.7	8.4	4.2	---	---	0
C	3419.4	H	398152	6253637	11.0	24.6	104.8	199.3	19.2	47.6	0.6	0	0
D	3430.3	H	398468	6253633	9.1	12.2	69.6	139.9	11.7	27.9	0.9	9	0
E	3600.0	S?	401761	6253543	1.4	3.9	0.0	5.6	0.0	6.9	---	---	508
F	3748.2	S	404340	6253438	5.0	0.1	18.7	6.1	29.2	0.5	---	---	0
G	3760.8	S	404505	6253440	5.2	2.7	29.4	8.5	31.9	1.2	---	---	0
H	3798.0	S?	405035	6253473	7.0	3.8	23.8	10.4	34.3	2.1	2.4	45	0
I	3840.0	S?	405460	6253428	0.5	1.3	0.0	5.1	0.0	6.6	---	---	172
J	4082.0	S?	410164	6253302	2.8	4.6	0.7	11.3	1.6	2.4	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52830			FLIGHT 185										
A	2485.0	S	395605	6253549	1.1	8.1	6.9	32.7	5.1	4.9	---	---	0
B	2348.4	H	397764	6253480	1.1	2.9	4.3	12.4	2.3	2.2	---	---	0
C	2343.5	E	397914	6253477	13.4	20.6	74.7	120.7	3.0	29.2	0.9	0	41
D	2338.9	B	398078	6253472	11.9	11.8	74.7	120.7	18.5	29.2	1.4	7	0
E	2157.5	E	402153	6253342	13.6	16.0	68.5	100.2	3.2	21.4	1.2	3	0
F	2152.4	B	402247	6253343	12.9	11.1	98.2	100.2	9.7	21.4	1.7	18	0
G	2147.9	B	402332	6253347	9.4	5.8	98.2	75.7	9.7	37.7	2.3	48	0
H	2015.7	S?	404393	6253300	4.8	5.5	16.1	14.9	18.8	2.8	---	---	143
I	1665.3	S?	408859	6253182	2.9	3.8	21.1	26.8	1.3	7.9	0.6	11	191
J	1612.0	S?	410478	6253137	0.7	3.8	6.4	43.5	1.4	7.6	---	---	83
LINE 52840			FLIGHT 184										
A	8988.5	S?	395751	6253396	0.9	6.1	3.4	21.7	3.8	3.6	---	---	0
B	9099.3	S?	397873	6253326	12.5	18.6	97.1	182.1	4.5	41.6	0.9	8	0
C	9107.7	H	398091	6253334	0.0	0.1	27.1	75.0	18.1	30.2	0.4	270	0
D	9114.7	H	398281	6253334	8.9	16.5	52.6	117.2	14.1	23.4	0.7	0	0
E	9166.5	S?	399393	6253272	3.7	2.9	8.0	9.8	2.4	1.5	---	---	0
F	9323.2	H	402243	6253211	3.9	4.0	19.1	14.8	3.5	7.2	---	---	0
LINE 52842			FLIGHT 185										
A	1133.0	S?	407339	6253083	1.0	1.5	4.8	5.1	2.9	1.4	---	---	0
B	1228.0	S?	408892	6253069	2.1	2.7	10.5	12.2	2.6	3.3	---	---	134
C	1301.0	S	410869	6252966	2.1	1.0	11.2	24.3	9.9	3.1	---	---	19

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52850			FLIGHT 184										
A	7389.1	H	397816	6253150	7.5	21.2	115.5	193.0	22.3	55.5	0.4	0	0
B	7142.5	S	403007	6253061	3.8	7.4	9.3	13.7	1.6	2.3	---	---	0
C	6904.7	S?	407292	6252938	4.8	7.2	27.9	36.8	2.0	9.6	0.6	14	0
D	6786.2	B?	408237	6252899	3.5	3.4	19.0	18.8	5.8	9.8	0.9	25	0
E	6741.9	S?	408841	6252886	6.5	5.8	39.5	67.2	0.5	16.7	1.3	24	0
F	6633.4	E	411669	6252787	4.9	0.2	21.5	0.0	26.6	0.4	---	---	0
LINE 52851			FLIGHT 184										
A	8618.0	S?	395642	6253247	0.8	1.0	4.6	10.6	2.7	1.8	---	---	0
LINE 52860			FLIGHT 226										
A	4210.5	S?	395616	6253110	2.2	2.4	4.9	11.4	0.9	1.7	---	---	0
B	4106.0	E	397552	6253017	7.5	10.9	8.6	15.0	1.1	5.1	0.8	0	32
C	4099.4	H	397792	6253011	5.0	12.2	82.7	103.8	20.3	31.5	0.4	0	0
D	4064.1	S?	399180	6252976	4.5	1.3	5.2	3.4	0.9	1.5	---	---	0
E	3941.5	B	402174	6252910	5.8	4.4	14.3	9.3	1.0	5.2	---	---	0
LINE 52870			FLIGHT 226										
A	4822.2	S	394505	6252943	2.3	1.1	5.9	5.2	1.0	0.8	---	---	0
B	4884.5	S?	395623	6252942	1.3	2.9	6.5	7.8	1.2	2.1	---	---	13
C	4973.0	E	397598	6252907	15.2	18.5	111.1	170.6	27.2	43.0	---	---	38
D	4977.1	H	397744	6252904	9.2	25.6	111.1	170.6	27.2	43.0	0.5	0	18
E	5024.5	S?	399137	6252862	1.2	1.1	4.4	3.8	1.5	0.9	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52870			FLIGHT 226										
F	5087.7	S	400440	6252841	1.6	1.8	3.4	1.8	0.8	0.9	---	---	0
G	5167.8	D	401987	6252771	10.0	6.4	36.5	21.3	5.0	13.6	2.2	12	0
LINE 52880			FLIGHT 226										
A	5498.1	S?	395971	6252789	1.4	3.4	6.1	12.2	0.9	2.2	---	---	0
B	5416.7	E	397486	6252724	10.7	26.3	130.4	225.0	31.5	54.8	---	---	25
C	5413.0	H	397615	6252720	5.8	16.9	112.1	205.0	31.5	52.7	0.4	4	21
D	5398.9	H	398098	6252718	4.2	6.4	44.9	47.2	19.6	16.4	0.6	26	0
E	5371.1	S?	398922	6252701	2.8	1.5	4.1	7.5	0.6	1.1	---	---	0
F	5262.0	E	401372	6252641	1.9	1.1	32.0	3.9	32.0	1.2	---	---	0
G	5247.7	S?	401668	6252618	3.4	7.1	21.8	16.8	46.0	3.6	---	---	0
H	5239.0	D	401881	6252616	6.2	4.0	11.1	8.4	8.5	3.6	1.9	8	0
LINE 52890			FLIGHT 226										
A	6269.0	S?	394433	6252689	0.6	0.7	2.0	6.1	2.7	0.9	---	---	0
B	6368.0	S?	396195	6252637	0.4	1.2	4.4	4.2	1.9	1.3	---	---	0
C	6427.6	H	397523	6252598	8.1	24.1	116.3	207.5	32.6	49.0	0.4	0	17
D	6441.4	H	398011	6252597	5.5	7.9	39.9	31.8	19.4	18.4	0.7	0	10
E	6559.0	S	400920	6252509	1.2	0.9	2.3	5.4	1.7	1.2	---	---	0
F	6587.0	S?	401300	6252491	2.2	1.4	13.0	6.5	15.0	1.0	---	---	0
G	6603.1	B?	401588	6252479	12.0	9.5	69.9	35.7	26.1	14.5	1.8	0	0
LINE 52900			FLIGHT 226										
A	7062.3	S?	392817	6252552	1.1	0.3	2.1	4.0	0.9	0.8	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52900			FLIGHT 226										
B	7020.0	S	394294	6252515	0.4	1.2	3.6	3.4	2.6	1.2	---	---	0
C	6928.1	S?	396135	6252484	1.2	1.6	7.2	14.9	0.7	2.9	---	---	0
D	6854.9	H	397625	6252414	1.9	4.7	74.4	128.9	21.1	26.9	0.3	17	12
E	6703.4	D	401553	6252315	14.6	6.8	78.4	39.6	19.2	25.5	3.8	1	0
F	6698.9	D	401661	6252316	13.1	11.5	78.4	39.6	19.2	25.5	1.6	0	0
LINE 52910			FLIGHT 226										
A	7384.7	S?	392636	6252428	0.9	1.1	2.4	5.9	1.6	1.1	---	---	0
B	7445.7	S	394359	6252368	0.9	0.9	3.1	4.5	2.3	0.6	---	---	0
C	7530.7	H	396210	6252336	1.4	1.2	7.3	10.4	0.3	1.9	---	---	0
D	7589.4	H	397597	6252299	1.6	6.3	110.1	134.4	22.1	39.6	0.2	4	0
E	7623.2	S	398553	6252276	1.3	2.5	4.7	9.3	2.4	1.6	---	---	0
F	7776.6	B	401592	6252185	4.5	2.9	17.3	10.7	4.9	3.1	1.7	23	0
LINE 52920			FLIGHT 226										
A	8363.5	S?	392413	6252260	0.5	0.6	4.0	8.9	0.8	1.5	---	---	0
B	8190.3	S?	396195	6252194	1.1	1.7	5.6	3.3	1.1	1.2	---	---	0
C	8134.9	H	397370	6252124	3.7	11.4	81.9	133.3	18.1	31.2	0.3	1	0
D	7973.3	S?	401517	6252028	1.1	0.5	4.0	4.3	2.4	1.4	---	---	0
LINE 52930			FLIGHT 226										
A	8654.0	S	392315	6252137	2.0	1.0	4.7	7.3	1.3	1.8	---	---	0
B	8759.0	S	394451	6252059	0.4	0.7	3.3	6.1	0.6	0.7	---	---	0
C	8835.5	S?	395867	6252056	0.6	0.1	4.8	5.3	2.0	1.9	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52930			FLIGHT 226										
D	8890.7	H	397286	6252003	3.9	6.5	53.2	60.5	17.5	19.3	0.5	21	0
E	8894.7	E	397428	6252004	8.0	7.6	53.2	60.5	17.5	19.3	1.3	0	0
F	8933.7	S?	398421	6251977	3.5	0.0	4.5	6.8	1.9	1.4	---	---	0
G	9030.0	S	400770	6251906	1.2	1.0	3.4	4.6	2.7	1.3	---	---	0
LINE 52940			FLIGHT 227										
A	1401.7	S	394428	6251930	4.6	1.6	4.5	5.7	1.3	1.4	---	---	0
B	1322.0	S	395896	6251887	0.7	1.3	4.5	17.0	1.1	3.2	---	---	0
C	1270.1	H	397162	6251839	0.4	0.3	20.0	5.6	8.7	5.7	---	---	214
D	1266.0	S	397291	6251832	3.6	0.7	20.0	9.9	8.7	8.3	8.7	65	0
E	1206.2	S?	398411	6251819	4.2	1.5	4.9	5.2	1.2	1.6	---	---	0
LINE 52950			FLIGHT 227										
A	1486.0	S	394414	6251768	0.6	0.3	3.3	5.9	1.5	1.7	---	---	0
B	1567.1	S?	395797	6251752	1.1	1.9	4.0	4.6	1.2	1.8	---	---	0
C	1606.2	H	397035	6251706	0.9	1.3	9.3	6.7	7.9	4.5	---	---	338
D	1660.7	S?	398383	6251680	1.6	0.9	7.1	8.0	0.7	2.4	---	---	0
LINE 52960			FLIGHT 227										
A	2263.7	H	397005	6251548	0.6	1.1	4.5	0.8	7.4	1.5	---	---	285
B	2256.8	E	397224	6251539	2.4	1.1	17.2	7.4	9.2	7.0	2.3	73	711
C	2190.2	S?	398526	6251510	2.2	1.2	8.4	9.6	0.8	2.1	---	---	0
D	2115.1	H	400183	6251471	3.7	3.3	8.6	15.1	1.3	4.1	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 52970			FLIGHT 227										
A	2564.2	H	396903	6251428	1.7	1.7	5.5	2.0	8.9	1.7	---	---	171
B	2623.1	H	398514	6251365	2.3	2.1	12.1	16.3	2.7	3.7	---	---	0
C	2697.7	S?	400064	6251325	0.5	1.0	4.1	8.3	1.5	1.7	---	---	0
LINE 52980			FLIGHT 227										
A	3096.0	H	396725	6251264	0.0	0.4	4.8	2.8	3.7	0.0	---	---	69
B	3082.2	E	397173	6251254	4.0	1.3	16.3	7.3	3.6	5.1	---	---	0
LINE 52990			FLIGHT 227										
A	3565.1	H	396577	6251131	0.2	0.4	3.3	1.5	5.0	0.9	---	---	0
LINE 53000			FLIGHT 227										
A	4151.0	S	394474	6251020	0.6	1.6	1.8	5.9	1.7	1.2	---	---	0
B	4089.0	H	396547	6250969	1.8	0.0	5.5	3.7	1.9	3.0	---	---	964
C	4031.3	S?	397903	6250932	1.4	1.8	10.9	13.4	2.5	3.8	---	---	0
LINE 53010			FLIGHT 227										
A	4249.7	S	394518	6250885	1.1	1.2	0.4	2.3	1.7	0.6	---	---	0
B	4303.7	H	396558	6250806	0.5	2.2	7.6	6.9	0.2	1.8	---	---	0
C	4345.8	B?	397813	6250787	0.1	5.1	18.4	21.8	2.6	7.1	0.1	0	0
LINE 53020			FLIGHT 227										
A	4835.7	H	396543	6250651	3.1	3.3	10.1	11.9	2.8	3.6	---	---	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 53020			FLIGHT 227										
B	4787.2	B?	397673	6250639	2.3	1.8	4.7	0.0	4.7	2.3	---	---	0
C	4734.1	H	399169	6250588	1.5	0.6	5.0	8.2	1.1	2.4	---	---	0
D	4613.8	H	401911	6250535	1.8	1.7	23.7	1.2	25.8	1.1	---	---	0
LINE 53030			FLIGHT 227										
A	5060.0	H	396524	6250521	1.2	1.5	12.4	13.7	2.6	5.3	---	---	0
B	5102.6	D	397657	6250495	7.4	3.2	23.1	28.7	13.5	11.9	3.3	17	0
C	5165.2	S	399221	6250468	0.9	3.5	12.5	16.6	3.5	3.1	---	---	0
LINE 53040			FLIGHT 233										
A	6324.7	H	397638	6250330	4.1	2.9	7.4	2.6	3.3	2.1	---	---	0
B	6268.0	H	398932	6250278	1.2	3.6	14.3	21.4	1.2	4.3	---	---	18
LINE 53050			FLIGHT 233										
A	6900.7	H	397244	6250215	2.1	0.5	5.1	0.0	3.4	2.4	---	---	0
LINE 53060			FLIGHT 234										
A	1630.0	S?	392975	6250170	0.9	1.3	33.1	11.9	37.3	1.9	---	---	118
B	1586.6	S?	393376	6250140	1.5	1.6	3.1	11.5	0.4	1.5	---	---	0
C	1460.5	H	396719	6250082	1.1	2.1	3.3	7.1	2.0	1.7	---	---	0
D	1370.0	H	398471	6250021	1.2	1.1	5.1	15.8	1.1	2.1	---	---	21
LINE 53070			FLIGHT 234										
A	1925.5	H	396244	6249934	4.3	1.5	13.9	4.2	4.3	6.3	---	---	1067

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 53070			FLIGHT 234										
B	2056.1	S?	399533	6249836	1.5	0.9	6.5	0.5	5.6	0.9	---	---	0
C	2169.5	S?	401421	6249787	3.4	0.5	3.0	6.1	3.3	2.1	---	---	0
D	2183.4	S?	401634	6249777	4.3	0.4	90.6	6.2	100.6	1.6	---	---	0
LINE 53080			FLIGHT 234										
A	2701.2	H	396215	6249785	1.4	0.0	20.1	2.8	19.2	9.3	507.3	99	586
B	2568.2	S	399681	6249694	3.0	1.6	4.8	3.1	4.8	1.4	---	---	0
C	2460.3	S?	401568	6249610	4.6	1.1	12.6	0.2	13.0	0.4	---	---	0
D	2434.5	S?	401856	6249600	9.9	1.8	10.6	0.9	7.5	0.5	---	---	40
E	2419.0	S?	402007	6249596	2.4	2.2	22.0	4.4	8.2	0.7	---	---	0
LINE 53090			FLIGHT 234										
A	3129.8	H	396109	6249649	4.7	0.2	42.2	0.4	35.8	10.1	85.2	61	611
LINE 53100			FLIGHT 234										
A	3891.0	H	396226	6249483	7.2	1.2	38.9	0.0	39.4	8.0	12.6	38	0
B	3794.0	S	398144	6249411	1.4	4.0	31.1	66.1	8.3	10.3	---	---	0
C	3774.0	S	398854	6249408	1.6	1.2	7.0	12.3	2.4	3.4	---	---	0
LINE 53110			FLIGHT 234										
A	4434.9	H	395953	6249357	2.4	0.6	20.6	0.0	25.2	6.5	5.2	46	0
B	4518.6	S	398086	6249293	2.0	2.3	62.9	72.9	9.6	16.3	0.7	43	0

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LINE 53120			FLIGHT 234										
A	5252.7	H	395878	6249194	3.3	2.1	37.0	14.3	32.9	10.8	1.6	40	443
B	5244.3	E	396168	6249168	5.5	0.7	28.0	1.9	25.9	7.6	---	---	944
C	5154.1	S	397755	6249147	1.5	2.2	9.1	17.3	3.7	2.7	---	---	13
LINE 53130			FLIGHT 234										
A	5385.2	H	395877	6249041	2.9	1.5	38.0	8.5	36.3	11.4	1.8	38	10
B	5412.2	S	396506	6249015	0.2	1.2	4.8	5.5	1.5	1.2	---	---	0
LINE 53140			FLIGHT 234										
A	6150.7	E	395718	6248887	6.2	0.8	38.5	12.7	32.0	13.2	---	---	396
B	6146.3	H	395853	6248882	5.8	1.1	38.5	12.7	32.0	13.2	10.7	25	364
LINE 53150			FLIGHT 234										
A	6300.8	E	395720	6248739	4.8	1.2	39.0	13.8	30.6	13.4	6.3	35	492
B	6303.8	H	395815	6248731	2.2	0.0	39.0	1.9	30.6	13.4	588.1	40	0
LINE 53160			FLIGHT 234										
A	7085.1	H	395781	6248597	4.9	1.1	46.6	9.6	35.1	15.6	7.1	34	0
B	6796.4	B?	400140	6248455	5.4	1.9	20.9	3.8	17.3	3.8	4.1	24	0
LINE 53170			FLIGHT 234										
A	7222.3	H	395723	6248453	7.1	2.4	92.0	20.6	73.4	31.1	4.8	8	0
B	7329.0	S?	398074	6248380	2.7	0.3	20.5	0.4	22.4	0.5	---	---	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 53170			FLIGHT 234										
C	7423.2	B?	400133	6248322	5.6	2.2	19.6	3.1	19.8	3.7	---	---	0
LINE 53180			FLIGHT 234										
A	8010.2	H	395821	6248292	4.0	2.1	64.6	14.5	56.3	19.4	2.1	2	0
B	8005.7	E	395942	6248280	13.4	1.7	64.6	14.5	56.3	19.4	---	---	0
C	7845.0	S?	398417	6248228	0.0	1.8	0.0	6.5	0.0	1.2	---	---	50
D	7727.9	B	400192	6248165	5.8	2.8	16.7	7.7	7.8	4.9	2.6	32	0
LINE 53190			FLIGHT 234										
A	8174.4	H	395785	6248145	7.4	2.0	60.7	5.3	53.3	16.8	6.4	27	510
B	8178.0	E	395905	6248146	8.5	0.5	60.7	5.3	53.3	16.8	---	---	0
C	8306.2	S?	398337	6248071	0.0	2.1	0.3	7.6	0.0	1.5	---	---	0
LINE 53200			FLIGHT 234										
A	8886.5	H	395736	6247972	5.2	1.8	41.2	0.3	36.1	9.7	3.9	14	32
B	8725.1	S?	398538	6247911	2.3	2.9	22.1	7.4	58.4	1.5	---	---	0
LINE 53210			FLIGHT 234										
A	9045.9	H	395680	6247868	9.2	2.1	55.0	4.1	44.8	15.0	8.9	14	0
B	9108.3	S?	396940	6247808	0.0	1.1	0.0	5.7	0.0	1.4	---	---	391
C	9138.7	S?	397606	6247798	0.1	1.1	3.5	11.3	4.9	1.3	---	---	0
LINE 53220			FLIGHT 236										
A	836.0	H	395674	6247696	4.8	1.6	7.4	1.2	3.7	2.2	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 53220			FLIGHT 236										
B	652.4	S?	399203	6247585	6.3	2.7	30.9	9.8	34.9	1.5	---	---	0
C	625.5	S?	399728	6247584	24.1	1.7	129.4	10.7	145.9	3.7	---	---	0
D	616.0	S?	399922	6247573	20.6	0.8	103.4	15.7	117.5	4.4	---	---	0
E	587.4	B?	400541	6247533	3.8	4.4	20.8	28.7	4.2	5.8	---	---	0
F	537.8	S?	401116	6247553	6.3	0.8	45.1	1.3	64.8	0.7	---	---	0
G	523.3	S?	401209	6247544	1.4	0.9	6.4	7.5	8.6	1.9	---	---	0
LINE 53230			FLIGHT 236										
A	1099.1	S?	395590	6247551	6.8	1.1	19.2	8.6	5.1	6.1	13.3	0	0
B	1175.1	S?	396842	6247497	3.1	0.7	16.0	1.4	18.3	0.2	---	---	0
C	1225.5	S?	397840	6247480	1.5	0.6	14.6	3.6	17.0	0.3	2.2	103	0
D	1352.0	S?	400616	6247418	1.4	1.7	6.7	3.0	7.6	1.0	---	---	0
LINE 53240			FLIGHT 236										
A	1875.2	S?	395553	6247401	4.3	1.6	7.1	6.2	2.4	2.6	---	---	0
B	1582.8	D	400625	6247272	53.8	38.8	230.2	139.4	64.4	94.3	3.3	1	0
C	1580.7	D	400666	6247272	53.8	38.8	230.2	139.4	64.4	94.3	3.3	0	0
LINE 53250			FLIGHT 236										
A	2022.2	S?	395488	6247249	3.1	2.0	5.0	6.8	0.1	1.7	---	---	0
B	2312.4	E	400778	6247127	10.5	4.0	44.3	21.0	25.2	13.3	4.4	36	0
C	2316.4	D	400823	6247123	5.7	3.7	47.7	7.5	26.7	16.3	1.8	40	0
D	2323.9	D	400906	6247120	11.5	5.0	47.7	16.3	26.7	16.3	3.8	24	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 53260			FLIGHT 236										
A	2728.2	S	399389	6246982	2.2	0.5	19.7	5.7	23.9	1.3	---	---	0
B	2704.0	S?	399932	6246972	1.1	1.4	11.4	5.5	22.4	1.0	---	---	0
C	2659.7	B	400866	6246948	4.0	2.4	25.3	8.8	18.2	7.2	1.8	49	0
LINE 53270			FLIGHT 236										
A	3386.0	S?	399834	6246838	4.4	5.3	30.8	3.0	31.8	1.1	0.8	0	0
B	3412.2	S	400431	6246811	5.4	1.6	23.2	4.4	27.6	1.3	---	---	0
C	3433.1	S	400797	6246811	3.9	2.6	31.2	17.5	31.8	2.3	---	---	0
D	3446.0	S?	400968	6246811	12.5	1.5	7.1	27.1	10.3	4.9	---	---	0
LINE 53280			FLIGHT 236										
A	3807.0	S?	397539	6246726	0.0	1.8	0.0	20.2	0.0	6.3	---	---	0
B	3771.9	S?	397986	6246730	4.0	1.0	13.5	7.4	15.0	1.5	---	---	0
C	3686.2	S	399758	6246683	1.5	2.8	12.8	9.5	9.6	1.2	---	---	0
D	3671.2	S?	400169	6246660	4.8	21.4	34.6	171.1	27.4	23.8	---	---	0
E	3664.4	S?	400342	6246670	3.5	14.9	18.1	107.2	11.8	13.8	---	---	0
F	3648.5	S?	400656	6246659	0.2	0.0	0.1	22.1	0.0	3.8	---	---	0
LINE 53290			FLIGHT 236										
A	4237.3	H	396100	6246629	1.2	0.4	11.3	7.4	0.5	1.8	---	---	0
B	4390.0	S?	399161	6246547	0.0	0.2	11.5	17.7	5.7	2.9	---	---	0
C	4402.9	S?	399419	6246538	1.3	3.0	24.8	27.1	49.2	3.8	0.3	17	0
D	4415.7	S?	399623	6246544	6.3	7.6	32.2	50.0	53.6	6.6	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 53290			FLIGHT 236										
E	4424.0	S	399806	6246526	4.1	1.2	48.6	0.0	56.8	1.9	4.9	24	0
F	4444.0	S?	400104	6246523	0.0	2.9	12.4	18.2	15.8	3.6	---	---	0
G	4485.4	S?	400683	6246521	34.7	3.8	139.0	22.0	166.0	4.7	---	---	0
H	4512.3	S?	400991	6246517	10.6	1.3	6.0	27.3	9.4	4.2	---	---	0
LINE 53300			FLIGHT 236										
A	4950.0	S?	396463	6246472	1.6	1.3	5.1	8.0	2.8	2.0	---	---	0
B	4924.3	S?	396825	6246456	13.9	0.4	1.0	11.2	6.5	2.3	---	---	0
C	4851.0	S?	398482	6246418	1.5	1.0	7.9	2.4	7.6	0.2	---	---	0
D	4823.4	S?	399072	6246400	1.3	2.7	11.7	15.9	6.2	2.1	---	---	0
LINE 53310			FLIGHT 236										
A	5350.0	S	398887	6246263	2.3	4.4	7.3	19.6	3.1	3.5	---	---	0
B	5452.2	S?	400524	6246225	3.1	2.6	21.5	8.4	23.6	2.1	---	---	0
LINE 53320			FLIGHT 181										
A	8646.6	S	398528	6246121	1.0	2.2	8.4	14.8	9.5	1.7	---	---	0
LINE 53330			FLIGHT 181										
A	8260.0	S	398426	6245965	0.0	1.1	7.8	1.6	2.2	1.0	---	---	0
LINE 53340			FLIGHT 181										
A	7806.1	S	396358	6245861	1.2	2.0	3.1	18.3	1.1	3.0	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 62860			FLIGHT 226										
A	3752.6	S?	407209	6252776	0.0	0.9	13.9	30.6	0.3	4.7	---	---	17
B	3635.8	S?	408721	6252742	1.8	3.9	39.1	36.2	3.0	12.2	0.3	3	0
LINE 62870			FLIGHT 226										
A	9248.7	S	406562	6252650	2.1	2.0	3.4	15.8	3.2	2.6	---	---	29
B	9280.0	S	407187	6252636	0.4	1.9	5.6	12.1	0.9	2.0	---	---	18
C	9360.4	H	408744	6252606	3.4	3.3	40.9	39.9	4.9	13.7	0.9	22	0
LINE 63100			FLIGHT 225										
A	9865.5	S?	407324	6249170	1.5	10.8	18.6	57.8	1.4	10.1	0.1	0	251
B	9992.7	S	409525	6249132	3.9	2.5	9.7	22.1	0.1	4.4	---	---	0
C	10076.7	S?	411045	6249083	4.5	7.8	8.8	28.7	2.7	4.6	---	---	0
D	10174.6	D	412956	6249020	5.3	16.9	14.4	48.6	2.7	7.7	0.4	5	22
LINE 63110			FLIGHT 225										
A	9490.7	S	407335	6249033	2.4	5.4	12.2	22.2	1.0	4.9	---	---	161
B	9363.2	S	409658	6248963	2.8	2.2	6.8	10.9	1.4	2.7	---	---	63
C	9296.9	B?	411068	6248945	5.1	9.3	13.7	30.6	2.7	5.6	0.6	3	0
LINE 63120			FLIGHT 225										
A	8834.7	S?	407316	6248889	4.1	8.0	12.9	33.6	1.1	6.3	0.5	0	104
B	8969.7	S	409709	6248822	4.9	1.7	7.8	11.1	0.5	2.5	---	---	0
C	9047.7	S?	411143	6248778	3.6	4.4	12.5	28.9	5.0	5.4	0.7	35	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 63120			FLIGHT 225										
D	9151.3	H	412976	6248712	1.8	2.3	11.3	9.9	2.3	2.6	---	---	0
LINE 63130			FLIGHT 225										
A	8314.2	S	407282	6248730	3.1	2.4	8.4	7.2	1.5	1.7	---	---	37
B	8180.7	S?	409847	6248666	2.2	1.1	10.0	10.9	2.6	2.3	---	---	108
C	8115.1	S?	411272	6248608	2.9	2.9	4.1	8.2	0.8	1.6	---	---	0
D	8036.0	H	412986	6248567	0.5	1.2	7.2	4.7	1.2	2.6	---	---	0
LINE 63140			FLIGHT 225										
A	7536.3	S	405051	6248637	1.7	1.5	49.1	8.3	66.3	1.5	---	---	0
B	7817.7	S	409886	6248529	2.0	1.5	8.3	10.0	1.4	2.4	---	---	0
C	7889.7	S?	411442	6248459	0.6	0.9	4.8	9.5	2.1	1.8	---	---	0
D	7967.5	H	413033	6248426	0.9	4.7	14.5	6.4	4.0	4.0	---	---	0
LINE 63150			FLIGHT 225										
A	7150.6	S?	405145	6248478	7.1	0.7	36.8	3.6	40.0	1.4	---	---	413
B	7005.2	S?	407186	6248425	2.8	2.0	7.7	6.3	1.4	1.7	---	---	0
C	6845.9	S?	409977	6248357	3.0	2.1	14.6	19.2	0.6	4.0	1.4	36	116
D	6774.0	S?	411499	6248311	3.0	2.0	10.2	18.5	5.2	2.7	---	---	0
E	6691.1	H	413073	6248268	0.6	5.8	16.0	32.6	2.2	6.1	---	---	0
LINE 63160			FLIGHT 225										
A	6075.3	S	404577	6248364	3.1	1.2	19.1	7.0	19.0	1.8	---	---	0
B	6093.0	S?	405042	6248346	0.0	3.9	6.5	14.6	0.0	2.2	---	---	1348

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CX 7200 HZ Real ppm	CX 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 63160		FLIGHT 225											
C	6351.1	S	410006	6248222	2.7	1.3	8.1	7.4	0.6	2.6	---	---	0
D	6412.0	S	411490	6248156	1.6	1.7	7.0	10.2	2.9	3.1	---	---	0
E	6488.3	H	413057	6248106	4.2	7.5	51.1	52.4	11.6	16.1	0.5	2	0
LINE 63170		FLIGHT 225											
A	6012.7	S?	404896	6248183	0.1	3.2	3.6	11.4	0.0	2.1	---	---	0
B	5970.2	S	406021	6248164	1.8	0.3	8.2	2.8	8.6	0.7	---	---	0
C	5881.1	S	407131	6248135	4.2	0.8	7.4	6.3	0.6	2.0	---	---	13
D	5703.6	S?	410018	6248071	4.4	4.0	28.3	26.8	3.8	6.3	1.1	35	0
E	5631.6	S?	411612	6248015	2.5	2.1	11.8	12.5	2.5	3.5	---	---	0
F	5560.6	B?	413230	6247966	3.2	4.3	28.2	50.1	7.1	11.5	---	---	0
G	5454.0	S?	415341	6247891	14.8	3.4	64.7	14.9	71.9	1.8	---	---	785
H	5396.2	S	416900	6247839	2.4	1.9	4.2	5.0	3.4	1.4	---	---	0

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LINE 49121			FLIGHT 70										
A	4787.4	H?	391704	6271608	1.0	4.2	9.5	25.6	0.0	8.3	---	---	111
LINE 49132			FLIGHT 70										
A	5068.7	S	393220	6272532	0.7	3.7	1.5	18.6	1.3	3.2	---	---	0
B	5042.4	S	393205	6272092	1.2	7.6	12.7	39.5	1.3	7.5	0.1	0	0
LINE 49141			FLIGHT 70										
A	5762.0	S	394698	6270771	1.8	2.7	14.9	37.4	0.8	8.2	0.5	23	0
LINE 51320			FLIGHT 66										
A	1048.4	H	387416	6276442	4.1	3.6	22.0	29.7	4.8	8.3	---	---	0
LINE 51330			FLIGHT 66										
A	1472.0	H	387271	6276267	2.6	2.3	13.0	13.2	1.4	3.9	---	---	0
LINE 51340			FLIGHT 66										
A	1560.1	H	387451	6276121	4.2	4.0	32.6	18.5	4.7	9.8	---	---	0
LINE 51350			FLIGHT 66										
A	2009.0	H	387368	6275984	2.8	1.1	19.8	13.2	2.5	7.7	---	---	0
LINE 51360			FLIGHT 66										
A	2111.4	H	387441	6275818	0.8	2.1	24.6	16.9	1.8	8.7	---	---	0
LINE 51370			FLIGHT 66										
A	2521.0	H	387479	6275676	0.6	2.0	17.5	14.2	0.2	5.9	---	---	0
B	2373.6	B?	390231	6275566	0.0	10.8	124.8	42.1	170.4	5.1	---	---	341
LINE 51380			FLIGHT 66										
A	2813.3	H	387619	6275526	3.4	5.2	17.7	24.7	1.3	6.0	0.6	16	0
B	3002.0	S?	390332	6275455	4.6	0.6	30.3	2.2	36.6	0.8	---	---	0
LINE 51390			FLIGHT 66										
A	3132.0	S?	389099	6275294	1.8	0.6	9.6	3.5	11.1	1.0	---	---	0
LINE 51420			FLIGHT 66										
A	4023.9	H	387294	6274938	1.1	2.6	9.1	14.5	2.6	3.7	---	---	0

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LINE 51420			FLIGHT 66										
B	4166.6	S?	390279	6274841	0.0	5.7	11.5	21.1	12.5	4.4	---	---	0
LINE 51470			FLIGHT 72										
A	5757.2	H?	392731	6273987	11.7	0.8	6.1	4.8	9.5	0.7	---	---	516
LINE 51480			FLIGHT 72										
A	5189.9	S	389702	6273944	1.7	2.2	0.2	28.1	0.1	4.8	---	---	0
LINE 51490			FLIGHT 72										
A	4466.0	S	386951	6273886	1.0	1.9	4.8	22.4	0.5	4.0	---	---	28
B	4520.7	S?	388295	6273874	0.0	6.2	21.3	17.1	26.6	3.2	---	---	124
LINE 51500			FLIGHT 72										
A	4259.0	H	386977	6273752	0.6	4.5	7.0	33.9	0.2	5.6	---	---	24
LINE 51510			FLIGHT 72										
A	3588.0	S?	390538	6273495	0.0	3.5	0.0	35.9	6.6	6.3	---	---	0
LINE 51520			FLIGHT 72										
A	3178.0	S?	390558	6273340	0.2	5.6	10.2	39.7	0.0	8.9	---	---	0
LINE 51530			FLIGHT 72										
A	2527.9	S?	387518	6273278	0.0	2.5	6.8	17.1	9.0	2.6	---	---	95
B	2686.0	H	390697	6273188	3.0	2.1	14.5	10.5	2.3	5.1	---	---	774
LINE 51540			FLIGHT 72										
A	2100.0	H	390877	6273018	0.9	0.5	18.9	6.1	0.9	5.6	---	---	888
LINE 51550			FLIGHT 72										
A	1449.0	B?	388418	6272940	0.0	0.6	72.2	11.2	317.7	1.4	---	---	381
B	1462.0	B?	388626	6272905	26.7	0.1	272.3	10.5	354.3	0.5	---	---	144
C	1579.2	H	390962	6272873	2.8	3.2	24.9	19.8	0.8	9.5	---	---	1068
LINE 51560			FLIGHT 72										
A	1261.8	S?	387453	6272802	3.8	4.0	43.8	16.6	56.3	2.8	---	---	0
B	1036.4	H	391069	6272716	3.0	1.4	23.0	22.8	0.5	8.8	---	---	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 51571			FLIGHT 71										
A	2053.6	S	395282	6272509	1.4	2.7	2.3	21.3	0.5	3.3	---	---	0
B	1867.7	S	399614	6272354	1.0	5.9	6.2	42.6	3.2	7.5	---	---	13
LINE 51580			FLIGHT 65										
A	2468.5	S	393709	6272356	1.4	3.6	1.5	21.8	0.8	3.1	---	---	0
B	2526.5	S?	394591	6272320	0.9	7.4	1.3	37.0	0.4	6.3	---	---	11
LINE 51581			FLIGHT 71										
A	2831.8	S	399241	6272200	2.8	6.2	5.0	32.7	0.6	6.1	---	---	0
LINE 51590			FLIGHT 71										
A	3273.6	H	391305	6272241	1.5	1.6	25.0	23.7	1.1	9.9	---	---	354
B	3113.5	S?	394633	6272149	1.3	1.6	4.2	13.3	1.3	2.0	---	---	0
LINE 51600			FLIGHT 71										
A	4152.7	H	391384	6272129	1.3	1.2	14.6	8.9	1.0	6.0	---	---	0
B	4191.4	S	392387	6272065	0.9	1.2	7.7	20.9	0.7	3.6	0.4	59	0
C	4234.1	S	393055	6272077	0.1	2.1	9.4	41.2	0.5	7.9	0.1	16	0
D	4263.0	S	393361	6272060	0.1	3.7	6.3	27.0	0.7	3.8	0.1	23	0
E	4271.0	S	393443	6272052	0.3	6.0	10.6	49.1	1.1	8.8	0.1	4	0
F	4499.6	S	398084	6271926	2.7	2.0	0.5	15.9	2.1	2.1	1.3	71	0
LINE 51610			FLIGHT 71										
A	4956.3	H	391495	6271953	2.4	3.2	28.4	32.5	3.5	14.6	0.6	30	110
B	4856.9	S	393568	6271911	1.9	6.0	11.2	47.3	0.9	9.0	---	---	0
C	4700.6	S	397336	6271788	1.3	2.5	7.1	23.7	0.4	4.5	---	---	0
D	4621.7	S	399658	6271731	2.9	7.7	18.3	46.8	1.9	10.6	0.3	0	0
LINE 51620			FLIGHT 71										
A	5471.6	S	386172	6271944	3.6	6.8	9.4	46.3	0.5	8.7	0.5	10	0
B	5810.6	H	391687	6271803	2.2	2.8	23.3	23.9	0.3	10.6	0.6	26	0
C	5868.2	S?	393010	6271759	1.1	2.5	6.0	16.7	1.1	4.2	0.3	32	0
D	5923.6	S?	393712	6271777	1.4	2.7	7.2	41.2	0.0	7.7	0.4	41	14
E	5960.4	H	394567	6271701	1.4	4.3	4.4	30.0	0.2	5.2	0.2	30	0
F	5992.6	H	394963	6271724	1.7	1.3	1.3	22.4	0.5	3.6	1.0	74	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 51631			FLIGHT 70										
A	6607.9	H	391686	6271650	0.3	2.7	21.5	28.3	1.2	10.7	0.1	0	0
B	6430.1	S	395461	6271581	2.5	6.6	2.6	28.8	0.8	4.6	---	---	0
C	6275.0	S	399560	6271454	2.2	3.6	15.7	36.2	0.2	8.9	0.5	27	370
LINE 51641			FLIGHT 70										
A	2518.0	H	391797	6271493	1.9	2.8	19.2	19.8	0.0	9.2	---	---	0
B	2174.8	S	399435	6271291	2.9	6.7	11.5	56.0	0.3	10.5	0.4	13	643
LINE 52051			FLIGHT 38										
A	2774.6	S	392868	6265321	0.7	5.9	2.8	23.4	0.9	4.2	---	---	0
B	2800.7	S	393328	6265314	2.3	11.5	5.8	65.8	0.8	10.7	---	---	0
C	2844.3	H?	394110	6265297	5.0	4.6	9.2	16.3	0.6	4.5	1.2	9	0
D	2933.0	S	395249	6265251	1.3	2.7	13.3	37.0	1.3	7.1	---	---	0
E	2963.7	H?	395599	6265244	1.4	2.5	4.5	18.3	2.6	3.2	---	---	17
LINE 52061			FLIGHT 38										
A	3222.2	S	392985	6265171	2.3	5.6	3.7	46.1	0.1	7.9	0.4	27	0
B	3209.2	S	393102	6265163	2.3	5.4	0.8	14.8	2.8	3.1	0.4	29	0
C	3182.7	S	393440	6265155	2.2	8.7	7.4	46.2	2.3	7.5	0.2	5	0
D	3079.6	S	395135	6265110	3.8	8.3	7.4	35.1	5.6	5.9	---	---	26
LINE 52071			FLIGHT 38										
A	3473.9	B?	392223	6265042	5.3	6.8	32.0	6.6	10.4	14.8	0.8	32	0
B	3524.7	S	392906	6265015	2.5	7.9	4.9	33.7	0.8	6.8	---	---	0
C	3549.1	S	393332	6265014	1.8	8.7	3.8	38.0	1.5	7.4	---	---	0
D	3558.2	S	393506	6265008	1.7	6.2	0.4	26.3	1.9	4.3	---	---	0
E	3658.5	S	395032	6264959	2.1	8.0	11.1	36.1	7.4	6.5	---	---	0
F	3699.0	S	395414	6264961	2.3	3.1	5.3	17.4	5.5	5.6	---	---	0
LINE 52081			FLIGHT 38										
A	4101.9	D	392191	6264896	111.5	54.8	280.1	187.2	80.6	141.9	7.2	0	0
B	4000.3	S	392899	6264881	3.4	3.8	4.6	33.9	3.2	5.4	0.8	44	0
C	3949.8	S	393429	6264856	1.7	3.3	2.6	21.3	0.3	4.1	0.4	50	0
D	3936.2	S	393527	6264855	1.3	12.5	4.1	46.8	2.4	6.9	0.1	0	0
E	3904.4	S	393878	6264835	1.3	7.2	7.9	45.8	0.6	8.8	0.1	0	86
F	3834.3	S	394936	6264812	2.7	5.8	1.1	18.2	1.8	3.8	---	---	0
G	3805.1	S	395333	6264814	3.5	2.6	3.1	16.7	4.7	3.2	---	---	0

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LINE 52091			FLIGHT 38										
A	4173.0	D	392169	6264739	225.7	203.4	1153.2	780.3	510.3	575.1	4.3	0	0
B	4240.8	S	393111	6264711	3.3	9.1	2.8	25.9	1.3	4.2	0.4	6	0
C	4262.8	S	393531	6264705	4.1	12.7	1.9	26.4	0.4	4.8	0.3	0	0
D	4267.0	S	393603	6264704	3.4	7.4	3.8	26.5	1.7	4.8	0.4	17	0
E	4277.4	S	393805	6264701	4.2	10.4	7.6	40.7	1.7	7.5	0.4	3	88
F	4341.7	S	394873	6264662	1.2	4.6	2.2	31.4	1.2	5.7	0.2	14	10
G	4370.3	S	395281	6264654	3.3	6.7	6.4	54.2	3.7	9.5	0.5	26	0
H	4391.7	B?	395566	6264644	19.5	46.3	29.5	142.4	3.2	23.0	0.7	0	0
LINE 52101			FLIGHT 38										
A	4741.0	D	392185	6264610	178.5	97.7	428.3	245.6	101.4	199.2	7.3	0	0
B	4658.1	H	392939	6264566	2.7	4.3	5.8	25.7	1.2	5.6	0.5	42	0
C	4624.5	S	393334	6264559	2.8	10.3	6.7	28.0	3.1	4.6	0.3	6	23
D	4607.4	S	393531	6264552	0.5	6.5	1.3	13.1	4.5	2.5	0.1	6	0
E	4594.6	S	393758	6264554	2.9	12.9	7.4	69.6	3.9	11.6	0.2	0	118
F	4516.5	S	394805	6264512	4.3	6.4	2.1	17.8	1.1	2.9	0.7	24	0
G	4464.2	S	395505	6264503	41.4	41.3	49.7	54.5	2.4	21.1	2.2	0	48
H	4462.0	D	395532	6264501	41.4	41.3	120.8	54.5	2.3	40.3	2.2	0	0
LINE 52111			FLIGHT 38										
A	4796.2	D	392188	6264424	243.4	98.9	580.1	253.7	246.2	333.5	12.1	0	13
B	4842.9	S	392925	6264413	1.7	14.9	8.5	43.6	0.3	8.1	0.1	0	0
C	4883.7	S	393729	6264402	3.1	6.1	4.4	27.3	2.4	4.0	0.4	19	74
D	4955.9	S	394832	6264374	2.2	4.6	5.6	28.7	2.3	6.3	0.4	28	0
E	5010.8	D	395471	6264340	42.0	44.2	127.0	104.5	4.0	38.9	2.1	0	35
LINE 52121			FLIGHT 38										
A	5473.7	D	392215	6264309	31.0	24.3	56.0	54.8	5.6	22.5	2.6	11	0
B	5421.8	H	392765	6264277	3.5	2.4	21.9	24.6	2.2	6.3	1.5	61	0
C	5412.7	S?	392894	6264273	2.9	4.1	7.2	25.8	2.8	5.9	0.6	43	0
D	5379.8	S	393377	6264257	1.8	3.9	3.9	16.2	1.1	2.5	---	---	0
E	5365.8	S	393646	6264268	2.3	4.0	3.7	31.4	1.2	5.1	---	---	11
F	5337.4	S	394166	6264235	4.1	9.3	13.8	44.4	0.5	8.3	0.4	9	16
G	5289.5	S	394761	6264214	1.0	3.9	3.3	35.3	0.5	5.3	---	---	0
H	5265.9	S	395091	6264219	2.7	11.3	1.7	38.7	0.2	6.7	---	---	0
I	5226.2	D	395568	6264200	64.4	53.9	120.9	134.5	115.7	27.2	3.1	0	0

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LINE 52131		FLIGHT 38											
A	5566.1	S	392634	6264127	4.7	14.4	18.6	65.2	1.0	10.7	0.4	0	0
B	5605.8	S	393555	6264114	2.7	5.5	3.8	27.2	1.1	4.1	---	---	0
C	5652.5	S	394346	6264086	0.3	2.2	3.8	20.0	0.0	5.3	---	---	0
D	5695.0	S	394722	6264099	2.3	6.6	4.1	31.4	3.8	5.2	0.3	15	0
E	5717.5	S	394985	6264068	1.8	4.8	4.3	20.2	1.3	3.6	0.3	20	0
LINE 52141		FLIGHT 65											
A	3259.6	H?	392328	6264001	4.4	6.2	23.8	24.8	8.7	12.1	0.7	33	0
B	3186.1	S	393218	6263959	0.4	5.1	3.0	29.0	2.5	5.2	0.1	8	12
C	3176.7	S	393396	6263958	1.7	8.6	4.3	48.7	4.0	7.7	0.2	2	0
D	3059.3	S?	395486	6263900	1.3	5.3	3.6	28.8	0.5	4.1	0.2	2	0
LINE 52151		FLIGHT 52											
A	4254.9	D	392158	6263868	19.2	17.8	64.6	48.1	9.1	26.5	---	---	0
B	4265.4	D	392299	6263858	16.5	15.7	22.5	24.7	5.3	10.3	---	---	0
C	4293.8	S	392695	6263839	1.0	2.3	4.9	16.5	2.5	3.3	---	---	0
D	4340.6	S	393343	6263810	1.3	6.2	1.6	34.8	0.4	5.8	---	---	0
LINE 52161		FLIGHT 52											
A	4776.3	B	392322	6263693	12.8	14.3	35.6	32.9	14.0	18.4	---	---	0
B	4764.8	B?	392583	6263679	9.8	14.2	15.7	25.9	3.6	11.2	---	---	0
C	4713.7	S	393115	6263666	0.4	2.9	3.4	15.8	3.4	3.9	---	---	0
D	4691.2	S	393509	6263666	1.1	4.7	2.7	23.2	0.5	3.7	---	---	0
E	4655.6	S	393972	6263654	1.9	5.5	3.9	22.0	1.8	3.8	---	---	0
LINE 52171		FLIGHT 52											
A	4921.6	H	392622	6263535	5.2	9.8	21.8	21.5	4.7	8.4	---	---	0
B	4940.3	S	392874	6263521	2.5	4.1	10.6	33.3	1.0	6.6	---	---	18
C	4945.0	S	392945	6263523	4.8	11.4	3.5	33.3	1.5	6.6	---	---	0
D	4979.2	S	393468	6263496	0.5	12.3	0.3	38.4	0.5	7.2	---	---	29
LINE 52181		FLIGHT 52											
A	5667.0	B	392367	6263376	5.6	13.0	72.9	167.5	5.0	38.2	---	---	0
B	5659.8	B	392415	6263380	8.7	22.9	91.1	128.8	6.8	36.7	---	---	0
C	5635.0	B	392564	6263386	10.7	28.5	93.7	131.0	10.2	41.4	---	---	0
D	5620.9	H?	392650	6263381	8.0	10.9	42.3	42.6	8.2	18.4	---	---	0
E	5606.6	B	392740	6263382	4.7	5.3	28.8	37.7	6.2	13.7	---	---	0

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LINE 52181			FLIGHT 52										
F	5592.4	H?	392848	6263381	0.9	3.3	15.5	19.6	2.7	6.5	---	---	0
G	5575.7	S	393011	6263374	2.9	9.6	7.2	28.7	0.9	5.6	---	---	0
H	5524.6	S	393509	6263362	1.4	5.6	0.7	31.9	1.0	4.3	---	---	0
LINE 52191			FLIGHT 52										
A	5816.2	B	392175	6263225	109.1	244.6	492.3	514.8	62.2	225.7	1.3	0	13
B	5825.1	B	392291	6263236	0.0	44.2	115.3	201.4	17.6	53.3	---	---	0
C	5829.5	D	392346	6263243	24.5	40.6	115.3	201.4	17.6	53.3	---	---	0
D	5833.8	D	392400	6263244	19.2	22.2	35.2	28.2	2.5	12.7	---	---	0
E	5846.8	H?	392561	6263229	6.2	16.9	68.6	72.5	10.3	31.2	---	---	0
F	5878.4	S	392980	6263229	2.2	10.2	10.6	50.8	0.4	9.1	---	---	0
LINE 52201			FLIGHT 52										
A	6356.3	B	392287	6263086	18.5	26.5	164.7	195.8	10.2	62.5	---	---	44
B	6352.3	H	392333	6263086	17.8	34.9	164.7	195.8	10.2	62.5	---	---	0
C	6325.9	B	392557	6263081	20.4	27.6	134.9	161.0	16.8	64.8	---	---	0
D	6314.0	B	392656	6263075	13.2	21.8	98.3	144.1	14.1	49.1	---	---	0
E	6262.9	S	393149	6263064	0.7	4.9	12.7	33.8	2.0	9.4	---	---	0
F	6199.2	S?	393846	6263064	1.6	21.9	7.9	81.2	5.9	12.9	---	---	0
G	6157.7	S	394559	6263030	3.0	5.4	7.3	23.8	0.3	5.3	---	---	140
LINE 52211			FLIGHT 65										
A	2824.1	H	392220	6262904	2.1	1.5	17.3	16.8	6.4	12.8	1.2	69	0
B	2794.1	D	392353	6262903	5.6	22.2	106.4	152.5	3.3	36.5	0.3	0	29
C	2782.1	D	392431	6262898	14.0	4.3	88.0	152.5	1.9	34.8	7.0	17	15
D	2771.4	D	392497	6262907	12.8	9.6	99.9	110.4	10.8	40.1	2.1	4	0
E	2750.9	H	392666	6262917	1.4	2.2	10.4	22.2	3.5	5.4	0.5	43	0
F	2737.0	H	392749	6262919	3.4	1.6	26.6	67.3	1.8	14.8	2.5	58	0
G	2686.3	S	393055	6262911	1.8	7.1	6.6	49.1	0.8	8.2	0.2	6	0
H	2610.6	S	393496	6262904	0.4	3.4	3.7	27.3	4.6	4.7	0.1	10	21
I	2598.8	S	393658	6262897	1.3	8.6	4.7	29.9	4.2	4.0	0.1	4	0
J	2451.6	S?	396494	6262818	1.9	8.9	1.5	28.1	0.3	4.2	0.2	10	0
K	2420.9	S	397207	6262814	1.4	7.0	2.0	33.8	1.1	5.1	0.2	7	0
LINE 52771			FLIGHT 74										
A	7286.0	H?	408210	6254116	5.3	3.0	6.0	4.8	0.4	1.6	2.2	18	75
B	7241.6	H	409087	6254062	1.3	1.9	20.7	16.7	1.5	8.4	0.5	56	0

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LINE 52941			FLIGHT 42										
A	7722.7	H	392006	6251989	2.2	1.0	15.4	20.6	9.3	4.6	---	---	31
LINE 52951			FLIGHT 42										
A	6204.4	H	390238	6251894	8.2	7.8	26.8	60.9	14.9	12.7	---	---	146
B	6256.0	S?	391786	6251861	2.4	3.4	11.7	34.1	4.1	6.4	---	---	42
C	6265.4	E	392063	6251856	5.8	6.4	12.9	27.6	9.6	5.9	---	---	22
LINE 52961			FLIGHT 42										
A	6133.3	H	390386	6251740	2.9	5.5	33.3	42.5	19.5	9.9	---	---	0
B	6101.3	H	391250	6251710	2.3	6.1	13.9	59.1	23.3	10.0	---	---	0
LINE 52971			FLIGHT 42										
A	4593.9	S	390899	6251579	3.9	5.9	4.8	20.0	13.1	4.0	---	---	166
B	4729.3	H?	393200	6251503	18.5	1.7	0.0	5.2	0.0	0.5	---	---	342
LINE 52981			FLIGHT 42										
A	4426.6	S	390942	6251425	9.4	2.4	22.9	7.1	29.2	1.8	---	---	170
B	4300.2	H?	393087	6251361	6.4	0.9	38.5	1.5	55.9	3.0	---	---	100
C	4149.2	H	394167	6251342	3.2	3.3	6.3	14.4	6.4	2.4	---	---	2608
LINE 52991			FLIGHT 42										
A	3108.3	H	394198	6251194	1.4	2.4	11.3	17.3	7.6	4.1	---	---	0
LINE 62861			FLIGHT 43										
A	1029.6	E	407148	6252790	2.7	5.9	29.5	49.4	0.7	11.5	---	---	0
B	1013.1	B	407240	6252785	7.8	21.6	28.2	53.9	2.2	9.7	---	---	0
C	833.5	H	408747	6252752	7.3	11.5	56.8	84.4	8.7	24.6	---	---	0
D	712.2	S?	411245	6252667	5.1	5.3	14.3	38.8	22.2	6.2	---	---	32
E	688.6	S?	411845	6252664	0.0	6.7	0.7	27.8	6.1	5.1	---	---	0
LINE 62871			FLIGHT 43										
A	1347.4	S	406578	6252642	1.4	5.1	4.7	24.1	11.7	4.3	---	---	50
B	1385.3	S	407199	6252625	2.5	8.0	9.7	36.7	1.9	6.8	---	---	21
C	1477.5	H	408591	6252594	6.1	7.1	63.5	93.2	7.7	31.9	---	---	20
D	1483.5	B?	408758	6252591	5.0	11.3	63.5	93.2	3.1	31.9	---	---	0
E	1662.4	S?	411511	6252515	7.0	3.6	8.0	46.9	13.8	7.6	---	---	14
F	1676.0	S?	411847	6252505	0.0	5.6	28.3	23.4	34.3	3.1	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 62880			FLIGHT 43										
A	2201.7	S	406603	6252498	1.5	8.3	9.0	27.8	13.0	3.5	---	---	0
B	2120.6	S	407225	6252486	2.2	3.7	4.7	23.2	0.8	3.9	---	---	0
C	1966.8	H	408759	6252455	7.7	11.2	56.3	69.0	7.6	28.1	---	---	0
D	1822.2	S?	410881	6252378	7.6	10.9	8.9	16.7	31.4	10.8	---	---	625
E	1775.8	S	411616	6252375	0.7	10.4	14.5	41.2	23.9	6.8	---	---	18
LINE 62890			FLIGHT 43										
A	2531.6	S	405887	6252372	0.8	5.4	13.3	34.0	9.9	5.4	---	---	0
B	2689.4	H	408648	6252301	4.9	10.7	61.7	74.6	3.3	30.3	---	---	103
C	2864.7	B?	411018	6252234	0.0	2.1	16.6	15.3	9.2	6.4	---	---	0
D	2901.9	S?	411802	6252200	1.1	13.3	*	*	*	*	---	---	0
LINE 62901			FLIGHT 46										
A	1526.9	S?	405680	6252227	2.1	4.3	6.1	19.7	3.5	4.0	0.4	17	0
B	1711.3	H	408610	6252142	6.4	11.6	51.0	66.7	1.7	26.7	0.6	2	116
LINE 62910			FLIGHT 46										
A	1040.1	E	408572	6251987	3.5	13.9	56.7	63.2	23.8	30.7	0.3	0	124
B	1032.0	H	408795	6251979	5.8	19.6	56.7	121.9	1.8	30.7	0.4	0	0
C	900.8	S?	410829	6251922	4.1	1.8	15.6	16.7	24.5	2.6	---	---	0
LINE 62920			FLIGHT 47										
A	2342.8	H?	405414	6251933	0.2	6.0	28.6	18.7	43.5	4.2	---	---	0
B	2321.2	S	405896	6251921	1.7	6.2	18.9	13.8	11.4	4.0	0.2	16	0
C	2253.3	S	406976	6251887	1.4	2.8	2.4	16.2	0.6	2.8	0.3	41	0
D	2119.5	H	408717	6251838	4.2	22.7	49.9	123.1	21.3	30.8	0.2	0	0
E	1973.5	S?	410859	6251779	16.1	1.7	54.3	37.9	71.3	6.5	---	---	291
LINE 62930			FLIGHT 47										
A	2553.2	H?	406143	6251754	0.8	2.5	0.9	21.9	1.5	4.1	---	---	0
B	2699.4	H	408626	6251693	1.8	8.4	43.0	82.8	0.0	21.0	---	---	69
LINE 62940			FLIGHT 47										
A	3542.5	H?	405734	6251619	4.8	7.1	19.9	37.2	25.5	6.8	---	---	108
B	3330.7	S?	408742	6251539	1.0	15.4	21.8	106.6	5.1	21.4	0.1	0	0
C	3222.7	S	410356	6251496	0.8	7.3	6.7	41.6	4.7	6.2	---	---	0
D	3186.0	S?	410857	6251479	22.1	5.2	38.4	27.5	53.4	3.5	---	---	168

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 62950			FLIGHT 47										
A	3723.3	S?	405650	6251464	0.6	5.5	2.3	28.3	0.0	4.6	---	---	0
B	3759.5	S?	406252	6251454	2.4	5.1	9.8	24.9	13.2	3.7	---	---	0
C	3895.5	S?	408603	6251395	0.3	14.4	14.5	82.9	2.4	15.3	---	---	0
D	4020.7	S	410373	6251337	2.0	4.0	6.6	15.9	5.1	3.7	0.4	8	0
E	4052.1	S?	410784	6251333	3.6	3.8	0.1	30.0	0.0	5.1	---	---	0
LINE 62960			FLIGHT 47										
A	4597.1	S?	405825	6251315	1.2	4.6	4.5	18.5	2.8	3.2	---	---	0
B	4554.3	S?	406521	6251298	0.2	2.6	4.8	16.4	7.1	3.1	---	---	0
C	4428.2	S?	408570	6251244	0.0	15.7	11.2	69.8	0.0	11.4	---	---	0
D	4351.5	S?	409935	6251215	7.5	15.0	18.0	34.6	10.9	6.2	0.6	10	0
E	4314.7	S	410423	6251196	2.7	7.2	19.9	33.3	13.0	5.0	---	---	0
F	4295.0	S?	410706	6251183	0.8	8.4	21.8	34.6	25.8	6.9	---	---	-13
LINE 62970			FLIGHT 47										
A	4929.6	S?	405892	6251159	3.5	6.6	13.1	31.0	17.1	5.0	---	---	0
B	5085.8	S?	408572	6251108	5.2	6.9	28.0	61.2	39.8	10.5	---	---	137
C	5199.4	H	410057	6251030	0.0	0.8	15.7	8.3	1.9	7.2	---	---	0
D	5226.1	S	410438	6251023	0.9	3.6	11.3	43.4	2.0	6.2	---	---	0
LINE 62980			FLIGHT 47										
A	5746.5	S	406719	6250998	1.2	4.0	2.6	22.7	2.2	4.0	---	---	31
B	5654.2	S	408083	6250949	4.9	5.1	7.3	19.3	3.8	4.3	---	---	0
C	5623.3	S	408642	6250947	1.2	5.1	2.3	26.9	0.1	4.4	---	---	404
D	5539.3	D	409913	6250915	20.7	18.7	29.3	47.3	1.3	15.3	1.9	9	0
E	5516.2	B?	410201	6250900	1.6	5.8	7.2	6.3	4.1	1.4	---	---	97
F	5492.4	S?	410516	6250887	2.7	7.7	19.7	65.7	6.5	12.0	---	---	0
LINE 62990			FLIGHT 47										
A	6079.9	H	407895	6250811	3.8	2.8	17.9	22.9	5.7	5.1	1.4	50	0
B	6137.2	S	408671	6250784	2.0	5.4	1.1	18.3	1.1	3.3	0.3	0	0
C	6243.3	B?	409823	6250746	9.6	15.7	23.0	36.4	25.3	8.9	0.8	8	670
D	6256.7	B	409897	6250748	7.9	7.2	14.0	14.3	9.5	2.0	1.4	20	0
E	6297.4	S	410569	6250733	3.2	8.8	43.4	82.0	23.7	14.3	0.4	8	0
LINE 63000			FLIGHT 47										
A	7041.4	S	404999	6250742	1.2	11.1	8.4	48.2	4.0	7.6	---	---	121

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EM Anomaly List

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LINE 63000		FLIGHT 47											
B	7007.8	S	405771	6250715	0.8	5.2	11.6	24.0	14.7	4.0	---	---	77
C	6871.8	H	407813	6250660	2.6	3.5	16.7	22.7	2.8	6.2	---	---	0
D	6722.6	B?	409852	6250610	12.7	12.6	30.5	43.4	19.5	10.8	1.5	14	0
E	6671.5	S?	410614	6250589	6.0	28.0	61.2	147.9	15.0	26.6	---	---	391
LINE 63010		FLIGHT 47											
A	7107.7	S	405100	6250583	0.8	11.5	6.2	46.1	3.6	6.1	---	---	0
B	7147.7	S	405727	6250583	0.3	5.5	2.4	22.8	3.4	3.5	---	---	0
C	7264.0	H	407811	6250512	2.0	5.8	16.5	23.6	2.3	5.9	0.3	15	98
D	7332.7	S	408838	6250494	1.4	4.1	2.7	25.4	5.7	4.1	0.3	11	0
E	7443.5	H?	409747	6250459	2.6	0.0	2.7	25.8	3.9	7.3	---	---	517
F	7461.3	B?	409851	6250458	3.8	7.0	6.6	16.5	7.7	3.7	0.5	25	0
G	7504.0	S?	410720	6250431	11.5	21.5	46.3	125.9	31.8	23.1	0.7	5	0
H	7515.3	E	410986	6250426	3.9	11.3	17.4	50.3	26.4	8.8	---	---	0
LINE 63020		FLIGHT 47											
A	8076.0	S	404877	6250444	0.4	0.9	2.1	17.2	6.1	3.0	---	---	62
B	8050.3	S	405230	6250446	2.7	2.6	9.6	22.0	12.0	2.8	0.9	61	168
C	8039.8	S	405454	6250441	0.1	8.8	8.2	28.7	7.1	6.7	---	---	0
D	8010.2	S	405963	6250413	2.3	3.5	2.7	15.8	1.8	2.4	0.5	40	0
E	7835.3	S	408838	6250330	0.4	1.7	0.8	25.2	0.0	4.4	0.1	18	37
F	7749.2	B?	409861	6250295	8.5	10.0	10.9	20.9	2.0	2.8	1.1	8	52
G	7719.4	S	410251	6250311	2.1	5.7	9.0	39.3	4.1	6.4	0.3	16	0
H	7694.9	S	410757	6250283	4.5	26.6	54.0	196.3	31.5	33.3	0.2	0	0
I	7688.6	S?	410899	6250273	8.0	38.7	54.0	196.3	26.0	35.8	0.3	0	0
LINE 63030		FLIGHT 48											
A	671.7	S	405678	6250276	0.7	0.8	4.9	15.9	3.9	2.8	---	---	0
B	780.1	H	407728	6250214	4.9	3.6	25.8	37.9	2.3	9.2	---	---	0
C	852.9	S?	408877	6250178	4.4	7.4	4.1	29.6	4.4	6.2	---	---	0
D	973.1	S	409844	6250158	2.4	4.7	9.1	14.5	12.0	1.6	---	---	0
E	1001.2	S	410226	6250143	1.8	5.9	6.9	28.5	3.2	5.8	---	---	0
F	1028.5	S?	410768	6250134	2.4	12.5	23.5	30.0	10.6	7.0	---	---	0
G	1039.2	S?	410957	6250133	7.2	31.1	41.6	114.1	25.8	19.9	---	---	176
H	1060.1	S?	411372	6250113	14.0	8.3	52.0	40.3	68.0	6.4	---	---	476
I	1068.8	S	411497	6250110	2.3	8.9	67.2	47.7	30.9	8.6	---	---	0
J	1175.2	S?	412393	6250096	2.6	6.4	15.1	30.9	2.5	6.7	---	---	0
K	1184.8	S	412456	6250093	4.4	9.8	2.5	18.1	6.6	2.6	---	---	0

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LINE 63040			FLIGHT 48										
A	1751.2	S	406552	6250102	3.2	7.3	9.8	23.5	9.6	4.3	---	---	125
B	1728.9	S	407135	6250075	1.8	8.3	3.8	32.5	8.2	5.2	---	---	0
C	1697.3	S	407877	6250061	7.3	14.6	28.8	77.7	1.7	16.4	---	---	0
D	1463.5	S	410414	6249997	0.3	4.8	0.9	22.0	1.0	4.2	---	---	158
E	1426.4	S?	411029	6249976	22.1	18.9	48.4	86.9	38.6	17.2	---	---	0
F	1397.8	S	411537	6249960	3.0	8.0	25.3	29.0	31.7	5.6	---	---	0
G	1313.4	D	412733	6249913	9.2	21.5	36.7	50.6	31.8	8.7	---	---	0
LINE 63050			FLIGHT 48										
A	1963.5	S	405806	6249962	0.3	8.6	8.0	36.4	10.4	6.5	---	---	0
B	2089.6	S?	407807	6249916	2.4	7.3	12.8	44.8	0.0	8.9	---	---	0
C	2179.9	S	409048	6249854	3.8	4.2	6.9	17.2	6.2	3.0	---	---	0
D	2312.3	S?	410758	6249829	4.8	6.5	5.5	8.7	3.1	1.9	---	---	0
E	2321.3	S?	411023	6249821	10.0	24.3	42.1	102.6	26.6	19.2	0.6	0	0
F	2344.7	S	411574	6249802	1.9	5.0	14.1	36.7	13.9	5.8	---	---	0
G	2457.0	H?	412488	6249789	5.3	12.6	34.6	63.1	17.1	11.4	0.5	13	0
H	2462.4	D	412596	6249785	3.0	10.5	38.9	63.1	18.0	10.6	0.3	7	0
LINE 63060			FLIGHT 48										
A	3203.6	S	405932	6249812	0.8	4.8	5.5	17.5	5.1	3.0	---	---	35
B	3112.5	H	407425	6249765	6.0	4.2	11.4	11.8	3.7	4.9	---	---	0
C	2958.6	S	409264	6249725	2.2	5.2	4.2	34.3	5.0	5.8	---	---	324
D	2846.7	S	410631	6249689	0.6	0.7	10.6	27.2	20.1	4.8	---	---	0
E	2838.6	S	410758	6249681	4.7	7.8	9.6	12.1	23.5	1.0	---	---	0
F	2824.8	S?	411008	6249673	15.3	34.3	33.1	77.4	17.5	14.7	---	---	0
G	2816.1	S	411194	6249668	3.5	13.1	33.1	54.8	17.5	10.8	---	---	0
H	2794.0	S	411628	6249662	2.5	16.8	15.8	67.3	15.1	11.3	---	---	69
I	2732.0	D	412617	6249621	16.2	54.6	53.3	106.1	10.1	20.8	0.5	0	0
J	2724.6	B?	412771	6249612	10.9	18.1	37.5	54.9	10.3	18.4	---	---	0
LINE 63070			FLIGHT 48										
A	3428.4	S	406263	6249645	0.0	3.0	34.7	19.5	46.7	2.7	---	---	92
B	3505.1	H	407359	6249613	5.1	4.3	13.9	21.1	1.1	6.4	---	---	34
C	3755.8	S	410767	6249533	3.8	9.5	6.2	22.2	11.0	4.8	0.4	7	0
D	3764.6	S	411007	6249521	6.5	16.7	9.8	36.8	2.0	8.8	0.5	0	0
E	3772.5	S	411230	6249513	0.5	8.0	9.8	41.1	1.7	6.8	---	---	0
F	3789.0	S	411618	6249511	2.2	11.6	15.5	70.8	10.8	12.9	0.2	0	0

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LINE 63080			FLIGHT 28										
A	5027.8	S	406251	6249492	3.1	5.2	2.1	23.1	0.9	3.7	---	---	82
B	5093.3	S	407371	6249483	1.3	4.1	11.2	16.2	1.5	5.4	---	---	94
C	5339.6	S?	410612	6249374	6.9	11.0	41.4	32.9	55.9	6.4	---	---	708
D	5363.8	S	411011	6249365	5.5	8.9	11.8	22.7	14.2	4.5	0.7	14	0
E	5389.9	S	411624	6249360	1.7	0.2	16.3	36.3	13.6	6.8	10.6	94	0
F	5397.1	S	411766	6249355	2.6	6.6	8.2	35.9	11.2	6.6	0.3	0	50
LINE 63090			FLIGHT 28										
A	4447.6	S	406745	6249352	0.5	2.7	1.4	17.1	1.3	3.6	---	---	0
B	4403.5	D	407247	6249325	8.9	13.9	18.0	20.7	16.2	9.0	0.8	2	168
C	4395.9	S	407370	6249323	1.4	11.9	18.0	55.3	1.4	11.1	---	---	141
D	4211.1	S	409480	6249271	2.6	8.4	13.8	50.4	0.1	10.2	---	---	0
E	4097.2	S	411246	6249227	7.7	6.9	23.8	9.2	28.2	3.3	---	---	111
F	4091.7	S?	411350	6249229	6.4	4.6	19.1	17.6	26.9	4.6	---	---	428
G	4083.2	S	411512	6249217	4.3	2.5	10.4	45.5	7.8	9.3	---	---	0
H	4074.5	S	411676	6249212	2.4	7.8	11.8	43.6	12.7	7.9	---	---	0
I	3982.4	S	412958	6249176	7.9	4.3	57.3	15.2	74.6	3.4	---	---	74
LINE 63180			FLIGHT 28										
A	2589.2	H	407121	6247975	5.5	4.9	20.8	33.0	2.4	9.1	---	---	0
B	2369.4	S?	410012	6247913	6.7	9.0	33.8	34.9	4.8	10.7	---	---	0
C	2284.6	H?	411680	6247867	2.4	3.6	15.8	16.8	8.6	3.8	---	---	0
D	2245.9	S?	412273	6247846	3.5	10.9	1.2	15.7	15.2	3.2	---	---	103
E	2191.6	S?	413216	6247823	8.2	19.2	90.1	95.7	27.6	26.9	0.6	0	0
F	2164.2	B	413434	6247817	18.7	28.4	68.7	114.7	7.2	31.0	1.1	9	0
G	2019.6	S	414983	6247777	1.3	2.6	0.6	13.0	0.1	3.7	---	---	0
H	1896.3	S?	416826	6247704	0.6	6.4	0.0	20.7	0.5	3.4	---	---	0
LINE 63190			FLIGHT 28										
A	2856.6	S	406014	6247840	5.4	1.1	24.4	10.5	30.9	1.8	---	---	0
B	3107.0	S	410055	6247765	5.1	5.0	32.6	28.5	8.3	12.2	1.1	0	0
C	3259.3	D	413324	6247663	9.4	39.0	18.0	78.9	5.4	13.2	0.4	0	0
D	3271.9	D	413511	6247660	8.8	9.7	42.6	56.2	6.9	16.1	1.2	15	50
LINE 63200			FLIGHT 28										
A	926.0	S?	407094	6247683	1.3	6.2	17.1	44.5	2.5	9.5	---	---	0
B	1142.0	H	410193	6247607	1.7	3.0	29.6	23.3	3.3	11.6	0.4	41	82

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 63200			FLIGHT 28										
C	1317.2	B?	413388	6247503	1.5	2.3	29.3	21.9	6.8	9.7	---	---	0
D	1329.7	B?	413512	6247501	3.4	4.6	33.9	61.2	8.6	17.4	0.7	35	0
E	1502.8	S	416293	6247433	1.0	4.8	11.6	30.4	10.9	5.5	---	---	0
LINE 63210			FLIGHT 27										
A	8158.6	H	410283	6247451	4.9	9.9	67.0	67.7	5.4	25.4	0.5	0	0
B	8230.0	S	411796	6247401	3.5	6.7	7.6	16.2	6.4	3.1	0.5	14	0
C	8335.5	D	413634	6247355	57.9	63.8	193.6	283.6	46.5	88.2	2.2	3	0
LINE 63220			FLIGHT 27										
A	7297.5	S	407198	6247372	2.6	3.4	10.3	17.5	2.6	4.7	0.6	16	0
B	7044.9	B?	410470	6247292	15.1	47.9	164.7	253.7	16.2	75.5	0.5	0	226
C	6978.7	H	411749	6247274	3.3	4.8	6.5	18.5	2.4	4.5	0.6	33	0
D	6957.9	S	412104	6247245	2.5	6.4	16.2	23.8	23.6	4.8	---	---	0
E	6939.3	S	412433	6247242	0.6	3.0	10.8	14.0	10.9	2.5	---	---	878
F	6871.7	D	413482	6247216	1.1	10.9	10.6	19.8	9.0	8.3	---	---	0
G	6852.7	D	413728	6247204	38.0	52.3	110.8	126.7	28.6	46.9	1.5	0	0
H	6720.8	S	415646	6247138	1.8	4.6	6.4	3.9	3.8	1.1	---	---	0
I	6703.5	S	415865	6247138	2.1	6.4	3.5	12.0	1.7	2.5	0.3	0	0
LINE 63230			FLIGHT 27										
A	5506.3	H	407152	6247232	2.8	6.0	14.4	19.6	1.0	6.7	0.4	5	0
B	5745.2	D	410621	6247133	22.3	47.7	145.1	287.8	0.0	67.7	0.8	0	302
C	5964.5	D	413792	6247054	8.1	6.3	97.5	93.4	28.7	40.6	1.7	31	0
D	5972.9	E	413911	6247052	9.9	17.6	11.5	58.5	0.0	9.2	0.7	8	0
LINE 63240			FLIGHT 27										
A	4934.6	S	406958	6247080	5.3	9.9	17.6	36.1	4.5	9.4	0.6	0	0
B	4874.7	S	408011	6247055	2.5	7.0	8.0	19.2	8.6	4.0	---	---	0
C	4857.5	S	408360	6247056	0.5	6.5	13.3	13.0	15.2	0.9	---	---	0
D	4761.4	S	409543	6247015	0.1	2.9	1.6	17.1	0.1	3.5	---	---	0
E	4683.7	E	410587	6246992	4.1	4.7	49.3	26.0	11.0	19.0	0.8	32	0
F	4673.4	S?	410817	6246979	11.3	18.1	72.2	112.8	10.5	30.7	0.9	0	418
G	4615.6	H	411865	6246954	4.7	9.4	18.1	34.5	3.4	8.1	0.5	15	0
H	4594.9	S	412187	6246944	2.9	7.8	9.7	31.9	5.5	5.6	---	---	0
I	4500.2	H?	413825	6246909	2.1	14.2	22.5	46.8	9.0	12.8	0.2	0	0
J	4485.4	D	413976	6246903	6.8	10.2	51.9	65.8	19.4	23.5	0.8	17	20
K	4479.0	E	414034	6246904	12.5	15.1	51.9	65.8	19.4	23.5	1.2	13	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 63240			FLIGHT 27										
L	4380.4	S?	415735	6246845	2.4	9.1	11.8	47.9	4.8	9.0	---	---	363
M	4343.3	S?	416327	6246838	1.1	6.6	4.7	14.7	7.0	3.5	---	---	17
LINE 63250			FLIGHT 27										
A	3545.0	S	406935	6246938	1.0	3.7	19.6	23.3	2.3	6.6	0.2	0	0
B	3571.1	H	407432	6246922	2.2	1.8	10.0	26.6	0.6	4.5	---	---	0
C	3608.7	S	408102	6246902	2.1	4.0	14.5	17.2	14.6	5.4	---	---	0
D	3782.8	E	410690	6246835	4.9	4.9	51.3	29.3	10.5	19.6	1.1	36	0
E	3797.0	S?	411048	6246817	4.6	17.9	50.3	96.0	2.8	22.0	0.3	0	0
F	3839.2	H	411940	6246794	2.4	2.9	15.0	21.0	0.1	8.3	0.7	46	0
G	3936.3	D	414142	6246738	28.9	29.6	52.2	48.7	10.8	23.6	1.9	0	0
LINE 63260			FLIGHT 27										
A	2825.2	S	406694	6246781	1.4	4.0	9.1	22.2	0.0	4.7	0.3	0	64
B	2709.3	S?	408667	6246747	0.8	3.7	6.5	20.9	1.3	3.8	---	---	144
C	2531.9	E	410716	6246694	4.2	4.5	46.3	33.4	8.5	18.2	0.9	31	0
D	2513.8	S?	411255	6246672	6.2	13.0	40.6	64.5	0.1	19.8	0.6	0	0
E	2380.0	D	414259	6246603	14.7	14.9	47.7	48.1	15.3	22.1	1.5	6	0
F	2352.2	S	414930	6246572	0.0	2.7	3.3	17.7	1.1	2.9	0.1	20	282
G	2324.9	S	415487	6246551	6.5	5.7	24.9	28.0	31.8	4.7	1.4	31	249
H	2253.0	S	416785	6246526	1.9	3.6	8.0	14.4	7.4	2.7	---	---	0
LINE 63270			FLIGHT 26										
A	2667.3	S	406644	6246650	1.7	7.0	14.0	21.7	0.3	4.8	---	---	210
B	2888.2	E	410702	6246533	4.8	4.1	32.4	33.4	4.9	16.1	---	---	0
C	2914.3	H?	411412	6246525	13.6	20.9	73.6	100.6	4.1	38.3	0.9	0	0
D	3020.7	S?	414366	6246408	4.6	6.6	7.4	11.5	0.3	3.4	---	---	0
E	3052.9	S	415343	6246404	3.3	4.2	10.5	38.4	18.2	6.7	---	---	0
LINE 63280			FLIGHT 26										
A	2084.4	S	406501	6246483	3.3	4.9	21.2	36.3	3.3	8.4	---	---	133
B	1964.0	S	408783	6246441	3.6	5.1	9.9	13.9	8.3	1.8	---	---	0
C	1864.2	S	410069	6246395	1.8	4.3	6.0	15.4	3.9	2.5	---	---	0
D	1819.8	E	410724	6246384	2.8	2.6	31.0	24.1	7.9	11.6	---	---	0
E	1792.4	H	411578	6246362	11.4	24.1	83.2	115.6	9.5	41.2	0.7	0	40
F	1751.1	H	412747	6246334	3.1	4.9	10.7	25.6	5.0	5.9	---	---	0
G	1667.2	S	414452	6246279	6.9	24.8	14.3	56.6	12.4	9.2	---	---	0
H	1645.9	S	414917	6246268	1.6	7.7	7.9	46.3	9.8	8.2	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 63280			FLIGHT 26										
I	1633.8	S	415163	6246267	0.3	13.4	2.9	67.1	10.3	11.6	---	---	331
J	1509.7	S	417773	6246190	7.6	4.7	10.8	33.7	23.0	6.0	---	---	395
LINE 63290			FLIGHT 26										
A	832.4	S?	406446	6246360	4.1	4.5	7.8	16.1	2.4	4.6	---	---	0
B	1105.1	H	411687	6246204	8.4	15.1	72.9	121.7	9.2	36.0	0.7	8	20
C	1236.6	S	415292	6246107	1.2	15.6	14.1	87.6	16.1	16.4	---	---	66
D	1288.0	S	416163	6246084	3.0	2.8	10.9	35.9	0.9	6.6	---	---	0
E	1314.0	S	416916	6246066	3.3	7.7	27.5	47.7	38.2	7.2	---	---	39
F	1321.0	S	417128	6246063	4.6	6.3	0.4	41.3	0.0	5.5	---	---	38
G	1336.5	S	417630	6246048	1.2	6.5	32.3	25.7	1.9	6.6	---	---	372
H	1351.2	S	418047	6246042	5.2	1.7	25.4	24.3	31.6	4.9	---	---	0
LINE 63300			FLIGHT 21										
A	6180.8	H	406344	6246201	3.7	4.3	13.6	20.6	4.3	4.6	0.8	31	0
B	6058.1	S	409208	6246124	0.0	4.4	7.1	22.5	6.5	4.2	---	---	140
C	5927.0	H	411861	6246068	6.0	25.1	69.1	163.8	0.0	40.5	0.3	0	0
D	5881.5	S	413293	6246025	3.0	5.0	10.6	30.5	3.2	5.9	---	---	66
E	5816.3	S	415057	6245967	2.0	5.6	6.3	29.9	2.7	6.8	---	---	19
F	5799.9	S	415509	6245952	2.6	4.9	12.6	38.0	1.3	9.2	---	---	77
G	5710.8	S	418091	6245871	4.1	1.4	18.5	17.4	23.9	3.0	---	---	0
LINE 63310			FLIGHT 21										
A	4871.7	S?	405598	6246049	6.1	3.4	0.3	20.2	0.3	3.1	---	---	0
B	5050.0	S	409276	6245965	0.5	3.6	0.8	22.9	11.7	3.3	---	---	50
C	5160.1	H	411455	6245909	2.4	3.8	18.0	23.1	2.9	7.1	0.5	33	0
D	5180.5	H	412050	6245902	8.6	10.3	22.3	40.8	3.0	11.0	1.0	2	0
E	5212.4	S	412934	6245877	0.7	5.6	14.1	43.3	1.6	8.2	---	---	230
F	5269.6	S	414175	6245838	1.2	3.9	5.0	20.7	1.7	4.2	---	---	0
G	5327.5	S	415278	6245802	2.8	4.8	11.7	30.3	4.2	5.1	0.5	26	0
H	5349.4	S?	415704	6245807	1.0	16.8	7.2	95.2	0.0	14.9	0.1	0	0
I	5413.5	S	416829	6245761	1.0	3.4	2.7	19.5	1.8	3.8	---	---	188
J	5447.2	S	417482	6245750	6.7	6.2	29.2	7.2	38.8	1.0	1.3	34	0
LINE 63320			FLIGHT 21										
A	4596.5	S	405557	6245925	0.0	3.3	8.9	15.0	0.0	2.5	---	---	539
B	4548.2	S	406258	6245889	1.6	4.0	24.8	35.5	37.7	6.6	---	---	0
C	4422.5	S	409049	6245834	1.9	7.8	9.7	33.7	7.0	6.8	---	---	146

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 63320			FLIGHT 21										
D	4408.9	S	409372	6245819	1.2	2.3	2.9	17.5	2.1	3.4	---	---	110
E	4275.5	S?	412157	6245737	14.2	18.5	52.5	79.3	3.2	20.2	1.1	0	50
F	4259.4	H	412718	6245740	3.1	3.0	16.6	25.4	3.4	6.5	---	---	374
G	4148.8	S	415370	6245662	0.4	6.9	6.7	28.7	6.4	5.1	---	---	0
H	4133.1	S?	415780	6245647	3.2	4.3	17.1	28.3	9.0	7.3	---	---	0
I	4068.9	S?	417089	6245611	2.8	9.7	19.4	18.7	25.0	3.6	---	---	450
LINE 63330			FLIGHT 21										
A	3033.5	S	405497	6245765	4.5	5.4	12.0	24.9	22.4	4.1	---	---	0
B	3122.2	S	407126	6245721	0.4	4.5	3.5	21.0	6.2	5.1	---	---	0
C	3212.9	S?	408949	6245668	1.2	7.3	28.1	34.1	53.6	7.5	---	---	317
D	3229.2	S	409336	6245654	0.6	7.4	11.4	13.8	14.2	2.7	---	---	0
E	3364.4	S?	412194	6245605	9.8	21.1	84.4	127.2	1.1	31.6	0.6	0	0
F	3386.2	H	412742	6245568	1.5	2.2	10.8	21.3	2.4	5.4	---	---	0
G	3517.6	S	415495	6245517	0.6	2.5	2.6	17.4	0.0	2.3	0.1	14	0
H	3540.8	S?	416049	6245496	1.5	1.8	1.3	21.2	2.2	3.1	0.6	66	57
I	3610.0	S	417118	6245463	2.4	5.4	9.4	17.5	8.7	1.9	0.4	19	431
LINE 63341			FLIGHT 51										
A	7262.9	S	405443	6245612	6.8	6.6	5.3	33.5	9.2	5.8	---	---	76
B	7300.2	S?	405962	6245610	27.7	2.7	87.6	21.4	115.1	3.6	---	---	0
C	7311.6	S?	406067	6245604	13.9	16.9	69.9	70.5	66.3	11.6	---	---	0
D	7509.8	S	409303	6245516	3.2	5.6	47.5	17.8	49.1	3.1	---	---	0
E	7529.4	S	409641	6245507	0.0	10.7	23.7	31.0	42.4	5.1	---	---	448
F	7542.8	S	409900	6245499	4.6	8.0	18.1	31.3	25.0	5.2	---	---	101
G	7672.9	S	412257	6245439	9.5	13.6	64.8	97.1	1.0	24.6	0.9	3	0
H	7799.6	S	414838	6245373	0.1	11.9	8.2	52.8	10.5	8.8	---	---	44
I	7812.2	S	415154	6245369	0.6	5.9	5.9	20.9	18.1	2.8	---	---	0
J	7872.9	S	416262	6245337	1.3	2.9	1.1	16.5	2.1	2.8	---	---	0
K	7909.8	S	416718	6245316	0.7	3.6	0.2	16.6	0.4	3.6	---	---	16
LINE 63351			FLIGHT 51										
A	8494.6	S	409365	6245370	3.6	9.0	36.0	30.7	45.4	5.5	---	---	0
B	8350.6	S?	412337	6245276	7.4	27.2	125.2	241.4	12.3	54.8	0.4	0	59
C	8345.2	S?	412409	6245275	13.1	37.5	125.2	241.4	1.4	54.8	0.5	0	41
LINE 63352			FLIGHT 52										
A	3030.3	S?	403263	6245546	10.8	10.3	37.0	41.8	44.6	7.1	---	---	0

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LINE 63352			FLIGHT 52										
B	2863.3	S	405370	6245481	1.4	6.1	19.9	14.8	30.4	1.6	---	---	0
C	2816.9	S	405951	6245455	4.0	14.9	33.4	97.8	2.0	18.0	---	---	0
D	2703.8	S	407952	6245402	2.8	0.6	6.9	23.2	5.2	4.7	---	---	91
E	2667.3	S	408640	6245389	4.0	7.9	62.5	16.3	89.7	2.9	---	---	169
LINE 63360			FLIGHT 24										
A	821.2	S	398213	6245501	0.9	7.1	13.1	56.0	3.4	10.3	0.1	2	0
B	847.6	S	398666	6245508	1.3	3.6	2.9	27.2	0.0	3.9	0.3	17	0
C	890.1	S	399334	6245492	1.4	8.8	12.9	36.9	1.3	6.4	0.1	0	0
D	1097.0	S	403082	6245388	2.1	4.0	13.3	31.0	16.8	5.3	---	---	0
E	1229.0	D	405285	6245345	16.5	9.0	0.0	28.3	0.0	5.7	---	---	332
F	1260.8	S?	405879	6245321	6.7	18.0	29.5	97.8	6.9	16.8	0.5	0	0
G	1366.9	S	407450	6245269	1.8	4.4	4.0	23.7	4.2	4.7	---	---	0
H	1419.6	S	408461	6245241	0.0	4.2	35.0	22.7	44.2	3.7	---	---	0
I	1467.7	S?	408982	6245234	3.5	11.2	36.4	47.5	47.0	7.8	---	---	0
J	1667.5	S	412452	6245135	7.9	17.5	72.9	95.6	1.8	27.2	0.6	0	43
K	1843.6	S?	414981	6245070	0.8	9.8	0.0	17.7	2.7	2.4	---	---	0
L	1896.4	S	415901	6245046	2.5	4.3	6.3	26.0	0.8	4.9	---	---	0
M	1939.9	S	416681	6245025	0.4	6.6	0.6	47.7	3.1	9.1	---	---	0
N	2013.5	S	417278	6245005	1.4	2.4	0.1	20.2	14.8	3.2	---	---	43
LINE 63370			FLIGHT 24										
A	3517.5	S	396968	6245408	4.0	5.1	11.0	18.5	11.9	2.5	---	---	0
B	3487.8	H	397696	6245387	4.6	3.5	39.5	18.9	43.3	12.6	---	---	0
C	3449.5	S?	398679	6245357	10.9	5.4	40.0	59.7	76.3	10.5	---	---	122
D	3441.9	S?	398882	6245358	2.8	8.1	62.1	65.6	76.3	10.6	---	---	58
E	3249.7	S?	403001	6245236	3.7	3.6	29.9	23.8	38.0	3.5	---	---	148
F	3020.8	S?	405780	6245143	8.4	13.5	13.4	77.9	13.6	13.0	---	---	0
G	2922.2	S	407627	6245121	3.6	2.7	19.2	26.7	39.2	4.0	---	---	0
H	2841.5	S?	408680	6245092	9.1	13.1	49.6	25.1	61.2	3.1	---	---	734
I	2763.1	S?	410245	6245041	4.6	4.1	4.9	14.5	2.1	2.0	---	---	0
J	2620.2	S?	412585	6244979	8.8	17.1	61.6	88.2	4.3	22.1	---	---	0
K	2480.6	D	415042	6244924	6.1	16.3	14.8	17.9	25.7	3.1	---	---	0
L	2367.1	S?	417330	6244850	2.1	5.8	0.0	19.3	0.1	4.0	---	---	187
LINE 63380			FLIGHT 24										
A	3932.0	H?	396475	6245275	1.8	5.2	22.4	29.7	2.6	11.2	0.3	1	0
B	3996.8	H	397585	6245240	7.6	6.0	67.5	57.7	19.2	24.0	1.6	29	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 63380			FLIGHT 24										
C	4001.7	D	397696	6245233	14.6	16.8	67.5	57.7	20.3	24.0	1.3	5	0
D	4210.0	S	401456	6245127	0.0	3.9	25.5	18.0	34.5	3.0	---	---	0
E	4463.3	S	405230	6245015	4.2	5.0	20.5	16.5	23.7	3.7	---	---	0
F	4488.9	S	405719	6245029	7.9	10.7	16.8	48.3	19.2	8.6	0.9	0	0
G	4612.3	S	407560	6244958	4.3	12.6	6.0	74.1	10.1	11.1	---	---	0
H	4687.0	S	408681	6244937	8.4	7.6	44.6	32.6	57.8	4.2	---	---	308
I	4724.6	S	409211	6244918	4.5	5.0	20.0	20.4	24.3	3.5	---	---	53
J	4915.1	S	412568	6244851	3.3	9.0	42.0	58.0	1.2	14.6	0.4	0	0
K	5010.8	S	413622	6244808	0.0	1.8	1.8	20.2	3.6	3.2	0.1	20	0
L	5076.5	S	414709	6244774	1.8	9.6	7.8	45.5	9.4	7.0	0.2	0	0
M	5095.5	S	415087	6244760	3.2	8.0	5.4	15.8	8.5	3.0	0.4	13	0
N	5208.2	S?	416988	6244729	1.8	8.8	10.5	49.2	5.5	11.6	0.2	4	15
LINE 63390			FLIGHT 24										
A	7005.8	S	396146	6245133	6.8	5.7	11.5	17.9	7.8	3.9	1.5	0	0
B	6740.4	S	401199	6244999	2.3	3.1	15.8	15.7	18.9	2.6	---	---	22
C	6484.1	S	405175	6244898	0.5	6.1	2.3	12.4	22.5	2.1	---	---	26
D	6437.4	S	405651	6244846	5.0	9.0	25.6	60.9	12.7	10.4	---	---	0
E	6300.3	S	408258	6244786	12.5	11.6	40.4	68.9	40.1	10.3	---	---	0
F	6284.6	S	408402	6244780	1.6	3.3	7.8	39.3	128.9	6.5	---	---	0
G	6261.2	S	408759	6244783	19.4	13.8	15.0	47.4	17.2	6.9	---	---	186
H	6051.9	S	412658	6244683	2.6	17.4	30.1	84.6	8.9	16.1	---	---	0
I	5973.7	S	413793	6244648	1.7	3.9	3.9	21.3	5.1	3.6	---	---	0
J	5915.4	S	414701	6244629	2.4	7.7	17.2	33.4	16.2	4.8	---	---	0
K	5886.4	S?	415124	6244610	9.2	27.9	8.3	35.0	13.6	5.6	---	---	454
L	5732.5	S	417335	6244546	1.5	3.7	7.7	19.5	3.8	4.5	---	---	0
LINE 63400			FLIGHT 24										
A	7336.9	H	396672	6244948	5.6	2.9	32.7	27.8	15.4	16.5	2.6	50	0
B	7897.1	S	405633	6244722	2.9	15.1	30.8	94.0	0.0	17.0	0.2	0	0
C	8043.3	S	407940	6244652	1.6	4.2	1.3	33.1	3.4	5.0	0.3	24	29
D	8063.7	S	408313	6244643	1.8	8.4	8.2	40.5	14.9	6.7	---	---	75
E	8090.7	S?	408787	6244658	3.2	6.1	54.4	45.2	72.9	8.2	---	---	288
F	8100.1	S?	408902	6244638	0.2	2.3	54.4	35.3	72.9	5.6	---	---	350
G	8198.9	S	410942	6244573	2.2	6.5	4.8	20.1	7.0	3.1	0.3	13	0
H	8220.8	S	411355	6244558	1.9	1.2	0.6	15.6	4.0	1.8	---	---	74
I	8295.4	S	412856	6244510	2.8	7.7	7.6	27.1	1.9	7.2	0.3	0	344
J	8440.8	S?	415104	6244457	4.7	15.1	7.6	32.4	0.1	5.2	0.4	1	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 63400			FLIGHT 24										
K	8569.8	S	417379	6244409	1.6	5.2	1.4	12.4	1.3	1.3	0.2	15	0
LINE 63410			FLIGHT 25										
A	635.4	H?	395282	6244854	3.8	3.0	10.6	21.5	5.3	3.6	1.3	45	0
B	661.0	H	395891	6244841	3.6	2.8	29.1	13.5	13.4	14.3	1.2	56	0
C	1263.8	S	404099	6244619	9.7	2.5	32.4	17.9	34.0	3.0	---	---	0
D	1358.8	S	405571	6244569	6.4	7.0	17.0	35.6	0.9	8.0	---	---	0
E	1613.1	S	408897	6244479	2.2	1.7	21.3	45.7	29.9	7.4	---	---	0
F	1621.3	S	408989	6244476	0.0	3.5	21.3	40.9	29.9	6.4	---	---	480
G	1722.6	S	410753	6244432	5.3	4.9	31.4	22.3	38.0	3.9	---	---	0
H	1731.0	S	410885	6244422	3.8	2.3	8.5	22.7	8.8	3.5	---	---	57
I	1842.9	S	412942	6244367	6.0	13.5	20.1	65.2	1.3	12.0	---	---	0
J	2006.7	S?	414735	6244327	2.2	5.7	22.1	17.3	31.5	4.4	---	---	0
K	2177.2	S	417355	6244249	1.8	4.8	3.8	25.4	1.9	3.9	0.3	16	0
LINE 63420			FLIGHT 52										
A	1090.7	S	402076	6244516	0.0	10.1	19.5	54.1	19.4	8.1	---	---	19
B	1274.8	S?	405525	6244436	4.6	6.1	16.5	51.9	0.1	9.5	---	---	0
C	1429.7	S	407226	6244367	0.7	4.0	6.6	26.7	3.1	4.8	---	---	0
D	1520.8	S?	408821	6244357	6.5	10.4	60.1	54.9	80.0	8.0	---	---	0
E	1536.8	S?	409071	6244350	5.2	6.5	22.0	37.0	28.7	5.3	---	---	399
F	1578.9	S?	409751	6244287	31.1	13.9	53.7	67.3	67.2	10.7	---	---	0
G	1664.5	S	411339	6244266	1.0	10.6	10.2	31.3	19.1	5.4	---	---	47
H	1757.1	S	413022	6244222	5.7	8.6	11.3	42.1	2.3	7.7	---	---	0
I	1937.1	S	415396	6244147	0.4	4.1	14.7	22.1	17.5	3.6	---	---	0
J	2117.7	S	417708	6244100	6.9	2.8	2.9	14.7	9.4	3.9	---	---	119
LINE 63430			FLIGHT 25										
A	4443.5	H	395561	6244532	1.8	4.2	9.0	31.8	0.8	6.0	0.3	31	0
B	4890.8	S?	401496	6244391	2.5	4.6	25.2	20.8	34.5	2.8	0.4	31	76
C	4922.4	S?	402140	6244361	0.1	5.0	27.6	29.4	34.3	5.1	0.1	28	76
D	4995.1	S?	403818	6244314	5.9	3.7	1.4	18.8	1.6	3.4	---	---	0
E	5008.4	S	404088	6244313	3.9	0.0	42.7	13.5	56.8	2.6	---	---	0
F	5089.0	S	405431	6244291	8.1	10.5	11.9	48.9	7.2	7.6	0.9	0	0
G	5321.8	S	408124	6244205	3.2	4.0	6.6	25.4	7.5	4.6	0.7	35	210
H	5368.3	S?	409165	6244181	9.2	4.7	57.8	11.9	75.4	3.1	---	---	0
I	5396.5	S	409669	6244155	2.3	10.4	83.1	35.3	106.5	4.2	---	---	312
J	5458.2	S	410948	6244127	6.1	5.1	14.1	29.4	12.0	5.2	1.4	37	185

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 63430			FLIGHT 25										
K	5559.8	S	412610	6244067	2.7	5.2	6.3	22.4	0.8	5.5	0.4	11	179
L	5580.1	S	413162	6244065	1.8	4.2	9.8	31.9	0.6	6.0	0.3	26	368
M	5673.7	S	414353	6244026	3.5	5.7	8.2	16.0	10.7	2.5	0.6	35	0
N	5746.4	S?	415449	6243995	2.0	5.3	8.3	20.0	8.3	3.1	0.3	17	0
LINE 63440			FLIGHT 35										
A	2933.0	S	403632	6244171	0.0	5.5	12.2	47.2	24.1	7.3	---	---	162
B	2918.4	S	403934	6244166	12.2	8.3	51.4	61.8	19.8	10.7	---	---	0
C	2812.7	S	405373	6244120	13.3	13.5	47.1	49.2	37.5	8.0	1.5	0	0
D	2552.6	S	409151	6244027	3.8	6.4	342.9	24.8	501.2	3.4	---	---	0
E	2540.3	S?	409374	6244018	0.0	3.5	355.2	25.8	481.1	1.5	---	---	480
F	2462.7	S	411042	6243978	3.9	9.5	24.1	35.6	34.0	5.5	---	---	260
G	2315.0	S	413128	6243924	4.9	13.8	21.6	61.2	3.7	11.3	0.4	0	227
H	2310.9	S?	413202	6243921	1.3	11.8	21.6	61.2	3.7	11.3	0.1	0	228
I	2290.1	S	413601	6243898	0.5	6.7	8.8	27.4	11.3	4.6	---	---	0
J	2177.6	S?	415255	6243857	6.8	5.2	0.9	18.1	1.5	3.0	---	---	138
LINE 63450			FLIGHT 35										
A	4357.5	S?	403697	6244021	20.9	5.1	51.0	28.3	64.6	4.9	---	---	0
B	4374.9	S	403961	6244016	18.0	6.0	60.7	37.3	73.4	6.7	---	---	0
C	4463.6	S	405285	6243995	6.1	6.2	58.7	28.4	64.9	5.7	1.1	8	0
D	4621.8	S	406857	6243935	0.7	2.1	32.9	17.6	44.1	2.8	---	---	162
E	4745.6	S?	409156	6243887	0.9	5.0	98.2	17.6	127.3	2.8	---	---	0
F	4779.8	S?	409740	6243856	8.9	2.1	109.1	12.1	140.3	2.5	---	---	521
G	4841.6	S	411093	6243821	1.9	2.5	19.0	16.7	28.6	2.9	---	---	0
H	4947.2	S	412718	6243772	1.3	3.7	14.7	24.2	6.0	5.5	---	---	0
I	4969.6	S	413289	6243764	5.1	12.4	16.5	53.5	0.1	9.0	0.5	0	485
J	5014.1	S	413982	6243740	2.2	1.6	3.2	15.3	2.7	4.1	1.2	80	0
LINE 63460			FLIGHT 35										
A	6958.0	S?	397782	6244034	16.7	2.8	49.7	14.0	67.3	2.0	---	---	753
B	6744.4	S?	400653	6243950	14.4	7.4	32.1	15.0	38.1	2.9	3.4	28	0
C	6565.6	S?	403492	6243875	6.4	3.9	16.6	8.1	22.1	3.6	2.1	32	0
D	6555.6	S	403567	6243876	8.4	6.0	34.3	33.6	43.2	5.8	---	---	0
E	6520.0	S	404168	6243870	7.5	5.1	27.1	13.6	28.0	2.7	---	---	0
F	6441.2	S?	405222	6243826	3.6	2.6	8.3	18.4	2.5	3.4	1.4	22	0
G	6117.8	S?	409604	6243713	0.0	3.4	171.5	19.3	230.1	2.1	---	---	1132
H	5979.1	S?	411791	6243643	0.0	5.7	8.4	32.1	0.0	5.0	---	---	0

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 63460			FLIGHT 35										
I	5880.7	S?	413338	6243619	3.5	9.8	12.5	43.2	7.6	8.8	0.4	0	521
LINE 63470			FLIGHT 36										
A	1147.3	S?	400619	6243812	2.7	5.5	12.6	16.2	16.8	2.2	---	---	0
B	1326.1	S?	403011	6243733	3.9	2.2	29.2	18.2	37.9	3.6	---	---	0
C	1355.3	S?	403439	6243724	17.3	3.3	28.2	12.9	38.3	2.1	---	---	23
D	1481.0	S	405105	6243693	3.5	4.3	10.3	22.4	3.9	3.8	---	---	0
E	1875.5	S?	409709	6243562	0.1	13.2	23.6	30.5	30.0	4.2	---	---	1057
F	1990.4	S	411697	6243513	1.6	4.3	26.8	20.4	19.1	4.5	---	---	79
G	2001.8	S?	411886	6243505	5.0	2.4	1.7	20.9	0.0	3.1	---	---	0
H	2073.4	S	412978	6243468	4.0	12.0	14.2	40.9	3.5	8.4	---	---	0
I	2094.0	S	413392	6243457	3.8	11.3	17.9	67.3	11.8	11.6	---	---	0
J	2104.4	S	413582	6243447	0.0	5.5	9.3	52.4	1.0	8.6	---	---	0
K	2234.1	S	414775	6243413	3.4	3.5	35.8	15.3	43.7	2.3	---	---	281
LINE 63480			FLIGHT 36										
A	3731.8	S?	403339	6243572	1.9	9.6	19.5	11.5	26.4	1.0	---	---	0
B	3700.2	S	403729	6243577	6.7	7.3	23.5	23.9	28.1	4.1	---	---	0
C	3590.5	S	405042	6243537	4.4	5.2	13.5	29.9	3.8	5.5	0.8	0	0
D	3556.7	D	405579	6243518	9.4	11.6	47.6	35.7	7.7	21.4	1.1	12	0
E	3244.9	S?	409798	6243408	0.9	4.7	75.6	38.9	101.1	4.7	---	---	1349
F	3211.0	S?	410499	6243404	11.4	10.3	49.1	42.4	59.3	6.6	---	---	509
G	3190.8	S	410962	6243380	0.1	4.0	33.5	15.1	44.1	4.3	---	---	87
H	3167.1	S?	411204	6243393	5.2	3.0	8.3	21.4	10.6	4.9	---	---	23
I	3136.3	S?	411602	6243346	0.0	10.0	5.2	42.5	7.6	6.3	---	---	102
J	3097.4	S?	412170	6243338	4.1	2.7	8.5	15.9	13.3	2.5	---	---	0
K	3017.6	S	412994	6243325	4.2	10.3	18.3	57.0	4.4	11.7	0.4	4	0
L	3003.5	S	413290	6243324	2.4	3.4	3.1	12.7	7.1	2.6	0.6	10	316
M	2975.0	S	413908	6243299	2.6	8.1	15.4	34.9	18.0	6.0	---	---	267
N	2872.4	S?	415411	6243259	0.4	2.7	36.5	10.8	49.2	1.3	---	---	182
LINE 63490			FLIGHT 36										
A	4595.3	S	396250	6243612	6.4	1.7	30.6	10.2	40.8	1.1	6.3	48	0
B	4874.9	S?	400355	6243507	1.4	2.3	17.4	16.0	16.7	2.8	---	---	153
C	5092.9	S?	403690	6243427	9.2	2.1	54.1	15.8	70.5	4.8	---	---	0
D	5123.0	S	404404	6243398	4.2	1.6	16.4	19.3	23.3	3.3	3.4	69	0
E	5168.9	S	405057	6243402	2.4	6.5	14.4	24.0	4.2	3.8	0.3	11	0
F	5426.5	S?	407803	6243308	1.8	5.8	11.5	27.2	18.5	4.7	0.3	16	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 63490			FLIGHT 36										
G	5522.7	S?	409891	6243258	6.7	5.8	0.0	60.7	0.0	9.2	---	---	346
H	5547.6	S?	410513	6243237	0.0	6.3	41.9	40.4	52.6	5.5	---	---	0
I	5609.0	S	411713	6243213	1.9	3.7	9.7	16.9	7.8	3.0	0.4	41	0
J	5703.0	H?	413444	6243179	1.1	5.5	16.1	47.5	2.0	9.5	0.2	15	0
K	5737.8	S	414079	6243132	0.4	5.3	1.2	20.2	0.1	3.3	0.1	9	0
L	5847.7	S	415061	6243120	1.1	1.8	2.7	22.2	16.6	3.7	0.4	57	0
M	5870.4	S	415601	6243088	0.3	3.5	10.9	18.9	10.8	3.2	0.1	3	42
LINE 63500			FLIGHT 36										
A	6297.5	S	413118	6243025	6.7	10.3	23.2	35.5	3.9	8.1	0.7	0	0
B	6277.8	S	413691	6242998	2.6	1.8	15.6	28.9	7.5	4.5	1.3	49	252
C	6267.3	S	413931	6242990	1.6	5.1	7.2	29.4	2.6	5.9	---	---	0
D	6177.1	S	415193	6242962	1.7	6.9	4.6	32.5	3.1	5.4	0.2	16	0
E	6151.1	S?	415748	6242949	0.1	4.3	13.7	16.2	21.5	3.1	---	---	115
F	6138.4	S	416065	6242944	2.9	8.9	12.2	27.1	8.5	4.9	---	---	0
LINE 63501			FLIGHT 37										
A	807.7	S?	396107	6243476	0.0	2.4	9.9	18.1	15.2	3.9	---	---	356
B	827.5	S	396345	6243475	8.6	3.1	13.7	10.8	18.6	2.3	---	---	0
C	1110.3	S?	400241	6243356	2.8	6.6	4.1	36.0	1.9	6.2	---	---	0
D	1410.8	S?	403956	6243271	2.6	9.8	51.9	27.2	42.0	5.0	---	---	0
E	1483.1	S	404922	6243240	3.4	8.4	21.1	52.8	2.2	10.6	---	---	0
F	1787.7	S	407843	6243161	3.8	6.4	5.5	16.5	5.2	4.8	---	---	0
G	1861.5	S?	409114	6243127	10.1	2.8	3.5	5.5	3.8	1.1	---	---	92
H	1895.2	S?	409964	6243096	7.9	11.9	55.8	71.8	80.1	11.5	---	---	125
I	1943.0	S?	410876	6243067	11.5	5.8	36.7	21.8	48.9	3.1	---	---	124
J	1963.0	S?	411173	6243070	0.0	8.2	72.9	30.7	97.3	4.9	---	---	90
LINE 63510			FLIGHT 44										
A	2837.3	S?	404916	6243109	2.5	4.6	17.2	21.6	6.6	4.1	0.5	5	0
LINE 63511			FLIGHT 44										
A	3434.6	S?	410173	6242956	0.0	10.3	27.0	70.6	0.0	10.7	---	---	0
B	3657.4	H?	413756	6242817	3.8	5.8	11.5	23.7	0.5	4.9	0.6	19	0
LINE 63513			FLIGHT 52										
A	2412.8	S	415495	6242804	2.5	5.0	6.0	27.4	3.8	5.5	---	---	52

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Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 63520			FLIGHT 48										
A	4937.8	S	404832	6242939	2.0	3.3	16.5	25.2	5.9	5.4	---	---	0
B	4740.5	S?	408108	6242857	8.0	8.2	28.8	20.5	36.4	3.2	---	---	0
C	4478.2	S?	412580	6242729	3.4	8.7	12.0	17.1	12.0	3.4	---	---	0
D	4421.1	S?	413163	6242722	5.0	1.4	11.0	29.7	5.1	5.7	---	---	0
E	4390.9	S?	413684	6242706	5.8	12.8	21.9	37.5	5.6	7.2	---	---	0
F	4372.9	S	414109	6242694	0.5	3.5	1.3	24.6	11.8	4.6	---	---	0
G	4293.4	S	415216	6242664	1.2	5.3	2.0	39.8	0.1	6.6	---	---	0
H	4270.4	S	415524	6242657	1.5	3.1	4.5	19.4	3.4	3.4	---	---	116
I	4262.6	S	415720	6242658	2.0	7.2	4.1	36.0	1.2	6.7	---	---	0
LINE 63530			FLIGHT 48										
A	5201.5	S	404769	6242792	1.4	5.1	13.2	23.0	2.7	4.8	0.2	0	0
B	5273.2	S	405719	6242760	0.9	2.6	7.4	45.8	29.7	8.4	0.2	42	41
C	5321.3	S?	406690	6242728	0.0	9.6	0.0	45.6	14.1	6.5	---	---	86
D	5338.1	S	406939	6242733	6.0	1.4	14.5	25.5	18.4	4.1	7.9	61	0
E	5366.7	S	407282	6242719	1.1	3.1	12.4	22.5	8.0	4.4	0.2	19	0
F	5471.0	S	408173	6242701	2.1	12.1	34.8	32.8	45.4	6.1	---	---	57
G	5751.9	S?	413116	6242570	0.7	8.7	15.9	38.4	13.5	7.4	---	---	0
H	5763.6	S	413359	6242565	6.8	15.3	19.1	54.0	20.9	9.4	0.5	0	0
I	5785.5	H	413725	6242552	6.6	12.8	27.6	49.8	6.5	8.9	0.6	8	0
J	5915.3	S	415270	6242494	1.9	7.8	6.0	40.0	9.2	6.2	0.2	11	0
LINE 63540			FLIGHT 49										
A	1568.4	S	404743	6242632	4.4	7.4	18.2	35.3	9.9	7.0	---	---	0
B	1520.2	S	405576	6242621	8.7	5.4	1.8	16.1	0.5	2.4	---	---	121
C	1462.2	S	406709	6242604	0.1	12.4	12.5	45.7	17.7	7.8	---	---	0
D	1341.7	S	408362	6242538	2.2	3.4	11.7	18.5	21.5	3.4	---	---	0
E	1173.5	S	411585	6242461	4.7	3.4	11.8	19.7	14.0	2.7	---	---	0
F	999.4	S?	413733	6242411	7.7	19.7	25.3	54.2	6.3	10.4	---	---	394
G	970.7	S	414283	6242396	0.2	6.1	1.0	22.4	3.3	4.3	---	---	0
H	894.9	S	415357	6242357	3.3	5.4	6.7	12.4	5.5	1.7	---	---	0
I	861.3	S	415908	6242350	3.8	3.4	3.6	17.1	5.2	3.6	---	---	28
LINE 63550			FLIGHT 49										
A	1778.4	S?	404642	6242510	3.7	6.8	26.1	27.3	24.4	5.7	0.5	16	0
B	1854.0	S	405492	6242475	4.2	6.1	10.5	21.6	15.2	3.9	---	---	39
C	1890.0	S?	405947	6242450	69.7	0.8	84.7	29.8	610.4	0.2	---	---	636

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LINE 63550		FLIGHT 49											
D	1964.0	S	407061	6242422	1.0	0.9	17.0	27.1	14.3	3.7	---	---	0
E	2293.6	S	412523	6242285	5.0	7.2	23.6	25.8	34.1	4.2	---	---	67
F	2339.4	S	413166	6242281	0.8	4.3	9.1	27.6	13.2	4.9	---	---	0
G	2417.8	S	414672	6242213	1.2	3.4	14.6	18.2	0.1	3.0	0.2	33	0
H	2479.6	S	415259	6242192	0.0	4.8	8.1	25.0	5.5	4.0	---	---	0
I	2507.1	S	415541	6242200	1.2	2.8	2.4	18.3	2.7	3.9	---	---	37
LINE 63560		FLIGHT 49											
A	3291.1	S?	404559	6242336	16.3	26.8	45.1	94.2	41.6	17.0	0.9	0	0
B	3156.5	S	406828	6242289	0.1	3.4	12.1	20.6	15.4	3.3	---	---	0
C	3130.1	D	407262	6242290	12.4	18.1	69.4	78.5	10.9	24.0	1.0	3	0
D	3080.6	D	408227	6242249	8.5	5.2	13.3	32.9	17.8	5.4	---	---	667
E	3054.9	S?	408625	6242243	12.8	3.0	0.0	15.5	0.0	2.4	---	---	669
F	3032.9	S?	408959	6242229	0.0	8.5	71.3	9.8	96.8	2.3	---	---	0
G	2965.7	S	410373	6242186	0.9	1.8	3.0	21.4	5.4	4.1	---	---	0
H	2835.5	S	412544	6242144	0.7	0.8	15.7	17.8	22.2	4.0	---	---	23
I	2794.9	S	412920	6242136	1.0	2.2	7.9	17.3	11.0	3.0	---	---	435
J	2762.8	S	413581	6242097	4.0	5.3	22.1	37.3	0.7	8.0	---	---	0
LINE 63570		FLIGHT 49											
A	3733.8	S	407353	6242115	4.5	17.5	8.9	62.2	13.1	10.7	0.3	0	0
B	3746.5	H	407617	6242111	5.5	2.9	19.7	18.2	3.6	7.1	2.4	50	0
C	4073.5	S	413643	6241949	1.8	8.6	42.4	56.3	18.3	11.8	0.2	0	0
D	4114.7	S	414516	6241917	0.4	3.1	2.8	25.7	1.8	5.1	---	---	0
E	4175.0	S	415208	6241901	11.4	1.9	30.3	15.3	38.8	2.2	---	---	426
F	4220.5	S	415780	6241892	3.6	7.1	19.5	25.3	24.9	6.1	---	---	163
LINE 63580		FLIGHT 49											
A	4842.4	S	407652	6241958	4.7	9.9	24.1	38.7	19.8	6.9	---	---	0
B	4813.0	S	408362	6241951	16.5	9.1	59.4	29.0	82.2	4.9	---	---	538
C	4585.5	S	412255	6241845	0.8	3.7	48.1	15.0	49.7	2.7	---	---	0
D	4569.5	S?	412374	6241850	9.7	4.5	44.6	23.9	63.0	4.8	---	---	426
E	4495.7	S?	413193	6241821	2.0	3.5	41.8	17.8	55.2	3.3	---	---	303
F	4467.6	H?	413712	6241814	2.9	11.1	23.9	66.9	2.4	12.7	---	---	434
G	4432.9	S?	414462	6241776	2.3	5.3	1.2	21.1	0.0	3.8	---	---	387
H	4410.2	S	414827	6241770	4.7	4.5	10.7	28.9	13.6	5.3	---	---	0
I	4357.7	S?	415630	6241748	6.6	14.2	31.2	44.5	33.1	7.9	---	---	0

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 63590			FLIGHT 49										
A	5470.7	S	407422	6241820	1.2	3.1	6.0	22.5	10.7	4.9	0.3	28	77
B	5529.0	S?	408699	6241786	0.9	1.7	18.6	7.9	25.2	1.6	---	---	334
C	5747.3	S?	412743	6241681	1.9	2.6	32.9	9.0	59.0	2.7	0.5	59	0
D	5808.7	S	413728	6241656	3.1	5.2	32.5	54.4	11.8	10.1	0.5	34	334
E	5871.3	S	414918	6241611	0.4	4.3	7.8	22.4	13.6	3.8	0.1	0	0
F	5924.0	S	415654	6241601	11.0	20.7	16.7	51.9	14.6	6.3	0.7	5	0
LINE 63600			FLIGHT 49										
A	6765.5	S	406034	6241706	2.0	5.2	4.0	20.8	2.2	4.1	---	---	0
B	6741.0	S?	406369	6241708	0.5	4.9	13.4	27.3	0.5	6.1	---	---	0
C	6677.3	S?	407515	6241680	0.0	6.2	9.5	37.6	9.4	6.9	---	---	40
D	6607.2	S?	408924	6241629	0.1	1.5	10.2	16.1	14.4	2.5	---	---	375
E	6574.7	S?	409498	6241624	0.2	3.8	19.6	16.4	29.6	3.0	---	---	0
F	6549.6	S	409892	6241596	8.2	2.6	12.2	9.0	7.8	1.2	---	---	0
G	6400.5	S	412179	6241561	0.5	2.6	12.8	17.1	25.4	2.4	---	---	0
H	6380.4	S?	412532	6241536	2.0	2.0	11.4	20.1	14.5	3.7	---	---	177
I	6278.2	S	413823	6241504	1.9	5.0	28.5	31.4	5.0	6.4	---	---	201
J	6170.4	S	415649	6241441	1.5	4.4	9.7	21.7	13.7	3.6	---	---	0
LINE 63610			FLIGHT 50										
A	1067.9	S	413940	6241344	3.2	7.2	17.4	50.4	31.8	9.7	---	---	110
B	1001.8	S	415025	6241310	2.1	2.8	13.4	12.8	19.3	3.0	---	---	150
C	960.3	S?	415599	6241300	0.4	6.7	3.3	25.0	10.5	5.1	---	---	56
LINE 63620			FLIGHT 50										
A	1488.8	S	412270	6241234	3.3	6.1	4.7	25.6	8.7	5.1	---	---	0
B	1603.3	S	413915	6241196	5.5	10.1	32.1	52.8	27.0	10.4	---	---	0
C	1711.2	S	415768	6241142	3.0	3.7	18.2	15.3	20.5	2.8	---	---	0
LINE 63630			FLIGHT 50										
A	2131.6	S	412406	6241104	1.6	1.9	9.0	29.7	12.0	4.9	---	---	40
B	1993.8	S	414075	6241040	2.0	12.0	20.5	73.1	15.8	13.7	---	---	0
LINE 63640			FLIGHT 50										
A	2575.0	S?	414162	6240899	0.0	13.5	16.9	117.6	22.2	22.4	---	---	300
B	2674.3	S	415794	6240840	2.1	4.5	7.2	18.5	12.1	2.8	---	---	0

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LINE 63650			FLIGHT 50										
A	2913.4	D	413826	6240742	2.2	5.3	10.3	23.9	6.9	4.0	0.4	3	0
B	2895.5	D	414057	6240736	15.1	21.3	88.8	81.3	29.0	21.7	1.1	15	0
C	2889.7	B?	414178	6240737	10.9	32.6	88.8	138.9	29.0	34.2	0.5	0	275
D	2850.1	S	415141	6240714	3.5	3.3	13.4	21.7	16.3	4.2	---	---	0
LINE 63660			FLIGHT 50										
A	3359.9	D	414255	6240602	14.9	27.9	45.9	87.7	0.5	20.3	0.8	5	0
B	3409.3	S	415518	6240538	1.1	4.9	6.5	33.5	1.6	5.8	---	---	181
LINE 63670			FLIGHT 51										
A	2587.4	S	414050	6240460	3.8	4.4	9.3	27.3	11.6	5.9	0.8	38	0
B	2635.8	S?	414754	6240418	0.0	4.4	26.6	23.3	34.2	3.5	---	---	40
C	2680.4	S	415819	6240393	0.4	5.7	17.0	34.9	18.3	5.8	0.1	8	0
LINE 63690			FLIGHT 51										
A	3995.3	S	413610	6240159	1.2	6.8	7.2	31.4	10.2	4.2	0.1	9	127
B	3973.5	S?	413927	6240147	1.5	4.2	30.3	27.1	1.9	5.4	---	---	48
C	3836.0	S	416157	6240091	2.8	6.2	6.4	19.1	6.9	2.8	---	---	14
LINE 63700			FLIGHT 37										
A	6626.1	S	413538	6240011	2.8	5.1	4.4	18.1	3.4	3.9	---	---	0
B	6788.6	S	416189	6239928	2.2	2.2	0.1	21.0	0.4	4.2	---	---	0
C	6827.7	S	416517	6239921	5.5	3.6	5.0	23.1	6.9	3.8	---	---	0
LINE 63710			FLIGHT 37										
A	6108.4	H?	413796	6239843	2.3	1.5	38.8	12.8	22.7	16.5	---	---	90
LINE 63730			FLIGHT 37										
A	5004.8	S	413473	6239575	4.0	7.0	22.8	17.3	20.2	4.2	0.5	15	0
LINE 63740			FLIGHT 37										
A	4478.6	H?	413571	6239401	2.1	1.2	18.7	33.4	4.8	8.4	1.5	70	14
B	4676.0	S	415907	6239335	4.6	3.2	12.8	20.8	14.2	3.0	---	---	0
LINE 63750			FLIGHT 37										
A	3937.8	D	413543	6239251	4.3	9.4	31.6	45.5	13.7	14.0	---	---	20
B	3724.4	S	415962	6239192	0.9	1.7	2.5	18.3	2.6	2.8	---	---	0

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LINE 63760			FLIGHT 37										
A	3063.1	S	411359	6239164	1.0	4.3	6.6	10.9	11.6	5.3	---	---	0
B	3121.8	S?	412037	6239156	2.6	7.3	8.5	20.1	9.8	2.6	---	---	0
C	3229.2	B?	413411	6239109	23.5	20.1	112.6	73.8	33.9	51.0	2.1	0	0
LINE 63770			FLIGHT 37										
A	2757.2	B?	413418	6238959	7.1	13.7	36.1	60.3	13.7	17.7	---	---	13
LINE 63780			FLIGHT 34										
A	3641.8	S	412239	6238837	4.6	3.3	3.9	17.4	1.6	2.7	---	---	30
B	3710.0	S	413392	6238823	6.4	8.6	12.8	42.8	7.1	8.9	---	---	13
LINE 63790			FLIGHT 34										
A	3169.5	S	413478	6238655	2.6	9.3	17.0	52.0	8.4	8.7	---	---	0
B	2954.0	S?	416145	6238592	2.2	5.1	7.7	8.7	6.8	1.8	---	---	0
LINE 63800			FLIGHT 34										
A	2613.0	S	413292	6238514	1.8	4.6	6.8	17.5	12.6	4.1	---	---	15
B	2622.1	S	413506	6238512	2.9	4.8	10.3	24.8	12.6	3.7	---	---	15
LINE 63810			FLIGHT 34										
A	2149.8	S	413587	6238351	4.0	6.7	10.1	56.9	1.5	9.7	---	---	22
B	2119.9	S	414118	6238343	3.0	3.9	7.8	13.6	9.1	2.8	---	---	0
LINE 63820			FLIGHT 34										
A	1619.3	S	413474	6238209	4.2	8.8	11.8	50.4	15.4	8.6	---	---	0
LINE 63830			FLIGHT 34										
A	1137.0	S	413551	6238060	4.3	8.9	17.5	76.0	5.1	12.6	---	---	0
LINE 63840			FLIGHT 33										
A	6028.3	S	413611	6237914	1.0	8.5	15.6	86.1	0.8	14.7	---	---	0
LINE 63850			FLIGHT 33										
A	5572.0	S	413662	6237747	0.8	15.4	13.3	84.7	19.1	13.7	---	---	28
LINE 63860			FLIGHT 33										
A	5091.9	S	413367	6237615	1.1	3.2	5.6	28.7	14.1	4.8	---	---	0

CX = COAXIAL
CP = COPLANAR

Note:EM values shown above are local amplitudes

*Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 63860			FLIGHT 33										
B	5101.0	S	413626	6237599	0.9	6.2	1.0	41.9	13.7	7.4	---	---	0
LINE 63870			FLIGHT 33										
A	4486.3	S	413370	6237467	2.2	7.4	18.4	23.3	26.7	4.1	---	---	224
B	4475.6	S	413685	6237446	0.3	7.4	0.0	48.3	6.1	8.1	---	---	18
LINE 63880			FLIGHT 33										
A	3888.2	S?	412403	6237334	1.2	4.6	0.6	21.6	0.6	3.5	---	---	0
B	3965.0	S	413442	6237302	3.7	12.4	11.7	47.0	16.5	7.9	---	---	161
C	3977.9	S	413809	6237295	2.9	9.1	19.9	37.2	29.0	5.7	---	---	106
D	4034.7	S?	414762	6237268	2.7	5.3	0.4	24.4	2.1	3.8	---	---	437
LINE 63890			FLIGHT 33										
A	3402.3	S	413508	6237156	2.5	9.8	19.1	21.0	30.6	3.3	---	---	78
B	3389.9	S	413836	6237148	2.4	6.8	10.8	25.9	11.5	4.2	---	---	78
C	3344.3	S?	414696	6237127	0.0	2.5	33.1	14.2	47.5	1.9	---	---	1155
LINE 63900			FLIGHT 33										
A	2782.7	S	413525	6237012	1.9	7.1	4.2	34.1	2.6	5.1	---	---	212
B	2796.9	S	413891	6237005	0.0	6.5	37.4	25.3	57.0	4.3	---	---	58
LINE 63910			FLIGHT 33										
A	2309.6	S?	413607	6236840	1.1	7.6	0.2	29.4	1.3	4.2	---	---	134
LINE 63920			FLIGHT 33										
A	1838.4	S?	413574	6236704	5.8	9.7	0.9	56.2	2.4	9.5	---	---	113
B	1845.6	S?	413735	6236702	9.3	7.6	20.4	28.3	32.3	4.0	---	---	0
LINE 63930			FLIGHT 33										
A	1264.5	S?	413651	6236547	4.9	7.3	20.1	49.3	21.9	7.4	---	---	0
B	1249.2	S?	414101	6236537	6.1	0.3	35.0	4.3	35.6	1.2	---	---	0
LINE 63940			FLIGHT 33										
A	808.8	S?	413610	6236395	1.6	8.2	64.0	56.1	81.3	8.4	---	---	408
B	814.2	S?	413730	6236394	16.8	5.3	64.0	66.9	84.0	10.6	---	---	0
C	859.3	S?	414580	6236382	1.7	6.4	3.3	25.0	3.5	3.6	---	---	179
D	975.4	S	415800	6236349	2.8	6.3	2.8	18.3	2.8	2.6	---	---	14

CX = COAXIAL
CP = COPLANAR

Note:EM values shown above are local amplitudes

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 63950			FLIGHT 31										
A	6277.8	S	413778	6236243	1.4	5.1	8.5	42.1	6.6	7.2	---	---	0
B	6215.2	S?	415143	6236208	2.3	4.2	0.8	15.3	1.0	3.0	---	---	0
C	6178.4	S	415688	6236194	4.1	5.5	8.8	16.1	7.9	2.9	---	---	0
D	6165.5	S	415855	6236199	4.8	5.2	12.1	17.5	9.8	2.5	1.0	35	0
LINE 63960			FLIGHT 31										
A	5808.9	S	413730	6236100	0.5	5.0	11.6	25.2	0.0	4.2	---	---	129
B	5900.4	S	415409	6236046	2.8	4.9	8.1	13.8	6.0	2.2	0.5	28	0
C	5922.5	S	415815	6236042	3.5	5.9	5.1	14.5	7.4	2.4	0.6	23	0
LINE 63970			FLIGHT 31										
A	5392.4	D	412501	6235983	7.2	13.2	16.1	18.1	9.6	5.6	0.6	12	0
B	5324.9	S?	414175	6235940	3.7	5.0	0.5	33.0	15.9	5.0	---	---	0
C	5244.2	B?	415711	6235896	2.7	10.7	2.5	25.5	3.3	4.8	0.2	0	0
LINE 63980			FLIGHT 31										
A	4947.7	S?	414118	6235780	0.0	6.3	0.0	53.9	0.0	8.2	---	---	0
B	5028.3	S	415618	6235738	4.0	4.9	20.9	24.4	12.4	4.6	0.8	28	0
LINE 63990			FLIGHT 31										
A	4704.0	S	413308	6235663	0.7	2.8	3.9	26.1	6.4	3.6	---	---	0
B	4669.7	S	414347	6235624	1.9	3.1	11.5	39.5	7.7	6.7	---	---	0
C	4570.0	S?	416204	6235585	2.7	2.3	25.4	9.6	34.7	2.4	---	---	0
LINE 64000			FLIGHT 31										
A	4235.7	S	414298	6235475	2.8	9.0	3.9	60.3	9.1	9.4	---	---	0
B	4340.1	S?	416327	6235415	0.0	8.4	80.0	20.4	96.1	2.6	---	---	522
LINE 64010			FLIGHT 31										
A	3832.4	S	414440	6235329	4.0	10.0	5.3	56.4	3.0	9.4	---	---	29
B	3766.3	S?	415685	6235310	3.2	20.3	30.6	95.9	7.2	15.9	---	---	62
C	3761.4	S	415821	6235307	9.5	17.4	30.6	46.4	7.2	10.3	---	---	0
D	3745.2	S?	416196	6235293	0.0	10.2	17.1	32.0	20.5	5.6	---	---	120
LINE 64020			FLIGHT 31										
A	3405.1	S?	413479	6235196	1.1	1.7	5.4	16.6	21.0	3.4	---	---	38
B	3458.7	S	414483	6235175	3.0	12.8	24.6	88.0	17.2	14.5	---	---	0

CX = COAXIAL
CP = COPLANAR

Note:EM values shown above are local amplitudes

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EM Anomaly List

Label	Fid	Interp	XUTM m	YUTM m	CX 5500 HZ Real ppm	CX 5500 HZ Quad ppm	CP 7200 HZ Real ppm	CP 7200 HZ Quad ppm	CP 900 HZ Real ppm	CP 900 HZ Quad ppm	Vertical Dike COND siemens	Vertical Dike DEPTH* m	Mag. Corr NT
LINE 64020			FLIGHT 31										
C	3517.4	S	415661	6235140	3.4	16.3	17.1	50.6	10.3	8.1	---	---	0
D	3524.6	B?	415854	6235137	6.4	19.3	17.1	63.3	14.6	10.2	---	---	0
E	3537.3	S?	416134	6235130	0.5	3.5	24.2	25.4	34.0	5.5	---	---	282
LINE 64030			FLIGHT 31										
A	2867.2	S	414587	6235025	4.5	15.8	19.2	80.9	16.6	12.9	---	---	0
B	2808.3	S	415780	6234989	5.9	4.4	24.8	67.9	43.3	10.4	---	---	11
C	2780.0	S	416324	6234970	0.0	11.9	10.2	31.7	60.0	4.9	---	---	128
LINE 64041			FLIGHT 51										
A	4827.1	S?	414058	6234887	0.0	4.4	11.2	21.8	8.8	3.8	---	---	133
B	4858.3	S	414618	6234874	1.7	20.5	21.6	101.9	13.2	16.4	---	---	0
C	4910.7	S	415702	6234839	0.9	7.3	8.0	16.5	12.4	2.6	---	---	0

CX = COAXIAL
CP = COPLANAR

Note:EM values shown above
are local amplitudes

*Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

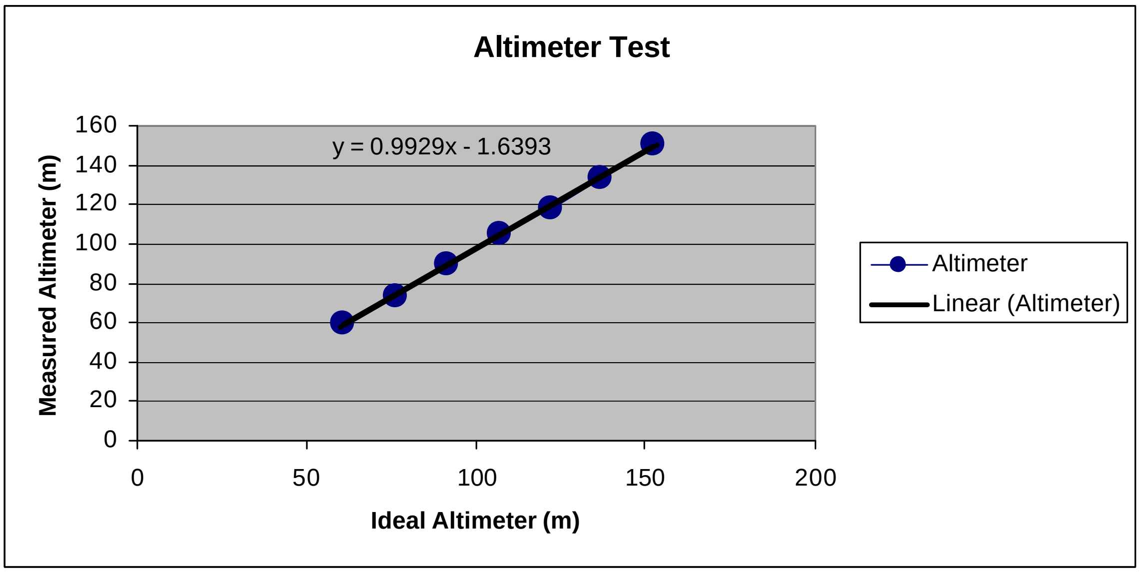
APPENDIX F

TESTS AND CALIBRATIONS

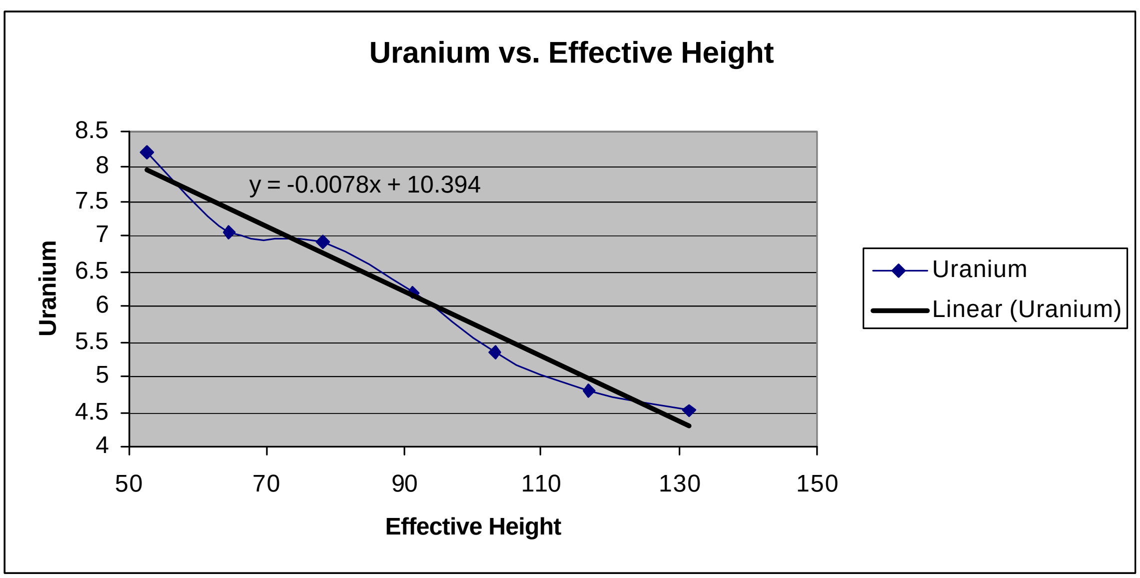
APPENDIX F

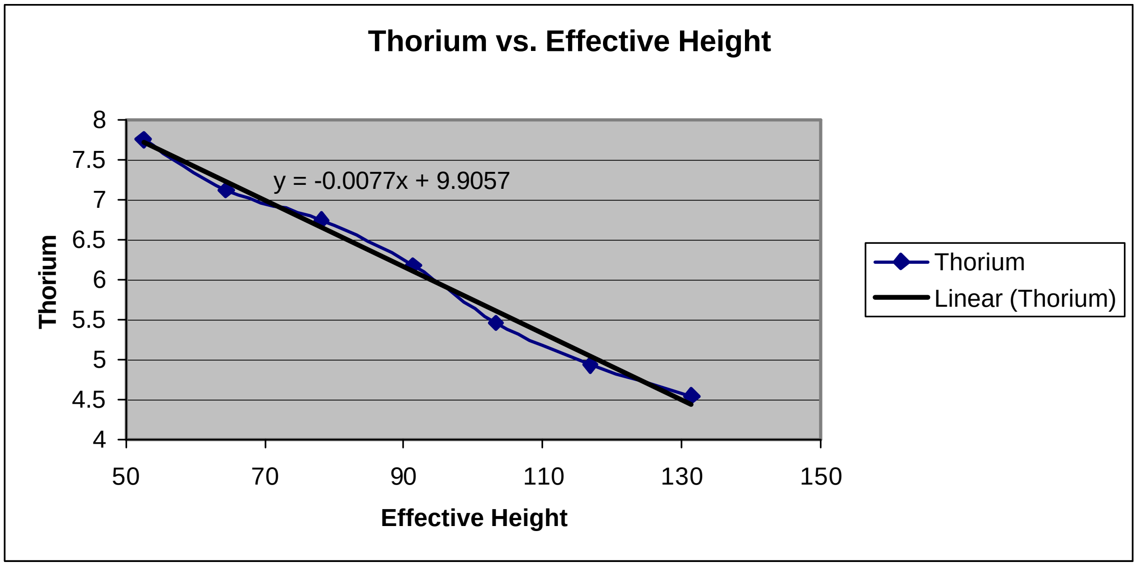
TESTS AND CALIBRATIONS (2006 Phase)

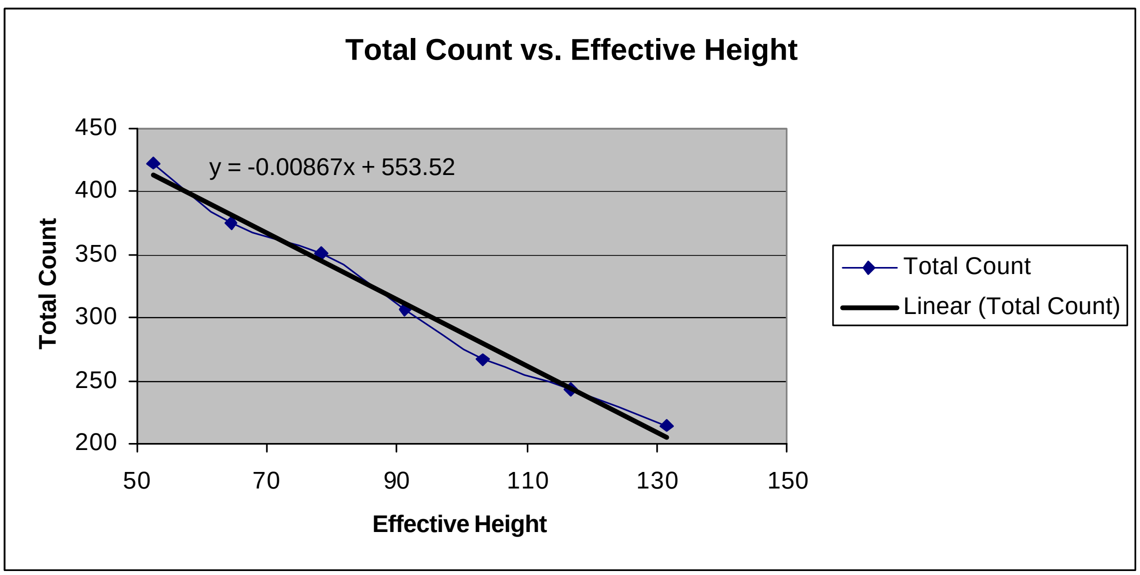
ALTIMETER TEST

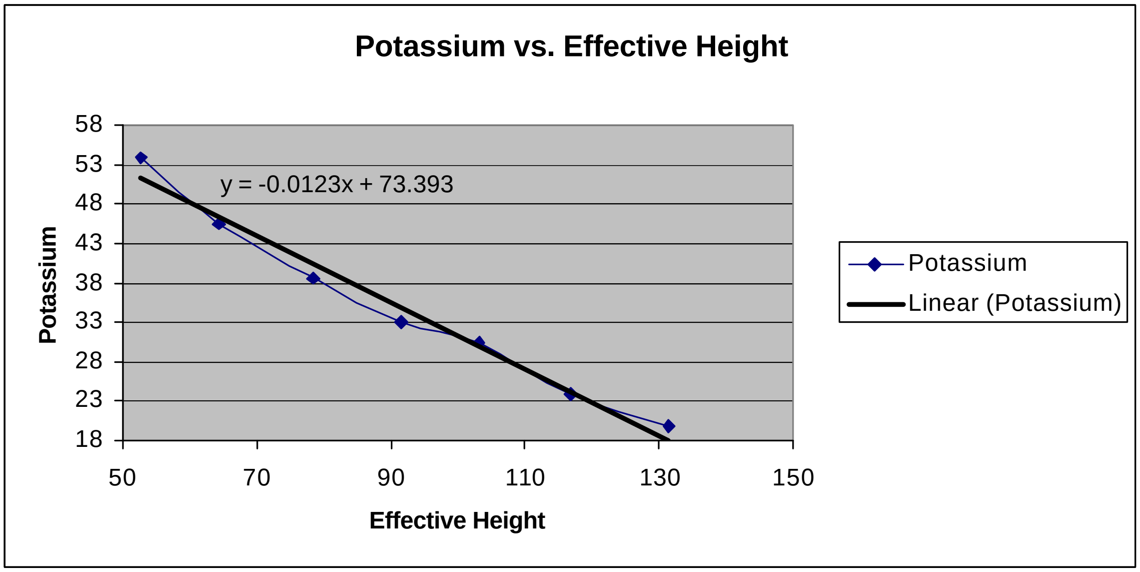


ALTITUDE ATTENUATION TESTS

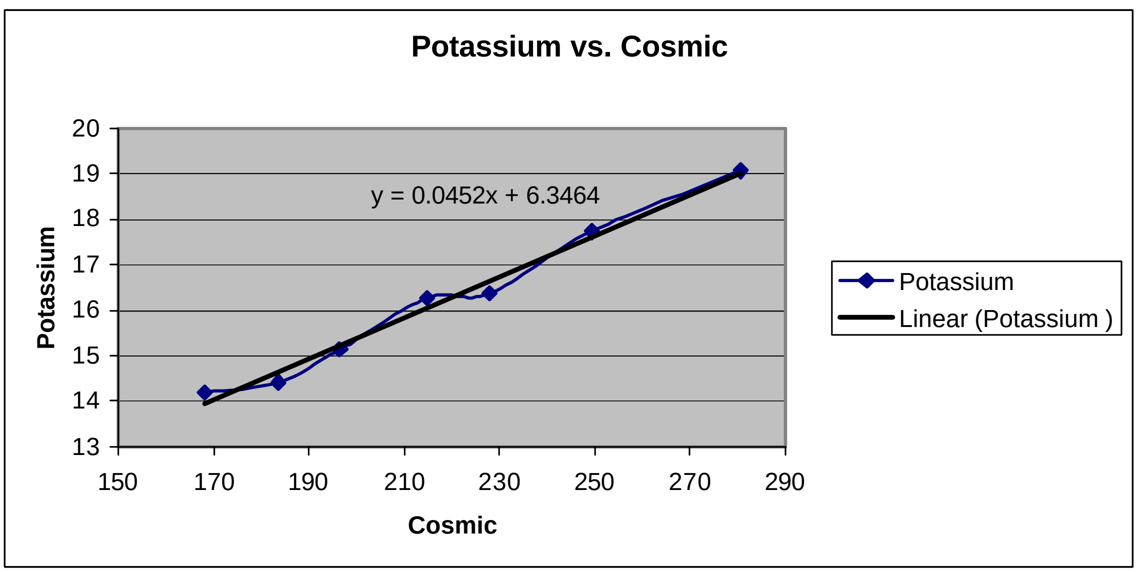



Thorium vs. Effective Height
y = -0.0077x + 9.9057
Thorium
8
7.5
7
6.5
6
5.5
5
4.5
4
50
70
90
110
130
150
Effective Height
Thorium
Linear (Thorium)

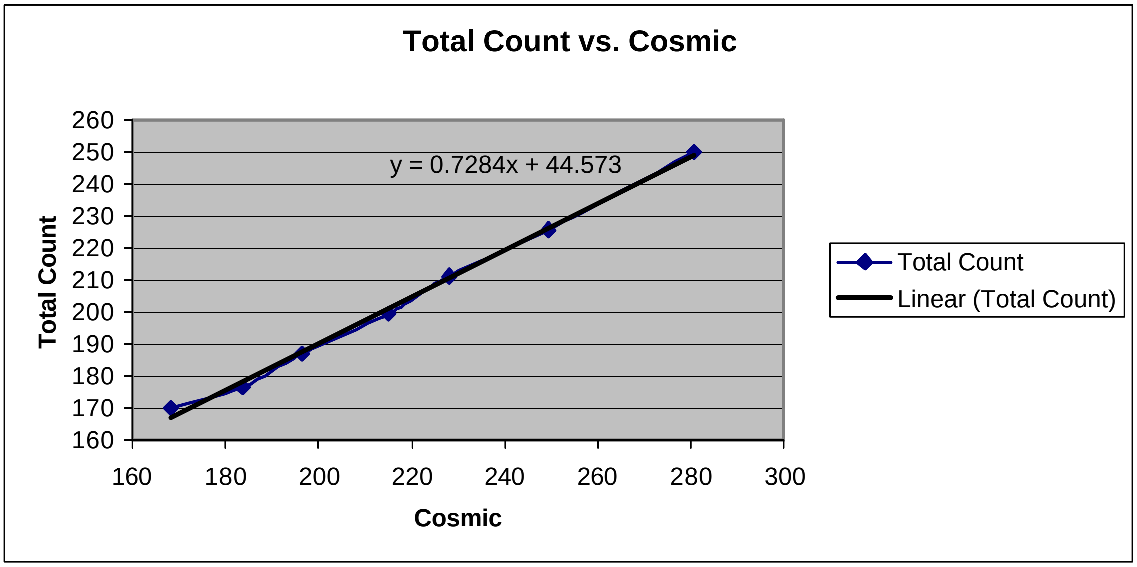

Total Count vs. Effective Height
y = -0.00867x + 553.52
Total Count
450
400
350
300
250
200
50
70
90
110
130
150
Effective Height
Total Count
Linear (Total Count)

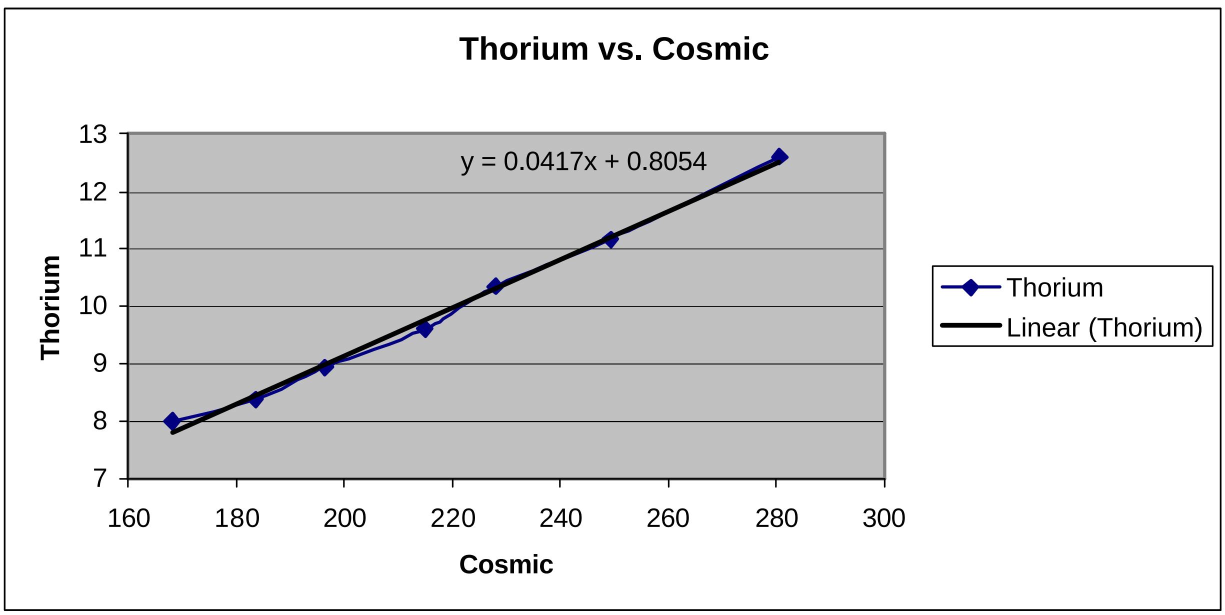


COSMIC TESTS

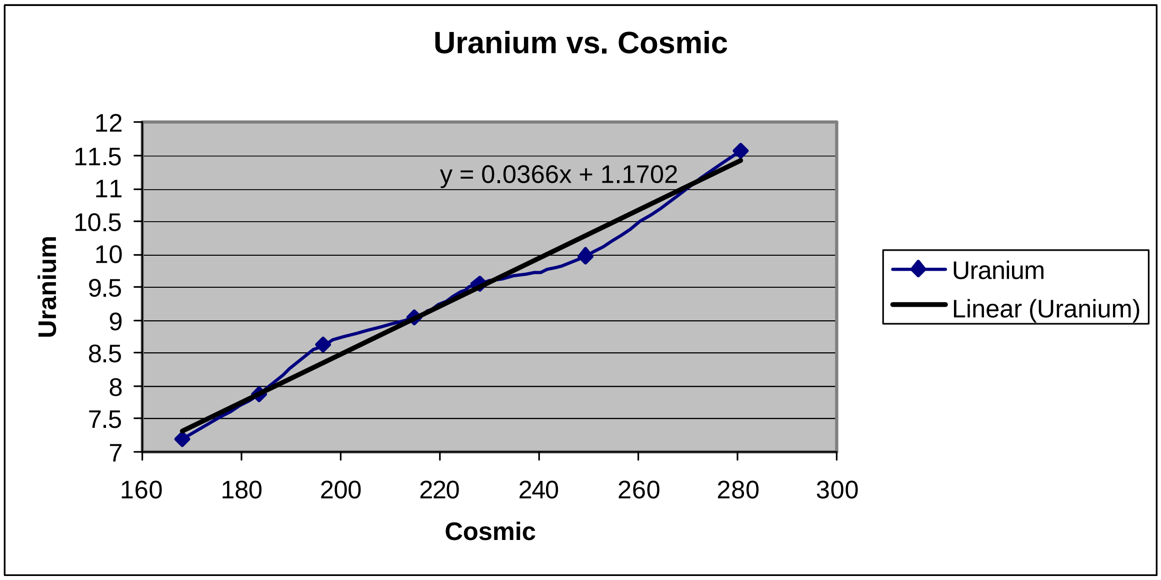


- Appendix F.4 -

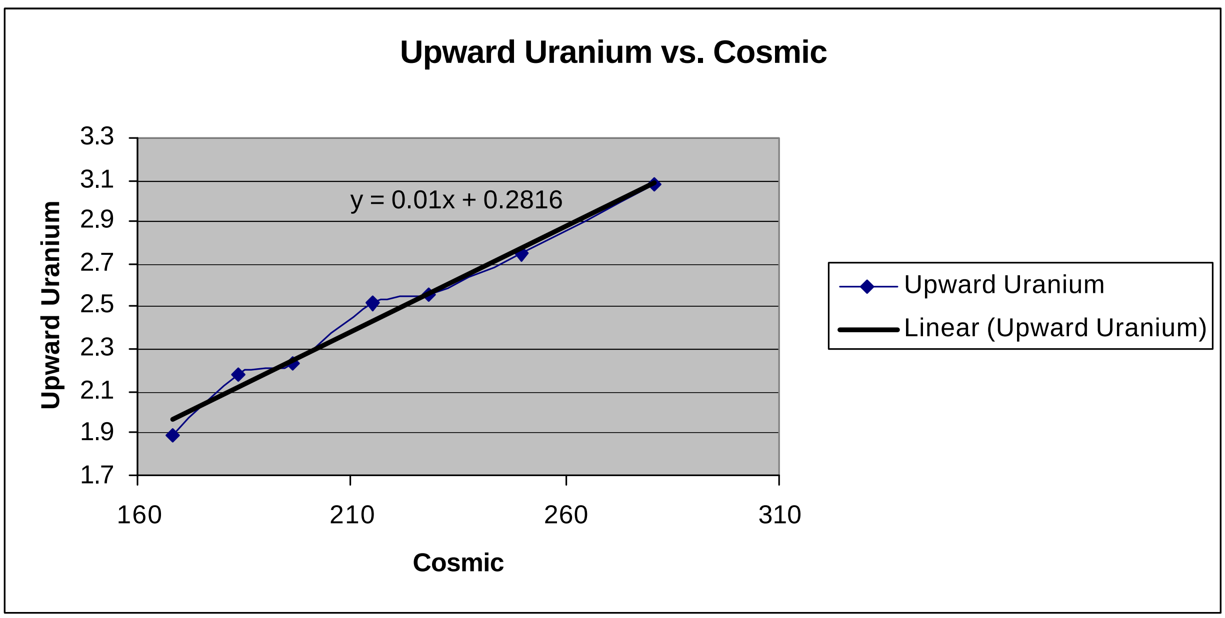

Total Count vs. Cosmic
260
250
240
230
220
210
200
190
180
170
160
Total Count
y = 0.7284x + 44.573
160
180
200
220
240
260
280
300
Cosmic
Total Count
Linear (Total Count)


Thorium vs. Cosmic
13
12
11
10
9
8
7
Thorium
y = 0.0417x + 0.8054
160
180
200
220
240
260
280
300
Cosmic
Thorium
Linear (Thorium)

- Appendix F.5 -



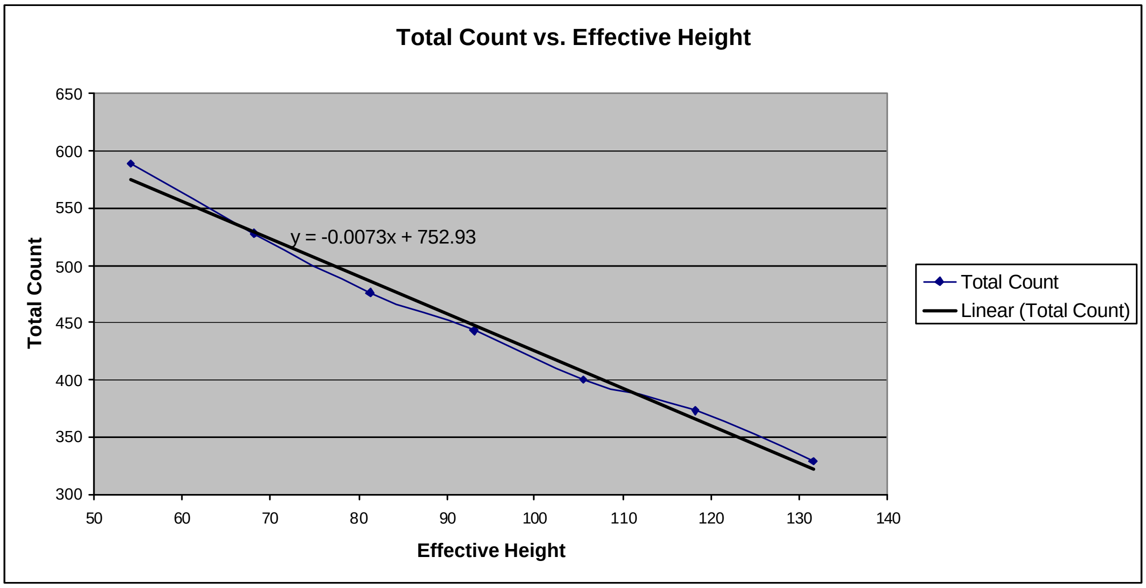
Uranium vs. Cosmic
y = 0.0366x + 1.1702
Uranium
Cosmic
12
11.5
11
10.5
10
9.5
9
8.5
8
7.5
7
160
180
200
220
240
260
280
300
Uranium
Linear (Uranium)

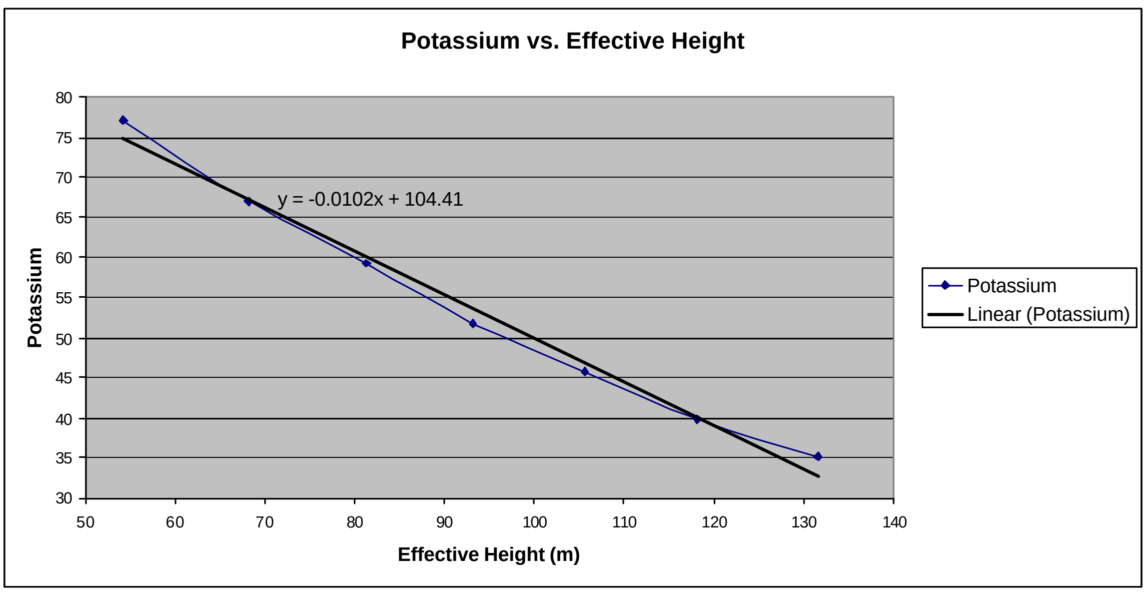


Upward Uranium vs. Cosmic
y = 0.01x + 0.2816
Upward Uranium
Cosmic
3.3
3.1
2.9
2.7
2.5
2.3
2.1
1.9
1.7
160
210
260
310
Upward Uranium
Linear (Upward Uranium)

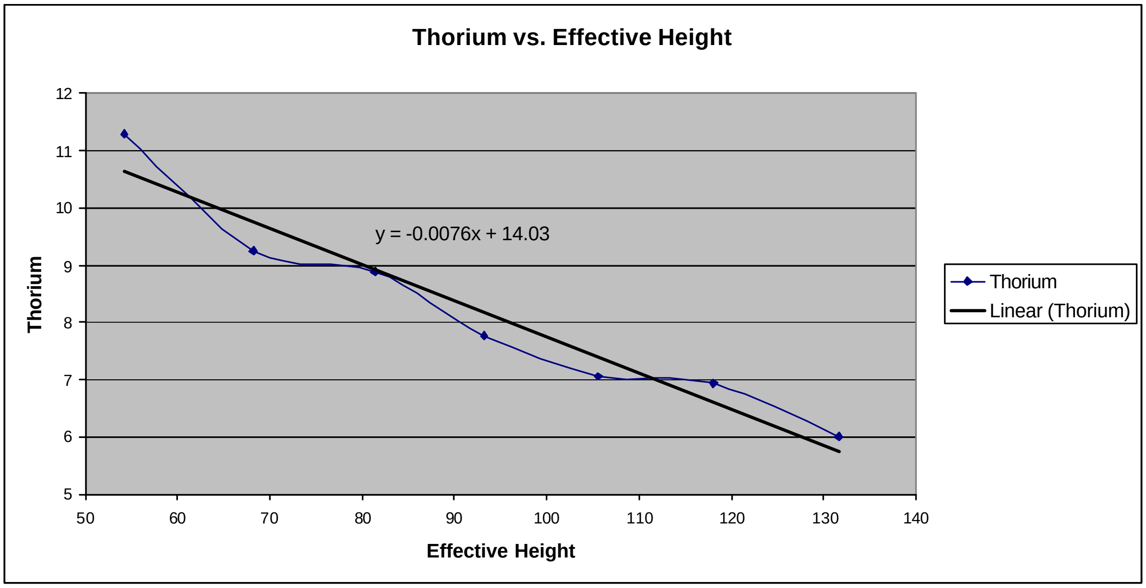
TESTS AND CALIBRATIONS (2007 Phase)

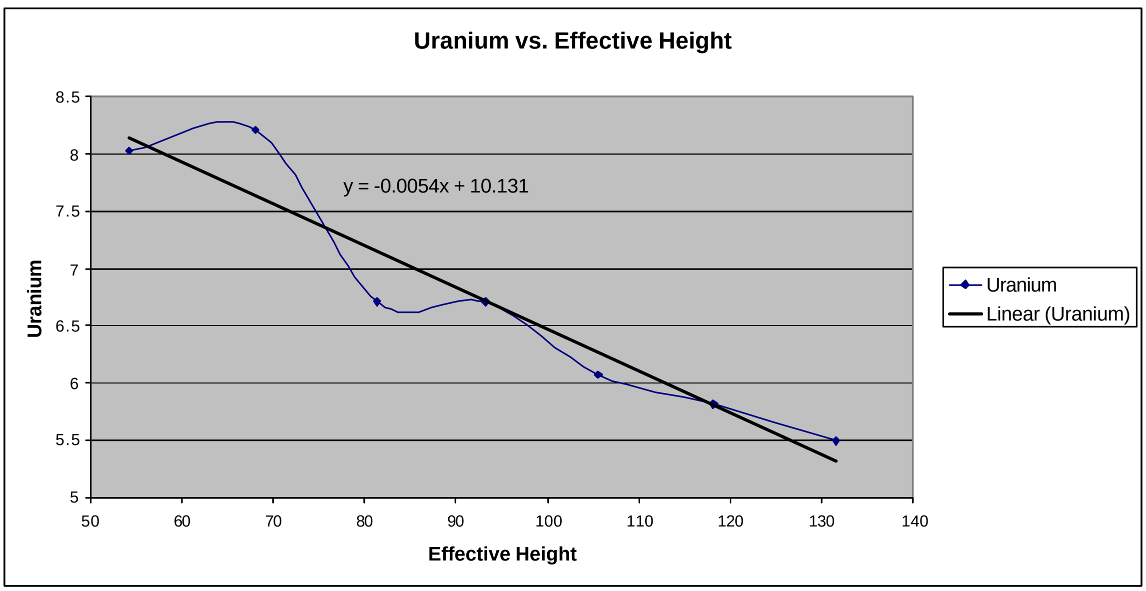
ALTITUDE ATTENUATION TESTS



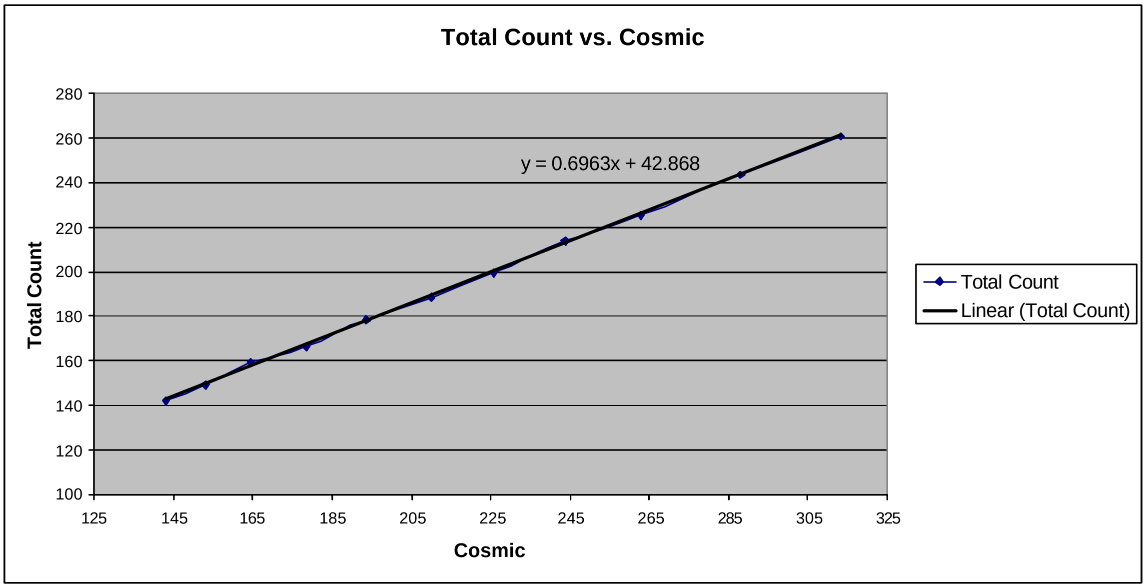


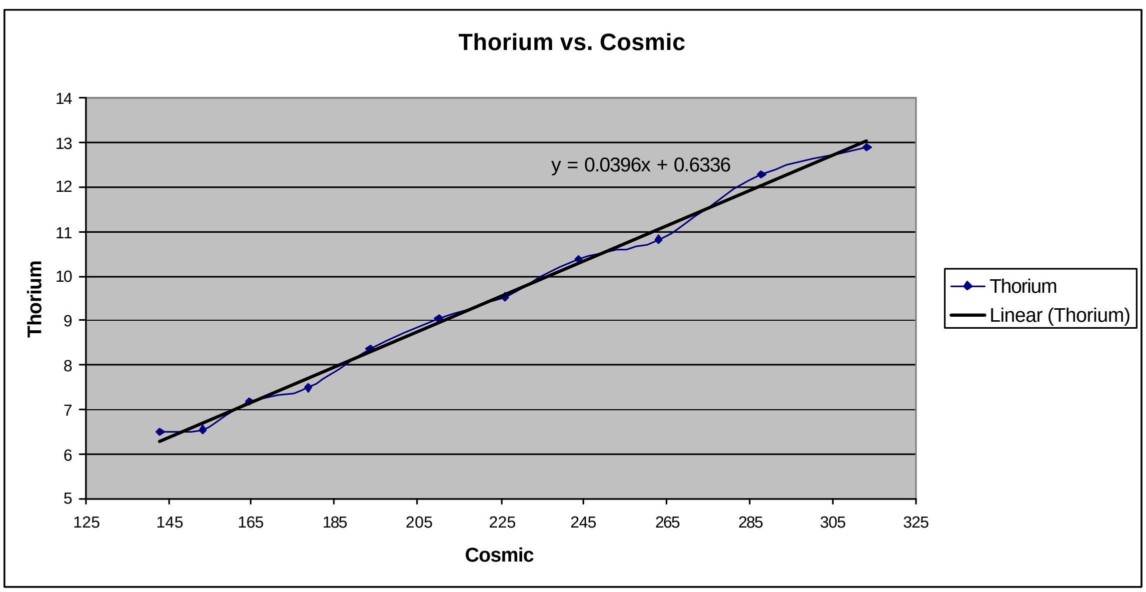
- Appendix F.7 -


Thorium vs. Effective Height
y = -0.0076x + 14.03
Thorium
Effective Height
12
11
10
9
8
7
6
5
50
60
70
80
90
100
110
120
130
140
Thorium
Linear (Thorium)

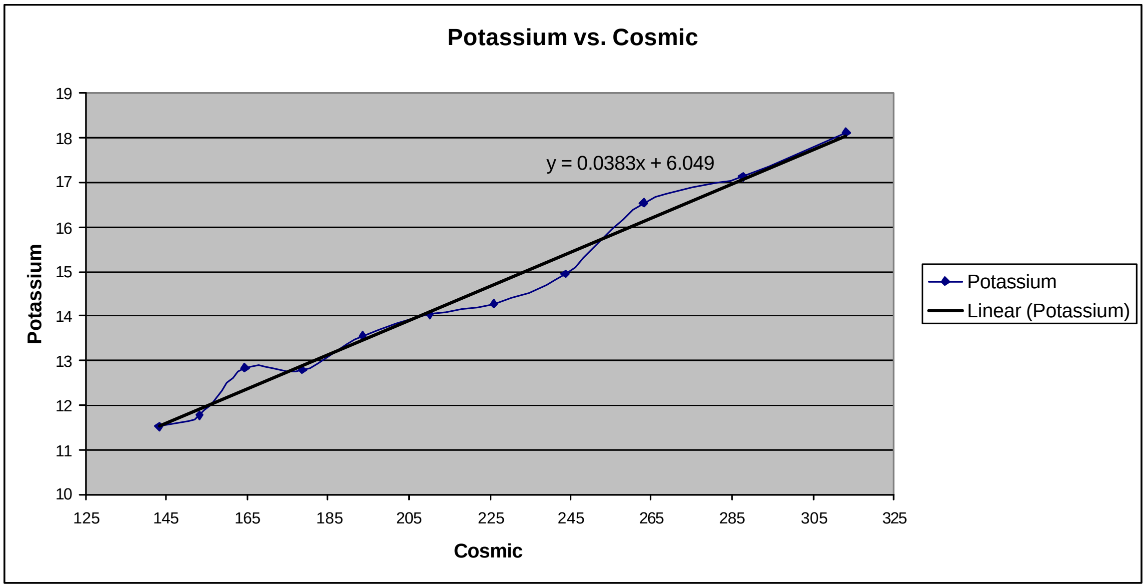

Uranium vs. Effective Height
y = -0.0054x + 10.131
Uranium
Effective Height
8.5
8
7.5
7
6.5
6
5.5
5
50
60
70
80
90
100
110
120
130
140
Uranium
Linear (Uranium)

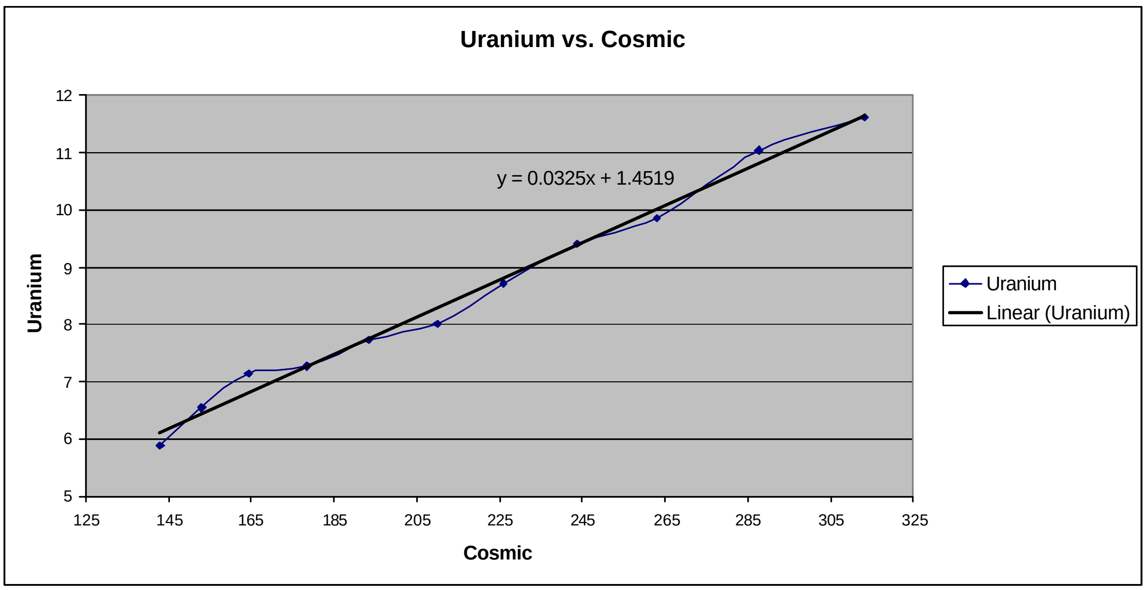
COSMIC TESTS

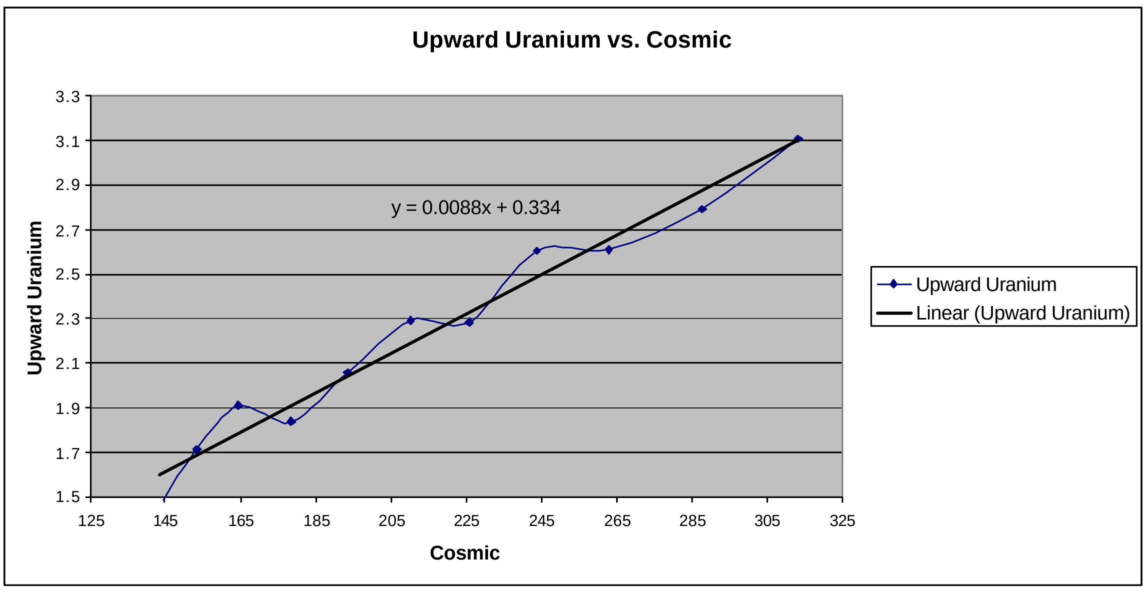




- Appendix F.9 -


Potassium vs. Cosmic
y = 0.0383x + 6.049
Potassium
Cosmic
Potassium
Linear (Potassium)
19
18
17
16
15
14
13
12
11
10
125
145
165
185
205
225
245
265
285
305
325


Uranium vs. Cosmic
y = 0.0325x + 1.4519
Uranium
Cosmic
Uranium
Linear (Uranium)
12
11
10
9
8
7
6
5
125
145
165
185
205
225
245
265
285
305
325



Upward Uranium vs. Cosmic
y = 0.0088x + 0.334
Upward Uranium
Cosmic
3.3
3.1
2.9
2.7
2.5
2.3
2.1
1.9
1.7
1.5
125
145
165
185
205
225
245
265
285
305
325
Upward Uranium
Linear (Upward Uranium)

APPENDIX G

RADIOMETRIC PROCESSING CONTROL FILE

APPENDIX G

RADIOMETRIC PROCESSING CONTROL FILE (2006 Phase)

```
///////////////////////////////////////////////////
 Atlas Control/Workspace File
///////////////////////////////////////////////////

CONTROL_BEGIN

  PROGRAM  = AGSCorrection
  VERSION  = 1.4.0


   ### Corrections to apply ###
       CorrectionType = Yes  Filtering
       CorrectionType = Yes  LiveTimeCorrection
       CorrectionType = Yes  CosmicAircraftBGRemove
       CorrectionType = Yes  CalcEffectiveHeight
       CorrectionType = No   RadonBGRemove
       CorrectionType = Yes  ComptonStripping
       CorrectionType = Yes  HeightCorrection
       CorrectionType = No   ConvertToConcentration


   ### Main I/O settings ###
       MainChannelIO|TC       = TC_DOWN    --> TC_1
       MainChannelIO|K        = K_DOWN     --> K_1
       MainChannelIO|U        = U_DOWN     --> U_1
       MainChannelIO|Th       = TH_DOWN    --> TH_1
       MainChannelIO|UpU      = U_UP       --> U_UP_1
       MainChannelIO|Cosmic   = COSMIC     --> COSMIC_1
       MainChannelIO|Spectrum = GR820_DOWN --> GR820_DOWN_1

   ### Control Channel I/O settings ###
       ControlChannel|RadarAltimeter     = ALTRAD_MT   [metres]
       ControlChannel|Pressure/Barometer = KPA         [kPa]
       ControlChannel|Temperature        = TEMP_EXT


   ### Input for correction ###
       InputForCorrection    = ROIs


   ### Pre-filtering settings ###
       Filtering|TC      = 0
       Filtering|K       = 0
       Filtering|U       = 0
       Filtering|Th      = 0
```

```
    Filtering|UpU     = 0
    Filtering|Cosmic  = 9
    Filtering|RadarAltimeter     = 3
    Filtering|Pressure/Barometer = 3
    Filtering|Temperature        = 3

### Live-time correction settings ###
    LiveTimeChannel             = LIVE_TIME
    LiveTimeUnits               = milli-seconds
    ApplyLiveTimeCorrToUpU      = Yes

### Cosmic correction settings ###
    CosmicCorrParam|TC      = 0.728377,  44.5732
    CosmicCorrParam|K       = 0.045203,  6.34639
    CosmicCorrParam|U       = 0.036585,  0.88524
    CosmicCorrParam|Th      = 0.041705,  0.225439
    CosmicCorrParam|UpU     = 0.009999,  0.281611
    CosmicCorrParam|SpectrumBackgroundFile    =

### Effective-Height settings ###
    EffectiveHeightOutputChannel = EffectiveHeight
    EffectiveHeightOutputUnits   = metres

### Special Stripping (Compton Stripping) ###
    ComptonCorrParam_Stripping_Alpha     = 0.235000
    ComptonCorrParam_Stripping_Beta      = 0.395000
    ComptonCorrParam_Stripping_Gamma     = 0.738000
    ComptonCorrParam_AlphaPerMetre       = 0.000000
    ComptonCorrParam_BetaPerMetre        = 0.000000
    ComptonCorrParam_GammaPerMetre       = 0.000000
    ComptonCorrParam_GrastyBackscatter_a = 0.055000
    ComptonCorrParam_GrastyBackscatter_b = 0.001000
    ComptonCorrParam_GrastyBackscatter_g = 0.002000

### Height Correction settings ###
    SurveyHeightDatum     = 85.000000
    AttenuationCorrControl = 0
    HeightCorrParam|TC      = -0.008677, 200.000000
    HeightCorrParam|K       = -0.012332, 200.000000
    HeightCorrParam|U       = -0.007869, 200.000000
    HeightCorrParam|Th      = -0.007701, 200.000000

### Concentration settings ###
   ConcentrationParam|K       = Concentration_K,  0.000000
   ConcentrationParam|U       = Concentration_U,  0.000000
   ConcentrationParam|Th      = Concentration_Th,  0.000000
   AirAbsorbedDoseRateParam   = DoseRate,  0.000000
```

```
      NaturalAirAbsorbedDoseRateParam = NaturalDoseRate,  0.000000,
0.000000, 0.000000


CONTROL_END
```

RADIOMETRIC PROCESSING CONTROL FILE (2007 Phase)

```
///////////////////////////////////////////////////
// Atlas Control/Workspace File
// # or // for commment
///////////////////////////////////////////////////

CONTROL_BEGIN

  PROGRAM  = AGSCorrection
  VERSION  = 1.4.0

   ### Process or Calibration? ###
       WhatToDo = Process Survey Line

   ### Corrections to apply ###
       CorrectionType = Yes  Filtering
       CorrectionType = Yes  LiveTimeCorrection
       CorrectionType = Yes  CosmicAircraftBGRemove
       CorrectionType = Yes  CalcEffectiveHeight
       CorrectionType = Yes  RadonBGRemove
       CorrectionType = Yes  ComptonStripping
       CorrectionType = Yes  HeightCorrection
       CorrectionType = No   ConvertToConcentration


   ### Main I/O settings ###
       MainChannelIO|TC       = GR820_TC_DOWN --> TC_R
       MainChannelIO|K        = GR820_K_DOWN --> K_R
       MainChannelIO|U        = GR820_U_DOWN --> U_R
       MainChannelIO|Th       = GR820_TH_DOWN --> TH_R
       MainChannelIO|UpU      = GR820_U_UP --> U_UP_R
       MainChannelIO|Cosmic   = GR820_COSMIC --> COSMIC_R
```

```
    MainChannelIO|Spectrum = GR820_DOWN --> DOWN_COR

### Control Channel I/O settings ###
    ControlChannel|RadarAltimeter     = ALTR_M      [metres]
    ControlChannel|Pressure/Barometer = KPA         [kPa]
    ControlChannel|Temperature        = TEMP_EXT


### Input for correction ###
    InputForCorrection    = ROIs


### Pre-filtering settings ###
    Filtering|TC      = 0
    Filtering|K       = 0
    Filtering|U       = 0
    Filtering|Th      = 0
    Filtering|UpU     = 0
    Filtering|Cosmic  = 9
    Filtering|RadarAltimeter     = 3
    Filtering|Pressure/Barometer = 3
    Filtering|Temperature        = 3

### Live-time correction settings ###
    LiveTimeChannel            = GR820_LIVE_TIME
    LiveTimeUnits              = milli-seconds
    ApplyLiveTimeCorrToUpU     = Yes

### Cosmic correction settings ###
    CosmicCorrParam|TC      = 0.696350,  42.868000
    CosmicCorrParam|K       = 0.038285,  3.049010
    CosmicCorrParam|U       = 0.032501,  0.251860
    CosmicCorrParam|Th      = 0.039573,  0.133575
    CosmicCorrParam|UpU     = 0.008828,  0.133958
    CosmicCorrParam|SpectrumBackgroundFile    =

### Effective-Height settings ###
    EffectiveHeightOutputChannel = EffectiveHeight
    EffectiveHeightOutputUnits   = metres

### Radon correction settings ###
    RadonCorrMethod                         = UpU
    RadonCorrParam_FilterWidth              = 71
    RadonCorrParam_UseRadonMeanForFewData    = Yes
    RadonOutputChannel                      = Radon
    RadonCorrParam_UgInUpU(A1) = 0.020000
    RadonCorrParam_ThInUpU(A2) = 0.100000
    RadonCorrParam|TC      = 14.000000,  0.000000
```

```
        RadonCorrParam|K       = 0.930000,  0.000000
        RadonCorrParam|Th      = 0.070000,  0.000000
        RadonCorrParam|UpU     = 0.280000,  0.000000

    ### Special Stripping (Compton Stripping) ###
        ComptonCorrParam_Stripping_Alpha     = 0.224000
        ComptonCorrParam_Stripping_Beta      = 0.393000
        ComptonCorrParam_Stripping_Gamma     = 0.717000
        ComptonCorrParam_AlphaPerMetre       = 0.000490
        ComptonCorrParam_BetaPerMetre        = 0.000650
        ComptonCorrParam_GammaPerMetre       = 0.000690
        ComptonCorrParam_GrastyBackscatter_a = 0.051000
        ComptonCorrParam_GrastyBackscatter_b = 0.004000
        ComptonCorrParam_GrastyBackscatter_g = 0.001000

    ### Height Correction settings ###
        SurveyHeightDatum     = 60.000000
        AttenuationCorrControl = 0
        AttenuationForNegROIs  = Yes
        HeightCorrParam|TC      = -0.007341, 300.000000
        HeightCorrParam|K       = -0.010257, 300.000000
        HeightCorrParam|U       = -0.005414, 300.000000
        HeightCorrParam|Th      = -0.007608, 300.000000

    ### Concentration settings ###
       ConcentrationParam|K       = Concentration_K,  0.000000
       ConcentrationParam|U       = Concentration_U,  0.000000
       ConcentrationParam|Th      = Concentration_Th,  0.000000
       AirAbsorbedDoseRateParam   = DoseRate,  0.000000
       NaturalAirAbsorbedDoseRateParam = NaturalDoseRate,  0.000000,
0.000000, 0.000000


CONTROL_END
```

APPENDIX H

GLOSSARY

APPENDIX H

GLOSSARY OF AIRBORNE GEOPHYSICAL TERMS

Note: The definitions given in this glossary refer to the common terminology as used in airborne geophysics.

altitude attenuation: the absorption of gamma rays by the atmosphere between the earth and the detector. The number of gamma rays detected by a system decreases as the altitude increases.

apparent- : the ***physical parameters*** of the earth measured by a geophysical system are normally expressed as apparent, as in "apparent ***resistivity*"**. This means that the measurement is limited by assumptions made about the geology in calculating the response measured by the geophysical system. Apparent resistivity calculated with ***HEM***, for example, generally assumes that the earth is a ***homogeneous half-space*** – not layered.

amplitude: The strength of the total electromagnetic field. In ***frequency domain*** it is most often the sum of the squares of ***in-phase*** and ***quadrature*** components. In multi-component electromagnetic surveys it is generally the sum of the squares of all three directional components.

analytic signal: The total amplitude of all the directions of magnetic ***gradient***. Calculated as the sum of the squares.

anisotropy: Having different ***physical parameters*** in different directions. This can be caused by layering or fabric in the geology. Note that a unit can be anisotropic, but still **homogeneous**.

anomaly: A localized change in the geophysical data characteristic of a discrete source, such as a conductive or magnetic body: something locally different from the **background**.

B-field: In time-domain **electromagnetic** surveys, the magnetic field component of the (electromagnetic) **field**. This can be measured directly, although more commonly it is calculated by integrating the time rate of change of the magnetic field **dB/dt**, as measured with a receiver coil.

background: The "normal" response in the geophysical data – that response observed over most of the survey area. **Anomalies** are usually measured relative to the background. In airborne gamma-ray spectrometric surveys the term defines the **cosmic**, radon, and aircraft responses in the absence of a signal from the ground.

base-level: The measured values in a geophysical system in the absence of any outside signal. All geophysical data are measured relative to the system base level.

base frequency: The frequency of the pulse repetition for a ***time-domain electromagnetic*** system. Measured between subsequent positive pulses.

bird: A common name for the pod towed beneath or behind an aircraft, carrying the geophysical sensor array.

bucking: The process of removing the strong ***signal*** from the ***primary field*** at the ***receiver*** from the data, to measure the ***secondary field***. It can be done electronically or mathematically. This is done in ***frequency-domain EM***, and to measure ***on-time*** in ***time-domain EM***.

calibration coil: A wire coil of known size and dipole moment, which is used to generate a field of known ***amplitude*** and ***phase*** in the receiver, for system calibration. Calibration coils can be external, or internal to the system. Internal coils may be called Q-coils.

coaxial coils: **[CX]** Coaxial coils in an HEM system are in the vertical plane, with their axes horizontal and collinear in the flight direction. These are most sensitive to vertical conductive objects in the ground, such as thin, steeply dipping conductors perpendicular to the flight direction. Coaxial coils generally give the sharpest anomalies over localized conductors. (See also ***coplanar coils***)

coil: A multi-turn wire loop used to transmit or detect electromagnetic fields. Time varying ***electromagnetic*** fields through a coil induce a voltage proportional to the strength of the field and the rate of change over time.

compensation: Correction of airborne geophysical data for the changing effect of the aircraft. This process is generally used to correct data in ***fixed-wing time-domain electromagnetic*** surveys (where the transmitter is on the aircraft and the receiver is moving), and magnetic surveys (where the sensor is on the aircraft, turning in the earth's magnetic field.

component: In ***frequency domain electromagnetic*** surveys this is one of the two **phase** measurements – ***in-phase or quadrature***. In "multi-component" electromagnetic surveys it is also used to define the measurement in one geometric direction (vertical, horizontal in-line and horizontal transverse – the Z, X and Y components).

Compton scattering: gamma ray photons will bounce off electrons as they pass through the earth and atmosphere, reducing their energy and then being detected by ***radiometric*** sensors at lower energy levels. See also ***stripping***.

conductance: See ***conductivity thickness***

conductivity: [s] The facility with which the earth or a geological formation conducts electricity. Conductivity is usually measured in milli-Siemens per metre (mS/m). It is the reciprocal of ***resistivity***.

conductivity-depth imaging: see ***conductivity-depth transform***.

conductivity-depth transform: A process for converting electromagnetic measurements to an approximation of the conductivity distribution vertically in the earth, assuming a ***layered earth***. (Macnae and Lamontagne, 1987; Wolfgram and Karlik, 1995)

conductivity thickness: [s**t**] The product of the ***conductivity***, and thickness of a large, tabular body. (It is also called the "conductivity-thickness product") In electromagnetic geophysics, the response of a thin plate-like conductor is proportional to the conductivity multiplied by thickness. For example a 10 metre thickness of 20 Siemens/m mineralization will be equivalent to 5 metres of 40 S/m; both have 200 S conductivity thickness. Sometimes referred to as conductance.

conductor: Used to describe anything in the ground more conductive than the surrounding geology. Conductors are most often clays or graphite, or hopefully some type of mineralization, but may also be man-made objects, such as fences or pipelines.

coplanar coils: **[CP]** In HEM, the coplanar coils lie in the horizontal plane with their axes vertical, and parallel. These coils are most sensitive to massive conductive bodies, horizontal layers, and the ***halfspace***.

cosmic ray: High energy sub-atomic particles from outer space that collide with the earth's atmosphere to produce a shower of gamma rays (and other particles) at high energies.

counts (per second): The number of ***gamma-rays*** detected by a gamma-ray ***spectrometer*.** The rate depends on the geology, but also on the size and sensitivity of the detector.

culture: A term commonly used to denote any man-made object that creates a geophysical anomaly. Includes, but not limited to, power lines, pipelines, fences, and buildings.

current channelling: See current gathering.

current gathering: The tendency of electrical currents in the ground to channel into a conductive formation. This is particularly noticeable at higher frequencies or early time channels when the formation is long and parallel to the direction of current flow. This tends to enhance anomalies relative to inductive currents (see also ***induction***). Also known as current channelling.

daughter products: The radioactive natural sources of gamma-rays decay from the original "parent" element (commonly potassium, uranium, and thorium) to one or more lower-energy "daughter" elements. Some of these lower energy elements are also radioactive and decay further. ***Gamma-ray spectrometry*** surveys may measure the gamma rays given off by the original element or by the decay of the daughter products.

dB/dt: As the ***secondary electromagnetic field*** changes with time, the magnetic field [**B**] component induces a voltage in the receiving ***coil***, which is proportional to the rate of change of the magnetic field over time.

decay: In ***time-domain electromagnetic*** theory, the weakening over time of the ***eddy currents*** in the ground, and hence the ***secondary field*** after the ***primary field*** electromagnetic pulse is turned off. In ***gamma-ray spectrometry***, the radioactive breakdown of an element, generally potassium, uranium, thorium, or one of their ***daughter*** products.

decay constant: see time constant.

decay series: In ***gamma-ray spectrometry***, a series of progressively lower energy ***daughter products*** produced by the radioactive breakdown of uranium or thorium.

depth of exploration: The maximum depth at which the geophysical system can detect the target. The depth of exploration depends very strongly on the type and size of the target, the contrast of the target with the surrounding geology, the homogeneity of the surrounding geology, and the type of geophysical system. One measure of the maximum depth of exploration for an electromagnetic system is the depth at which it can detect the strongest conductive target – generally a highly conductive horizontal layer.

differential resistivity: A process of transforming ***apparent resistivity*** to an approximation of layer resistivity at each depth. The method uses multi-frequency HEM data and approximates the effect of shallow layer ***conductance*** determined from higher frequencies to estimate the deeper conductivities (Huang and Fraser, 1996)

dipole moment: [NIA] For a transmitter, the product of the area of a ***coil***, the number of turns of wire, and the current flowing in the coil. At a distance significantly larger than the size of the coil, the magnetic field from a coil will be the same if the dipole moment product is the same. For a receiver coil, this is the product of the area and the number of turns. The sensitivity to a magnetic field (assuming the source is far away) will be the same if the dipole moment is the same.

diurnal: The daily variation in a natural field, normally used to describe the natural fluctuations (over hours and days) of the earth's magnetic field.

dielectric permittivity: **[**e**]** The capacity of a material to store electrical charge, this is most often measured as the relative permittivity [ε_r], or ratio of the material dielectric to that of free space. The effect of high permittivity may be seen in HEM data at high frequencies over highly resistive geology as a reduced or negative ***in-phase***, and higher ***quadrature*** data.

drape: To fly a survey following the terrain contours, maintaining a constant altitude above the local ground surface. Also applied to re-processing data collected at varying altitudes above ground to simulate a survey flown at constant altitude.

drift: Long-time variations in the base-level or calibration of an instrument.

eddy currents: The electrical currents induced in the ground, or other conductors, by a time-varying ***electromagnetic field*** (usually the ***primary field***). Eddy currents are also induced in the aircraft's metal frame and skin; a source of ***noise*** in EM surveys.

electromagnetic: **[EM]** Comprised of a time-varying electrical and magnetic field. Radio waves are common electromagnetic fields. In geophysics, an electromagnetic system is one which transmits a time-varying ***primary field*** to induce ***eddy currents*** in the ground, and then measures the ***secondary field*** emitted by those eddy currents.

energy window: A broad spectrum of ***gamma-ray*** energies measured by a spectrometric survey. The energy of each gamma-ray is measured and divided up into numerous discrete energy levels, called windows.

equivalent (thorium or uranium): The amount of radioelement calculated to be present, based on the gamma-rays measured from a **daughter** element. This assumes that the ***decay series*** is in equilibrium – progressing normally.

exposure rate: in radiometric surveys, a calculation of the total exposure rate due to gamma rays at the ground surface. It is used as a measurement of the concentration of all the **radioelements** at the surface. See also: **natural exposure rate**.

fiducial, or fid: Timing mark on a survey record. Originally these were timing marks on a profile or film; now the term is generally used to describe 1-second interval timing records in digital data, and on maps or profiles.

Figure of Merit: **(FOM)** A sum of the 12 distinct magnetic noise variations measured by each of four flight directions, and executing three aircraft attitude variations (yaw, pitch, and roll) for each direction. The flight directions are generally parallel and perpendicular to planned survey flight directions. The FOM is used as a measure of the **manoeuvre noise** before and after **compensation.**

fixed-wing: Aircraft with wings, as opposed to "rotary wing" helicopters.

footprint: This is a measure of the area of sensitivity under the aircraft of an airborne geophysical system. The footprint of an ***electromagnetic*** system is dependent on the altitude of the system, the orientation of the transmitter and receiver and the separation between the receiver and transmitter, and the conductivity of the ground. The footprint of a ***gamma-ray spectrometer*** depends mostly on the altitude. For all geophysical systems, the footprint also depends on the strength of the contrasting ***anomaly***.

frequency domain: An ***electromagnetic*** system which transmits a ***primary field*** that oscillates smoothly over time (sinusoidal), inducing a similarly varying electrical current in the ground. These systems generally measure the changes in the ***amplitude*** and ***phase*** of the ***secondary field*** from the ground at different frequencies by measuring the **in-phase** and **quadrature** phase components. See also ***time-domain***.

full-stream data: Data collected and recorded continuously at the highest possible sampling rate. Normal data are stacked (see ***stacking***) over some time interval before recording.

gamma-ray: A very high-energy photon, emitted from the nucleus of an atom as it undergoes a change in energy levels.

gamma-ray spectrometry: Measurement of the number and energy of natural (and sometimes man-made) gamma-rays across a range of photon energies.

gradient: In magnetic surveys, the gradient is the change of the magnetic field over a distance, either vertically or horizontally in either of two directions. Gradient data is often measured, or calculated from the total magnetic field data because it changes more quickly over distance than the ***total magnetic field***, and so may provide a more precise measure of the location of a source. See also ***analytic signal***.

ground effect: The response from the earth. A common calibration procedure in many geophysical surveys is to fly to altitude high enough to be beyond any measurable response from the ground, and there establish ***base levels*** or ***backgrounds***.

half-space: A mathematical model used to describe the earth – as infinite in width, length, and depth below the surface. The most common halfspace models are ***homogeneous*** and ***layered earth***.

heading error: A slight change in the magnetic field measured when flying in opposite directions.

HEM: Helicopter ElectroMagnetic, This designation is most commonly used for helicopter-borne, ***frequency-domain*** electromagnetic systems. At present, the transmitter and receivers are normally mounted in a ***bird*** carried on a sling line beneath the helicopter.

herringbone pattern: A pattern created in geophysical data by an asymmetric system, where the **anomaly** may be extended to either side of the source, in the direction of flight.

Appears like fish bones, or like the teeth of a comb, extending either side of centre, each tooth an alternate flight line.

homogeneous: This is a geological unit that has the same ***physical parameters*** throughout its volume. This unit will create the same response to an HEM system anywhere, and the HEM system will measure the same apparent ***resistivity*** anywhere. The response may change with system direction (see ***anisotropy***).

HTEM: Helicopter Time-domain ElectroMagnetic, This designation is used for the new generation of helicopter-borne, ***time-domain*** electromagnetic systems.

in-phase: the component of the measured ***secondary field*** that has the same phase as the transmitter and the ***primary field***. The in-phase component is stronger than the ***quadrature*** phase over relatively higher ***conductivity***.

induction: Any time-varying electromagnetic field will induce (cause) electrical currents to flow in any object with non-zero ***conductivity***. (see ***eddy currents***)

induction number: also called the “response parameter”, this number combines many of the most significant parameters affecting the ***EM*** response into one parameter against which to compare responses. For a ***layered earth*** the response parameter is mws$\mathbf{h}^2$ and for a large, flat, ***conductor*** it is mws**th**, where m is the ***magnetic permeability***, w is the angular ***frequency***, s is the **conductivity**, t is the thickness (for the flat conductor) and h is the height of the system above the conductor.

inductive limit: When the frequency of an EM system is very high, or the **conductivity** of the target is very high, the response measured will be entirely **in-phase** with no **quadrature** (**phase** angle =0). The in-phase response will remain constant with further increase in conductivity or frequency. The system can no longer detect changes in conductivity of the target.

infinite: In geophysical terms, an “infinite’ dimension is one much greater than the ***footprint*** of the system, so that the system does not detect changes at the edges of the object.

International Geomagnetic Reference Field: **[IGRF]** An approximation of the smooth magnetic field of the earth, in the absence of variations due to local geology. Once the IGRF is subtracted from the measured magnetic total field data, any remaining variations are assumed to be due to local geology. The IGRF also predicts the slow changes of the field up to five years in the future.

inversion, or **inverse modeling**: A process of converting geophysical data to an earth model, which compares theoretical models of the response of the earth to the data measured, and refines the model until the response closely fits the measured data (Huang and Palacky, 1991)

layered earth: A common geophysical model which assumes that the earth is horizontally layered – the ***physical parameters*** are constant to ***infinite*** distance horizontally, but change vertically.
magnetic permeability: **[m]** This is defined as the ratio of magnetic induction to the inducing magnetic field. The relative magnetic permeability [μ_r] is often quoted, which is the ratio of the rock permeability to the permeability of free space. In geology and geophysics, the ***magnetic susceptibility*** is more commonly used to describe rocks.

magnetic susceptibility: **[k]** A measure of the degree to which a body is magnetized. In SI units this is related to relative ***magnetic permeability*** by $k=\mu_r-1$, and is a dimensionless unit. For most geological material, susceptibility is influenced primarily by the percentage of magnetite. It is most often quoted in units of 10^{-6}. In HEM data this is most often apparent as a negative ***in-phase*** component over high susceptibility, high ***resistivity*** geology such as diabase dikes.

manoeuvre noise: variations in the magnetic field measured caused by changes in the relative positions of the magnetic sensor and magnetic objects or electrical currents in the aircraft. This type of noise is generally corrected by magnetic **compensation**.

model: Geophysical theory and applications generally have to assume that the geology of the earth has a form that can be easily defined mathematically, called the model. For example steeply dipping **conductor**s are generally modeled as being **infinite** in horizontal and depth extent, and very thin. The earth is generally modeled as horizontally layered, each layer infinite in extent and uniform in characteristic. These models make the mathematics to describe the response of the (normally very complex) earth practical. As theory advances, and computers become more powerful, the useful models can become more complex.

natural exposure rate: in radiometric surveys, a calculation of the total exposure rate due to natural-source gamma rays at the ground surface. It is used as a measurement of the concentration of all the natural **radioelements** at the surface. See also: **exposure rate**.

noise: That part of a geophysical measurement that the user does not want. Typically this includes electronic interference from the system, the atmosphere (***sferics***), and man-made sources. This can be a subjective judgment, as it may include the response from geology other than the target of interest. Commonly the term is used to refer to high frequency (short period) interference. See also ***drift***.

Occam's inversion: an ***inversion*** process that matches the measured ***electromagnetic*** data to a theoretical model of many, thin layers with constant thickness and varying resistivity (Constable et al, 1987).

off-time: In a ***time-domain electromagnetic*** survey, the time after the end of the ***primary field pulse***, and before the start of the next pulse.

on-time: In a ***time-domain electromagnetic*** survey, the time during the ***primary field pulse***.

overburden: In engineering and mineral exploration terms, this most often means the soil on top of the unweathered bedrock. It may be sand, glacial till, or weathered rock.

Phase, phase angle: The angular difference in time between a measured sinusoidal electromagnetic field and a reference – normally the primary field. The phase is calculated from $\tan^{-1}$(***in-phase / quadrature***).

physical parameters: These are the characteristics of a geological unit. For electromagnetic surveys, the important parameters are ***conductivity, magnetic permeability*** (or ***susceptibility***) and ***dielectric permittivity***; for magnetic surveys the parameter is magnetic susceptibility, and for gamma ray spectrometric surveys it is the concentration of the major radioactive elements: potassium, uranium, and thorium.

permittivity: see ***dielectric permittivity***.

permeability: see ***magnetic permeability***.

primary field: the EM field emitted by a transmitter. This field induces ***eddy currents*** in (energizes) the conductors in the ground, which then create their own ***secondary*** **fields**.

pulse: In time-domain EM surveys, the short period of intense ***primary*** field transmission. Most measurements (the ***off-time***) are measured after the pulse. **On-time** measurements may be made during the pulse.

quadrature: that component of the measured ***secondary field*** that is phase-shifted 90° from the ***primary field***. The quadrature component tends to be stronger than the ***in-phase*** over relatively weaker ***conductivity***.

Q-coils: see ***calibration coil***.

radioelements: This normally refers to the common, naturally-occurring radioactive elements: potassium (K), uranium (U), and thorium (Th). It can also refer to man-made radioelements, most often cobalt (Co) and cesium (Cs)

radiometric: Commonly used to refer to ***gamma ray*** spectrometry.

radon: A radioactive daughter product of uranium and thorium, radon is a gas which can leak into the atmosphere, adding to the non-geological background of a gamma-ray spectrometric survey.

receiver: the ***signal*** detector of a geophysical system. This term is most often used in active geophysical systems – systems that transmit some kind of signal. In airborne ***electromagnetic*** surveys it is most often a ***coil***. (see also, ***transmitter***)

resistivity: **[**r**]** The strength with which the earth or a geological formation resists the flow of electricity, typically the flow induced by the ***primary field*** of the electromagnetic transmitter. Normally expressed in ohm-metres, it is the reciprocal of ***conductivity***.

resistivity-depth transforms: similar to ***conductivity depth transforms***, but the calculated ***conductivity*** has been converted to ***resistivity***.

resistivity section: an approximate vertical section of the resistivity of the layers in the earth. The resistivities can be derived from the ***apparent resistivity***, the ***differential resistivities***, ***resistivity-depth transforms***, or ***inversions***.

Response parameter: another name for the **induction number**.

secondary field: The field created by conductors in the ground, as a result of electrical currents induced by the ***primary field*** from the ***electromagnetic*** transmitter. Airborne ***electromagnetic*** systems are designed to create and measure a secondary field.

Sengpiel section: a ***resistivity section*** derived using the ***apparent resistivity*** and an approximation of the depth of maximum sensitivity for each frequency.

sferic: Lightning, or the ***electromagnetic*** signal from lightning, it is an abbreviation of "atmospheric discharge". These appear to magnetic and electromagnetic sensors as sharp "spikes" in the data. Under some conditions lightning storms can be detected from hundreds of kilometres away. (see ***noise***)

signal: That component of a measurement that the user wants to see – the response from the targets, from the earth, etc. (See also ***noise***)

skin depth: A measure of the depth of penetration of an electromagnetic field into a material. It is defined as the depth at which the primary field decreases to 1/e of the field at the surface. It is calculated by approximately 503 x √(resistivity/frequency). Note that depth of penetration is greater at higher ***resistivity*** and/or lower ***frequency***.

spectrometry: Measurement across a range of energies, where ***amplitude*** and energy are defined for each measurement. In gamma-ray spectrometry, the number of gamma rays are measured for each energy ***window***, to define the ***spectrum***.

spectrum: In ***gamma ray spectrometry***, the continuous range of energy over which gamma rays are measured. In ***time-domain electromagnetic*** surveys, the spectrum is the energy of the **pulse** distributed across an equivalent, continuous range of frequencies.

spheric: see ***sferic***.

stacking: Summing repeat measurements over time to enhance the repeating ***signal***, and minimize the random ***noise***.
stripping: Estimation and correction for the gamma ray photons of higher and lower energy that are observed in a particular ***energy window***. See also ***Compton scattering***.

susceptibility: See ***magnetic susceptibility***.

tau: [t] Often used as a name for the ***time constant***.

TDEM: ***time domain electromagnetic***.

thin sheet: A standard model for electromagnetic geophysical theory. It is usually defined as a thin, flat-lying conductive sheet, ***infinite*** in both horizontal directions. (see also ***vertical plate***)

tie-line: A survey line flown across most of the ***traverse lines***, generally perpendicular to them, to assist in measuring ***drift*** and ***diurnal*** variation. In the short time required to fly a tie-line it is assumed that the drift and/or diurnal will be minimal, or at least changing at a constant rate.

time constant: The time required for an ***electromagnetic*** field to decay to a value of 1/e of the original value. In ***time-domain*** electromagnetic data, the time constant is proportional to the size and ***conductance*** of a tabular conductive body. Also called the decay constant.

Time channel: In ***time-domain electromagnetic*** surveys the decaying ***secondary field*** is measured over a period of time, and the divided up into a series of consecutive discrete measurements over that time.

time-domain: ***Electromagnetic*** system which transmits a pulsed, or stepped ***electromagnetic*** field. These systems induce an electrical current (***eddy current***) in the ground that persists after the ***primary field*** is turned off, and measure the change over time of the ***secondary field*** created as the currents ***decay***. See also ***frequency-domain***.

total energy envelope: The sum of the squares of the three ***components*** of the ***time-domain electromagnetic secondary field***. Equivalent to the ***amplitude*** of the secondary field.

transient: Time-varying. Usually used to describe a very short period pulse of ***electromagnetic*** field.

transmitter: The source of the ***signa*l** to be measured in a geophysical survey. In airborne ***EM*** it is most often a **coil** carrying a time-varying electrical current, transmitting the ***primary field***. (see also ***receiver***)

traverse line: A normal geophysical survey line. Normally parallel traverse lines are flown across the property in spacing of 50 m to 500 m, and generally perpendicular to the target geology.

vertical plate: A standard model for electromagnetic geophysical theory. It is usually defined as thin conductive sheet, ***infinite*** in horizontal dimension and depth extent. (see also ***thin shee***t)

waveform: The shape of the ***electromagnetic pulse*** from a ***time-domain*** electromagnetic transmitter.

window: A discrete portion of a ***gamma-ray spectrum*** or ***time-domain electromagnetic decay***. The continuous energy spectrum or ***full-stream*** data are grouped into windows to reduce the number of samples, and reduce ***noise***.

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- Appendix H.13 -

Common Symbols and Acronyms

k Magnetic susceptibility
e Dielectric permittivity
m, m_r Magnetic permeability, relative permeability
r, r_a Resistivity, apparent resistivity
s, s_a Conductivity, apparent conductivity
s**t** Conductivity thickness
t Tau, or time constant
W**m** ohm-metres, units of resistivity
AGS Airborne gamma ray spectrometry.
CDT Conductivity-depth transform, conductivity-depth imaging (Macnae and Lamontagne, 1987; Wolfgram and Karlik, 1995)
CPI, CPQ Coplanar in-phase, quadrature
CPS Counts per second
CTP Conductivity thickness product
CXI, CXQ Coaxial, in-phase, quadrature
FOM Figure of Merit
fT femtoteslas, normal unit for measurement of B-Field
EM Electromagnetic
keV kilo electron volts – a measure of gamma-ray energy
MeV mega electron volts – a measure of gamma-ray energy 1MeV = 1000keV
NIA dipole moment: turns x current x Area
nT nanotesla, a measure of the strength of a magnetic field
nG/h nanoGreys/hour – gamma ray dose rate at ground level
ppm parts per million – a measure of secondary field or noise relative to the primary or radioelement concentration.
pT/s picoteslas per second: Units of decay of secondary field, dB/dt
S siemens – a unit of conductance
x: the horizontal component of an EM field parallel to the direction of flight.
y: the horizontal component of an EM field perpendicular to the direction of flight.
z: the vertical component of an EM field.

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