

**Ministry of Energy & Mines**  
Energy & Minerals Division  
Geological Survey Branch

**ASSESSMENT REPORT  
TITLE PAGE AND SUMMARY**

<b>TITLE OF REPORT [type of survey(s)]</b> Resource Modelling and Estimation of the Harper Creek Deposit	<b>TOTAL COST</b> 43,347.00
---	--------------------------------

AUTHOR(S) Christopher O. Naas

SIGNATURE(S) 

NOTICE OF WORK PERMIT NUMBER(S)/DATE(S) MX-4-429

YEAR OF WORK 2010

STATEMENT OF WORK - CASH PAYMENT EVENT NUMBER(S)/DATE(S) 4806688

PROPERTY NAME Harper Creek

CLAIM NAME(S) (on which work was done) 220771, 220772, 220773, 220774, 220775, 220776, 220777, 220778, 220779, 220780, 220781, 220785, 220786, 220877, 220961, 501225, 501799, 502498, 509215, 514183, 517483

COMMODITIES SOUGHT Copper, silver, gold, zinc

MINERAL INVENTORY MINFILE NUMBER(S), IF KNOWN 082M 009

MINING DIVISION Kamloops

NTS 082M05, 082M12

LATITUDE 51 ° 30 ' 10 " LONGITUDE 119 ° 49 ' 04 " (at centre of work)

OWNER(S)

1) Yellowhead Mining Inc.

2) \_\_\_\_\_

MAILING ADDRESS

2130-21331 Gordon Way

Richmond BC Canada V6W1J9

OPERATOR(S) [who paid for the work]

1) Yellowhead Mining Inc.

2) \_\_\_\_\_

MAILING ADDRESS

2130-21331 Gordon Way

Richmond BC Canada V6W1J9

PROPERTY GEOLOGY KEYWORDS (lithology, age, stratigraphy, structure, alteration, mineralization, size and attitude):

Property is underlain by the Paleozoic Eagle Bay Assemblage. The Harper Creek deposit is a large, tabular, low-grade copper deposit enclosed within a series of sericite and/or chlorite-rich phyllites and very siliceous horizons. Copper mineralization includes disseminated sulphides and massive to semi-massive sulphide and sulphide-magnetite layers

REFERENCES TO PREVIOUS ASSESSMENT WORK AND ASSESSMENT REPORT NUMBERS \_\_\_\_\_

PBK Engineering, 1988 (AR17), Naas, C.O. 2004, 2005, 2006, 2007, 2008a, 2008b, 2009, 2010

(OVER)

TYPE OF WORK IN THIS REPORT	EXTENT OF WORK (IN METRIC UNITS)	ON WHICH CLAIMS	PROJECT COSTS APPORTIONED (incl. support)
GEOLOGICAL (scale, area)			
Ground, mapping			
Photo interpretation			
GEOPHYSICAL (line-kilometres)			
Ground			
Magnetic			
Electromagnetic			
Induced Polarization			
Radiometric			
Seismic			
Other			
Airborne			
GEOCHEMICAL (number of samples analysed for ...)			
Soil			
Silt			
Rock			
Other			
DRILLING (total metres; number of holes, size)			
Core			
Non-core			
RELATED TECHNICAL			
Sampling/assaying			
Petrographic			
Mineralographic	Resource modelling and estimation	220771, 220772, 220773, 220774, 220775, 220776, 220777, 220778, 220779, 220780, 220781, 220785, 220786, 220877, 220961, 501225, 501799, 502498, 509215, 514183, 517483	43,347.00
Metallurgic			
PROSPECTING (scale, area)			
PREPARATORY/PHYSICAL			
Line/grid (kilometres)			
Topographic/Photogrammetric (scale, area)			
Legal surveys (scale, area)			
Road, local access (kilometres)/trail			
Trench (metres)			
Underground dev. (metres)			
Other			
TOTAL COST			43,347.00

BC Geological Survey  
Assessment Report  
31986

**ASSESSMENT REPORT**  
**RESOURCE MODELLING AND ESTIMATION**  
**of the**  
**Harper Creek Deposit**

(220771, 220772, 220773, 220774, 220775, 220776, 220777, 220778, 220779,  
220780, 220781, 501225, 501799, 502498, 509215, 514183, 517483)  
Kamloops Mining Division, British Columbia, Canada

Owner: Yellowhead Mining Inc.  
Operator: Yellowhead Mining Inc.  
by  
Christopher O. Naas, *P. Geo.*  
January 31, 2011

NTS 82M/12  
*Latitude: 51°32'N*  
*Longitude: 119°47'W*

## **SUMMARY**

The Harper Creek property is located in south central British Columbia, Canada, 90 kilometres north-northeast of the city of Kamloops. It consists of 95 cell claims and 34 legacy claims totaling 41,089.96 hectares.

A National Instrument 43-101 compliant resource estimate of the Harper Creek deposit was carried out between June 9 and August 16, 2010 by Scott Wilson Roscoe Postle Associates. The resource estimate updates the previous resources estimate with the addition of data from a further 23 diamond drill holes. Only the copper resource was calculated in this study.

The Indicated resources, at a 0.2% Cu cutoff, are currently estimated at 569,000,000 tonnes at 0.32 % copper. Inferred resources are estimated at 62,700,000 tonnes at 0.33% copper.

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- I. Abbreviations and Conversion Factors
- II. Technical Report on the Harper Creek Project, Clearwater, British Columbia, Canada.

## **1.0 INTRODUCTION**

This report summarizes the results of the National Instrument 43-101 (NI 43-101) compliant resource modeling and estimation of the Harper Creek deposit carried out by Scott Wilson Roscoe Postle Associates (SWRPA).

Work was undertaken between June 9 and August 16, 2010. The objectives of the work program were to provide an updated estimate of the copper resources based upon diamond drilling completed since the previous estimate was completed.

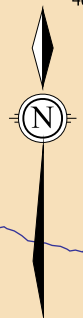
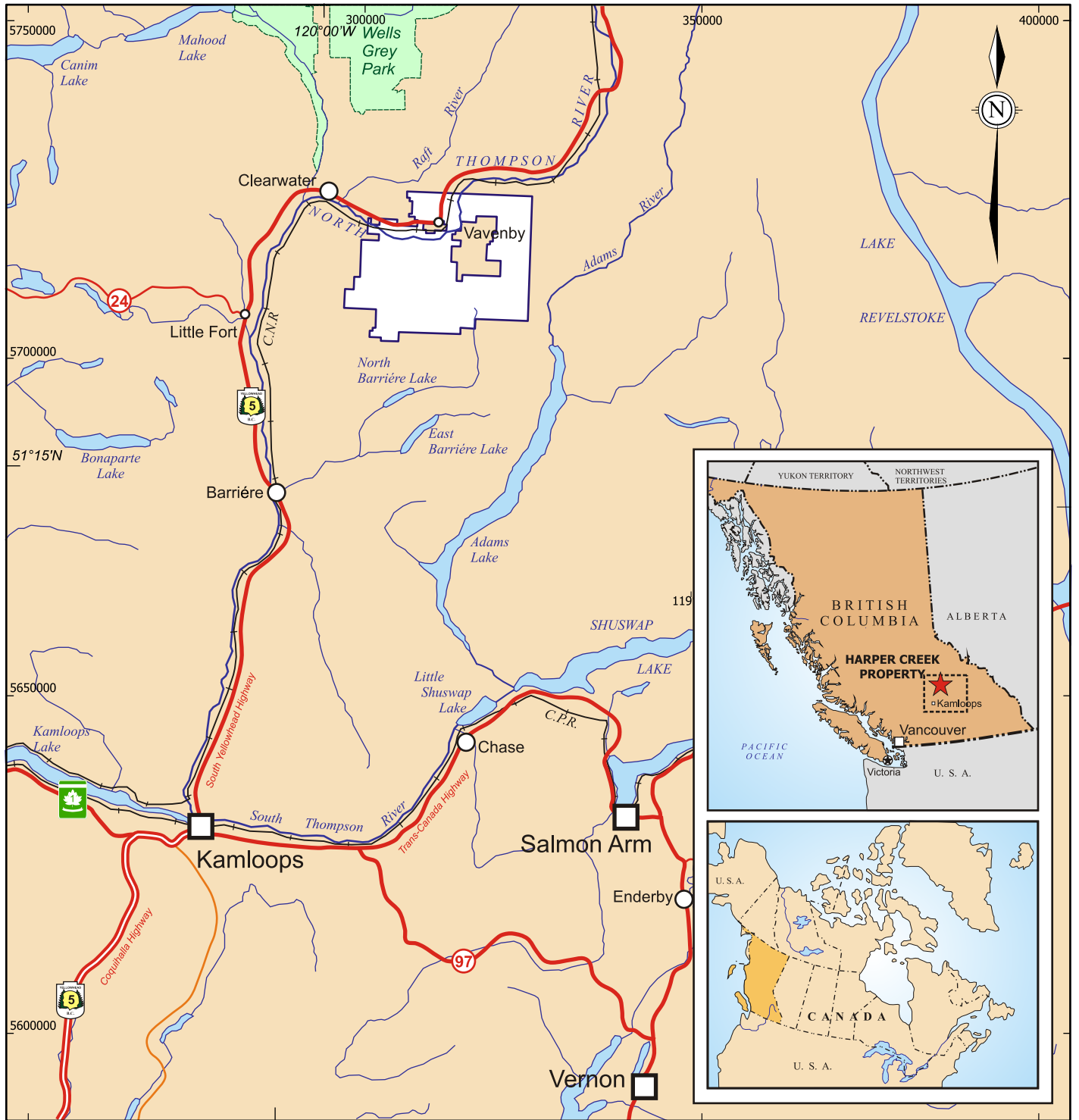
A list of definitions, abbreviations and conversion factors are presented in Appendix I. Structural orientations or Cartesian directions in this report are referenced to true north.

### **1.1 LOCATION AND ACCESS**

The Harper Creek property (the “Property”) is located in south central British Columbia, Canada, 90 kilometres north-northeast of the city of Kamloops (Figure 1).

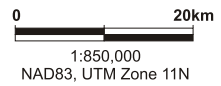
The Property is centered at approximately 51°33’N Latitude and 119°42’W Longitude within NTS map sheets 82M/12 and 82M/05. The Property is located wholly within the Kamloops Mining Division.

Road access is gained to the Study Area via the Yellowhead Highway (Highway 5) from the city of Kamloops to the town of Birch Island, then across the North Thompson River and eastward along the Birch Island-Lost Creek Forest Service Road (FSR) for approximately 6 kilometres east to the Jones Creek FSR. The Jones Creek FSR provides excellent access to the Study Area. At approximately the 10.6 kilometre mark of the Jones Creek FSR, the Road 5 junction is encountered. Access to the drilling sites of the Harper Creek deposit is gained 2 kilometres to the west of this junction.



**LEGEND**

 Yellowhead Mining's claim group (as of November 2, 2010)



**YELLOWHEAD MINING INC.**

**LOCATION MAP  
Harper Creek Property**

Harper Creek Project  
Kamloops M.D., British Columbia, Canada

Project No:	C111-HC	By:	TV
Scale:	1:850,000	Drawn:	TV
Figure:	1	Date:	January 2011



## 1.2 TITLE

In total, YMI holds: 95 cell claims totaling 40,239.96 hectares and 34 legacy claims totaling 850 hectares (Figure 2).

YMI wholly owns the mineral tenures on all cell claims as well as the 34 legacy claims.

Table 1: Claim Status, Harper Creek Property

Tenure Number	Area (ha)	Owner (100%)	Good To Date	Worked On	Claim Type
220771	25.0	Yellowhead	2011/nov/03	Yes	Legacy
220772	25.0	Yellowhead	2011/nov/03	Yes	Legacy
220773	25.0	Yellowhead	2011/nov/03	Yes	Legacy
220774	25.0	Yellowhead	2011/nov/03	Yes	Legacy
220775	25.0	Yellowhead	2011/nov/03	Yes	Legacy
220776	25.0	Yellowhead	2011/nov/03	Yes	Legacy
220777	25.0	Yellowhead	2011/nov/03	Yes	Legacy
220778	25.0	Yellowhead	2011/nov/03	Yes	Legacy
220779	25.0	Yellowhead	2011/nov/03	Yes	Legacy
220780	25.0	Yellowhead	2011/nov/03	Yes	Legacy
220781	25.0	Yellowhead	2011/nov/03	Yes	Legacy
220782	25.0	Yellowhead	2011/nov/03		Legacy
220783	25.0	Yellowhead	2011/nov/03		Legacy
220784	25.0	Yellowhead	2011/nov/03		Legacy
220785	25.0	Yellowhead	2011/nov/03	Yes	Legacy
220786	25.0	Yellowhead	2011/nov/03	Yes	Legacy
220787	25.0	Yellowhead	2011/nov/03		Legacy
220788	25.0	Yellowhead	2011/nov/03		Legacy
220789	25.0	Yellowhead	2011/nov/03		Legacy
220790	25.0	Yellowhead	2011/nov/03		Legacy
220791	25.0	Yellowhead	2011/nov/03		Legacy
220792	25.0	Yellowhead	2011/nov/03		Legacy
220793	25.0	Yellowhead	2011/nov/03		Legacy
220794	25.0	Yellowhead	2011/nov/03		Legacy
220795	25.0	Yellowhead	2011/nov/03		Legacy
220796	25.0	Yellowhead	2011/nov/03		Legacy
220797	25.0	Yellowhead	2011/nov/03		Legacy
220798	25.0	Yellowhead	2011/nov/03		Legacy
220799	25.0	Yellowhead	2011/nov/03		Legacy
220800	25.0	Yellowhead	2011/nov/03		Legacy
220877	25.0	Yellowhead	2011/nov/03	Yes	Legacy
220878	25.0	Yellowhead	2011/nov/03		Legacy
220879	25.0	Yellowhead	2011/nov/03		Legacy
220961	25.0	Yellowhead	2011/nov/03	Yes	Legacy
501147	342.023	Yellowhead	2011/nov/03		Mineral
501225	301.712	Yellowhead	2011/nov/03	Yes	Mineral



Table 1: Claim Status, Harper Creek Property (*cont'd*)

Tenure Number	Area (ha)	Owner (100%)	Good To Date	Worked On	Claim Type
501608	221.325	Yellowhead	2011/nov/03		Mineral
501799	181.048	Yellowhead	2011/nov/03	Yes	Mineral
502498	583.317	Yellowhead	2011/nov/03	Yes	Mineral
502603	603.425	Yellowhead	2011/nov/03		Mineral
502606	502.873	Yellowhead	2011/nov/03		Mineral
506422	562.992	Yellowhead	2011/nov/03		Mineral
509215	603.167	Yellowhead	2011/nov/03	Yes	Mineral
509217	422.206	Yellowhead	2011/nov/03		Mineral
513235	321.698	Yellowhead	2011/nov/03		Mineral
513237	80.434	Yellowhead	2011/nov/03		Mineral
513239	140.745	Yellowhead	2011/nov/03		Mineral
514183	40.221	Yellowhead	2011/nov/03	Yes	Mineral
517483	20.112	Yellowhead	2011/nov/03	Yes	Mineral
519327	502.428	Yellowhead	2011/nov/03		Mineral
519329	502.428	Yellowhead	2011/nov/03		Mineral
519330	502.426	Yellowhead	2011/nov/03		Mineral
519331	502.408	Yellowhead	2011/nov/03		Mineral
519332	502.467	Yellowhead	2011/nov/03		Mineral
519333	502.270	Yellowhead	2011/feb/12		Mineral
519334	462.093	Yellowhead	2011/feb/12		Mineral
530337	502.325	Yellowhead	2011/feb/12		Mineral
530338	502.674	Yellowhead	2011/feb/12		Mineral
532054	482.979	Yellowhead	2011/nov/03		Mineral
532057	241.483	Yellowhead	2011/nov/03		Mineral
538962	501.812	Yellowhead	2011/feb/12		Mineral
538963	501.606	Yellowhead	2011/feb/12		Mineral
538966	501.813	Yellowhead	2011/feb/12		Mineral
538968	501.879	Yellowhead	2011/feb/12		Mineral
538970	501.610	Yellowhead	2011/feb/12		Mineral
538971	421.485	Yellowhead	2011/feb/12		Mineral
538972	501.609	Yellowhead	2011/feb/12		Mineral
538973	501.606	Yellowhead	2011/feb/12		Mineral
538974	200.631	Yellowhead	2011/feb/12		Mineral
538996	502.013	Yellowhead	2011/feb/12		Mineral
538997	502.141	Yellowhead	2011/feb/12		Mineral
538999	421.767	Yellowhead	2011/feb/12		Mineral
539000	502.106	Yellowhead	2011/feb/12		Mineral
539001	421.730	Yellowhead	2011/feb/12		Mineral
539002	421.729	Yellowhead	2011/feb/12		Mineral
539004	281.142	Yellowhead	2011/feb/12		Mineral
539770	442.840	Yellowhead	2011/nov/03		Mineral
539771	322.005	Yellowhead	2011/nov/03		Mineral
564330	503.009	Yellowhead	2011/feb/12		Mineral
564331	503.009	Yellowhead	2011/feb/12		Mineral

Table 1: Claim Status, Harper Creek Property (*cont'd*)

Tenure Number	Area (ha)	Owner (100%)	Good To Date	Worked On	Claim Type
564333	503.230	Yellowhead	2011/nov/03		Mineral
564334	503.338	Yellowhead	2011/nov/03		Mineral
564335	463.183	Yellowhead	2011/nov/03		Mineral
564337	362.592	Yellowhead	2011/feb/12		Mineral
564338	502.820	Yellowhead	2011/feb/12		Mineral
564339	502.782	Yellowhead	2011/feb/12		Mineral
564340	503.009	Yellowhead	2011/feb/12		Mineral
564341	442.814	Yellowhead	2011/feb/12		Mineral
564342	503.008	Yellowhead	2011/feb/12		Mineral
564343	502.782	Yellowhead	2011/feb/12		Mineral
564344	503.102	Yellowhead	2011/feb/12		Mineral
564346	442.546	Yellowhead	2011/feb/12		Mineral
564347	462.501	Yellowhead	2011/feb/12		Mineral
564348	402.026	Yellowhead	2011/feb/12		Mineral
564349	502.328	Yellowhead	2011/feb/12		Mineral
564350	502.330	Yellowhead	2011/feb/12		Mineral
564351	461.877	Yellowhead	2011/feb/12		Mineral
564352	502.100	Yellowhead	2011/feb/12		Mineral
564353	401.515	Yellowhead	2011/feb/12		Mineral
564354	501.687	Yellowhead	2011/feb/12		Mineral
564355	501.692	Yellowhead	2011/feb/12		Mineral
564356	461.552	Yellowhead	2011/feb/12		Mineral
564357	120.733	Yellowhead	2011/feb/12		Mineral
564358	401.226	Yellowhead	2011/feb/12		Mineral
564360	200.611	Yellowhead	2011/feb/12		Mineral
564361	501.595	Yellowhead	2011/feb/12		Mineral
564362	501.824	Yellowhead	2011/feb/12		Mineral
564363	502.053	Yellowhead	2011/feb/12		Mineral
564364	502.282	Yellowhead	2011/feb/12		Mineral
564365	502.510	Yellowhead	2011/feb/12		Mineral
564366	502.738	Yellowhead	2011/feb/12		Mineral
564367	502.966	Yellowhead	2011/feb/12		Mineral
564368	503.192	Yellowhead	2011/feb/12		Mineral
564370	322.088	Yellowhead	2011/feb/12		Mineral
569337	261.635	Yellowhead	2011/nov/03		Mineral
572094	503.391	Yellowhead	2011/feb/12		Mineral
572095	483.086	Yellowhead	2011/feb/12		Mineral
572096	483.085	Yellowhead	2011/feb/12		Mineral
572097	503.417	Yellowhead	2011/feb/12		Mineral
572098	382.565	Yellowhead	2011/feb/12		Mineral
572099	382.574	Yellowhead	2011/feb/12		Mineral
572100	463.178	Yellowhead	2011/feb/12		Mineral
582783	201.286	Yellowhead	2011/feb/12		Mineral
592574	503.120	Yellowhead	2011/nov/03		Mineral

Table 1: Claim Status, Harper Creek Property (*cont'd*)

Tenure Number	Area (ha)	Owner (100%)	Good To Date	Worked On	Claim Type
592579	502.925	Yellowhead	2011/nov/03		Mineral
592580	462.539	Yellowhead	2011/nov/03		Mineral
592581	442.716	Yellowhead	2011/nov/03		Mineral
606977	415.444	Yellowhead	2011/feb/12		Mineral
627844	301.709	Yellowhead	2011/feb/12		Mineral
663643	502.399	Yellowhead	2011/feb/12		Mineral
663658	401.968	Yellowhead	2011/feb/12		Mineral

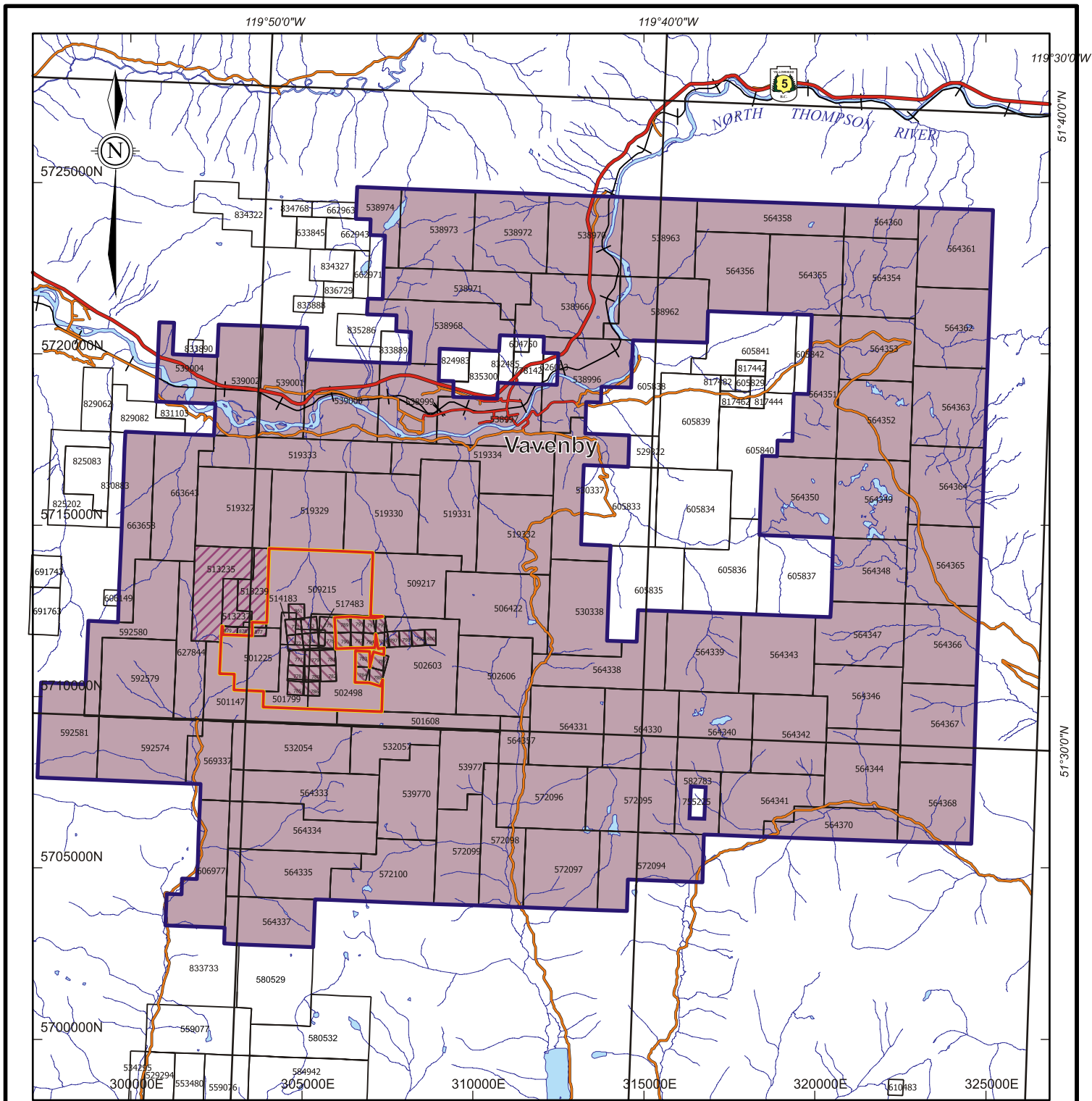
## 2.0 GEOLOGICAL SETTING

### 2.1 REGIONAL GEOLOGY

The Harper Creek project is located within structurally complex, low-grade metamorphic rocks of the Eagle Bay Assemblage part of the pericratonic Kootenay Terrane on the western margin of the Omineca Belt in south-central British Columbia (Figure 3). This assemblage is unconformably overlain by Fennell Formation rocks of the Slide Mountain Terrane to the west and flanked by high-grade metamorphic rocks of the Shuswap Complex to the east, also part of the Kootenay Terrane. Other factors contributing to the complexity of the area are its situation immediately east of the Quesnel Terrane representing a Late Triassic to Early Jurassic magmatic arc that formed along or near the western North American continental margin and that the project area also lies within the Cretaceous Bayonne plutonic belt (Logan, 2002). The Bayonne plutonic belt rocks are represented by two large batholiths, the Baldy batholith to the south and the Raft batholith to the north of the deposit.

Both the Eagle Bay Assemblage rocks and the Fennell Formation rocks were folded and metamorphosed to lower greenschist during the Jurassic-Cretaceous Columbian Orogeny. Greenschist metamorphism increases sharply in grade to amphibolite facies to the east and northeast. Late Devonian granitic orthogneiss locally intrudes Eagle Bay rocks. The Paleozoic rocks are cut by mid-Cretaceous granodiorite and quartz monzonite of the Bayonne plutonic belt, the Raft and Baldy batholiths, and by Early Tertiary quartz feldspar porphyry, basalt and lamprophyre dykes. They are locally overlain by Eocene sedimentary and volcanic rocks of the Kamloops Group and by Miocene plateau lavas (Schiarizza and Preto, 1987).

Mapping in the Harper Creek area conducted by the British Columbia Geological Survey (BCGS) in the 1980's resulted in the subdivision of the Eagle Bay stratigraphy as described in Table 2.



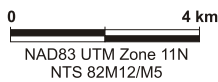
Topographic data © Department of Natural Resources. All rights reserved.

**LEGEND**

- Yellowhead Mining Inc. claims (100% owned)
- Subject to 2.5% NSR
- Subject to 3% NSR capped at a further \$2.5 million
- Yellowhead Mining's Harper Creek claim group (as of November 2, 2010) labelled with tenure number (last three digits for legacy claims; all with 220 prefix)
- Other tenures (as of November 2, 2010)
- Study Area

**Topography**

- Paved road
- Gravel road
- Rough road
- Railway
- Waterbody
- Watercourse



**YELLOWHEAD MINING INC.**

**CLAIM MAP**  
**Harper Creek Property**

Harper Creek Project  
Kamloops M.D., British Columbia, Canada

Project No: C111-HC	By: TV
Scale: 1:160,000	Drawn: TV
Figure: 2	Date: January 2011

**CME**

Table 2: Geological units, Schiarizza and Preto (1987)

Age	Unit	Description
Lower Cambrian and/or Older	EBH	Dominantly quartzite, chlorite-muscovite-quartz schist and grit, intercalated with minor amounts of grey phyllite and dolomitic chlorite schist
	EBQ	Micaceous quartzite, grit, phyllite and quartz mica schist, accompanied by minor amounts of chlorite schist, limestone, calcareous phyllite, talc-silicate schist and amphibolite
Early Cambrian	EBG	Dominantly calcareous chlorite schist derived from mafic volcanic and volcanoclastic rocks. Limestone, including the Tshinakin limestone, is common within the unit, and quartzite, grit, phyllite, dolostone, conglomerate and intermediate to felsic metavolcanic rocks are present locally
Ordovician to Cambrian	EBS	A heterogeneous rock package dominated by fine to coarse-grained clastic metasediments, intercalated with carbonate and mafic to felsic volcanic and volcanoclastic horizons
Silurian or older	EBL	Limestone and calcareous phyllite
Devonian and/or Older	EBK	Calc-silicate schists and skarn
Devonian	EBA	Dominantly light grey chlorite-sericite-quartz phyllite and schist derived from felsic to intermediate volcanic and volcanoclastic rocks. Green chlorite schist derived from mafic volcanic rocks is present locally. Bands of dark grey phyllite and siltstone comprise approximately 10% of the unit
Devonian and/or Mississippian	EBM	Massive and pillowed greenstone, chlorite schist, quartzite, phyllite and bedded chert
	EBF	Gritty and fragmental feldspathic rocks, derived from a series of crystal-lithic tuffs and volcanic breccias. Epiclastic as well as pyroclastic varieties are present and a minor component may have been derived from porphyritic flows. Compositions range from andesitic to rhyolitic, with dacitic predominating
Mississippian	EBP	Dominantly dark grey slate, phyllite and siltstone, together with sandstone, granule to pebble conglomerate, limestone, dolostone and intermediate to felsic volcanoclastic rocks

Further regional mapping was carried out by the BCGS and reported by Höy (1996). Paleozoic rocks of the Eagle Bay assemblage collectively contain a succession of Cambrian (and possibly Late Proterozoic) quartzites, grits and quartz mica schists (Units EBH and EBQ), mafic metavolcanic rocks and limestone (EBG), and overlying schistose sandstones and grits (EBS) with minor calcareous and mafic volcanic units. These are overlain by a Devono-Mississippian succession of mafic to intermediate metavolcanic rocks (Units EBA and EBF) intercalated with and overlain by dark grey phyllite, sandstone and grit (EBP).

Höy (1996) divided the EBA into metavolcanic units and metasedimentary units as described in Table 3.

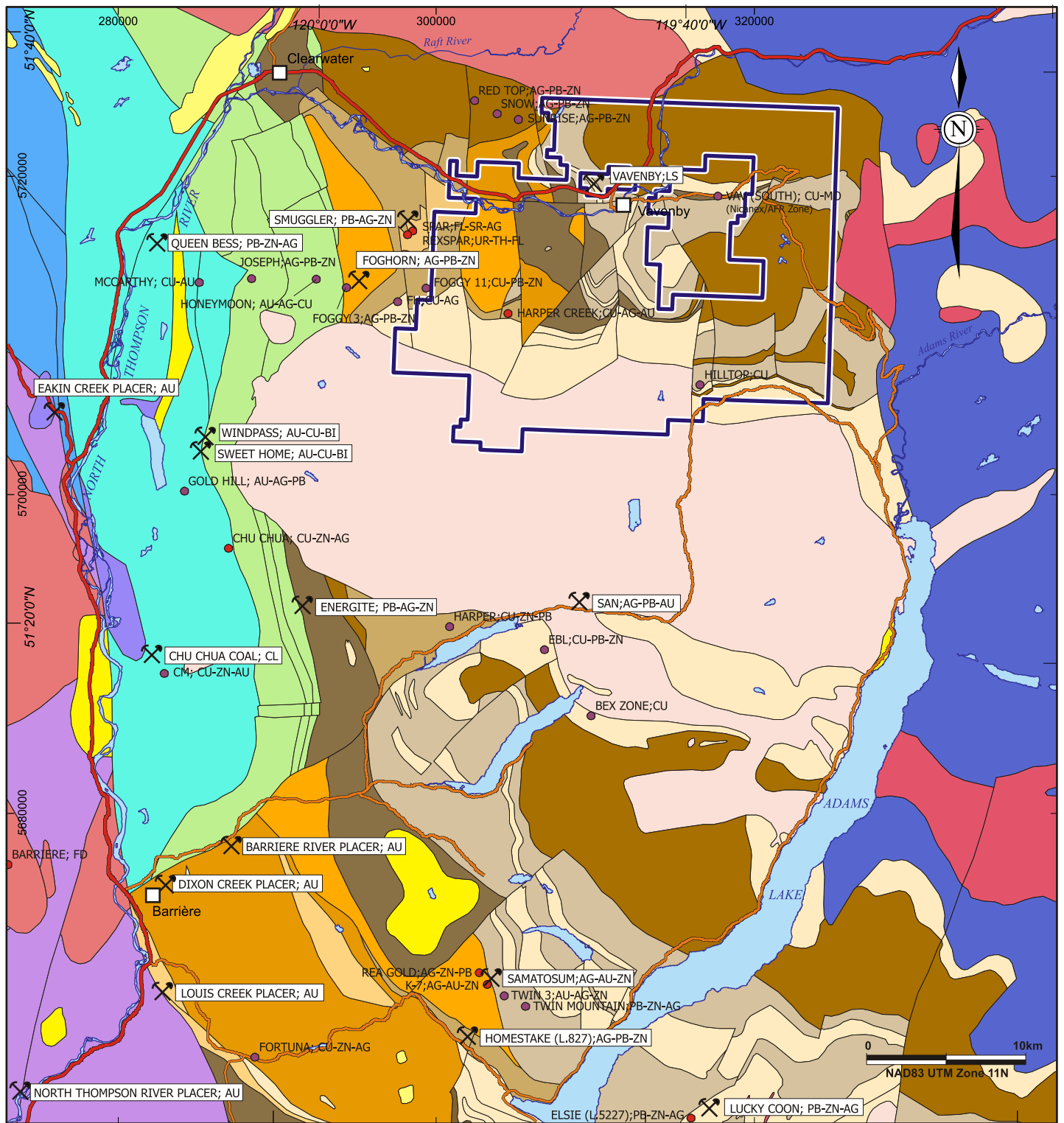
Table 3: Geological sub-units of Unit EBA, Höy (1996)

Unit No.	Sub-unit	Description
1 (Metavolcanic)	a	Foliated, massive to fragmental greenstone with lesser chlorite phyllite.
	b	Olivine basalt; cinder cones, blocky flows, breccia, and agglomerate
	c	Chlorite phyllite with minor sericite or quartz-sericite phyllite
	d	Lustrous, silvery-grey to tan coloured quartz-sericite phyllite, with quartz occurring interstitial to sericite, in thin foliation parallel laminae and as prominent quartz “eyes”
	e	Prominent quartz-eye phyllite with abundant elliptical to subrounded quartz eyes up to a centimetre in length
2 (Metasedimentary)	a	Predominantly quartzites; white to light green, resistant orthoquartzite, sericite quartzite and albite-sericite quartzite
	b	Consists of sericite, quartz-sericite and chlorite-sericite phyllites that appear similar to “intermediate” tuffs of Unit 1c
	c	Includes dark grey to black carbonaceous phyllite, pale grey calcareous phyllite, grey limestone and minor tan dolomite
3 (Sulphide Layers)	a	Massive to semi-massive pyrite, minor chalcopyrite
	b	Massive magnetite, pyrite, pyrrhotite, chalcopyrite

## 2.2 REGIONAL MINERALIZATION

The Eagle Bay Assemblage hosts a large number and wide variety of mineral occurrences. Their general characteristics allow the more important ones to be grouped into several types (Schiarizza and Preto, 1987), such as Ag, Pb, Zn stratabound massive sulphides within metasedimentary rocks (Units EBG and EBQ), Cu, Zn, Co volcanogenic massive sulphides (Fennell Formation) and Au, Ag, Zn, Pb, Cu, barite volcanogenic massive sulphides (Units EBA and EBF).

Significant mineral occurrences are presented in Figure 3.



**LEGEND**

**Quaternary**

Basaltic volcanics

**Tertiary**

Kamloops Group: undifferentiated volcanics

**Tertiary-Mesozoic**

Granite, quartz porphyry

**Mesozoic**

Baldy Batholith: quartz monzonite

Granodiorite

Nicola Group: sediments

**Mesozoic-Paleozoic**

Harper Ranch and(?) Nicola Groups: seds

**Paleozoic**

Fennell Assemblage: Upper/Lower Structural Division

basaltic volcanic/marine sediments, volcanics

Mount Ida Assemblage: metamorphics (calcsilicates)

**Proterozoic-Paleozoic**

Shuswap Assemblage

Eagle Bay Assemblage: undifferentiated

Dixon Ridge Unit

Foghorn Mountain Unit

Forest Lake Unit

Graffunder Lakes Unit

Johnson Lake Unit

Rexspar Unit

Skwaam Bay Unit

Slate Creek Unit

**Mineral Occurrences (BC Minfile)**

Past Producer

Developed Prospect

Prospect

Geology after BCGS Open File 2005-1  
Mineral occurrences modified from BC Minfile

**YELLOWHEAD MINING INC.**

**REGIONAL GEOLOGY  
AND ECONOMIC SETTING**

Harper Creek Project  
Kamloops M.D., British Columbia, Canada

Project No:	C111-HC	By:	TV
Scale:	1:350,000	Drawn:	TV
Figure:	3	Date:	January 2011



### 3.0 PROPERTY GEOLOGY

Descriptions of the three dominant geological units of the Harper Creek deposit are presented in Table 4.

Table 4: Geological units, Naas and Soloviev (2008)

Rock Package	Description
Older Metavolcanic-dominant	Chlorite phyllite formed after mafic ash tuff. This package of rocks contains minor crystalloclastic mafic tuff containing coarser, angular fragments of feldspar crystals, mafic tuffs with felsic lapilli, mafic tuffs with numerous (<1mm) lenses of dolomite or siderite, and graphitic chlorite phyllites after mafic tuffs. The unit ranges from 200 to 400 metres in thickness. Corresponds to Höy, 1996 unit 1b. The chlorite phyllite dominantly consists of pale-green to dark-green chlorite, with variable quartz, carbonate, feldspar, sphene, and commonly contains scattered quartz “pebbles” up to 5-10 millimetres across converted into augen-like “quartz eyes”.
Younger Metasedimentary-dominant	This package is composed of essentially argillaceous sedimentary rocks varying from tuffaceous argillite and tuffite to either alternating thin-bedded tuffite and chert/jasper or alternating pelitic and carbonaceous argillite. Thin parallel to cross-laminations are common in these units, the latter being locally suggestive for unequal sliding of unlithified sediments. Syn-sedimentary brecciation is locally evident. Compared to the lower package, this upper rock package appears to be more “sedimentary” rather than volcanogenic, containing less tuffaceous but more carbonaceous and carbonate material. The uppermost parts of the section also incorporate thick (10-50m) horizons of calcareous argillite and tuffite, often with abundant siderite and calcite forming series of thin lenses and saturating the rock matrix. Lenses of graphitic limestone are also present. This unit ranges from 100 to 300 metres in thickness.
Transition zone	The transition zone between the above noted rock packages is approximately 100 to 200 metres thick. The upper part of the older metavolcanic-dominant package and the lower part of the younger metasedimentary-dominant package incorporate several continuous units of highly siliceous rocks that may be siliceous phyllite after felsic extrusives or felsic quartz-porphyry dykes or sills. In addition, this transition zone incorporates large lens-like bodies of quartzite as well as thick zones of intense silicification.

A number of discordant and sub concordant dykes, sills and larger intrusives representing various intrusive events were encountered which were subdivided into several intrusive suites, namely:

- intermediate to felsic dykes, sills and plugs;
- felsic (quartz-feldspar porphyry) dykes, sills and plugs;
- quartz-porphyry dykes, sills and plugs;
- mafic (lamprophyre?) dykes; and,
- Tertiary andesite (intermediate?) dykes.



## 4.0 WORK HISTORY

In April 1966, Noranda Exploration Company discovered copper mineralization at the headwaters of Baker Creek through a program of prospecting and stream sediment sampling. In June 1966, Quebec Cartier (a 100% wholly owned subsidiary of US Steel) discovered copper mineralization at the headwaters of Harper Creek through a similar program of prospecting and stream sediment sampling. Staking by the two companies in 1966 resulted in ground west of Harper Creek belonging to Noranda (Harper Creek Claims) and east of Harper Creek belonging to Quebec Cartier (Hail Claims).

Work was undertaken independently by the two companies on their respective properties from 1967 until mid-1970. In the latter part of 1970, the two companies began a joint venture exploration of their contiguous copper deposits that lasted until 1974. Extensive surface exploration consisting of rock and soil geochemistry and ground geophysical surveys and trenching was performed immediately over and surrounding the deposit area. Extensive diamond drilling during this period led to development of a resource which contained 85,500,000 tons of ore grading 0.43% copper. Subsequent studies reevaluated the resource to include gold, silver and molybdenum content.

The next recorded work program on either property was in 1986, when Aurun Mines Ltd. (“Aurun”) signed an option agreement with Quebec Cartier on April 22, 1986. Aurun commissioned a pre-feasibility study by Phillips Barratt Kaiser Engineering Ltd. (1988), which reported the following resources.

Table 5: Resource and reserve estimates, PBK (1988)

### Geological Resources

Zone	Tonnage (t)	Cu (%)	Au (g/t)	Ag (g/t)
East	42,500,000	0.39	0.043	2.4
West	53,500,000	0.42	0.047	2.6
Total	96,000,000	0.41	0.045	2.5

### Mineable Resources

Zone	Tonnage (t)	Cu (%)	Au (g/t)	Ag (g/t)
East	42,200,000	0.34	0.037	2.1
West	23,140,000	0.40	0.044	2.4
Total	65,340,000	0.36	0.040	2.2

(The above resource and reserve estimates are of historical value only as they may not be compliant with the definitions required by National Instrument 43-101. They are not to be relied upon as a resource/reserve calculation).

In 1996, American Comstock purchased the Noranda held claims and acquired an option on the Quebec Cartier claims (now held by Cygnus Mines Limited, but still a wholly-owned subsidiary of US Steel). American Comstock completed a total of 2,847.44 metres of NQ diamond drilling in eight holes from which 686 samples were analyzed for copper, molybdenum and silver. Seven of the eight holes were completed on the Cygnus portion of the property while one hole (96-6) was completed on the Noranda property.

YMI began exploring the Property in 2005 with a program of salvaging historical diamond drill core for relogging and resampling with a goal of confirming historically reported copper grades and conducting multi-element analysis. Relogging of the drill core was conducted to further understand the lithology of the host rocks and to develop controls on the mineralization. Resampling of the historical core was successful in demonstrating the reported historical copper grades. Furthermore, to determine the accuracy of historical drill hole locations, the work program also included GPS surveying of drill hole collars.

Through 2006 to present, YMI has conducted several phases of exploration consisting of geochemical surveys and geophysical surveys (airborne and ground), diamond drilling, continued relogging and resampling of historical core, as well as petrographic studies, environmental studies, and other associated work. Scott Wilson Roscoe Postle Associates (SWRPA) prepared a mineral resource estimate and technical report for the Harper Creek project in November 2007. Following an additional 12,655.95 m of diamond drilling in 34 holes, this estimate was updated in March 2008. The two estimates are summarized in Table 6.

Table 6: Resource Estimates, SWRPA, 2007 and 2008 update

Date	Cut-off Grade (% Cu)	Tonnage (t)	Grade (% Cu)	Cu (t)
<b>Indicated</b>				
Nov-07	0.2	450,900	0.32	1,457,800
Mar-08	0.2	538,000	0.32	1,735,000
<b>Inferred</b>				
Nov-07	0.2	142,000	0.33	463,900
Mar-08	0.2	65,000	0.34	221,000

Both resources are compliant with NI 43-101 standards of mineral resource reporting.

## 5.0 RESOURCE MODELING AND ESTIMATION

The objective of the resource estimate was to provide an updated estimation of the copper resource with the inclusion of a further 23 diamond drill holes (HC08-53 to HC08-75) completed after the 2008 resource estimate by SWRPA. The study was initiated on June 9 and completed on August 16, 2010. Two field visits by SWRPA personnel were made. Figure 4 presents the location of the collars of these drill holes as well as the surface extent of the resource pit used by SWRPA as part of the modeling constraints.

The estimate was conducted using a block model constrained by wireframe models (mineralization, faults and open pit), and copper grade was interpolated into the blocks using Ordinary Kriging. The kriging model was based on semi-variograms derived from a geostatistical analysis carried out by SWRPA.

The updated resource estimate for the Harper Creek deposit is presented in Table 7.

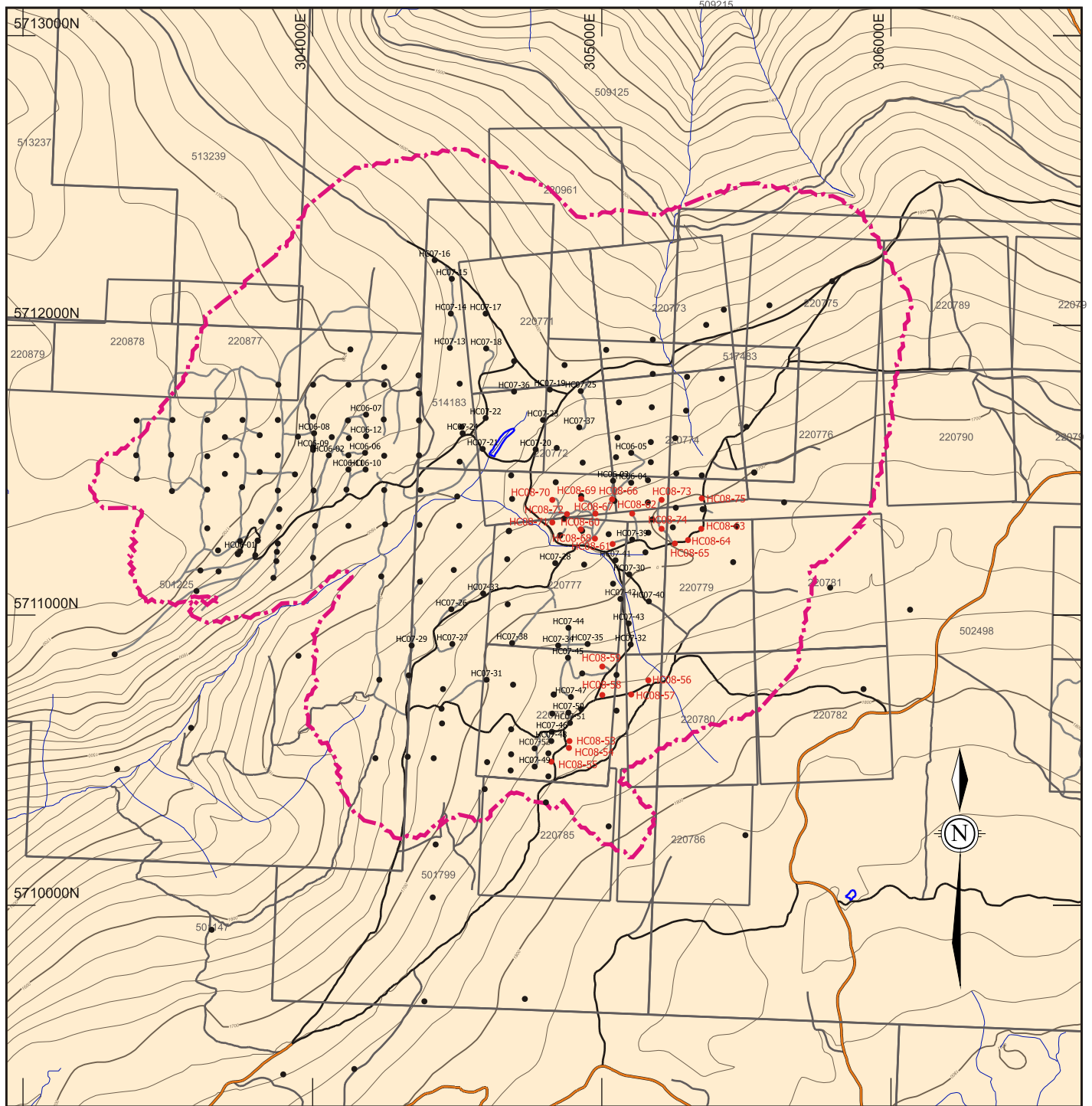
Table 7: Mineral Resource Estimate, Indicated and Inferred Categories

Cut-Off (% Cu)	Tonnage (kt)	Cu Grade (%)	Contained Cu (M lb)
<i>Indicated</i>			
0.5	39,800	0.58	509
0.4	102,000	0.49	1,100
0.3	256,000	0.40	2,260
0.2	569,000	0.32	4,010
0.1	973,000	0.25	5,360
<i>Inferred</i>			
0.5	6,810	0.59	88.6
0.4	14,900	0.51	168
0.3	30,100	0.43	285
0.2	62,700	0.33	456
0.1	102,000	0.26	585

Notes:

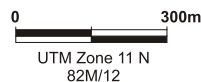
1. CIM definitions were followed for Mineral Resources.
2. Base case Mineral Resources are estimated at a cut-off grade of 0.20% Cu.
3. A minimum mining width of 5 metres was used.
4. The estimate is constrained by a pit shell.
5. Average bulk density is 2.79 t/m<sup>3</sup>.

The complete report by SWRPA detailing the methodology and results of the resource estimation is presented in Appendix II.



**LEGEND**

- HC08-59 Drill holes incorporated into 2010 resource estimate
  - HC06-01 YMI drill hole collar location and name
  - Historical drill hole collar location
  - - - Resource pit surface extent
- Topography**
- Watercourse
  - Contour (20m interval)
  - Paved or all-weather gravel road
  - Rough road
  - - - Trail
  - Waterbody
  - 501147 Mineral tenures (as of November 2, 2010)



**YELLOWHEAD MINING INC.**

**RESOURCE AREA  
Harper Creek Deposit**

Harper Creek Project  
Kamloops M.D., British Columbia, Canada

Project No:	C111-HC	By:	CN
Scale:	1:20,000	Drawn:	TV
Figure:	4	Date:	January 2011



## 6.0 CONCLUSIONS

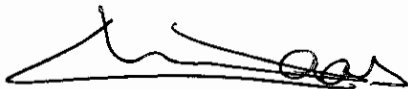
Among the conclusions of the SWRPA report the current resource estimate of Indicated Mineral Resources at a cut-off grade of 0.2% Cu are estimated to be 569.0 Mt grading 0.32% Cu. Inferred Mineral Resources total 62.7 Mt grading 0.33% Cu. This represents an overall 5% increase in tonnes over the last estimate, carried out in 2008. The drilling incorporated into the new resource was mainly situated within the previous resource limits, hence a fairly moderate increase in tonnage. There was also a shift of resources from the inferred resource category to the indicated resource category.

The presence of the appreciable associated gold and silver values will likely have an effect on the project economics, but due to limited gold and silver results, these could not be modeled in the current resource estimate.

The deposit still remains open along strike and dip, particularly to the north and east. Future drilling in these areas has the potential to significantly increase the resource size.

Respectfully Submitted,

Christopher O. Naas, *P. Geo.*



CME Consultants Inc.  
January 31, 2011.

## 7.0 REFERENCES

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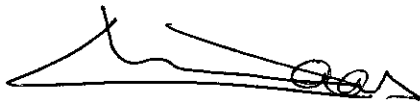
1987. Geology of the Adams Plateau-Clearwater-Vavenby Area: *B.C. Energy and Mines and Petroleum Resources*, Paper 1987-2.

## 8.0 CERTIFICATE

I, Christopher O. Naas, *P. Geo.*, do hereby certify that:

1. I am a member in good standing of the Association of Professional Engineers and Geoscientists of British Columbia (Registration Number 20082);
2. I am a graduate in geology of Dalhousie University (*B.Sc.*, 1984); and have practiced in my profession continuously since 1987;
3. Since 1987, I have been involved in mineral exploration for precious and/or base metals in Canada, United States of America, Chile, Venezuela, Ghana, Mali, Nigeria, and Democratic Republic of the Congo (Zaire); for diamonds in Venezuela; and for rare metals in Nigeria. I have also been involved in the determination of base metal and gold resources for properties in Canada and Ghana, respectively, and the valuation of properties in Canada and Equatorial Guinea.
4. I am presently a Consulting Geologist and have been so since November 1987;

Dated at Vavenby, British Columbia, this 31<sup>st</sup> day of January, 2011.



Christopher O. Naas, *P. Geo.*

## 9.0 STATEMENT OF COSTS

	Personnel	Days	Rate	Subtotal	Totals
<b>Office Work</b>					
Report Preparation	Ted VanderWart	1.0	600	600.00	
	Chris Naas	0.75	800	<u>600.00</u>	1,200.00
Drafting and Printing Costs				<u>44.71</u>	44.71
<b>Data Preparation</b>					
	Ted VanderWart	2.0	600	<u>1,200.00</u>	
	Data preparation, formatting and exporting for delivery to Scott Wilson				1,200.00
<b>Contract Services</b>					
	Scott Wilson RPA Resource Estimation and Reporting			<u>40,902.29</u>	<u>40,902.29</u>
					<b>43,347.00</b>



## **10.0 LIST OF SOFTWARE USED**

In the preparation of this report the following software was used:

Microsoft	Word 2000
	Excel 2000
Corel	CorelDraw x3
Adobe	Acrobat version 7

Software used by SWRPA in the preparation of the Resource Estimation include GEMS (block modeling and wireframing) and Whittle (pit design).

## **APPENDIX I**

### **ABBREVIATIONS AND CONVERSION FACTORS**

## ABBREVIATIONS

<b>Elements</b>		<b>Abbreviations</b>	
Ag	Silver	Az	azimuth
As	Arsenic	CDN\$	Canadian dollars
Au	Gold	ppm	parts per million
Ba	Barium	ppb	parts per billion
Cd	Cadmium	g/t	grams per metric tonne
Cu	Copper	oz/T	troy ounces per ton
Mo	Molybdenum	tpd	metric tonnes per day
Pb	Lead	Eq. Au	Gold equivalent
Sb	Antimony	UTM	Universal Transverse Mercator
Ti	Titanium	NAD83	North American Datum 1983
Zn	Zinc	° / ' / "	degree/minute/second of arc

## CONVERSION FACTORS

<b>Length</b>			
1 millimetre (mm)	0.03937 inches (in)	1 inch (in)	25.40 millimetre (mm)
1 centimetre (cm)	0.394 inches(in)	1 inch (in)	2.540 centimetres (cm)
1 metre (m)	3.281 feet (ft)	1 foot (ft)	0.3048 metres (m)
1 kilometre (km)	0.6214 mile (mi)	1 mile (mi)	1.609 kilometres (km)
<b>Area</b>			
1 sq. centimeter (cm <sup>2</sup> )	0.1550 sq. inches (in <sup>2</sup> )	1 sq inch (in <sup>2</sup> )	6.452 sq. centimetres (cm <sup>2</sup> )
1 sq. metre (m <sup>2</sup> )	10.76 feet (ft <sup>2</sup> )	1 foot (ft)	0.0929 sq. metres (m <sup>2</sup> )
1 hectare (ha) (10,000 m <sup>2</sup> )	2.471 acres	1 acre	0.4047 hectare (ha)
1 hectare (ha)	0.003861 sq. miles (m <sup>2</sup> )	1 sq. mile (m <sup>2</sup> )	640 acres
1 hectare (ha)	0.01 sq. kilometre (km <sup>2</sup> )	1 sq. mile (m <sup>2</sup> )	259.0 hectare (ha)
1 sq. kilometre (km <sup>2</sup> )	0.3861 sq. miles (mi <sup>2</sup> )	1 sq. mile (m <sup>2</sup> )	2.590 sq. kilometres (km <sup>2</sup> )
<b>Volume</b>			
1 cu. centimetre (cc)	0.06102 cu. inches (in <sup>3</sup> )	1 cu. inch (in <sup>3</sup> )	16.39 cu. centimetres (cm <sup>3</sup> )
1 cu. metre (m <sup>3</sup> )	1.308 cu. yards (yd <sup>3</sup> )	1 cu. yard (yd <sup>3</sup> )	0.7646 cu. metres (m <sup>3</sup> )
1 cu. metre (m <sup>3</sup> )	35.310 cu. feet (ft <sup>3</sup> )	1 cu. foot (ft <sup>3</sup> )	0.02832 cu. metres (m <sup>3</sup> )
1 litre (l)	0.2642 gallons (U.S.)	1 gallon (U.S.)	3.785 litres (l)
1 litre (l)	0.2200 gallons (U.K.)	1 gallon (U.K.)	4.546 litres (l)
<b>Weights</b>			
1 gram (g)	0.03215 troy ounce (20dwt)	1 troy ounce (oz)	31.1034 grams (g)
1 gram (g)	0.6430 pennyweight (dwt)	1 pennyweight (dwt)	1.555 grams (g)
1 gram (g)	0.03527 oz avoirdupois	1 oz avoirdupois	28.35 grams (g)
1 kilogram (g)	2.205 lb avoirdupois	1 lb avoirdupois	0.4535 kilograms (kg)
1 tonne (t) (metric)	1.102 tons (T) (short ton)	1 ton (T) (short ton) (2000 lb)	0.9072 tonnes (t)
1 tonne (t)	0.9842 long ton	1 long ton (2240 lb)	1.016 tonnes (t)
<b>Miscellaneous</b>			
1 cm/second	0.01968 ft/min	1 ft/min	50.81 cm/second
1 cu. m/second	22.82 million gal/day	1 million gal/day	0.04382 m <sup>3</sup> /second
1 cu. m/minute	264.2 gal/min	1 gal/min	0.003785 m <sup>3</sup> /minute
1 g/cu. m	62.43 lb/ cu. ft	1 lb/cu. ft <sup>3</sup>	0.01602 g/m <sup>3</sup>
1 g/cu. m	0.02458 oz/cu. yd	1 oz/cu. yd	40.6817 g/m <sup>3</sup>
1 Pascal (Pa)	0.000145 psi	1 psi	6985 Pascal
1 gram/tonne (g/t)	0.029216 troy ounce/ short ton (oz/T)	1 troy ounce/short ton (oz/T)	34.2857 grams/tonne (g/t)
1 g/t	0.583 dwt/short ton	1 dwt/short ton	1.714 g/t
1 g/t	0.653 dwt/long ton	1 dwt/long ton	1.531 g/t
1 g/t	0.0001 %		
1 g/t	1 part per million (ppm)		
1 %	10,000 part per million (ppm)		
1 part per million (ppm)	1,000 part per billion (ppb)		
1 part per billion (ppb)	0.001 part per million (ppm)		

**APPENDIX II**

**TECHNICAL REPORT ON THE HARPER CREEK PROJECT,  
CLEARWATER, BRITISH COLUMBIA, CANADA  
by D. Rennie and K. Scott  
Scott Wilson Roscoe Postle Associates**

**Scott Wilson Mining**



**YELLOWHEAD MINING INC.**

**TECHNICAL REPORT ON THE  
HARPER CREEK PROJECT,  
CLEARWATER, BRITISH COLUMBIA,  
CANADA**

**NI 43-101 Report**

**Authors:**

**David W. Rennie, P.Eng.**

**Kevin C. Scott, P.Eng.**

**August 16, 2010**

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**SCOTT WILSON ROSCOE POSTLE ASSOCIATES INC.**



## Report Control Form

Document Title	Technical Report on The Harper Creek Project, Clearwater, British Columbia								
Client Name & Address	Yellowhead Mining Inc. 2130 - 21331 Gordon Way Richmond, B.C. Canada V6W 1J9								
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Peer Reviewer	Deborah A. McCombe	(Signed)							
Project Manager Approval	David W. Rennie	(Signed)							
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# 1 SUMMARY

## EXECUTIVE SUMMARY

### INTRODUCTION

Scott Wilson Roscoe Postle Associates Inc. (Scott Wilson RPA) was retained by Ian Smith, P.Eng., CEO and Director of Yellowhead Mining Inc. (Yellowhead), to prepare an updated estimate of Mineral Resources and an independent Technical Report on the Harper Creek Project, located near Clearwater, British Columbia, Canada. This Technical Report conforms to National Instrument 43-101 Standards of Disclosure for Mineral Projects (NI 43-101). Scott Wilson RPA visited the property on May 23, 2007, and more recently on July 15, 2010.

Confirmatory and infill diamond drilling, carried out since the last Mineral Resource estimate in 2008, has been included in the new estimate. Additions to the database since the last estimate comprised 23 diamond drillholes totalling 7,602.92 m. The updated Mineral Resource estimate is summarized in Table 1-1.

**TABLE 1-1 MINERAL RESOURCE ESTIMATE – AUGUST 2010**  
**Yellowhead Mining Inc. – Harper Creek Property**

Cut-off (%Cu)	Tonnage Kt	Grade (% Cu)	Cu (M lb)
<b>Indicated</b>			
0.5	39,800	0.58	509
0.4	102,000	0.49	1,100
0.3	256,000	0.40	2,260
<b>0.2</b>	<b>569,000</b>	<b>0.32</b>	<b>4,010</b>
0.1	973,000	0.25	5,360
<b>Inferred</b>			
0.5	6,810	0.59	88.6
0.4	14,900	0.51	168
0.3	30,100	0.43	285
<b>0.2</b>	<b>62,700</b>	<b>0.33</b>	<b>456</b>
0.1	102,000	0.26	585

Notes:

1. CIM definitions were followed for Mineral Resources.
2. Base case Mineral Resources are estimated at a cut-off grade of 0.20% Cu.
3. A minimum mining width of 5 metres was used.
4. The estimate is constrained by a pit shell (see description in this report).
5. Average bulk density is 2.79 t/m<sup>3</sup>.

## CONCLUSIONS

Scott Wilson RPA draws the following conclusions:

- The Harper Creek deposit is interpreted as a volcanic-hosted massive sulphide (VHMS) deposit, comprising Cu sulphide-bearing (chalcopyrite) horizons with significant Au and Ag values. The mineralization occurs in shallowly to moderately dipping tabular zones that appear from the drill results obtained to date to be reasonably coherent and predictable and broadly concordant with the stratigraphy.
- The drilling, logging, and sampling work by Yellowhead is being carried out in an appropriate fashion using conventional industry-standard protocols.
- The early drilling results have been validated to a standard that makes them acceptable for use in the estimation of Mineral Resources up to and including the Inferred and Indicated categories. Yellowhead has reassayed 4,375 of 14,242 older samples (approximately 31% of the total), and there has been good agreement between the older and newer data.
- In Scott Wilson RPA's opinion, the samples are representative and unbiased.
- Several holes are without complete downhole surveys, resulting in survey inaccuracies. In Scott Wilson RPA's opinion, the survey inaccuracies should not affect the global mineral resource estimate. However, local block grades will probably be affected.
- Limited Au and Ag assay work suggests that there are areas of the deposit where grades of these components will be high enough to affect project economics. Assaying for Au and Ag was not routinely done during earlier programs. Yellowhead assays the newer core for Au and Ag and has resampled a number of the older drillholes. Scott Wilson RPA recommends that grades for Au and Ag be estimated into the block model.
- Preliminary metallurgical test work suggests that the Yellowhead ore can be processed using conventional methods (i.e., grinding and froth flotation). Preliminary test work has been completed on a relatively high grade sample (0.76% Cu) and on a sample representative of an average head grade over a potential mine life (0.35% Cu). Based on this test work, Scott Wilson RPA projects that the lower grade material should obtain copper recovery of 88% at concentrate grades above 25% Cu, while the higher grade material should obtain copper recovery of 92% at similar concentrate grades.
- Indicated Mineral Resources at a cut-off grade of 0.2% Cu are estimated to be 569.0 Mt grading 0.32% Cu. Inferred Mineral Resources total 62.7 Mt grading 0.33% Cu. This represents an overall 5% increase in tonnes over the last estimate, carried out in 2008. The reason for the increase is that additional diamond drilling has added Mineral Resources.
- Scott Wilson RPA notes that the average grade of the Mineral Resources tends to be close to the cut-off grade. This indicates that the tonnage above cut-off will be quite sensitive to variations in cut-off grade.

- A cut-off grade of 0.2% Cu has been applied to the Mineral Resource estimate and this cut-off grade was derived from experience that Scott Wilson RPA has from similar deposits. Further economic studies are required to rigorously define the cut-off grade.
- In Scott Wilson RPA's opinion, there is significant exploration potential at Harper Creek. The deposit remains open ended to the north, and there are sparsely drilled sections in the central portion of the deposit area that have good potential for expansion of the mineralized zones. Also, at some distance from the main deposit, there are additional exploration targets on the property which may increase the current Mineral Resources.
- In Scott Wilson RPA's opinion, the Harper Creek deposit warrants additional engineering and economic studies to determine the feasibility of developing an open pit mining and milling operation on the property.

## **RECOMMENDATIONS**

Scott Wilson RPA makes the following recommendations:

- Further metallurgical test work should be undertaken to optimize the reagent scheme and improve the flotation performance, particularly with respect to gold recovery. Variability test work should be undertaken to test the response of different samples to the optimized reagent and grinding scheme.
- Further mineralogical work should be undertaken to investigate the mode of mineralized particle locking in the locked cycle test products, in order to better understand how mineral separation, of Au and Ag in particular, can be improved in future metallurgical test work.
- Property exploration work should continue in order to find additional Mineral Resources on the Harper Creek property and upgrade the present Mineral Resources.
- Engineering, environmental, and economic studies should continue in order to determine if the Harper Creek deposit is economically feasible to exploit.

Yellowhead proposes to advance the project to Feasibility Stage, and this work is to be financed through a public offering of shares in the company. The initial stage of the planned work is to include diamond drilling to expand and upgrade the known Mineral Resources, as well as metallurgical, environmental, geotechnical, hydrological, and general site field studies. A preliminary economic assessment is scheduled for completion in November 2010. Planned expenditures for the first six months total C\$5 million, which includes the preliminary economic assessment. A summary of the budget is provided in Table 1-2. Field expenses are based on Yellowhead's experience on the property to date.

Scott Wilson RPA concurs with the planned work and budget, and recommends that the program be carried out.

**TABLE 1-2 PLANNED EXPENDITURES**  
**Yellowhead Mining Inc. – Harper Creek Property**

Item	C\$	Totals, C\$
<b>Geological Field Work</b>		
Personnel	350,000	
Mobilization	100,000	
Drilling and Related Fieldwork	300,000	
Camp Operations	300,000	
Equipment	100,000	
Construction	55,000	
Analyses	230,000	
Mineral Resource Report	60,000	
Reporting and Reproductions	20,000	
Contingency (15%)	227,250	
<b>Sub-Total</b>		<b>1,742,250</b>
<b>Other Technical Work</b>		
Environmental	200,000	
Geotechnical	15,000	
Project Management	550,000	
Metallurgy	200,000	
First Nations and Community Consultation	200,000	
Contingency (15%)	174,750	
<b>Sub-Total</b>		<b>1,339,750</b>
<b>Administration</b>		
Corporate Management	250,000	
Travel	100,000	
Legal	125,000	
Accounting	60,000	
Marketing and Promotion	75,000	
Office and Overhead	30,000	
US Steel Option Payment	500,000	
Contingency (15%)	171,000	
<b>Sub-Total</b>		<b>1,311,000</b>
Unallocated	500,000	
<b>Grand Total</b>		<b>4,893,000</b>
	say	<b>5,000,000</b>

## **TECHNICAL SUMMARY**

### **PROPERTY DESCRIPTION AND LOCATION**

The Harper Creek property is located approximately 90 km north-northeast of the city of Kamloops, British Columbia, at latitude 51°33' N and longitude 119°42' W. The property encompasses Cu-Au-Ag mineralization occurring in relatively near-surface, moderately to shallowly dipping tabular bodies. Mineralization was first discovered on the property in 1966, and exploration work has been undertaken intermittently ever since.

### **LAND TENURE**

Yellowhead holds 97 Mineral Title Online cell (MTO) claims totalling 41,786.48 ha and 34 legacy claims totalling 850 ha for a total controlled tenure of 42,636.48 ha.

Yellowhead wholly owns the mineral tenures on all of the cell claims and on three of the legacy claims (mineral tenures 220877-220879). The remaining 31 legacy claims are 100% owned by Cygnus Mines Limited, a subsidiary of US Steel, with Yellowhead holding an option to purchase. These claims are subject to a 3% net smelter return (NSR) royalty capped at \$2.5 million. On July 30, 2010, Yellowhead acquired title to the 31 Cygnus legacy claims by making an advance royalty payment of \$500,000. The royalty is an NSR royalty capped at \$3 million, which can be adjusted based on the Statistics Canada industrial price index over the period from conversion of the title to the actual royalty payment.

Through an original agreement with Noranda Exploration Company Ltd. (Noranda), Xstrata plc retains the rights to back into a 50% working interest in the original Noranda claims. These claims include legacy claims with tenure numbers 220877-220879 and legacy claims converted to MTO claims with tenure numbers 513235, 513237 and 513239.

### **SITE INFRASTRUCTURE**

A 130 KVA electrical power line traverses the property, as do several logging roads. Highway 5 and the Canadian National Railway line also cross the property.

Kamloops, a city with a population of 93,000, is the principal urban centre in the region. The city is served by regular flights from Vancouver, as well as by rail, bus, and a number of commercial trucking firms. The town of Clearwater is located 17 km southwest of the property.

## **HISTORY**

Copper mineralization was first discovered at Harper Creek in 1966 by Noranda Exploration Company (Noranda) and Québec Cartier Mining Company (Québec Cartier), a wholly-owned subsidiary of US Steel. Noranda staked the Harper Creek claims over what is now the western half of the known deposit, and Québec Cartier staked the Hail claims on adjacent ground to the east.

Both companies carried out surface exploration independently as well as cooperatively under a joint venture agreement. This work culminated in an economic assessment of the deposit in 1972. The study contemplated open pit “reserves” of 85 million tons grading 0.388% Cu, and concluded that the rate of return for the proposed operation was not sufficient to warrant production. Scott Wilson RPA notes that this historical resource estimate should not be relied upon. The joint venture was terminated in 1974.

The properties lay idle until 1986, when Aurun Mines Ltd. (Aurun) optioned the Québec Cartier ground. Aurun carried out trenching and resampling of core to investigate the potential for high-grade Cu-Mo, precious metal, and Ti-bearing mineralization, as well as the leachability of lower grade Cu mineralization. Québec Cartier terminated the agreement with Aurun in 1991.

The Québec Cartier claims were transferred to Cygnus Mines Limited (Cygnus), a wholly-owned subsidiary of US Steel. American Comstock Exploration Ltd. (American Comstock) purchased the Noranda ground in 1996, and acquired an option on the Cygnus claims. American Comstock drilled eight diamond holes, and shortly thereafter dropped the option. Over the next few years, some of the Noranda claims were abandoned, and in 2004, American Comstock sold six legacy claims to Argent Resources Ltd.

C. Naas, presently a director and exploration project manager with Yellowhead, staked claims over and surrounding the original Harper Creek/Hail property in 2002 for

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Callingham Limited (Callingham). During 2005 and early 2006, Yellowhead consolidated the property through a series of option agreements. Yellowhead has conducted exploration work comprising soil sampling, prospecting, resampling and relogging of old core, and diamond drilling from 2005 until the present time.

## **GEOLOGY**

The Harper Creek property is underlain by deformed and metamorphosed Lower Cambrian and Upper Devonian to Mississippian sedimentary and volcanic rocks, and foliated granite to diorite sills and dikes of the Eagle Bay Assemblage. These rocks have been intruded by Middle to Upper Jurassic and Cretaceous granitic plutons. Overlying the Eagle Bay Assemblage are Eocene-age Kamloops Group volcanic rocks.

The general orientation of the stratigraphy is east-west-striking with low to moderate northerly dips. Faulting is evident from juxtaposition of disparate rock units as well as surface lineaments. The stratigraphic sequence is disrupted by thrust-faults which have overthrust Cambrian rocks onto younger Paleozoic strata. Late northeast-striking, steeply southeast-dipping normal faults host Tertiary dikes.

Harper Creek is interpreted to be a polymetallic volcanogenic sulphide deposit, comprising lenses of disseminated, fracture-filling and banded Fe and Cu sulphides with accessory magnetite. Sulphide mineralization comprises chalcopyrite along with accessory pyrite, magnetite, and pyrrhotite. Minor components are bornite, covellite, sphalerite, galena, molybdenite, and arsenopyrite. The Cu mineralization is also accompanied by significant concentrations of Au and Ag. Mineralization is generally concordant with the host-rock stratigraphy. Sulphide lenses are observed to measure many tens of metres in thickness with kilometre-scale strike and dip extents.

## **EXPLORATION AND DRILLING**

### ***EARLY WORK***

In the period from 1967 until 1996, before the property was acquired by Yellowhead, diamond drilling totalled 29,285.8 m in 176 holes. Most of the drilling was BQ-size core (36.4 mm dia), although it is reported that Québec Cartier's initial program in 1967 used NQ (47.6 mm) equipment. American Comstock's core was NQTK (47.8 mm).

**RECENT WORK**

Yellowhead has drilled 27,584.3 m of NQ2 core in 75 holes. All drilling was done by Atlas Drilling Ltd. using a Longyear Super 38 drill. Collar locations were surveyed using differential GPS. Downhole surveys were performed using a variety of methods ranging from simple acid dip tests to Pajari, Flexit, and Icefield instruments.

**SAMPLING METHOD AND APPROACH**

Sampling methodology for the early drillholes was not documented, however, from inspection of the core, it would appear that a blade splitter was used. Maximum sample length was typically 10 ft., although some longer samples were taken.

Yellowhead employed a diamond saw for splitting. Maximum sample length was 2 m with breaks at changes in lithology, alteration, and mineralization.

Scott Wilson RPA reviewed the sampling procedures and inspected the facility for taking samples and considers both to be appropriate and of a standard consistent with common industry practice. The samples appeared, on the basis of the remaining core, to have been taken properly and the sample locations clearly marked. The samples are considered to be representative and, in Scott Wilson RPA's opinion, are unbiased.

**SAMPLE PREPARATION, ANALYSES AND SECURITY****EARLY WORK**

Detailed records of the sample preparation and assaying for the early drilling are not available. Assaying for the Noranda drill samples was done at an internal laboratory, operated by Noranda. Québec Cartier sent their samples to Bondar Clegg in North Vancouver (now ALS Chemex). The Aurun assaying was carried out by Chemex in North Vancouver, and the 1996 American Comstock samples were analyzed at Acme Analytical Laboratories Ltd. in Vancouver. All samples were assayed for Cu, while some, depending on the operator, were run for Au, Ag, Zn, and Mo.

**RECENT WORK**

Samples were assayed by Eco Tech Laboratory Ltd. (Eco Tech), in Kamloops, British Columbia, a division of Stewart Group. All sampling and on-site sample handling was carried out by principals or employees of CME Consultants Inc. (CME).

The samples were assayed for multi-elements via Inductively Coupled Plasma Spectrometry (ICP). Samples grading higher than 2,900 ppm Cu were reassayed by Atomic Absorption Spectrophotometry (AA) after digestion in aqua regia. Precious metals were determined by fire assay (FA) with an AA finish.

In Scott Wilson RPA's opinion, the assaying was done using conventional, industry-standard methods and carried out by an accredited commercial laboratory.

### **DATA VERIFICATION**

There are no records of assay quality assurance/quality control (QA/QC) for work carried out prior to Yellowhead's involvement with the Harper Creek property. In 2007, Yellowhead collected paired results for 1,245 individual sampled intervals from the early core, and supplied the results to Scott Wilson RPA for statistical analysis. In Scott Wilson RPA's opinion, the reassays agreed very well with the originals, and there is no reason to believe that the old assay data are unreliable.

Scott Wilson RPA carried out a block model interpolation exercise using first sample collected from only Yellowhead's drilling, and then using samples from the early drilling. The global block grades generated from the two data sets were virtually identical and indicate that there is no reason to believe the older drill results are invalid.

Scott Wilson RPA has conducted validation checks of the assay database against the original laboratory certificates and has found no errors. In Scott Wilson RPA's opinion, the Harper Creek database is reasonably free of errors and acceptable for use in estimation of Mineral Resources.

Scott Wilson RPA checked the drill collars on cross-section views against the updated topographic surface and found no significant discrepancies.

Scott Wilson RPA further notes that the early drillholes (Noranda and Québec Cartier) do not have complete downhole surveys. For this reason, Scott Wilson RPA recommends that the Measured category not be applied to the Mineral Resource estimate for blocks estimated solely with older drillholes.

Standards and blanks have been included with every batch of samples at a rate of one standard and one blank for every 50 (and, more recently, 40) samples. Pulps from five percent of the samples were collected and sent to a second laboratory as a duplicate check.

Scott Wilson RPA reviewed the QA/QC data and conducted an independent analysis. In Scott Wilson RPA's opinion, the sample QA/QC meets an acceptable standard for projects of this type. The results of the QA/QC sampling have been monitored in a timely fashion and used appropriately to address potential assay failures.

### **ADJACENT PROPERTIES**

Scott Wilson RPA is not aware of any significant exploration programs on the ground immediately adjacent to the Harper Creek Project. Harper Creek is the primary exploration project in the vicinity.

### **MINERAL PROCESSING AND METALLURGICAL TESTING**

A conventional mineral processing plant is being considered for the Harper Creek Project. Based on the test work, the proposed plant is expected to consist of standard crushing, grinding, and flotation to produce a high grade copper concentrate with payable precious metal values.

Process Research Associates Ltd. (PRA), located in Richmond, BC, undertook preliminary level test work in two phases during 2007 and 2008. Starting in January 2007, a series of flotation tests on a composite sample from the Harper Creek deposit were conducted to assess various grind sizes and flotation reagent schemes to extract copper and precious metals and produce a saleable copper concentrate. Subsequently, a second phase of test work was started in January 2008. The second phase of test work was similar to Phase 1 but was conducted on a lower grade sample that was considered more representative of an average mill feed grade over the life of mine. The assays of the two samples are shown in Table 1-3 for comparison.

**TABLE 1-3 COMPOSITE SAMPLE ASSAYS**  
**Yellowhead Mining – Harper Creek Project**

	<b>Cu (%)</b>	<b>Au (g/t)</b>	<b>Ag (g/t)</b>	<b>Fe (%)</b>	<b>S (%)</b>
Phase 1 HG sample	0.76	0.17	4.0	6.9	2.0
Phase 2 LG sample	0.35	0.05	1.0	3.7	1.3

***SUMMARY OF PHASE 1 METALLURGICAL TEST WORK AT PRA***

A total of 15 flotation tests were conducted on a single blended composite (HG composite) composed of 100 kg of individual samples taken from Harper Creek in December 2006. The first three tests were rougher flotation tests to assess the effects of different particle sizes on flotation followed by 11 cleaner flotation tests testing different reagent schemes with the objective of improving the concentrate grade and culminating in a locked cycle test (LCT).

Rougher flotation tests indicate copper recovery was essentially unaffected by the grinding sizes, however, the best Cu and Ag grades were obtained at 104 µm. Cleaner flotation tests achieved copper recoveries up to 96% using a variety of copper and gold collectors and iron sulphide depressants at different dosages.

A single LCT following the conditions established in a previous test provided very high copper recovery (94.9%) but at lower than expected grade (20.0% Cu and 2.54 g/t Au). This was thought to be due to the high recirculating load caused by the addition of a first cleaner scavenger.

***SUMMARY OF PHASE 2 METALLURGICAL TEST WORK AT PRA***

Additional samples were obtained to construct a composite sample that more closely represents an average mineable head grade over the potential mine life. In an attempt to replicate the resource grade at Harper Creek (0.32% Cu), a single composite composed of 330 kg of samples was blended and sent for testing in November 2007. The LG composite underwent metallurgical testwork, similar to Phase 1, in January 2008. A total of three rougher flotation tests followed by eight cleaner flotation tests and two LCTs were done.

Copper recovery was slightly better at the finer grind size, while gold recovery was poorer. The coarser primary grind was selected for further testing to remain consistent with Phase 1 and, as there was no clear indication that finer grinding would provide

significantly better results, the consideration of better project economics at coarser grinding was a determining factor.

Cleaner flotation tests employed the optimum reagent scheme developed in Phase 1, but a variety of different reagent dosages were investigated. The best overall results were achieved where 30% to 32% Cu grade was produced at copper recoveries of approximately 60%.

Locked cycle testing was increased to 10 cycles from the six cycles used in Phase 1 to improve test stability. The best results achieved a grade of 31% Cu, and overall recoveries of 87% Cu and 36% Au.

A single Bond ball mill work index test was conducted on the LG composite and indicates the Harper Creek ore is moderately soft.

Preliminary mineralogical examinations found copper to be entirely in the form of chalcopyrite.

Scott Wilson RPA projects that lower grade material from Harper Creek, representative of an average mine life head grade, should consistently obtain copper recovery of 88% at concentrate grades above 25% Cu.

Scott Wilson RPA recommends that further mineralogical work be undertaken to investigate the mode of mineralized particle locking in the locked cycle test products, in order to better understand how mineral separation, of Au and Ag in particular, can be improved in future metallurgical test work.

## **MINERAL RESOURCES**

Scott Wilson RPA has carried out an estimate of Mineral Resources for the Harper Creek deposit. The Mineral Resource estimate is summarized in Table 1-1. The estimate was conducted using a block model constrained by wireframe models, and Cu grade was interpolated into the blocks using Ordinary Kriging. The kriging model was based on semi-variograms derived from a geostatistical analysis carried out by Scott Wilson RPA. The wireframe and block models were constructed using GEMS software. The block model comprised blocks measuring 15 m long x 15 m wide x 15 m in height.

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High Cu assays were capped at 1.5% prior to compositing and grade interpolation. A mean bulk density of 2.79 t/m<sup>3</sup> was used for estimating the tonnage. The cut-off grade was 0.2% Cu.

Scott Wilson RPA carried out the following validation exercises on the block model:

- Visual inspection on plans and sections and comparison of the block grades to the composite grades.
- Comparison of global mean block and composite grades.
- Cross-validation or “jack-knifing”: Sequential removal of each composite from the database, and estimation of that composite using the surrounding composites.
- Re-estimation of the block model using an alternative method (Inverse Distance Squared, ID<sup>2</sup>).

The Mineral Resources were classified as follows:

- Indicated Mineral Resources are blocks within the resource shell estimated with a minimum of two drillholes (i.e., a minimum of four composites), with the anisotropic distance to the nearest composite less than or equal to 167 m.
- Inferred Mineral Resources are blocks within the resource shell estimated with a minimum of one composite out to a distance equal to the full variogram range.

Scott Wilson RPA generated a pit shell using Whittle and reported as Mineral Resources only those blocks captured within this pit shell.

## **OTHER RELEVANT DATA AND INFORMATION**

Scott Wilson RPA is not aware of any issues that exist which would prevent the advancement of the project.

## **2 INTRODUCTION**

Scott Wilson Roscoe Postle Associates Inc. (Scott Wilson RPA) was retained by Ian Smith, P.Eng., CEO and Director of Yellowhead Mining Inc. (Yellowhead), to prepare an updated estimate of Mineral Resources and an independent Technical Report on the Harper Creek Project, located near Clearwater, British Columbia, Canada. This Technical Report conforms to National Instrument 43-101 Standards of Disclosure for Mineral Projects (NI 43-101).

Yellowhead is a private British Columbia-based company, engaged in mineral exploration. The principal asset of the company is the Harper Creek Cu-Au-Ag deposit. The property comprises some 42,636 ha of mineral claims, located 90 km north-northeast of Kamloops, British Columbia. Exploration work including 29,285 m of diamond drilling was carried out on the deposit from 1969 to 1972 by Noranda Exploration Company (Noranda) and Québec Cartier Mining Company (Québec Cartier), and in 1996 by American Comstock Exploration Ltd. (American Comstock). Since 2006, Yellowhead has been conducting diamond drilling to confirm the older drill results and expand the known mineralization.

Previously, Scott Wilson RPA has produced two Mineral Resource estimates for Harper Creek; the initial disclosure of Mineral Resources in 2007 and an updated estimate in 2008.

### **SOURCES OF INFORMATION**

Site visits were carried out by David W. Rennie, P.Eng., Principal Consulting Geologist for Scott Wilson RPA, on May 23, 2007, and again on July 15, 2010.

Discussions were held with personnel from Yellowhead:

- Mr. Ian Smith, P. Eng., Chief Executive Officer and Director, Yellowhead Mining Inc.
- Mr. R. Handford, P. Eng., Executive Vice President, Yellowhead Mining Inc.
- Mr. G. Hawkins, P. Geo., Chairman, Yellowhead Mining Inc. and Executive Director of CME Consultants Inc. (CME)



- Mr. C. Naas, P.Ge., Director, Yellowhead Mining Inc., CME, and exploration project manager.

David Rennie, P. Eng., is responsible for the geology and mineral resource sections of this report. Kevin Scott, P. Eng., Scott Wilson RPA Consulting Metallurgical Engineer, is responsible for the metallurgy section of this report.

The documentation reviewed, and other sources of information, are listed at the end of this report in Section 21, References.

**LIST OF ABBREVIATIONS**

Units of measurement used in this report conform to the SI (metric) system. All currency in this report is Canadian dollars (C\$) unless otherwise noted.

μ	micron	kPa	kilopascal
°C	degree Celsius	kVA	kilovolt-amperes
°F	degree Fahrenheit	kW	kilowatt
μg	microgram	kWh	kilowatt-hour
A	ampere	L	litre
a	annum	L/s	litres per second
bbbl	barrels	m	metre
Btu	British thermal units	M	mega (million)
C\$	Canadian dollars	m <sup>2</sup>	square metre
cal	calorie	m <sup>3</sup>	cubic metre
cfm	cubic feet per minute	min	minute
cm	centimetre	MASL	metres above sea level
cm <sup>2</sup>	square centimetre	mm	millimetre
d	day	mph	miles per hour
dia.	diameter	MVA	megavolt-amperes
dmt	dry metric tonne	MW	megawatt
dwt	dead-weight ton	MWh	megawatt-hour
ft	foot	m <sup>3</sup> /h	cubic metres per hour
ft/s	foot per second	opt, oz/st	ounce per short ton
ft <sup>2</sup>	square foot	oz	Troy ounce (31.1035g)
ft <sup>3</sup>	cubic foot	oz/dmt	ounce per dry metric tonne
g	gram	ppm	part per million
G	giga (billion)	psia	pound per square inch absolute
Gal	Imperial gallon	psig	pound per square inch gauge
g/L	gram per litre	RL	relative elevation
g/t	gram per tonne	s	second
gpm	Imperial gallons per minute	st	short ton
gr/ft <sup>3</sup>	grain per cubic foot	stpa	short ton per year
gr/m <sup>3</sup>	grain per cubic metre	stpd	short ton per day
hr	hour	t	metric tonne
ha	hectare	tpa	metric tonne per year
hp	horsepower	tpd	metric tonne per day
in	inch	US\$	United States dollar
in <sup>2</sup>	square inch	USg	United States gallon
J	joule	USgpm	US gallon per minute
k	kilo (thousand)	V	volt
kcal	kilocalorie	W	watt
kg	kilogram	wmt	wet metric tonne
km	kilometre	yd <sup>3</sup>	cubic yard
km/h	kilometre per hour	yr	year
km <sup>2</sup>	square kilometre		

### **3 RELIANCE ON OTHER EXPERTS**

This report has been prepared by Scott Wilson RPA for Yellowhead. The information, conclusions, opinions, and estimates contained herein are based on:

- Information available to Scott Wilson RPA at the time of preparation of this report,
- Assumptions, conditions, and qualifications as set forth in this report, and
- Data, reports, and other information supplied by Yellowhead and other third party sources.

For the purpose of this report, Scott Wilson RPA has relied on ownership information provided by C. Naas, Manager of the Harper Creek Project, and director of Yellowhead. Mr. Naas staked most of the claims within the property, and assembled the land package for Yellowhead. Scott Wilson RPA has not researched property title or mineral rights for the Harper Creek property and expresses no opinion as to the ownership status of the property.

Except for the purposes legislated under provincial securities laws, any use of this report by any third party is at that party's sole risk.

## **4 PROPERTY DESCRIPTION AND LOCATION**

This section of the report is summarized from Rennie and Scott (2007) and Naas (2010).

The Harper Creek property is located approximately 90 km north-northeast of the city of Kamloops, British Columbia, at latitude 51°33' N and longitude 119°42' W (Figure 4-1). The original Harper Creek property comprised 21 Mineral Titles Online (MTO) claims and 34 legacy claims, totalling 9,233.706 ha. Through staking by Yellowhead the property now comprises 131 individual claims totalling 42,636.48 ha.

### **LAND TENURE**

Yellowhead holds 97 MTO cell claims totalling 41,786.48 ha and 34 legacy claims totalling 850 ha for a total controlled tenure of 42,636.48 ha.

Yellowhead acquired the original property via four separate agreements. Eighteen MTO claims were optioned from Callingham Limited (Callingham) for 5,000,000 shares of Yellowhead with a value of C\$50,000. This option was exercised on May 18, 2006.

An additional 21 legacy claims were obtained in an agreement with CM Resources Limited (CMR), who, in turn, had optioned the ground from Cygnus Mines Limited (Cygnus), a wholly-owned subsidiary of US Steel. The CMR agreement with Cygnus allows them to purchase a 100% interest subject to a 3% net smelter return (NSR) royalty, capped at C\$2.5 million. A purchase price of 1 million shares of Yellowhead (with a value of C\$10,000) was paid to CMR to exercise this option on August 10, 2006. On July 30, 2010, Yellowhead acquired title to the 31 Cygnus legacy claims by making an advance royalty payment of \$500,000. The royalty is an NSR royalty capped at \$3 million, which can be adjusted based on the Statistics Canada industrial price index over the period from conversion of the title to the actual royalty payment.

Three legacy (mineral tenures 220877-220879) and three MTO claims (mineral tenures 513235, 513237 and 513239) owned by Argent Resources Ltd. (Argent) were acquired for a payment of C\$10,000 and 100,000 Yellowhead shares (with a deemed value of C\$140,000). Argent acquired these claims from MBI Mining Brokers Inc. (MBI). They are subject to an underlying agreement between MBI and Noranda (now Xstrata plc).

Xstrata has the option to earn a 50% working interest in these six claims, and holds a 2.5% NSR royalty on production from these claims.

Seven mineral tenures were purchased from an individual for C\$55,000. They were fractional claims that underlay the Cygnus-optioned claims and six were abandoned following their acquisition.

Yellowhead staked additional MTO claims adjoining the original Harper Creek property to the north, south, and east (Figure 4-2). The property now comprises 131 individual claims totalling 42,636.48 ha. A table of the mineral tenures is in Appendix 1.

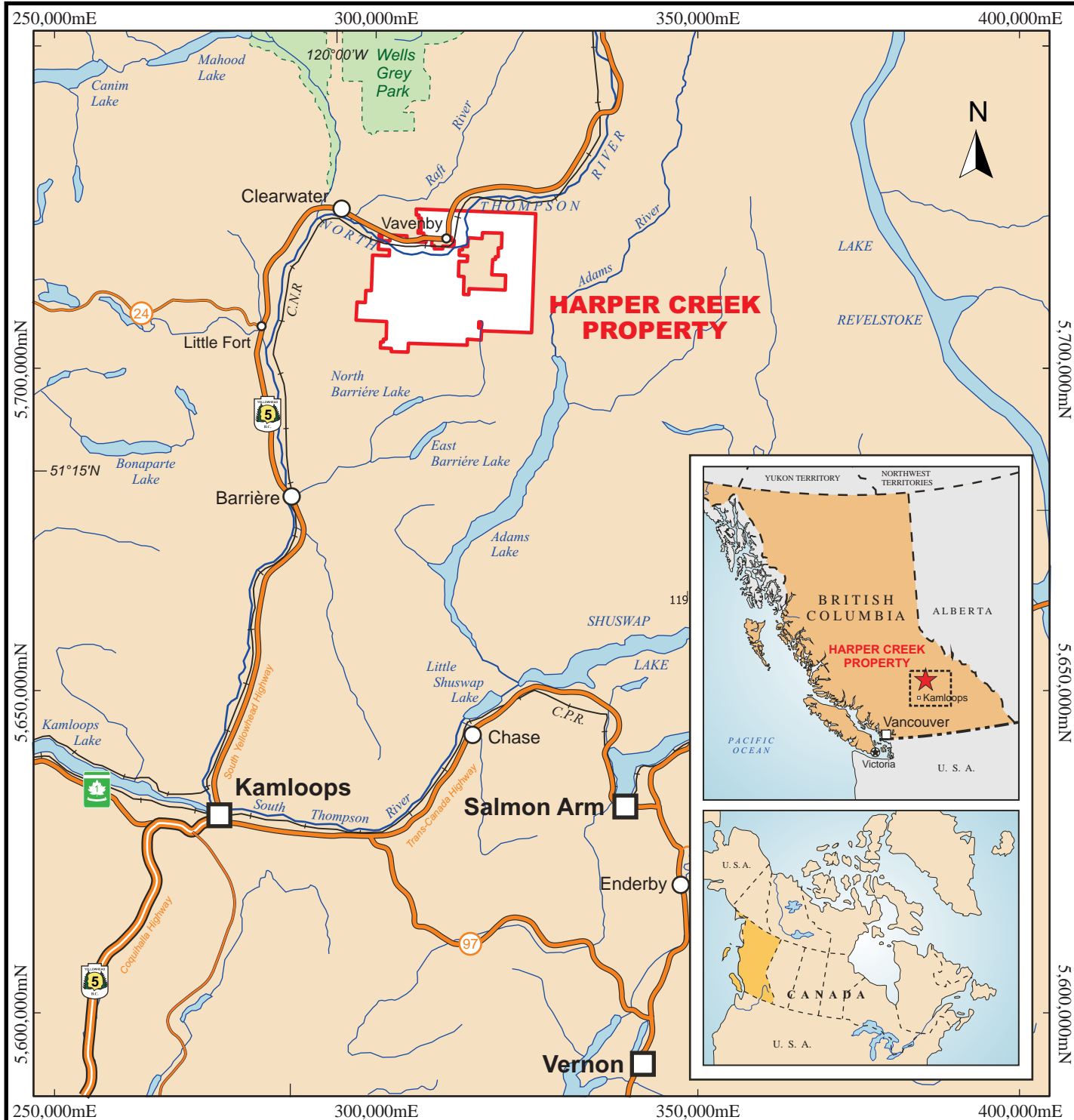


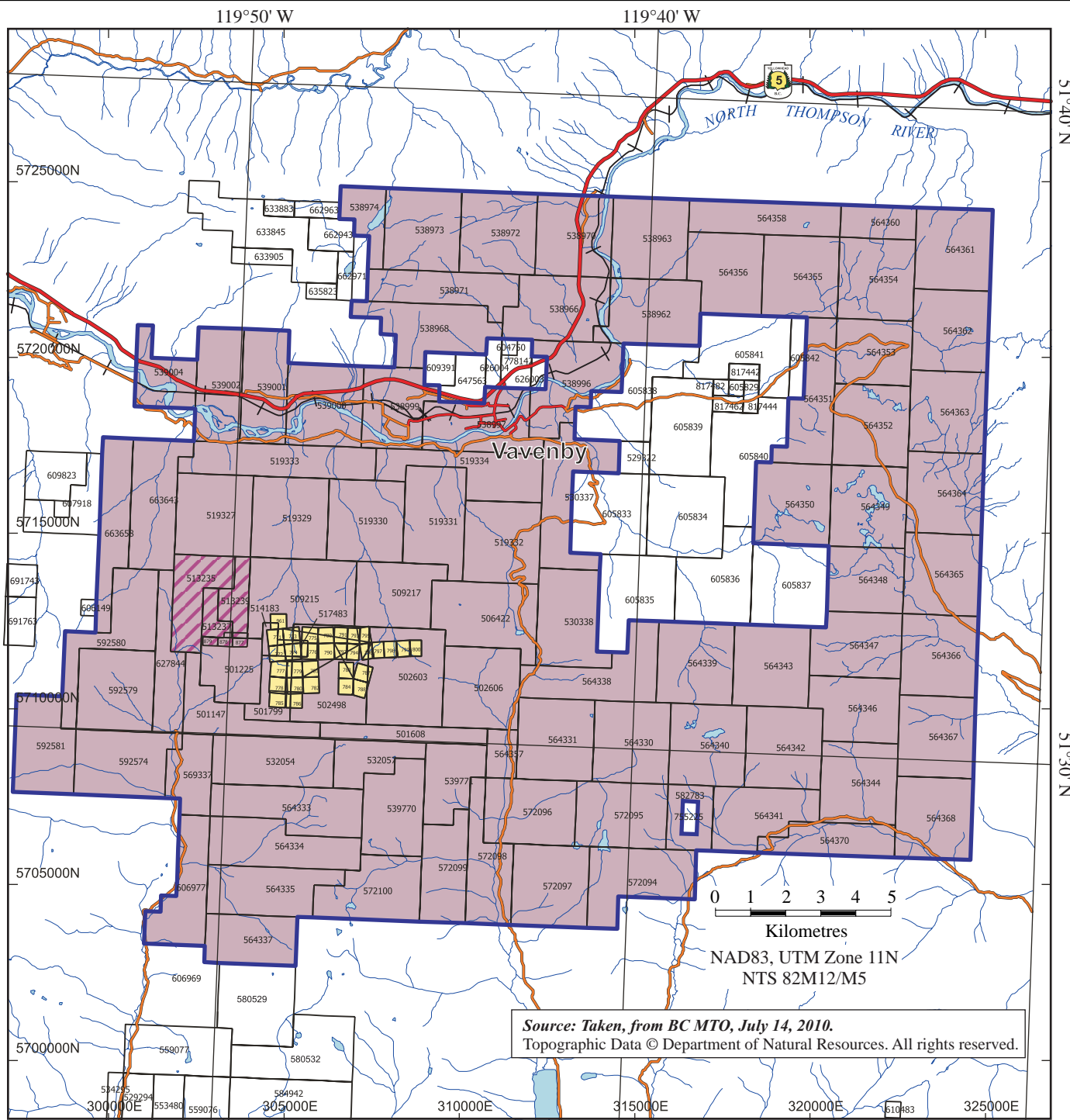
Figure 4-1

**Legend:**  
 Yellowhead Mining's Claim Group (as of July 14, 2010)

**Yellowhead Mining Inc.**  


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*Harper Creek Project*  
 Kamloops Mining Division  
 British Columbia Canada  
**Location Map**



**Legend:**

- Yellowhead Mining Inc. Claims (100% owned)
- Subject to 2.5% NSR
- Optioned from Cygnus Mines Ltd.
- Yellowhead Mining's Harper Creek Claim Group (as of July 14, 2010)  
Labelled with Tenure Number (last three digits for legacy claims;  
all with 220 prefix)
- Other Tenures (as of July 14, 2010)

**Topography**

- Paved Road
- Rough Road
- Waterbody
- Gravel Road
- ++ Railway
- Watercourse

August 2010

Figure 4-2

**Yellowhead Mining Inc.**

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**Harper Creek Project**  
British Columbia Canada

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**Tenure Map**

## **5 ACCESSIBILITY, CLIMATE, LOCAL RESOURCES, INFRASTRUCTURE AND PHYSIOGRAPHY**

### **ACCESSIBILITY**

Kamloops, a city with a population of 93,000, is the principal urban centre in the region. The city is served by regular flights from Vancouver, as well as by rail, bus, and a number of commercial trucking firms. The property encompasses the settlement of Vavenby, and straddles both the Canadian National Railway line and Highway 5. The town of Clearwater is located 17 km west of the property.

Access to the west side of the property is gained via the Birch Island – Lost Creek road for a distance of six kilometres east from the town of Birch Island, and thence via the Jones Creek Forest Service Road (FSR). On the east side, access is from Vavenby via the Vavenby Mountain FSR to the east and central portions of the property, and to the extreme eastern areas via the Barriere River FSR.

Scott Wilson RPA is not aware of any constraints to access to the deposit area.

### **CLIMATE**

The climate is typical of the central interior of British Columbia, with relatively short but warm summers and comparatively mild winters for Canada, generally lasting from late October until April. There is significant relief on the property, and local climatic conditions are very much dependent on elevation. Monthly average temperatures range from 26°C in August to -10°C in January.

Precipitation averages 474 mm annually, with approximately one quarter falling as snow. Maximum precipitation occurs in the month of June.

### **LOCAL RESOURCES**

The principal source of logistical support for the property is Clearwater, with additional support from Kamloops. Vavenby serves as the local base for exploration activities.



**INFRASTRUCTURE**

A 130 kVA electrical power line traverses the property, as do several logging roads. Highway 5 and the Canadian National Railway line also cross the property.

**PHYSIOGRAPHY**

The property is located in the Shuswap Highlands region of the central interior of British Columbia. Topographic relief is moderate, with elevations on the property ranging from 450 masl in the North Thompson River valley to 1,850 masl. The entire area has been glaciated and the mountain tops are somewhat rounded, although valley slopes can be quite steep in places. The claims are mostly covered by coniferous forest, and logging is the principal economic activity in the area. Much of the property has been logged at least once.

## **6 HISTORY**

Copper mineralization was first discovered at Harper Creek in 1966 by Noranda and Québec Cartier (a wholly-owned subsidiary of US Steel). Both companies made their discoveries through regional prospecting and stream sediment sampling. Noranda staked the Harper Creek claims over what is now the western half of the known deposit, and Québec Cartier staked the Hail claims on adjacent ground to the east. This effectively split the presently-defined deposit in half.

The following year both companies embarked on grid-based soil sampling and geophysical surveys. Québec Cartier carried out bulldozer trenching and drilled six diamond holes. Noranda commenced drilling in 1968, and continued until 1970 when a joint venture was established with Québec Cartier. Québec Cartier did not drill any holes in 1968 but resumed drilling the following year, continuing into 1970, when the joint venture came into effect.

Under the terms of the joint venture agreement, Noranda became operator of the project. Diamond drilling and a modest amount of geophysical surveying were carried out through 1972. In 1972, an economic assessment of the project was made to study the feasibility of open pit mining of what were then two separate deposits (now combined as one). The study contemplated open pit reserves of 85.5 million tons grading 0.388% Cu, and concluded that the rate of return for the proposed operation was not sufficient to warrant production. Scott Wilson RPA notes that this reserve figure is not compliant with NI 43-101 and is provided for historical reference only. Historical resource and reserve estimates should not be relied upon.

Additional studies were carried out in 1973 and 1974 which included addition of Au, Ag, and Mo credits to improve the value of the mineral resource and metallurgical studies to optimize estimates of recoveries. The study concluded that a return on investment of 10.7% could be achieved for the project, and that further improvements could be gained by additional optimization of the pit design. Computer optimization of the pit design was carried out which resulted in a decrease in waste tonnage from earlier designs, and a decrease in cut-off grade to 0.30% Cu. Additional work was recommended to further refine the project economics, but the joint venture was terminated in 1974.

The properties lay idle until 1986, when Aurun Mines (Aurun) optioned the Québec Cartier ground. Aurun carried out trenching and resampling of core to investigate the potential for high-grade Cu-Mo, precious metal, and Ti-bearing mineralization, as well as the leachability of lower grade Cu mineralization. Phillips Barratt Kaiser Engineering Ltd. (PBK) was commissioned by Aurun to carry out a pre-feasibility study on the project. The PBK study reported “geological resources” of 96 Mt grading 0.41% Cu, 0.045 g/t Au, and 2.5 g/t Ag, with a “mineable resource” of 65.34 Mt grading 0.36% Cu, 0.040 g/t Au, and 2.2 g/t Ag. Scott Wilson RPA notes that these resource estimates are not compliant with NI 43-101 and are provided for historical reference only.

The conclusion of the study was that the project was not economic, although additional exploration was warranted. Québec Cartier terminated the agreement with Aurun in 1991.

American Comstock purchased the Noranda ground in 1996, and acquired an option on the Québec Cartier claims. The Québec Cartier property was, by then, owned by Cygnus, another wholly-owned subsidiary of US Steel. American Comstock drilled eight diamond holes on the Cygnus ground, and shortly thereafter dropped the option. Over the next few years, some of the Noranda claims were allowed to lapse, and, in 2004, American Comstock sold six legacy claims to Argent.

C. Naas, currently a director and project manager with Yellowhead, staked claims over and surrounding the original Harper Creek/Hail property in 2002 for Callingham. The property was consolidated through a series of agreements (see Section 4 under Land Tenure) by Yellowhead. Yellowhead has conducted exploration work comprising soil sampling, geophysical surveys, prospecting, geological mapping, resampling and relogging of old core, and diamond drilling from 2005 until the present time. In 2007 and again in 2008, Scott Wilson RPA was retained to prepare an estimate of Mineral Resources for the project. Yellowhead has also commenced preliminary scoping level economic reviews, environmental baseline studies, and engagement of local First Nations groups.

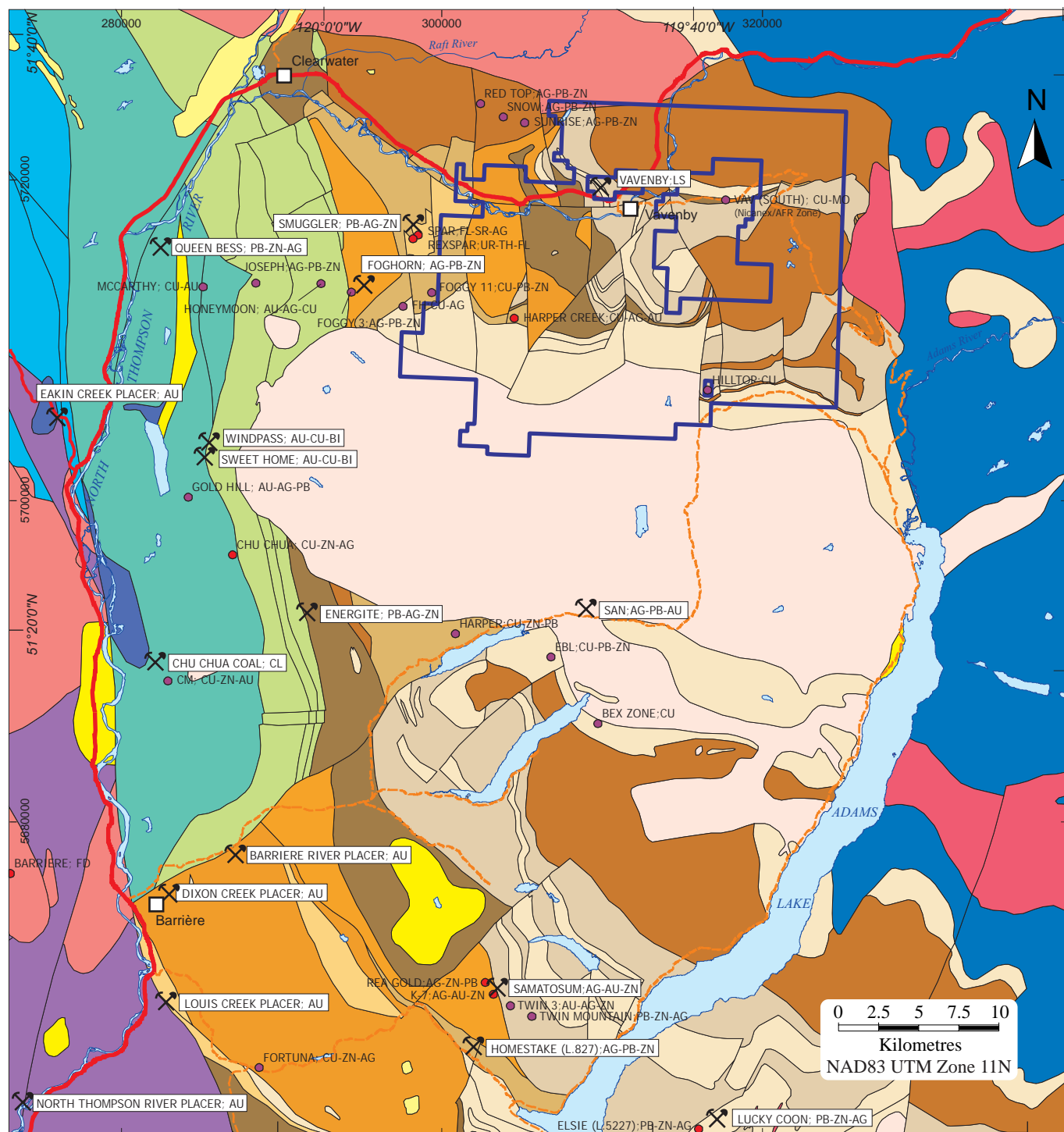
## 7 GEOLOGICAL SETTING

### REGIONAL GEOLOGY

The Harper Creek property lies within Kootenay terrane pericratonic rocks of the Omineca Complex (Figure 7-1). The area is underlain by deformed and metamorphosed Paleozoic sedimentary and volcanic rocks of the Eagle Bay Assemblage and Fennell Formation (Schiarizza and Preto, 1987; Paradis et al., 2006). The Eagle Bay Assemblage comprises deformed and metamorphosed Lower Cambrian to Mississippian sedimentary and volcanic rocks deposited along the western edge of the North American craton. They have been intruded by Devonian to Lower Mississippian foliated granite to diorite sills and dikes and by Middle to Upper Jurassic and Cretaceous granitic plutons (Paradis et al., 2006). The Fennell Formation is a package of Upper Devonian to Middle Permian volcanic and sedimentary rocks which have been overthrust onto the Eagle Bay rocks. All of these rocks underwent greenschist to lower amphibolite facies regional metamorphism during Jurassic to Cretaceous orogeny.

Overlying the Eagle Bay Assemblage are Eocene-age Kamloops Group volcanic rocks. The Eagle Bay Assemblage is bounded on the east by Shuswap metamorphic complex rocks, and on the west by the Upper Devonian to Middle Permian Fennell Formation.

Eagle Bay rocks are interpreted to have originated in an island arc setting with adjacent back-arc basin related to a Late Proterozoic to Early Paleozoic subduction zone, located along the west coast of the ancient North American continent (Paradis et al., 2006). Volcanic processes associated with arc-formation and rifting resulted in deposition of a wide variety of sulphide deposits of the types commonly found in this environment. Several such deposits occur in the area surrounding Harper Creek. These include volcanic-hosted massive sulphide (VHMS) deposits, such as Homestake, Rea Gold, and Beca, as well as volcanic-sedimentary-hosted massive sulphide or sedimentary exhalative (SEDEX) deposits such as Mosquito King, EX 1, and Cu5. Harper Creek is interpreted as a highly deformed VHMS deposit (Höy, 1999, quoted in Paradis et al., 2006).



Legend:	
<b>Quaternary</b>	<b>Proterozoic-Paleozoic</b>
Basaltic volcanics	Shuswap Assemblage
<b>Tertiary</b>	Eagle Bay Assemblage: undifferentiated
Kamloops Group: undifferentiated volcanics	Dixon Ridge Unit
<b>Tertiary-Mesozoic</b>	Foghorn Mountain Unit
Granite, quartz porphyry	Forest Lake Unit
<b>Mesozoic</b>	Graffunder Lakes Unit
Baldy Batholith: quartz monzonite	Johnson Lake Unit
Granodiorite	Rexspar Unit
Nicola Group: sediments	Skwaam Bay Unit
<b>Mesozoic-Paleozoic</b>	Slate Creek Unit
Harper Ranch and(?) Nicola Groups: seds	<b>Min. Occurrences (BC Minfile)</b>
<b>Paleozoic</b>	Past Producer
Fennell Assemblage: Upper/Lower Structural Division	Developed Prospect
basaltic volcanic/marine sediments, volcanics	Prospect
Mount Ida Assemblage: metamorphics (calcsilicates)	

0 2.5 5 7.5 10  
Kilometres  
NAD83 UTM Zone 11N

Figure 7-1

**Yellowhead Mining Inc.**

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*Harper Creek Project*  
British Columbia Canada

**Regional Geology**

August 2010 Source: Open File 2005-2, in Naas, 2006.

## **LOCAL AND PROPERTY GEOLOGY**

The earliest detailed geological work on the property was carried out by Noranda and Québec Cartier during the course of their tenure in the 1960s and 1970s. Gary Belik mapped the area for a 1973 M. Sc. thesis. Regional geological mapping encompassing the property was done on behalf of the BC Ministry of Energy, Mines, and Petroleum Resources (EMR) by Schiarizza and Preto (1987) and by Höy (1997). Compilation of available mapping in the area was carried out by EMR and released as part of a digital geological map of BC (Massey et al., 2005; available at <http://www.empr.gov.bc.ca/>). Most recently, CME Consultants Inc. (CME), an engineering firm based in Richmond, BC, has mapped the surface geology, logged drill core, and conducted petrographic and rock geochemical studies (Naas, 2006, 2007, and 2008; Naas and Soloviev, 2008).

The Harper Creek property is predominantly underlain by Late Proterozoic to Mississippian phyllites and schists of the Eagle Bay Assemblage. The southern portion of the property is underlain by Mid-Mesozoic granitic rocks of the Baldy batholith (Figure 7-2). The rocks have been fairly intensively metamorphosed and, in some cases, sheared, making identification of the protoliths in hand specimen difficult. CME has undertaken a series of programs to improve the naming conventions and overall understanding of the geological environment for the project area. The work being undertaken by CME is not complete, however, it has resulted in a reorganization and renaming of the principal rock units on the property. In addition, the revised descriptions and unit names have been correlated with those of earlier works.

CME geologists, Soloviev and Naas (2008), have split the stratigraphic succession into three principal domains:

- An older metamorphosed mafic volcanic-dominant package
- A younger metamorphosed sedimentary-dominant package
- A transition zone between the above two domains

Descriptions, extracted from Soloviev and Naas (2008), are provided below:

### ***OLDER METAVOLCANIC-DOMINANT***

Chlorite phyllite formed after mafic ash tuff. This package of rocks contains minor crystalloclastic mafic tuff containing coarser, angular fragments of feldspar crystals,

mafic tuffs with felsic lapilli, mafic tuffs with numerous (<1 mm) lenses of dolomite or siderite, and graphitic chlorite phyllites after mafic tuffs. The unit ranges from 200 m to 400 m in thickness and corresponds to Höy, 1996 unit 1b. The chlorite phyllite dominantly consists of pale green to dark green chlorite, with variable quartz, carbonate, feldspar, sphene, and commonly contains scattered quartz “pebbles” up to 5 mm to 10 mm across converted into augen-like “quartz eyes”.

#### ***YOUNGER METASEDIMENTARY-DOMINANT***

This package is composed of essentially argillaceous sedimentary rocks varying from tuffaceous argillite and tuffite to either alternating thin-bedded tuffite and chert/jasper or alternating pelitic and carbonaceous argillite. Thin parallel to cross-laminations are common in these units, the latter being locally suggestive of unequal sliding of unlithified sediments. Syn-sedimentary brecciation is locally evident. Compared to the lower package, this upper rock package appears to be more “sedimentary” rather than volcanogenic, containing less tuffaceous but more carbonaceous and carbonate material. The uppermost parts of the section also incorporate thick (10 m to 50 m) horizons of calcareous argillite and tuffite, often with abundant siderite and calcite forming series of thin lenses and saturating the rock matrix. Lenses of graphitic limestone are also present. This unit ranges from 100 m to 300 m in thickness.

#### ***TRANSITION ZONE***

The transition zone between the above noted rock packages is approximately 100 m to 200 m thick. The upper part of the older metavolcanic-dominant package and the lower part of the younger metasedimentary-dominant package incorporate several continuous units of highly siliceous rocks that may be siliceous phyllites after felsic extrusives or felsic quartz-porphyry dykes or sills. In addition, this transition zone incorporates large lens-like bodies of quartzite as well as thick zones of intense silicification.

Within the broader lithological domains described above, Naas and Soloviev (2008) have subdivided individual rock types and correlated them with those of earlier workers. These are summarized in Table 7-1 below.

**TABLE 7-1 LITHOLOGIC UNIT CORRELATIONS**  
**Yellowhead Mining Inc. – Harper Creek Property**

<b>Soloviev and Naas (2008)</b>	<b>Høy (1996)</b>	<b>Schiarizzo and Preto (1987)</b>	<b>Belik (1973)</b>	<b>Noranda (1969)</b>	<b>Quebec Cartier (1969)</b>
Baldy Batholith. (BB)	n/a	Kg: Cretaceous Granitic Rocks.	Baldy Batholith.	Granite and Biotite Granodiorite.	Granite and Biotite Granodiorite.
Chlorite Phyllite; after mafic tuffite or tuffaceous argillite; as well as after alternations of chert. (CP)	Unit 1a Greenstone; foliated, massive to fragmental, lesser chlorite phyllite.	EBF.	Unit 2 Foliated fragmental greenstone and chloritic phyllite.	Chloritic quartz phyllite.	Not observed on the property.
Hydrothermal Quartzite	Unit 2a Quartzite, sericitic quartzite, albite-sericite-quartzite.	EBQ and EBS.	Unit 6a Orthoquartzite, sericite quartzite, albite-sericite quartzite.	Quartzitic.	Quartzitic.
Sericite quartz phyllite. (SQP)	Unit 1a & 1b, 2b grey-green to tan sericite-quartz phyllite.	EBA but observed locally within all Eagle Bay rocks.	Unit 6a Orthoquartzite, sericite quartzite, albite-sericite quartzite.	Semi siliceous sericite phyllite, soft fawn coloured banded phyllite.	Unit 3 Green-grey phyllite, quartz-sericite schist, sericitic quartzite.
Graphitic Phyllite. (GP)	Unit 2c Carbonaceous and calcareous phyllite, grey limestone and minor tan dolomite.	EBA ~ 10% of the assemblage	Unit 5 Graphitic and carbonaceous phyllite with dolostone.	Black phyllite.	Unit 3 Black phyllitic slate.
Siliceous Phyllite. (Sil-P)	Unit 1d Quartz-sericite phyllite, minor schist, tan to silvery grey.	EBA.	Unit 1 Quartzofeldspathic phyllite.	Phyllite, Siliceous grey phyllite.	If observed likely incorporated into Unit 3.
Quartz Porphyry. (QP)	Unit 1e: Quartz eye phyllite.	Quartz-eye sericite schist (Quartz porphyry).	Included within Unit 4 – lustrous phyllite.	Quartz sericite chlorite augen schist.	Unit 2 Quartz-mica “augen” schist, sericitic quartzite.
Siliceous Chlorite Phyllite. (Sil-CP)	Unit 2a Quartzite, sericitic quartzite, albite-sericite-quartzite.	EBQ, possibly EBS.	Unit 4 White – light green, foliated lustrous phyllite.	Siliceous sericite phyllite, quartzitic phyllite.	Unit 3 Green-grey phyllite, qtz-ser schist, sericitic quartzite.
Chlorite Phyllite, possibly after mafic tuff. (CP)	Unit 1b Chlorite phyllite, minor sericite or quartz-sericite phyllite.	EBG but observed locally w/n all Eagle Bay rocks.	Unit 3 and 8 Foliated & fragmental Greenstone and Chlorite phyllite.	Dark chlorite phyllite, greenstone, siliceous chlorite phyllite.	Unit 4 Greenschist, Qtz-chl-ser schist. Also noted w/n Unit 3 as green-grey phyllite.
Limestone (Lst), locally graphitic.	Unit 2c Carbonaceous and calcareous phyllite, grey limestone and minor tan dolomite.	EBG and EBL the latter of which is graphitic with abundant calcite veining.	Unit 6b Carbonaceous quartzite.	n/a	Unit 5 Blue-grey crystalline limestone.



<b>Soloviev and Naas (2008)</b>	<b>Høy (1996)</b>	<b>Schiarizzo and Preto (1987)</b>	<b>Belik (1973)</b>	<b>Noranda (1969)</b>	<b>Quebec Cartier (1969)</b>
Devonian orthogneiss. (Dgn)	n/a	Devonian orthogneiss. (Dgn)	Unit 7&10 Chlorite-biotite gneiss and green fragmental phyllite.	Siliceous chlorite-(sericite) phyllite.	Unit 1 Quartzfeldspar-chlorite gneiss, diorite gneiss.

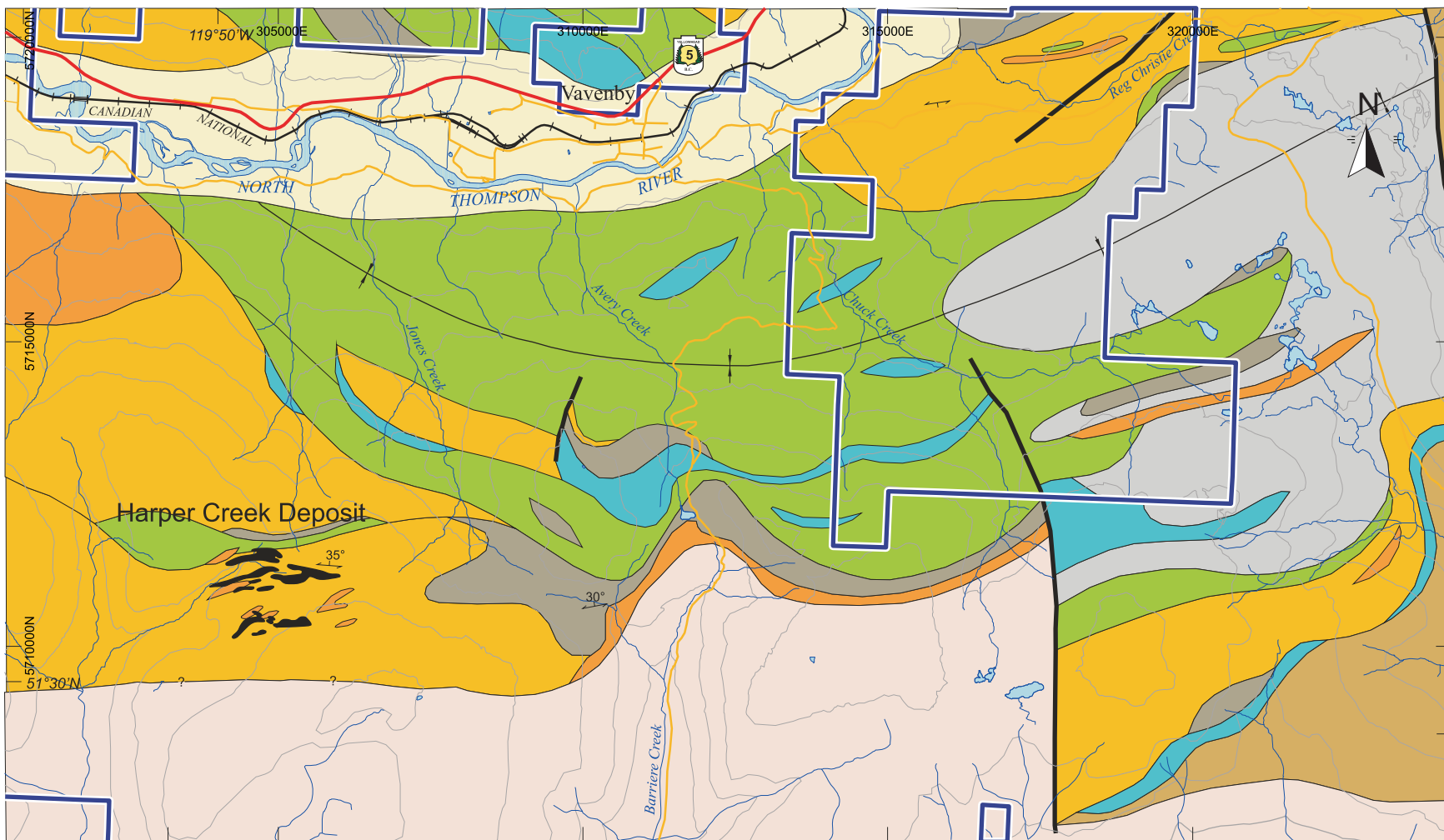
Several later dikes and sills, representing a number of intrusive events, have been noted on the property. These are described by Naas (Naas, 2010) as:

- Intermediate to felsic dikes, sills and plugs
- Felsic (quartz-feldspar porphyry) dikes, sills, and plugs
- Quartz-porphyry dikes, sills and plugs
- Mafic (lamprophyre?) dikes
- Tertiary andesite (intermediate?) dikes

The general orientation of the stratigraphy is east-west-striking, with low to moderate northerly dips (Figure 7-2). Faulting is evident from juxtaposition of disparate rock units as well as surface lineaments. Displacement across these structures has yet to be determined.

Naas (2006) reports three phases of deformation. D1 and D2 events have resulted in tight southeast-verging, northwest-striking isoclinal folds. Folding appears to have resulted in overturning of beds, and repetition of lithologies logged in diamond drillholes. A D3 event is associated with intrusion of the Baldy batholith.

7-7



**Legend:**

<b>GEOLOGY</b>	<b>SYMBOLS</b>
Alluvium	Syncline axis
<b>Baldy Batholith</b>	Fault
Granodiorite	Foliation
<b>Eagle Bay Formation</b>	Surface expression of mineralization
Sediments, ± felsic volcanics	Harper Creek Property (as of July 14, 2010)
Limestone	
Argillite	
Felsic volcanics	
Felsic flows	
Mafic volcanics	

August 2010

Source: Topographic data © Department of Natural Resources.  
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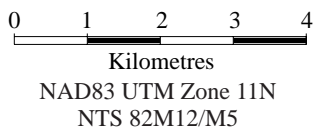


Figure 7-2

**Yellowhead Mining Inc.**

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**Harper Creek Project**  
British Columbia Canada

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**Property Geology**

## **8 DEPOSIT TYPES**

Harper Creek is interpreted to be a polymetallic volcanogenic sulphide deposit, comprising lenses of disseminated, fracture-filling and banded Fe and Cu sulphides with accessory magnetite. Mineralization is generally conformable with the host-rock stratigraphy, as is consistent with the volcanogenic model. Sulphide lenses are observed to measure many tens of metres in thickness with kilometre-scale strike and dip extents.

## 9 MINERALIZATION

Sulphide mineralization comprises chalcopyrite along with accessory pyrite, magnetite and pyrrhotite. Minor components are bornite, covellite, sphalerite, galena, molybdenite, and arsenopyrite. The copper mineralization is also accompanied by significant concentrations of gold and silver. Sulphides occur as coatings on joints and fractures, thin laminae, as grains distributed along foliation planes, as well as blebs and fracture-filling grains in quartz veins.

Copper grades are typically less than 1.0% although they can range up to several percent Cu. Gold grades are generally less than 0.5 g/t, and most commonly between 0.05 g/t and 0.1 g/t. Silver grades generally range in the order of 0.5 g/t to 10 g/t but can be as high as several tens of g/t.

Naas (2010) describes finely disseminated platy chalcopyrite in strongly sheared and chlorite-altered mafic volcanic host rocks. Coarse-grained strong chalcopyrite mineralization occurs in quartz-rich zones within quartz phyric felsic volcanic protoliths. These rocks are also host to strongly silicified and bleached zones with pyrite-bearing quartz stockworks. Cherty exhalite horizons occurring at sedimentary-volcanic contacts host semi-massive pyrrhotite ± pyrite, magnetite, chalcopyrite, sphalerite and rare galena, native gold, and tetrahedrite. Sphalerite usually occurs as lamellae within sheared graphitic argillite, in association with green altered tuff or volcanic sedimentary rocks.

Hydrothermal alteration associated with the mineralization comprises four phases (Naas, 2006), with the earliest event being silicification along with chlorite and/or sericite (silicic facies). Chlorite is most commonly found in mafic rocks but can occur in siliceous volcanic rocks as well. Quartz veins associated with this event are highly deformed and boudinaged. Siderite occurs with sulphide mineralization, particularly in association with semi-massive sulphide zones. Dolomite (ankerite?) is observed to overlie the mineralization.

The second alteration event appears to be related to the regional deformation which resulted in south-southeast-directed isoclinal folding. This alteration facies is typified by remobilization of quartz into tensional features such as fold hinges.

The third alteration style is related to the D3 deformation event associated with the intrusion of the Baldy batholith. It resulted in remobilization of sulphides, including chalcopyrite, into curvilinear tension veins.

The fourth alteration is a late clay carbonate phase that post-dates Tertiary dikes (Naas, 2010). Quartz-carbonate hydrothermal breccia shear veins occur with fine-grained brown and sheared brassy pyrite mineralization (north-south striking dipping at 60°). This event resulted in remobilization of sulphides, quartz, ankerite and siderite into steeply dipping to subvertical late fractures, and is responsible for widespread intense clay-carbonate overprinting. Locally, siderite is remobilized into late tensional dilatant zones, and clay alteration is especially strong where hydrothermal fluids were directed and trapped in D3 fold hinges. Widespread moderate to intense bleaching occurs with clay alteration of pre-existing chlorite (and sericite) to phengite, clay, and remobilized carbonate. This clay alteration can be very intense and has resulted in soft clayey lamellae which have weakened the rock mass, affecting core recovery. Pre-existing lithological and alteration features are often destroyed by this alteration phase.

# 10 EXPLORATION

## EARLY WORK

(Summarized from Sanguinetti and Lefebvre, 2006 and Naas, 2006 and 2010)

Earliest exploration work at Harper Creek began in 1967 and comprised grid-based soil geochemistry and geophysical surveys. Noranda conducted an initial program over the central part of the Harper Creek claims along lines oriented north-south and spaced 800 ft. apart, with samples every 200 ft. This grid was eventually in-filled with lines spaced at 400 ft. Québec Cartier carried out 12.9 line-km of soil sampling on 13 lines located in the north and south central areas of the Hail claims. Soil sampling grids were expanded in 1972, under the joint venture, to include areas in the north, south, and southwest extremities of the property. A total of 36.8 line-km of grid was added in this phase.

Soil sampling with analysis for Cu appeared to have been quite successful in locating buried mineralized bodies and led to successful trenching, particularly on the Québec Cartier ground on the K Zone. Québec Cartier outlined two principal target areas, termed the K and M Zones. Noranda's soil sampling resulted in the discovery of two anomalous zones, termed Areas 1 and 2 (see Figure 11-1).

Noranda's geophysical surveys carried out between 1967 and 1971 consisted of 11.5 line-km of ground magnetometer, 51.49 line-km of very low frequency electromagnetic (VLF-EM), and 57.92 line-km of induced polarization (IP) surveys. The Québec Cartier work initially consisted of 137.16 line-km of ground magnetometer surveys, carried out in 1967. In 1972, the geophysical work was expanded to peripheral areas of the property. VLF-EM was carried out over these areas, and four lines of IP were run over a Cu-in-soil anomaly in the southwest corner of the claims and six lines of IP, in the extreme southern part.

Québec Cartier's magnetometer survey detected small lenses of magnetite, but it is unclear as to how successful this was in defining drill targets. Noranda's magnetometer work did not detect either the Area 1 or Area 2 anomalies. The VLF-EM, however, detected anomalies over all mineralized zones. IP detected the Area 1 mineralized body, but anomalies in Areas A and B were interpreted to be due to graphitic zones.

Québec Cartier's initial work led to bulldozer trenching and diamond drilling. Seven trenches, totalling 1,524 m, were excavated over the central portion of the property in 1967. Diamond drilling also commenced in that year (see Section 11, Drilling). Noranda began diamond drilling in the following year. The total number of metres of drilling in the vicinity of the Harper Creek deposit, as indicated by the database supplied to Scott Wilson RPA, is 26,854.47 m in 155 holes.

Both Québec Cartier and Noranda routinely assayed the core for Cu and intermittently for other elements. Noranda assayed selected samples for Au, Ag, Pb, and Zn, and in some cases ran composited intervals for Au and Ag. For more details regarding the early diamond drilling, see Section 11, Drilling.

Aurun conducted resampling of the existing drill core and some of the trenches but did no new drilling or trenching.

In 1996, American Comstock conducted drilling along the northern, down-dip extension of the K Zone and Area 1. They drilled 2,847.4 m in eight holes and assayed all samples for Cu, Au, Ag, and Zn. The American Comstock drilling was successful in extending the boundaries of the known mineralization to the north.

## **YELLOWHEAD**

Yellowhead began exploration work in 2005 by embarking on a program of compilation and digitization of the existing database. Work also included verification of drillhole collar locations, collection of old drill core, and relogging and resampling of old drill core to compare with the original results. This work is described in an internal technical report by Sanguinetti and Lefebvre (2006). The results of the resampling program were favourable, and the report recommended a two-phase exploration and verification program with estimated expenditures of \$2.8 million in the first phase and \$5.3 million in the second.

### ***PHASE I***

In May 2006, Yellowhead initiated the Phase I exploration program. Aeroquest Limited was contracted to carry out a 1,097.4 line-km helicopter-borne magnetic and EM survey which encompassed the entire Harper Creek deposit area. This was followed by exploration field work which included road maintenance, 34.726 line-km of soil sampling,

rock geochemistry sampling, continuation of the sampling and logging of the old core, reclamation work, and 2,324.4 m of diamond drilling in seven holes. The number of drill samples totalled 993.

The geophysical surveys outlined a number of anomalies for follow-up. The soil sampling was conducted over four grids and one side-hill profile on some of these anomalies. Samples were analyzed for Zn and Cu. All sampled areas were outside of what is presently considered the boundary of the Harper Creek deposit, and all returned anomalous results which warranted additional work (Naas, 2006).

The diamond drilling focused on Area 1 and to a lesser degree on the North K Zone (see Figure 11-1). Drillholes were targeted to confirm earlier results and to fill in gaps. All drillholes intersected Cu mineralization similar in style and grade to the mineralization found by earlier workers.

#### ***PHASE II***

Phase II exploration, conducted in 2007, consisted of soil sampling on three high-priority airborne geophysical targets. A total of 516 soil samples were taken over 12.25 line-km of grid that delineated several prospective targets for follow-up. Drilling comprised five holes for an aggregate depth of 1,777 m to refine the geologic model and confirm historic results (Naas, 2007). A total of 1,534 core samples were taken.

#### ***PHASE III***

Phase III exploration, conducted between March and September 2007 consisted of an in-fill diamond drill program that totalled 11,664.25 m in 26 holes (8,844 samples). Regional exploration consisted of 31.82 line-km of soil sampling over a target known as the M Anomaly (located just over 2 km east of the Harper Creek deposit) along with the three areas identified by the 2006 airborne geophysical surveys, 81.25 line-km of ground magnetics, 44.63 line-km of HLEM and 210 km<sup>2</sup> of aerial photography. The aerial photography survey was conducted at 1:10,000 scale and was used in the creation of a one metre (10.56 km<sup>2</sup>) and five metre (40 km<sup>2</sup>) digital terrain model (DTM) and corresponding topographic maps over the study area (Naas, March 2008).



***PHASE IV***

Conducted between September 2007 and April 2008, Phase IV consisted of diamond drilling on the Harper Creek deposit as well as regional exploration work on the M anomaly. Work completed comprised the following:

- 37 diamond drillholes totalling 11,818.6 m and 10,716 samples
- Petrographic studies encompassing 99 thin sections and 50 polished thin sections
- 27 whole rock analyses
- 5 km of drill access trail
- 32 line-km of IP
- Reclamation of drill roads and pads

Drilling was done to increase confidence in the mineral resource and expand it along known trends. The holes were drilled to fill in gaps in the South Zone, and along the eastern part of the North Zone. Additional details regarding this program are provided in Section 11 of this report.

The petrographic work was carried out to improve the understanding of the rock types on the property to assist with interpretation and core logging. Similarly, the whole rock analyses provided additional means for identifying key rock types by protolith.

***PHASE V***

Phase V was carried out between April 2008 and January 2009 and consisted of the following:

- Relogging and resampling of old drill core: 73 holes, 10,479.75 m and 4,735 samples
- Establishment of 39.475 line-km of grid
- 1,598 soil samples
- 39.475 line-km of ground magnetometer survey
- Geological mapping on scales of 1:15,000 and 1:2,000
- 336 rock samples

Resampling of the historic drill core allowed for the introduction of multi-element and precious metal assay data into the resource model database and provided more confidence in the historic Cu grades.

The relogging was carried out to provide a basis for reconciliation of the older data with the more recent work. The geological mapping was for identification and understanding of the lithologies seen in the drill core, with the ultimate goal of a complete revision of the interpretation.

Soil sampling and ground geophysics were conducted over extended gridlines at the M Anomaly grid.

The magnetic survey was conducted on a grid established just south of the Harper Creek deposit boundary, as it is presently defined. The grid consisted of 33.53 line-km of cut line (15 lines) with 5.975 line-km of uncut line (3 lines). Data were collected using a GSM-19 Overhauser instrument, calibrated for diurnal variations by a GSM-19 Proton base station.

#### ***PHASE VI***

From January 16 to August 15, 2009, the Phase VI program encompassed a review of the geological data and interpretations to develop a consistent legend for all rock units, with a comparison and reconciliation to the work done by earlier geologists. The work included petrographic studies, whole rock and geochemical analyses on selected core and surface rock samples and core relogging of seven holes on two sections. Photographs of representative rock and core samples were collected for reference.

# 11 DRILLING

## EARLY WORK

Diamond drilling at Harper Creek commenced in 1967 and has continued intermittently until the present time. In this report, all drilling completed before Yellowhead's acquisition of the property is considered "early work". This includes holes drilled from 1967 until 1996. The early drilling is summarized in Table 11-1 and appears in Figure 11-1.

**TABLE 11-1 SUMMARY OF EARLY DRILLING, 1967-96**  
**Yellowhead Mining Inc. – Harper Creek Property**

Hole Series	Operator	Year	No. Holes	Metres
67-H	Québec Cartier	1967	6	546.19
NH	Noranda	1968	17	2,105.82
69-H	Québec Cartier	1969	27	4,739.19
NH	Noranda	1969	13	1,733.56
NH	Noranda	1970	57	8,315.51
J	Joint Venture	1970	12	2,328.69
J	Joint Venture	1971	27	5,593.82
J	Joint Venture	1972	4	456.74
J	Joint Venture	1973	5	625.45
96	Amer. Comstock	1996	8	2,847.44
<b>Total</b>			<b>176</b>	<b>29,292.41</b>

Notes:

1. Table 11-1 includes holes drilled in areas of the property outside of the Harper Creek deposit. Holes drilled in the deposit area prior to Yellowhead's involvement total 155 (26,854.5 m).

Most of the drilling was BQ-size core (36.4 mm dia), although it is reported that Québec Cartier's initial program in 1967 used NQ (47.6 mm) equipment. American Comstock's core was NQTK (47.8 mm).

Most of the collars were surveyed by independent legal surveyors, using transit and tying into local property grids. Downhole surveys were not done.

Noranda's holes were surveyed by McWilliam, Whyte, Goble and Associates, of Kamloops. Québec Cartier used McElhanney (now McElhanney Consulting Services Ltd.), a survey company based in Vancouver. In 1971, when the joint venture was in

effect, Noranda converted the Québec Cartier surveys to the Noranda grid. American Comstock personnel surveyed their drillhole collars using GPS.

Québec Cartier concentrated their drilling on what was known then as the “K” and “M” soil geochemistry anomalies. Noranda’s soil sampling outlined two anomalies on their half of the property, and these were termed Areas 1 and 2 (Figure 11-1). Almost all of the drilling done under the joint venture agreement was carried out in the North and South K Zones (Figure 11-1).

As mentioned in the previous section of this report, both Québec Cartier and Noranda routinely assayed the core for Cu and intermittently for Au, Ag, Pb, and Zn.

American Comstock drilled primarily along the northern, down-dip extension of the North K Zone. All of the samples from this program were analyzed for Cu, Au, Ag, and Zn.

## **RECENT WORK**

### **2006**

The Yellowhead diamond drilling in 2006 was contracted to Atlas Drilling Ltd. (Atlas), which employed a Longyear Super 38 drill to drill 12 holes to an aggregate depth of 4,101.40 m. Hole size was NQ2 (50.6 mm dia.). Hole collars were surveyed using a GeoExplorer XT GPS receiver that was differentially corrected using a public domain GPS Base Station located in Williams Lake, BC.

Scott Wilson RPA notes that some of the 2006 holes were checked using acid dip tests only (Holes HC06-01 and HC06-02). Drillholes HC06-03 to HC06-06 were surveyed using a Pajari directional survey tool, while drillhole HC06-07 was not surveyed (Naas, 2006). Drillholes HC06-08 to HC06-10 were surveyed using an Icefield MI-3 digital multishot directional survey tool. Due to equipment failure, drillholes HC06-11 and HC06-12 were not surveyed.

The core was transported by the drillers to the logging facility at Vavenby. There, the core was laid out on racks, where it was realigned, washed, and photographed. Metric conversions and locations of the footage blocks were made, and the downhole intervals for the core in each box were determined. The boxes were labelled with metal tags

containing the hole number, box number, from and to values. The core was then logged for RQD, recovery, and magnetic susceptibility.

Management of the drilling, sampling, and core logging was conducted by CME. CME is not independent of Yellowhead, owing to the fact that two of the directors of Yellowhead are principals of CME.

Wherever possible, the drillers marked the core for alignment. Technicians used these marks to realign the core and carry out oriented structural measurements. Once the geotechnical and structural logging was completed, a geologist logged the lithology, alteration, and mineralization. The core was then marked for sampling, and tags were stapled at each sample location. Two specimens of core from each sampled interval were taken and subjected to a bulk density determination. The bulk density was measured using a water-immersion method. Specimens are not sealed prior to immersion due to the generally low permeability of the rock mass.

Sampling procedures are discussed in Section 12, Sampling Method and Approach.

Once the core had been sampled, it was placed in outdoor racks for long-term storage.

### **2007**

In 2007, a total of 15,879.94 m of NQ2 diamond drilling was completed in 40 drill holes. The purpose of the program was to in-fill gaps in previous programs and to test the down dip extension of the North Zone of the Harper Creek deposit.

Drilling was performed by Atlas using a Longyear Super 38 drill. Collar coordinates were surveyed by CME personnel using a GeoExplorer XT GPS receiver that was differentially corrected using a public domain GPS Base Station located in Williams Lake, BC. Elevations were determined by draping the collar coordinates over the one metre DTM obtained by Yellowhead during the Phase 3 aerial photography study.

Downhole directional surveys were carried out using a Flexit multishot instrument on drillholes HC07-13 to HC38. Due to equipment failure, holes HC07-18 and HC07-21 were not surveyed (Naas, March 2008).

The Flexit measurements were based on magnetics and could be affected by local concentrations of magnetic minerals (i.e., magnetite and pyrrhotite), which are known to exist on the property. Yellowhead personnel measure magnetic susceptibility of the core and review all downhole survey measurements for orientations that appear suspect. The instrument also flags measurements that appeared to be radically different from adjacent readings. Suspect measurements were discarded.

Core handling, logging, sampling, bulk density, and storage procedures were unchanged from 2006.

**2008**

In 2008, 23 NQ2 drillholes were drilled for an aggregate depth of 7,602.92 m. The program was designed to infill gaps within the South zone and eastern portion of the North zone.

Atlas performed the drilling using the Longyear Super 38 drill. Collar locations were surveyed using the same method as for 2006-2007. Elevations were, once again, determined by draping the collar coordinates over the one metre contour DTM utilizing Micromine v.11 software.

Downhole directional surveys of drillholes HC07-39 and HC07-40 were carried out using a Flexit digital multishot tool. Drillholes HC07-41 through HC07-75 were surveyed using an Icefield Tools MI-3 digital multishot tool. The survey was done upon completion of the drillhole.

As a backup survey system, a single shot Sperry Sun downhole survey tool used on all drillholes. Data was collected at approximately 100 m intervals while the holes were being cored (Naas, June 2008)

Core handling, logging, sampling, bulk density. and storage procedures were unchanged from previous years' programs.

Throughout the property history, drilling has generally been done on sections spaced approximately 60 m to 120 m apart (Figure 11-1). There are many areas, particularly on the fringes of the deposit, where the holes are spaced much more broadly and these

areas require infill. Yellowhead plans to carry out in-fill drilling in order to upgrade the mineral resource classification. Scott Wilson RPA concurs with this plan and recommends that the drilling be undertaken.

11-6

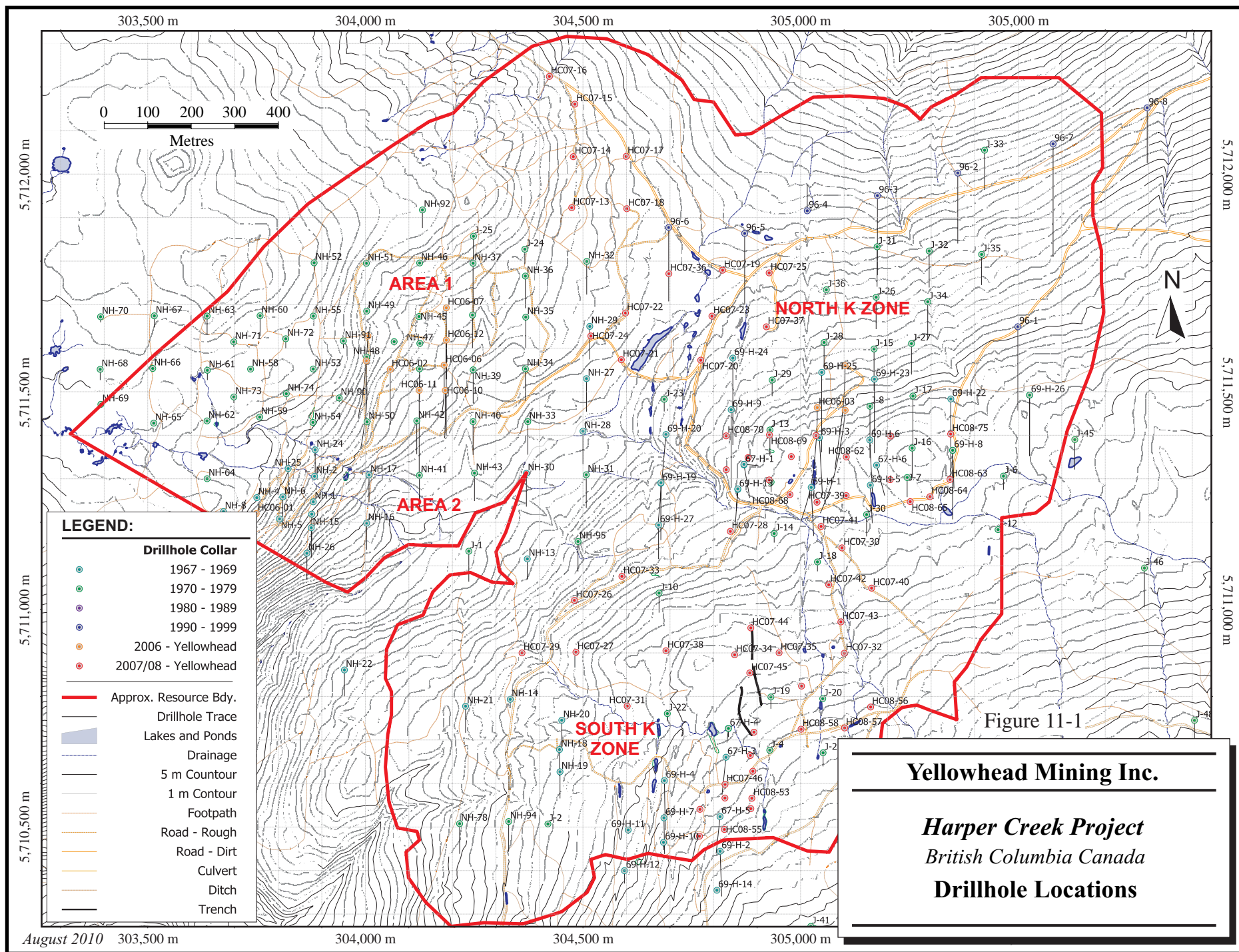


Figure 11-1

**Yellowhead Mining Inc.**

*Harper Creek Project*  
*British Columbia Canada*

**Drillhole Locations**

August 2010 303,500 m 304,000 m 304,500 m 305,000 m



## 12 SAMPLING METHOD AND APPROACH

### EARLY DRILLING

Detailed information regarding the sampling method for the early drilling is no longer available. From the remaining drill core, it is apparent that a blade splitter was used, and the sample records indicate that the maximum sample length was usually 10 ft. Sampling was generally carried out continuously through the entire mineralized interval and out into the surrounding lower grade material. In some holes, the sample size was greater than 10 ft., although the lengths are not uniform. This occurs most commonly in the drilling done by Noranda (NH-series holes) and the Noranda/Québec Cartier joint venture (J-series).

Scott Wilson RPA inspected some of the older drill core, viewed photos of the remaining core that was not inspected in person, reviewed the logs and the sample records, and observes that the sampling appears to have been done properly, in a manner appropriate for the mineralization style. Scott Wilson RPA further notes, however, that much of the early core has been resampled by Yellowhead and that the new assay data has replaced the older assays. A total of 4,375 intervals from the older core have been reassayed (Naas, 2009).

### RECENT DRILLING

Samples comprising half core were taken using a diamond saw. Maximum sample length was two metres, with breaks at changes in lithology, alteration, and mineralization. The mineralization has been observed to broadly follow the trend of the stratigraphy. However, changes in mineralization intensity are often gradual and cannot be easily discriminated by inspection only. Consequently, the sampling tended to be done over fairly consistent two metre lengths.

The project geologists marked the core and placed tags in the boxes to denote the sample intervals. A sampling technician collected the core boxes and cut the core, placing the samples into plastic bags, with the remaining half placed back in the box. The bags were stored in a locked, secure building to await packing for shipment to the laboratory.

Tags were stapled to the core boxes to identify where the samples were taken.

The drillholes are generally oriented such that they intersect the mineralization at right angles to the trend of the zones. This means that the downhole measurements of zone thickness are close to true thickness in most holes.

Scott Wilson RPA reviewed the sampling procedures and inspected the facility for taking samples and consider both to be appropriate and of a standard consistent with common industry practice. The samples appeared, on the basis of the remaining core, to have been taken properly and the sample locations clearly marked. The samples are considered to be representative, and in Scott Wilson RPA's opinion, are unbiased.

A summary of significant drill intercepts (i.e., greater than 0.3% Cu over a minimum of 5 m) is provided in Appendix 2.

## **13 SAMPLE PREPARATION, ANALYSES AND SECURITY**

### **EARLY WORK**

Detailed records of the sample preparation and assaying for the early drilling are not available. Assaying for the Noranda drill samples was done at an internal laboratory, operated by Noranda. Québec Cartier sent their samples to Bondar Clegg in North Vancouver (now ALS Chemex). The Aurun assaying was carried out by Chemex in North Vancouver, and the 1996 American Comstock samples were analyzed at Acme Analytical Laboratories Ltd. in Vancouver. American Comstock samples were reportedly delivered to the laboratory by site geological personnel.

All samples were assayed for Cu, while some, depending on the operator, were run for Au, Ag, Zn, and Mo. Québec Cartier analyzed for Cu only. Noranda assayed all samples for Cu, and select samples for Zn, Au, and Ag. Compositing intervals from individual drillholes were run for Cu, Au, and Ag. Aurun sampled some of the Québec Cartier core and analyzed it for Cu, Ag, and TiO<sub>2</sub>. American Comstock assayed for Cu, Mo, and Ag.

### **RECENT WORK**

Samples were assayed by Eco Tech Laboratory Ltd. (Eco Tech), in Kamloops, BC, a division of Stewart Group. Eco Tech is a commercial laboratory with ISO 9001-2000 certification. Scott Wilson RPA did not inspect the laboratory for this project but has in the past for other projects.

All sampling and on-site sample handling was carried out by principals or employees of CME. Samples were placed into plastic bags along with two bar-coded sample tags (one stapled to the rim of the bag) and heat-sealed. The sealed bags were scanned with a bar-code reader and placed into rice bags for shipment. A digital sample list and manifest for each shipment was produced by the bar-code system. The shipment lots were prepared by either the site manager or the project manager. Samples were collected by Eco Tech personnel for transport to the laboratory. When awaiting shipment, the samples were stored in a secure building at a site in Vavenby owned and continuously supervised (24/7) by Yellowhead personnel.

In Scott Wilson RPA's opinion, the sampling and sample-handling protocols at Harper Creek meet or exceed common industry standards.

All drill core samples were sent through a jaw crusher and cone or rolls crusher to -10 mesh. The crushed material was split through a Jones riffle down to a 250 g sub-sample. The split was pulverized in a ring and puck pulverizer to 95% - 140 mesh, and rolled to homogenize.

The samples were assayed for multi-elements via Inductively Coupled Plasma Spectrometry (ICP). Up until May 31, 2007, two digestion methods were employed: one using hydrochloric-nitric acid and the other a more aggressive four-acid process (hydrochloric and nitric acid followed by perchloric and hydrofluoric acids). Following May 31, 2007, only the more aggressive digestion method was used.

Samples grading higher than 2,900 ppm Cu were reassayed by Atomic Absorption Spectrophotometry (AA) after digestion in aqua regia.

Precious metals were determined by fire assay (FA) with an AA finish. A 30 g aliquot was mixed with flux, fused, and the resulting bead analyzed via AA for Au and Pd.

In Scott Wilson RPA's opinion, the assaying was done using conventional, industry-standard methods and carried out by an accredited commercial laboratory.

Assays results were conveyed digitally to CME in Vavenby where they were imported to an MS Access database. A copy of the data was sent to CME's office in Richmond, BC, where it was imported to Micromine for plotting and analysis. Both digital and paper copies of the assay certificates are stored in Vavenby. Scott Wilson RPA notes that, at the time of writing, Yellowhead was in the process of implementing a data management software package to expedite the processing of assay results.

## **14 DATA VERIFICATION**

### **VERIFICATION OF EARLY WORK**

There are no records of assay quality assurance/quality control (QA/QC) for work carried out prior to Yellowhead's involvement with the Harper Creek property. Some of the old core remains, but all of the pulps and rejects have been lost. Beginning in late 2005, Yellowhead embarked on a program of resampling and relogging the old core. Sanguinetti and Lefebvre (2006) compared new and original assay results of intervals composited over distances measuring several tens of metres. Direct comparison of individual samples was not conducted because the condition of the core made it impossible to determine the boundaries of many of the old samples. The results compared fairly closely, except in some of the higher grade zones, where it was reported that sections of the old core were missing. Yellowhead continued the resampling during 2006, using the same strategy as in 2005 (i.e., comparing assay results over fairly broad composited intervals). Samples from five intervals in hole NH-3 were reassayed and found to agree very well with the original sampling. Table 14-1 lists the results from reassayed core for the period 2005 to 2006.

In 2007, an attempt was made to determine where the limits of the original sampling were, and directly compare individual samples. Yellowhead collected paired results for 1,245 individual sampled intervals, and supplied the results to Scott Wilson RPA for statistical analysis. The results of this analysis are shown in Figure 14-1. In Scott Wilson RPA's opinion, the reassays agreed very well with the originals, and there is no reason to believe that the old assay data are unreliable.

As a further check, Scott Wilson RPA constructed a block model and interpolated Cu grade into the blocks using only data from holes drilled by Yellowhead. Yellowhead had so far drilled a limited portion of the deposit area and so a relatively small number of blocks received an estimate. These blocks were flagged, and then reinterpolated using only the old assay data. A total of 25,445 blocks were used in the analysis. The average grade of the blocks estimated with new data was 0.30% Cu, while the average grade of those same blocks estimated from the old data was 0.31% Cu. The mean block grades agreed quite closely, which, in Scott Wilson RPA's opinion, provides further support for the validity of the older drill results.

In Scott Wilson RPA's opinion, the Cu assay data from the older drilling is acceptable for use in estimation of Mineral Resources.

**TABLE 14-1 COMPARISON OF OLD AND NEW ASSAYS, 2005-06**  
**Yellowhead Mining Inc. – Harper Creek Property**

Hole	From	To	Length	Cu (%)	
				Historical	New
J-5	225.55	268.22	42.67	0.36	0.35
J-17	45.72	304.80	259.08	0.31	0.33
J-25	133.50	185.93	51.82	0.27	0.29
J-25	192.02	214.88	22.86	0.47	0.49
J-26	70.10	109.73	39.62	0.19	0.21
J-26	118.87	149.35	30.48	0.24	0.28
J-26	158.50	234.70	76.20	0.43	0.49
J-27	48.77	64.01	15.24	0.33	0.32
J-27	85.34	167.64	82.30	0.38	0.38
J-27	176.78	219.46	42.67	0.33	0.29
J-27	228.60	256.03	27.43	0.12	0.12
J-33	265.18	323.09	57.91	0.56	0.51
J-35	249.94	277.37	27.43	0.18	0.20
J-36	79.25	88.39	9.14	0.22	0.19
J-36	100.58	170.69	70.10	0.21	0.21
J-36	182.88	243.84	60.96	0.34	0.32
NH-11	33.53	103.63	70.10	0.55	0.46
96-3	138.00	168.00	30.00	0.24	0.24
96-4	174.00	315.00	141.00	0.33	0.34
96-5	321.00	342.00	21.00	0.17	0.18
96-4	159.00	189.00	30.00	0.23	0.27
96-4	195.00	240.00	45.00	0.25	0.25
NH-3	36.58	117.35	80.77	0.58	0.58
NH-3	44.20	62.48	18.28	1.13	1.13
NH-3	36.58	79.25	42.67	0.72	0.75
NH-3	88.39	102.11	13.72	0.76	0.72
NH-3	124.97	128.02	3.05	0.46	0.45

For the 2007 estimate, Scott Wilson RPA checked the digital database against the drill logs for all of the early work. A few insignificant discrepancies were found, but none that would affect the Mineral Resource estimate. Scott Wilson RPA verified the assay data for the Yellowhead holes by comparison with the electronic lab reports received from Eco Tech. The collar coordinates in the database were compared to the drill logs. No errors were found.

For this estimate, the Cu assays for 1,383 samples taken during the 2008 drilling program were checked against the lab certificates and no errors were found. In addition, all of the collar coordinates for drilling carried out since the date of the last estimate were checked against those recorded in the logs and no discrepancies were found. As a final check, the Gemcom database validation utility was used to check for overlaps and inconsistencies and none were found.

In Scott Wilson RPA's opinion, the Harper Creek database is reasonably free of errors and acceptable for use in estimation of Mineral Resources.

Collar surveys for the older holes were carried out several times by different operators. Survey control was generally tied into local property grids, and not routinely referenced to the UTM coordinate system or any specific datum. In 1971, Noranda had converted all the collar coordinates for the Québec Cartier drilling to the Noranda grid. In 2005, Yellowhead conducted a survey, using differential GPS, over a single Noranda hole and used this information to convert the grid to UTM Zone 11 on the 1983 North American Datum (NAD83). This conversion also involved changing the original Imperial units to metric. Yellowhead personnel then used the differential GPS to survey the collars of 20 of the early holes (14 Noranda/Québec Cartier and six American Comstock) and compared the results to the transformed coordinates. Differences of up to 15 m in northing and 4 m in easting were obtained (Sanguinetti and Lefebvre, 2006).

The topographic surface has since been updated by Yellowhead and is now based on one-metre resolution imagery. Scott Wilson RPA checked the drill collars on cross-section views against the updated topographic surface and found no significant discrepancies.

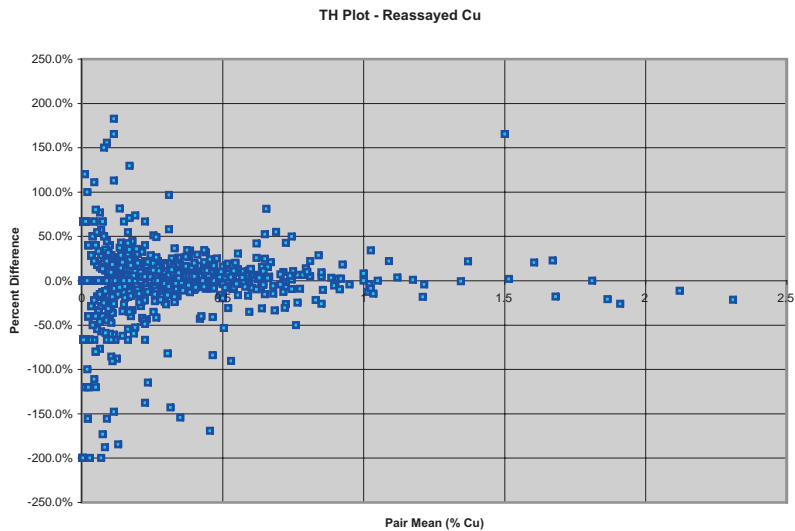
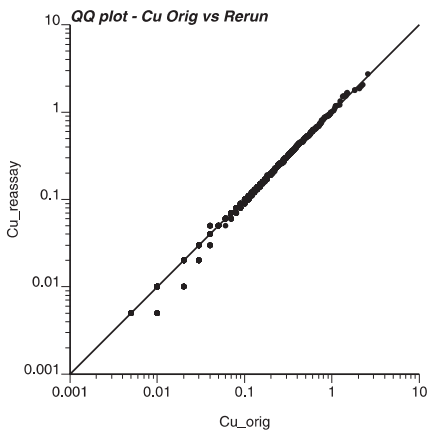
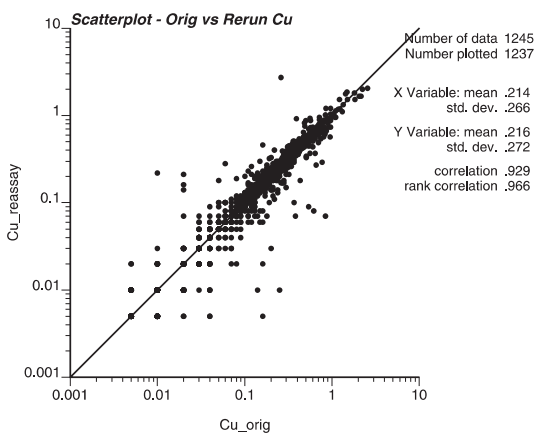
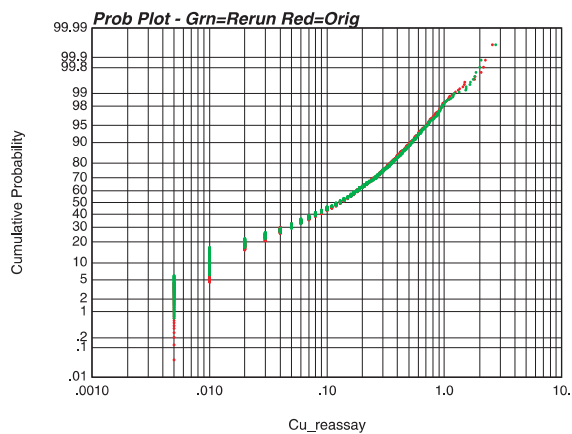
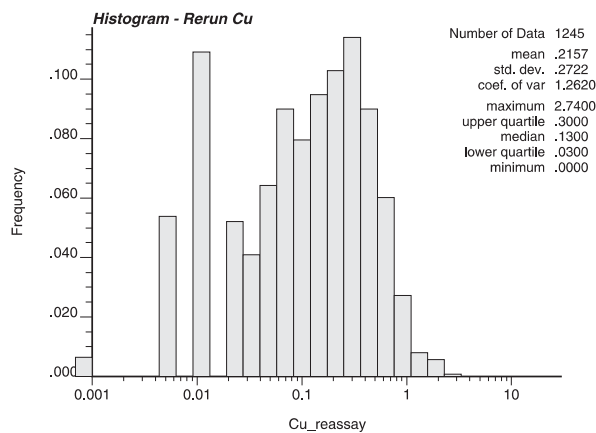
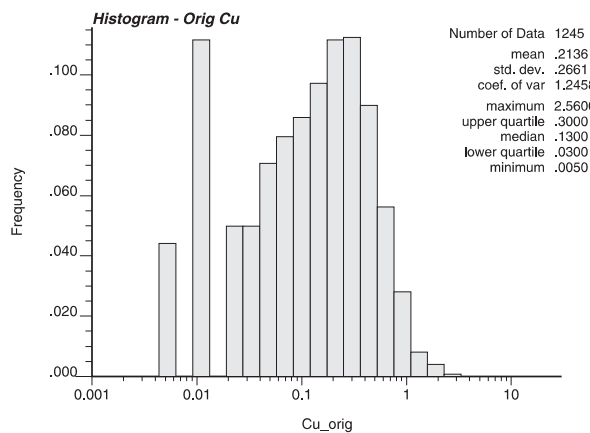


Figure 14-1

**Yellowhead Mining Inc.**  
*Harper Creek Project*  
*British Columbia Canada*  
**Comparative Statistics**  
**Old and New Assays**



Scott Wilson RPA further notes that the early drillholes (Noranda and Québec Cartier) do not have complete downhole surveys. Yellowhead surveyed the downhole trace of most of their drillholes, and it is apparent from these surveys that the holes deviate from their intended orientation somewhat. In Scott Wilson RPA's opinion, there will be some inaccuracies introduced by the lack of downhole surveys in many of the holes. These inaccuracies will not likely be large enough to impact on the global estimate of mineral resource but may affect local block estimates. For this reason, Scott Wilson RPA recommends that the Measured category not be applied to the Mineral Resource estimate for blocks estimated solely with older drillholes.

### **ASSAY QA/QC (YELLOWHEAD DRILLHOLES)**

Up until 2007, every shipment lot of 50 samples or less had included at least one standard and one blank. From 2007 onwards, the batch size was reduced to 40 samples. Two commercially prepared standards were used: one of medium grade, which approximates the overall deposit grade, and the other of high grade. The decision to include either the medium grade or high grade standard was made, more or less at random, by the individual packing the samples for shipment. The standards used on the project are shown in Table 14-2. Blank material comprised crushed marble purchased from a local garden supply store. Reference materials are placed in the sample stream using the same sample number series as the rest of the batch. This is done to reduce the conspicuousness of the reference material.

QA/QC data were collected from the laboratory and processed on a regular basis by the project manager. Standard assays that were outside of the acceptable range defined by the supplier of the standard (two standard deviations from the mean of the umpire assays) or blanks significantly above detection limit resulted in reassay of the entire batch.

Pulps from five percent of the samples were collected and sent to a second laboratory as a duplicate check. The secondary assay laboratories are Acme and Assayers Canada (AC), both in Vancouver, BC. AC was used for the Phase IV program while Acme was used for all others. The samples were not random but were deliberately selected to represent a range of grades. A standard was included with each batch of duplicate pulps.

**TABLE 14-2 CERTIFIED REFERENCE MATERIALS**  
**Yellowhead Mining Inc. – Harper Creek Project**

Producer	Certified Reference	Drilling Campaign(s)	Best Value	- 2 SD	+ 2 SD	Best Value	- 2 SD	+ 2 SD
			Au_g/t	Au_ppm	Au_ppm	Cu_%	Cu_%	Cu_%
CDN Labs	CGS-12	2007/2008	0.29	0.25	0.33	0.27	0.25	0.28
CDN Labs	CGS-13	2007	1.01	0.90	1.12	0.33	0.31	0.35
CDN Labs	CGS-15	2007/2008	0.57	0.51	0.63	0.45	0.43	0.47
CDN Labs	CGS-6	2005/2006	0.26	0.23	0.29	0.32	0.30	0.34
CDN Labs	CGS-9	2006/2007	0.34	0.31	0.37	0.47	0.45	0.50
CDN Labs	CM-1	2007/2008	1.85	1.69	2.01	0.85	0.83	0.87
CDN Labs	FCM-1	2005/2006	1.17	1.03	1.31	0.94	0.87	1.01
CDN Labs	HLLC	2007/2008	0.83	0.71	0.95	1.49	1.43	1.55

The external QA/QC data were compiled by CME personnel as the programs advanced and evaluated. Any discrepancies resulted in the reassay of the entire batch.

Scott Wilson RPA reviewed the QA/QC data and conducted an independent analysis. Standards data were plotted in chronological order and compared to the reference limits. In general, there were very few results outside of the tolerance limits for all standards. Blanks were plotted in a similar fashion to look for overlimit assays, and there was no evidence of persistent or systematic problems outside of a relatively few overlimit assays.

Paired sample results were plotted on relative difference (Thompson-Howarth) diagrams and scatter diagrams. No evidence of bias was discerned, nor was there excessive variability between paired duplicates.

In Scott Wilson RPA's opinion, the sample QA/QC meets an acceptable standard for projects of this type. The results of the QA/QC sampling have been monitored in a timely fashion and used appropriately to address potential assay failures.

## **15 ADJACENT PROPERTIES**

Scott Wilson RPA is not aware of any significant exploration programs on the ground immediately adjacent to the Harper Creek Project. Harper Creek is the primary exploration project in the vicinity.

## 16 MINERAL PROCESSING AND METALLURGICAL TESTING

A conventional mineral processing plant is being considered for the Harper Creek Project. Based on the test work completed to date the proposed plant is expected to consist of standard crushing, grinding, and flotation to produce a high grade copper concentrate containing payable precious metals values.

### METALLURGICAL TESTING

Process Research Associates Ltd. (PRA), located in Richmond, BC, undertook preliminary level test work in two phases during 2007 and 2008. Starting in January 2007, a series of flotation tests on a composite sample from the Harper Creek deposit were conducted to assess various grind sizes and flotation reagent schemes to extract copper and precious metals and produce a saleable copper concentrate. This work was initially directed by Mr. John Fox of Laurion Engineering Inc. and then followed up by Mr. Kevin Scott of Scott Wilson RPA. A Progress Report was issued by PRA in August 2007 (PRA, 2007) and the Phase 1 test work was completed in October 2007.

Subsequently, a second phase of test work was started in January 2008 under the direction of Mr. Scott and completed in July 2008 with a final report by PRA (PRA, 2008). The second phase of test work was similar to Phase 1 but was conducted on a lower grade sample that was considered more representative of an average mill feed grade over the life of mine. The assays of the two samples are shown in Table 16-1 for comparison. Both samples were provided by CME. Scott Wilson RPA was not provided with a detailed description of the origin of the individual samples.

**TABLE 16-1 COMPOSITE SAMPLE ASSAYS**  
Yellowhead Mining – Harper Creek Project

	Cu (%)	Au (g/t)	Ag (g/t)	Fe (%)	S (%)
Phase 1 HG sample	0.76	0.17	4.0	6.9	2.0
Phase 2 LG sample	0.35	0.05	1.0	3.7	1.3

Previous preliminary metallurgical test work was conducted by Noranda in 1970 and 1971 and by Lakefield Research in 1968.

**SUMMARY OF PHASE 1 METALLURGICAL TEST WORK AT PRA**

PRA received 100 kg of individual samples from Harper Creek in December 2006 which were blended into a single composite sample. A total of 15 flotation tests were conducted culminating in a locked cycle test (LCT). The first three tests were rougher flotation tests to assess the effects of different particle sizes on flotation followed by 11 cleaner flotation tests testing different reagent schemes with the objective of improving the concentrate grade.

Rougher flotation tests were performed at primary grinds with a  $P_{80}$  of 144  $\mu\text{m}$ , 104  $\mu\text{m}$ , and 81  $\mu\text{m}$ . Copper recovery was essentially unaffected by the grinding sizes, however, the best Cu and Ag grades were obtained at 104  $\mu\text{m}$ , so the subsequent cleaner tests utilized a nominal grind  $P_{80}$  of 105  $\mu\text{m}$ .

Cleaner flotation tests investigated a variety of copper and gold collectors and iron sulphide depressants at different dosages. A reagent scheme employing modest dosages of sodium isopropyl xanthate (SIPX) and Aerofloat 3418A as collectors and sodium cyanide (NaCN) as a pyrite depressant at a pH of 11.5 in cleaning proved to be the most successful. Rougher concentrate regrinding to a  $P_{80}$  of approximately 30  $\mu\text{m}$  was used in all cleaner tests. Copper recoveries up to 96% were achieved. The summary results for the cleaner tests are shown below in Table 16-2.

A single LCT following the conditions established in cleaner test F12 provided very high recovery (94.9% copper), but the grades were considerably lower than expected at 20.0% Cu and 2.59 g/t Au due to a very high mass pull. This was thought to be due to the high recirculating load caused by the addition of a first cleaner scavenger.

Test F14 provided similar results after two stages of cleaning as F12, with a Cu grade of 29% at 88% recovery. Although these are preliminary results and optimization and variability testing is required, Scott Wilson RPA projects that higher grade material from Harper Creek should be able to consistently obtain copper recovery of 92% at concentrate grades above 25% Cu.

From Table 16-2, it is evident that a high grade copper concentrate can be produced as seen in tests F8, F10, and F14.

**TABLE 16-2 SUMMARY PHASE 1 CLEANER FLOTATION RESULTS**  
**Yellowhead Mining – Harper Creek Project**

Test	Conditions	Mass (%)	Concentrate Grade			Recovery (%)		
			Cu (%)	Au (g/t)	Ag (g/t)	Cu	Au	Ag
F4	PEX/A3418 pH 10.5-11.0	3.6	18.9	2.30	53.4	91.2	52.5	60.7
F5	pH 11.5-12.5	<b>4.0</b>	17.0	2.39	51.9	<b>95.7</b>	<b>88.2</b>	65.1
F6	Add 1,000 g/t MBS	<b>4.0</b>	16.6	2.78	53.7	94.2	86.2	64.9
F7	1,000 g/t Ro / 500g/t CI MBS	3.7	17.5	2.81	53.9	92.7	81.9	62.3
F8	150 g/t NaCN in cleaning	1.5	30.9	3.93	91.0	61.9	47.7	40.2
F9	F4 but more lime and 4 <sup>th</sup> cleaner	2.8	22.5	2.86	69.6	87.1	59.1	66.6
F10	F8 but with ½ NaCN added	1.0	28.5	9.06	91.1	39.7	46.4	32.4
F11	F10 with less PEX and NaCN	2.0	19.6	3.13	93.6	84.2	56.0	61.7
F12	F11 with SIPX instead of PEX	2.4	25.9	3.11	81.7	90.3	64.3	<b>69.6</b>
F13	F11 with PAX instead of PEX	3.4	17.8	3.16	57.1	89.4	82.9	62.6
F14	F12 with 3 <sup>rd</sup> stage cleaner	2.0	<b>32.0</b>	<b>5.15</b>	<b>98.9</b>	85.5	61.2	64.2
F15	LCT with F12 conditions	3.3	20.0	2.59	73.2	94.9	73.2	77.9

#### **SUMMARY OF PHASE 2 METALLURGICAL TEST WORK AT PRA**

Generally higher grade ore will produce better metallurgical results and, as the resource grade at Harper Creek is expected to be 0.32% Cu, additional samples were obtained to construct a composite sample that more closely represents an average mineable head grade over the potential mine life. A total of 330 kg of samples from Harper Creek Project was sent to PRA in November 2007 and was blended into a single composite sample known as LG composite at 0.35% Cu. Metallurgical test work got underway in January 2008 and was carried out in similar manner to Phase 1 with a total of three rougher flotation tests, followed by eight cleaner flotation tests and concluding with two LCTs.

Rougher flotation tests were performed at primary grinds of P<sub>80</sub> of 104 µm, 84 µm, and 64 µm. Copper recovery was slightly better at the finer size, while gold recovery was poorer. The coarser primary grind was selected for further testing to remain consistent with Phase 1 and, as there was no clear indication that finer grinding would provide significantly better results, the consideration of better project economics at coarser grinding was a determining factor.

Cleaner flotation tests employed the optimum reagent scheme developed in Phase 1 with SIPX, 3418A and NaCN as a pyrite depressant with a pH of 11.5 in cleaning. A variety of different reagent dosages were investigated, while replacement collectors for

3418A were also tested in F10 and F11. The best overall results were achieved in tests F8 and F9, where a 30% to 32% Cu grade was produced at copper recoveries of approximately 60%, however, copper recoveries of 67% to 68% were obtained with less NaCN but at lower grade concentrates. Concentrate regrinding to a P<sub>80</sub> of 30 µm continued to be used. The summary results are shown below in Table 16-3.

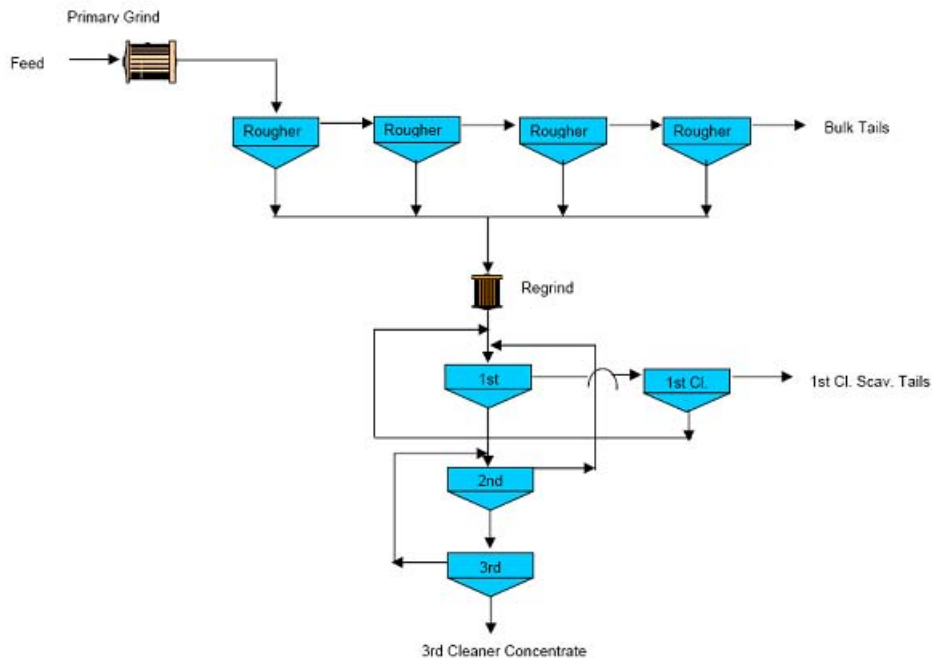
**TABLE 16-3 SUMMARY PHASE 2 (LG) CLEANER FLOTATION RESULTS**  
**Yellowhead Mining – Harper Creek Project**

Test	Conditions	Mass (%)	Concentrate Grade			Recovery (%)		
			Cu (%)	Au (g/t)	Ag (g/t)	Cu	Au	Ag
F4	SIPX/3418A/NaCN pH=11.5	0.8	29.0	1.44	77.4	<b>68.7</b>	34.3	36.8
F5	Similar to F12 in Phase 1	0.1	30.5	<b>10.38</b>	<b>125.0</b>	10.0	17.8	7.8
F6	F5 but 30% of NaCN in cleaning	0.9	25.0	1.38	83.9	67.4	33.7	51.3
F7	F6 but ½ all reagent dosages	<b>1.1</b>	21.2	1.91	99.0	66.8	42.0	<b>55.9</b>
F8	F7 with double NaCN to 10g/t	0.7	30.0	3.46	99.0	59.6	<b>46.8</b>	47.3
F9	F8 with increased collector	0.6	<b>32.2</b>	4.56	98.5	57.6	37.4	34.3
F10	F9 but XD5002 instead of A3418	0.5	<b>32.8</b>	3.55	99.3	49.0	28.7	29.0
F11	F9 but A3894 instead of A3418	0.6	31.2	3.45	113.2	56.4	33.4	43.1
<b>LC1</b>	<b>LCT with F9 conditions</b>	<b>1.1</b>	<b>31.3</b>	<b>1.91</b>	<b>105.7</b>	<b>87.3</b>	<b>36.5</b>	<b>64.7</b>
LC2	LC1 with finer regrind to 25 µm	1.2	27.4	1.54	91.3	83.4	34.4	91.6

Locked cycle testing was increased to 10 cycles from the six cycles used in Phase 1 to improve test stability. The flow sheet used is shown in Figure 16-1. Two LCTs were conducted with the LC1 performance being slightly better, obtaining an average product grade of 31% Cu and overall recoveries of 87% Cu and 36% Au over the last four cycles of the test.

It is clear that the metallurgical performance in Phase 2 on the LG composite is slightly inferior to that of Phase 1, particularly the gold recovery which is noticeably reduced from 73% to 36%. However, copper recovery in excess of 87% was realized at a very high grade of 31% Cu, and it is likely that recovery would improve at a slightly lower grade. Scott Wilson RPA projects that lower grade material from Harper Creek, representative of an average mine life head grade, should consistently obtain copper recovery of 88% at concentrate grades above 25% Cu.

FIGURE 16-1 LOCKED CYCLE TEST FLOW SHEET



Detailed ICP scans of the LC1 concentrate indicated the presence of some potential penalty elements, however, the concentrate is considered reasonably clean and should not present any concerns to smelters. Bulk samples of the tailing streams from the LCTs were kept wet and were sent to Klohn Crippen Berger for environmental testing.

A single Bond ball mill work index test was conducted on the LG composite and obtained a measurement of 11.0 kWh/t in grinding from an  $F_{80}$  of 1.65 mm to a  $P_{80}$  of 75  $\mu\text{m}$ . This indicates the Harper Creek ore is moderately soft.

### **MINERALOGY**

Preliminary mineralogical examinations have been conducted on rougher and cleaner concentrate from the PRA test work. Copper was found to be entirely in the form of chalcopyrite. The main diluent found in the concentrate is pyrite, however, it was observed that pyrite was essentially fully liberated, so it is expected that with adequate pyrite suppression a very clean concentrate can be produced at the grind size tested.

Scott Wilson RPA recommends that further mineralogical work be undertaken to investigate the mode of mineralized particle locking in the locked cycle test products, in



order to better understand how mineral separation, of Au and Ag in particular, can be improved in future metallurgical test work.

# 17 MINERAL RESOURCE AND MINERAL RESERVE ESTIMATES

## MINERAL RESOURCES

### SUMMARY

Scott Wilson RPA has carried out an update of the estimate of Mineral Resources for the Harper Creek deposit. The estimate was conducted using a block model constrained by wireframe models, and Cu grade was interpolated into the blocks using Ordinary Kriging (OK). The kriging model was based on semi-variograms derived from a geostatistical analysis carried out by Scott Wilson RPA. The wireframe and block models were constructed using GEMS software. The work was carried out by John Boyce, P. Eng., Systems Engineer for Scott Wilson RPA, and supervised by David W. Rennie, P.Eng., Principal Geologist for Scott Wilson RPA. Both Mr. Boyce and Mr. Rennie are independent of Yellowhead according to the definition in NI 43-101.

The estimate of Mineral Resources is summarized in Table 17-1.

**TABLE 17-1 MINERAL RESOURCE ESTIMATE – AUGUST 2010**  
**Yellowhead Mining Inc. – Harper Creek Property**

Cut-off (% Cu)	Tonnage Kt	Grade (% Cu)	Cu (M lb)
<b>Indicated</b>			
0.5	39,800	0.58	509
0.4	102,000	0.49	1,100
0.3	256,000	0.40	2,260
<b>0.2</b>	<b>569,000</b>	<b>0.32</b>	<b>4,010</b>
0.1	973,000	0.25	5,360
<b>Inferred</b>			
0.5	6,810	0.59	88.6
0.4	14,900	0.51	168
0.3	30,100	0.43	285
<b>0.2</b>	<b>62,700</b>	<b>0.33</b>	<b>456</b>
0.1	102,000	0.26	585

Notes:

1. CIM definitions were followed for Mineral Resources.
2. Base case Mineral Resources are estimated at a cutoff grade of 0.20% Cu.
3. A minimum mining width of 5 metres was used.
4. The estimate is constrained by a pit shell (see description in this report).
5. Average bulk density is 2.79 t/m<sup>3</sup>.

## DATABASE

The database used for the resource estimate contained records for 251 diamond drillholes, with an aggregate downhole length of 56,876.7 m. Of these, 75 were drilled by Yellowhead and the balance by earlier operators. The assay table contained records for 24,297 sampled intervals totalling 46,400 m of core, of which, 13,925 were contained within the constraining wireframe model of the deposit. Only those samples contained within the grade-shell were included in the grade interpolation. The cut-off date for the data used was the end of December 2009, and the Mineral Resource estimate is considered to be current to that date.

The most common sample length was 3.05 m (10 ft.), although approximately 65% of the samples were less than 3.05 m in length and roughly 0.5% were greater than 3.05 m. The maximum sample length was 8.23 m.

Sample statistics, histograms and probability plots for the samples are provided in Figure 17-1.

## PREVIOUS ESTIMATES

Scott Wilson RPA prepared a Mineral Resource estimate and Technical Report for the Harper Creek Project in November 2007. Following an additional 12,655.95 m of diamond drilling in 34 holes, this estimate was updated in March 2008. The two estimates are summarized in Table 17-2.

**TABLE 17-2 PREVIOUS ESTIMATES**  
**Yellowhead Mining Inc. – Harper Creek Property**

Date	Cut-off (%Cu)	Tonnage Kt	Grade (% Cu)	Cu (t)
<b>Indicated</b>				
Nov-07	0.2	450,900	0.32	1,457,800
Mar-08	0.2	538,000	0.32	1,735,000
<b>Inferred</b>				
Nov-07	0.2	142,200	0.33	463,900
Mar-08	0.2	65,000	0.34	221,000

Note that neither of the two estimates in Table 17-2 was constrained by a pit shell.

**BLOCK MODEL GEOMETRY**

The block model comprised blocks measuring 15 m long x 15 m wide x 15 m in height. The block origin was set to grid coordinates 303,000E and 5,709.850N, at an elevation of 1,800 masl. The total extent of the model was 200 columns x 180 rows x 160 levels, or 3,000 m E x 2,700 m N x 800 m elev.

**WIREFRAME MODELS**

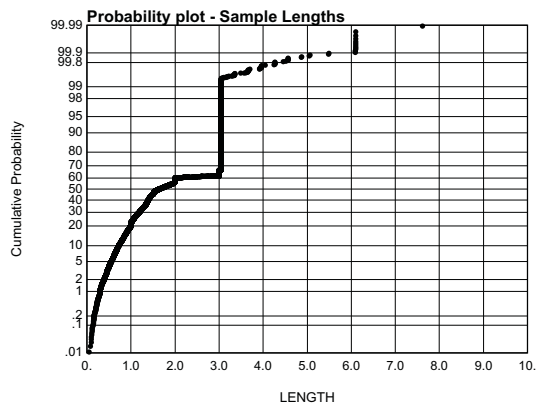
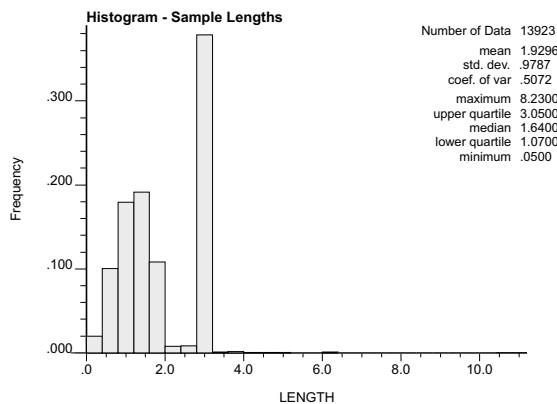
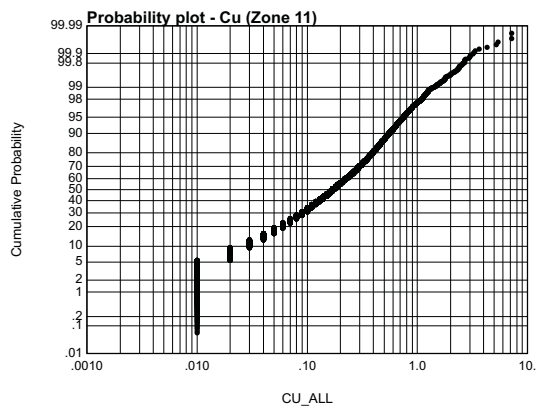
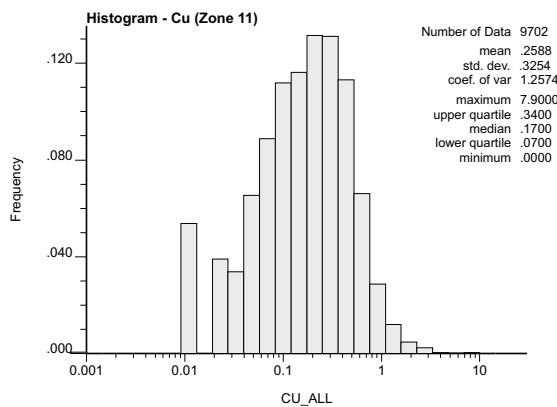
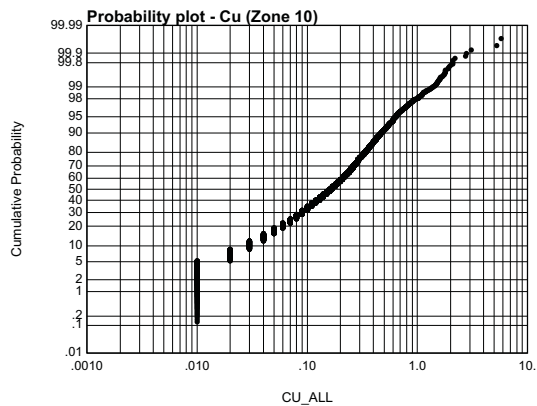
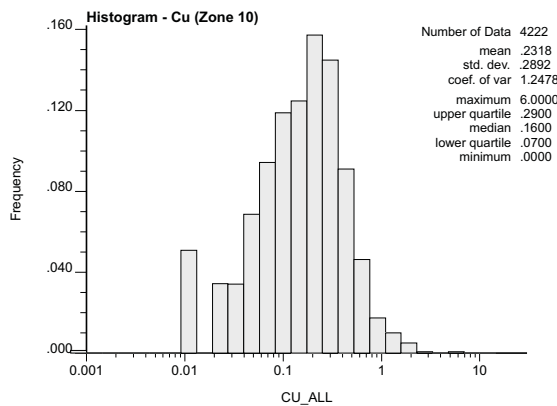
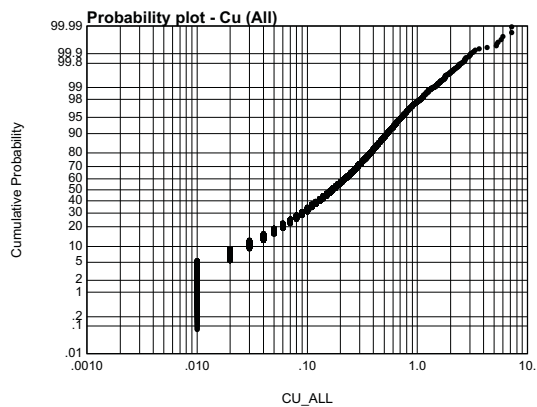
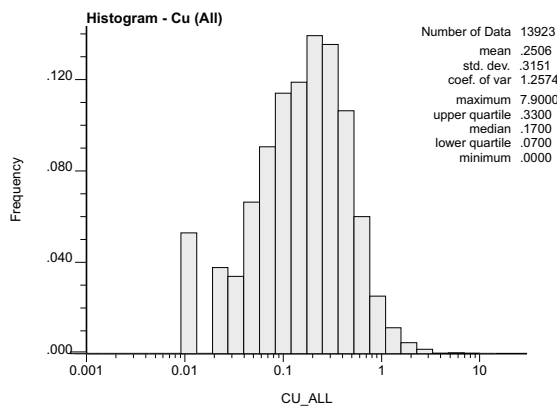
Scott Wilson RPA constructed wireframe models to constrain the block grade interpolation. A topographic DTM surface, consisting of the British Columbia government TRIM data, was provided by Yellowhead personnel. Scott Wilson RPA created a rough bedrock surface model based on the bottom of the casing of the drillholes. This surface model was used to prevent interpolation of grade into the overburden.

A grade-shell wireframe was constructed at a nominal 0.1% Cu cut-off. The drill samples were composited to minimum 0.1% Cu grades over a minimum of a 5 m downhole length with as much as 5 m of internal dilution allowed. The grade shell was constructed from these downhole composites. The mineralization is broadly stratabound and the grade-shell consists of a series of roughly tabular bodies that parallel the stratigraphy. The model was drawn out to a limit of 300 m from exterior intercepts, unless truncated by surface topography.

**CAPPING OF HIGH GRADES**

The Cu grades are not normally distributed and are observed to be somewhat positively skewed. The highest grade samples can have a disproportionately large impact on the block grade estimates, and this can lead to an overestimation of the Mineral Resources. Common practice is to cut (sometimes referred to as “capping”) high grade sample to some predetermined level to try and mitigate this risk.

Scott Wilson RPA carried out a statistical analysis of the Cu sample grades and defined the cutting value as 1.5% Cu. Capping at this value affected 0.9% of the sample population and resulted in a reduction of the unweighted, non-declustered mean to 0.82% Cu from 0.89% Cu. The cap was applied to sample values prior to compositing.



**COMPOSITING**

Samples were composited to 3.05 m downhole lengths. Sample lengths tended to be in the order of 3.05 m (10 ft.) in the early drilling, and approximately 99% of the samples measured 3.05 m or less in length. The compositing was configured to begin at the point of entry by a drillhole of the grade-shell, and progress from there in 3.05 m intervals to the exit point. At the exit point, there was invariably a short composite, measuring less than the requisite 3.05 m. Scott Wilson RPA inspected these remnants and determined that they did not differ statistically from the rest of the composites. Consequently, they were left in the database, and treated as normal composites.

Composite statistics are shown in Figure 17-2.

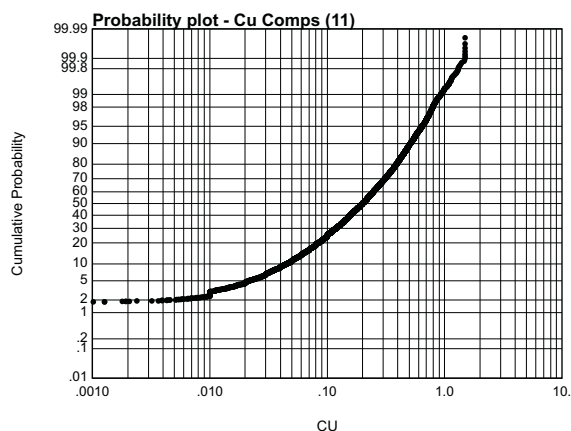
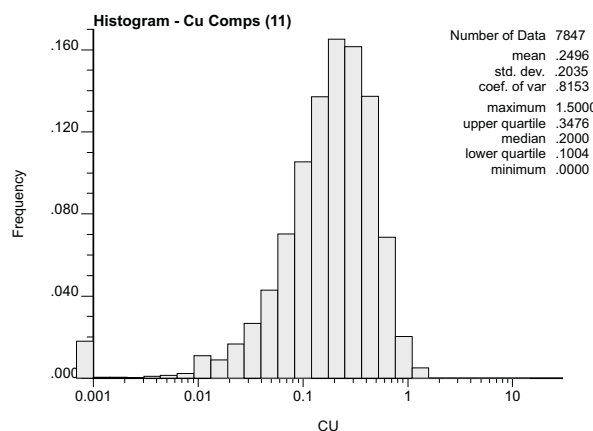
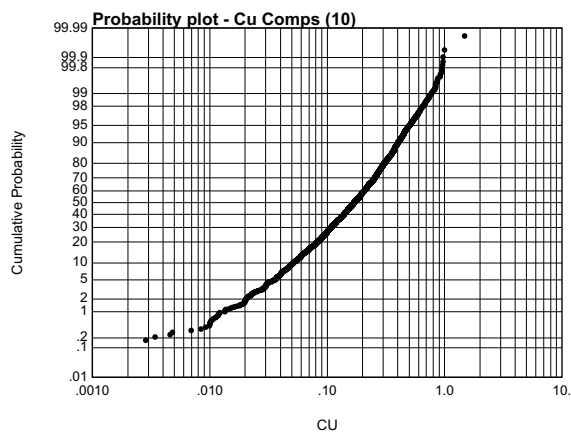
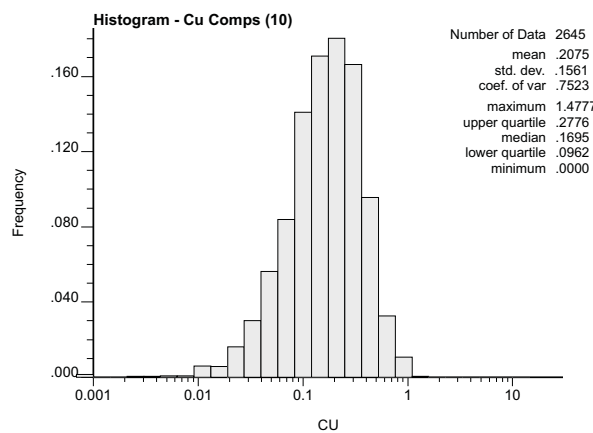
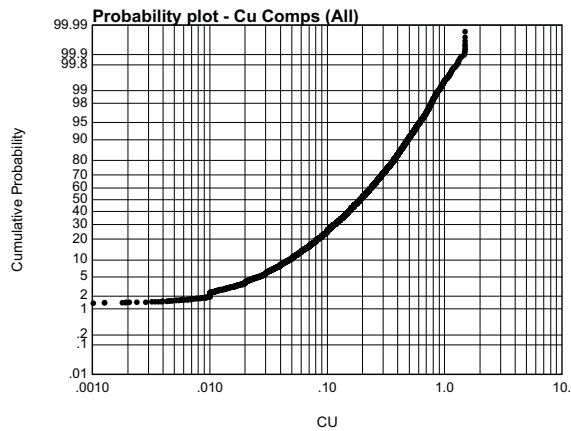
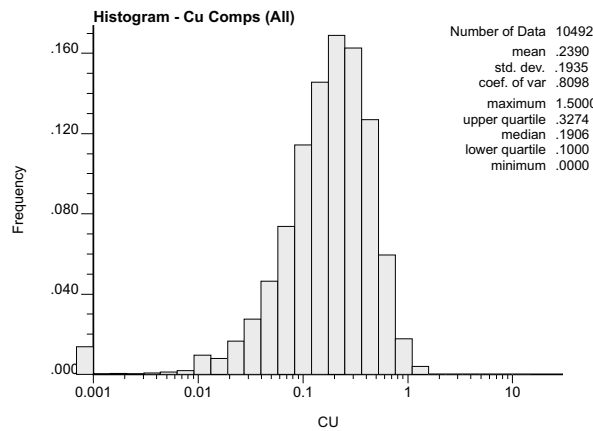
**BULK DENSITY**

Yellowhead personnel conduct routine measurements of the bulk density of core specimens. Pieces of core are weighed in air and water and the density is determined from the ratio of the weight in air to the difference between the weights in air and water. At the time of writing, Yellowhead had collected a total of 10,739 bulk density measurements, of which 5,080 were from specimens from within the grade-shell. The mean value of these 5,080 measurements is 2.79 t/m<sup>3</sup>.

Scott Wilson RPA compared the bulk density to the Cu grade and could find no significant correlation. In addition, there did not appear to be a significant difference between the density of different host rock lithologies, so the mean of the bulk density measurements was applied to the entire estimate volume.

**GEOSTATISTICS**

For the 2007 estimate, Scott Wilson RPA carried out a geostatistical analysis on the capped and composited Cu grades in order to derive the estimation parameters. The analysis was carried out using Sage2001 software, and the semi-variogram model derived from this analysis is summarized in Table 17-3.



**TABLE 17-3 ORIGINAL VARIOGRAM MODEL - CU**  
**Yellowhead Mining Inc. – Harper Creek Property**

Nugget	Sill	Ranges			Orientations			Aniso. Ratio
		Major	Semi	Minor	Major	Semi	Minor	
0.01	0.99	304	205	29	051/-15	315/-20	355/64	11:7:1

The model consists of a single exponential structure. The ellipsoid defined by the ranges and orientations is very flat and elongated in a plane that strikes more or less east-west and dips about 25° to the north. This orientation is reasonably close to the stratigraphy.

For this updated estimate, Scott Wilson RPA reran the geostatistical analysis. The model derived from the present data set is summarized in Table 17-4.

**TABLE 17-4 UPDATED VARIOGRAM MODEL - CU**  
**Yellowhead Mining Inc. – Harper Creek Property**

Nugget	Sill	Ranges			Orientations			Aniso. Ratio
		Major	Semi	Minor	Major	Semi	Minor	
0.01	0.99	282.6	125.9	29.6	050/-15	313/-23	350/63	9.5:2.2:1

In Scott Wilson RPA's opinion, the updated variogram model is similar to the older model in terms of the major and minor axes ranges and orientations. The semi-major axis is significantly shorter, although not enough to warrant changing the search parameters for this update. As a result, the search ranges and classification criteria were kept the same as for the previous estimates. The updated modelled semi-variograms generated along the principal axes are shown in Figure A3-1 in Appendix 3.

## ESTIMATION PARAMETERS

The grade interpolation was carried out in two passes, first at two-thirds the original (2007) variogram model range (203 m x 137 m x 19 m), then at the full range (304 m x 205 m x 29 m). The search was oriented parallel to the variogram model.



For the first pass, the search was constrained to a minimum of four and a maximum of 15 composites, with a maximum of three allowed from any one drillhole. For the second pass, the minimum composite constraint was reduced to one.

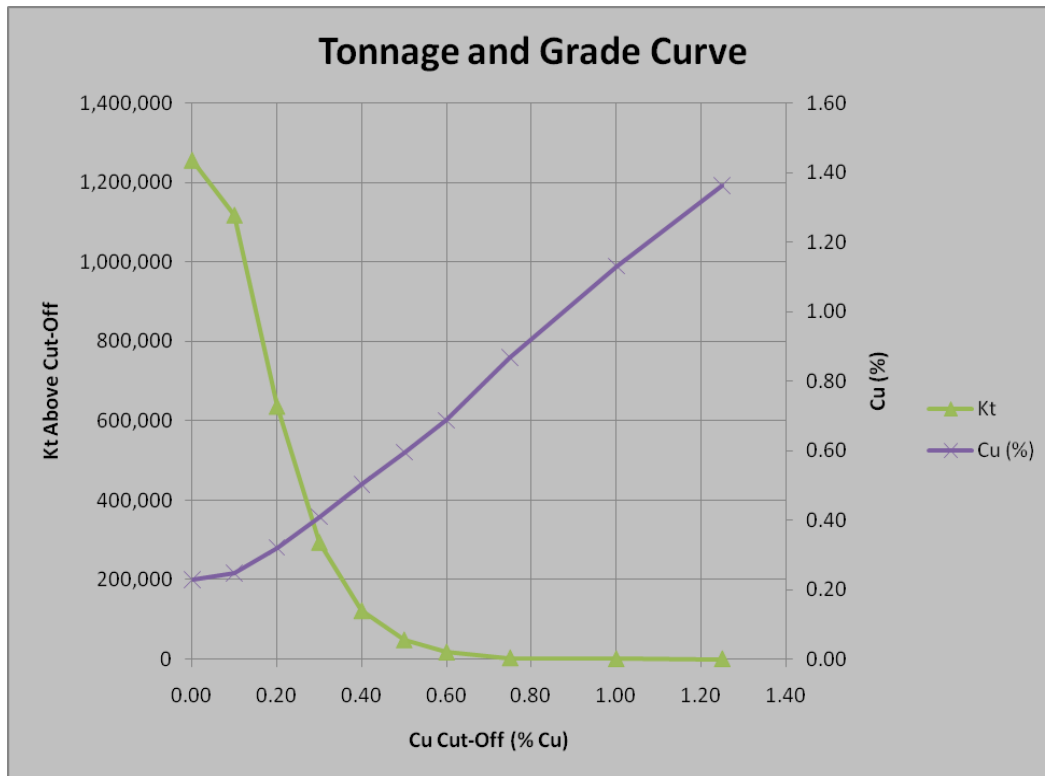
## BLOCK MODEL RESULTS

The unclassified block model results are shown in Table 17-5, at a range of cut-offs. The tonnage curve is provided in Figure 17-3.

**TABLE 17-5 UNCLASSIFIED BLOCK MODEL RESULTS**  
Yellowhead Mining Inc. – Harper Creek Property

<b>Cu Cut-off</b>	<b>Volume m<sup>3</sup> x 1,000</b>	<b>Density t per m<sup>3</sup></b>	<b>Tonnage Kt</b>	<b>CU % Cu</b>
<b>1.50</b>	0.000	0	0.000	0.00
<b>1.25</b>	9.156	2.79	25.546	1.36
<b>1.00</b>	130.845	2.79	365.059	1.13
<b>0.75</b>	920.555	2.79	2,568.349	0.87
<b>0.60</b>	6,130.533	2.79	17,104.187	0.69
<b>0.50</b>	17,123.605	2.79	47,774.858	0.60
<b>0.40</b>	43,527.085	2.79	121,440.567	0.50
<b>0.30</b>	105,278.781	2.79	293,727.800	0.41
<b>0.20</b>	228,056.047	2.79	636,276.371	0.32
<b>0.10</b>	400,924.568	2.79	1,118,579.545	0.25
<b>0.00</b>	450,575.514	2.79	1,257,105.685	0.23

FIGURE 17-3 TONNAGE AND GRADE CURVES



## VALIDATION

Scott Wilson RPA carried out the following validation exercises on the block model:

- Visual inspection on plans and section and comparison of the block grades to the composite grades.
- Comparison of global mean block and composite grades.
- Cross-validation or “jack-knifing”: Sequential removal of each composite from the database, and estimation of that composite using the surrounding composites.
- Re-estimation of the block model using an alternative method (Inverse Distance Squared, ID<sup>2</sup>).

In Scott Wilson RPA’s opinion, the block grades appear to have honoured the composite grades quite well. Refer to Figures 17-4, 17-5, 17-6, and 17-7 for examples of cross sections showing block grades along with the drillhole composites. Scott Wilson RPA notes that there are structural complexities within the deposit that are not reflected in the model. These areas comprise a relatively small proportion of the total mineral resource

volume; however, it would be advantageous to reconcile the block model with the geology. Scott Wilson RPA further notes that the process of geological interpretation for Harper Creek is ongoing and that additional geological controls to the deposit will likely be found. When this work is complete, Scott Wilson RPA recommends that the wireframe and block models be amended to incorporate the revised interpretation.

The global mean block and composite grades are observed to agree reasonably well with one another. The unweighted global mean of the non-zero blocks is 0.228% Cu, while the global composite mean is 0.239% Cu. This implies that the global grade estimate may be slightly conservative. In Scott Wilson RPA's opinion, the difference in the mean block and composite grades is not significant.

Cross-validation is a process wherein each composite is sequentially removed from the database and the grade for that point is then estimated using the surrounding samples. It serves as a test to see whether or not the kriging model has introduced a bias in the estimated grade relative to the composite grades. The mean of the estimated values was 0.239% Cu, which is exactly the same as the mean of the composites. The histogram of the error between original and estimated values is observed to be symmetrical about a mean of 0.001, which suggests the errors are essentially unbiased. In Scott Wilson RPA's opinion, the cross-validation results show that the kriging model is unbiased.

Scott Wilson RPA carried out a grade interpolation using ID<sup>2</sup> weighting. The ID<sup>2</sup> model results were very close to the kriged model. The two block models are compared to one another in Table 17-6.

**TABLE 17-6 KRIGED VS. ID<sup>2</sup> MODEL RESULTS**  
**Yellowhead Mining Inc. – Harper Creek Property**

**Kriged**

Volume m <sup>3</sup> x 1,000	Density t per m <sup>3</sup>	Tonnage Kt	CU % Cu	CU_P t Cu
0	0	0	0	0
9.15626173	2.79	25.54597022	1.363	348.2370757
130.845384	2.79	365.0586207	1.131	4,128.71
920.56	2.79	2,568.35	0.868	22,297.25
6,130.53	2.79	17,104.19	0.687	117,559.73
17,123.61	2.79	47,774.86	0.595	284,356.69
43,527.08	2.79	121,440.57	0.502	609,825.33
105,278.78	2.79	293,727.80	0.409	1,201,892.84
228,056.05	2.79	636,276.37	0.321	2,043,463.18
400,924.57	2.79	1,118,579.54	0.248	2,771,015.86
450,575.51	2.79	1,257,105.68	0.228	2,867,453.55
<b>450,575.51</b>	<b>2.79</b>	<b>1,257,105.68</b>	<b>0.228</b>	<b>2,867,453.55</b>

**ID<sup>2</sup>**

Volume m <sup>3</sup> x 1,000	Density t per m <sup>3</sup>	Tonnage Kt	CU % Cu	CU_P t Cu
0	0	0	0	0
32.6889349	2.79	91.2021283	1.357	1,237.84
131.924963	2.79	368.0706465	1.168	4,298.73
1,030.26	2.79	2,874.42	0.868	24,959.13
6,110.25	2.79	17,047.59	0.691	117,774.59
17,058.94	2.79	47,594.45	0.596	283,819.82
42,599.98	2.79	118,853.95	0.504	599,082.62
104,278.86	2.79	290,938.01	0.409	1,190,655.38
231,006.46	2.79	644,508.02	0.320	2,059,209.20
402,831.59	2.79	1,123,900.14	0.247	2,781,076.41
450,575.51	2.79	1,257,105.68	0.229	2,875,604.15
<b>450,575.51</b>	<b>2.79</b>	<b>1,257,105.68</b>	<b>0.229</b>	<b>2,875,604.15</b>

17-12

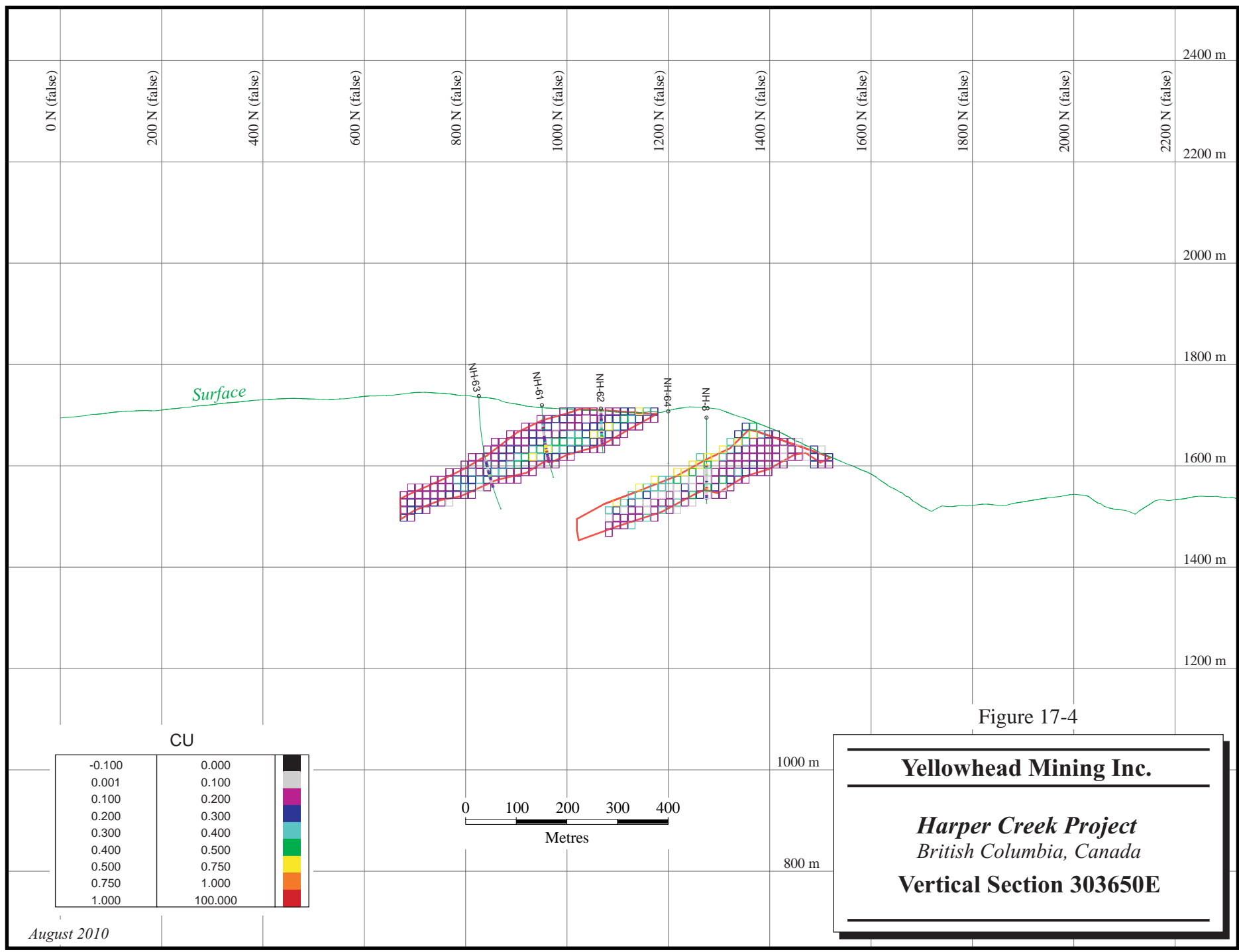


Figure 17-4

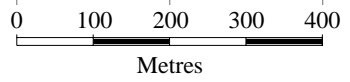
**Yellowhead Mining Inc.**

*Harper Creek Project*  
*British Columbia, Canada*

**Vertical Section 303650E**

CU

-0.100	0.000	
0.001	0.100	
0.100	0.200	
0.200	0.300	
0.300	0.400	
0.400	0.500	
0.500	0.750	
0.750	1.000	
1.000	100.000	



17-13

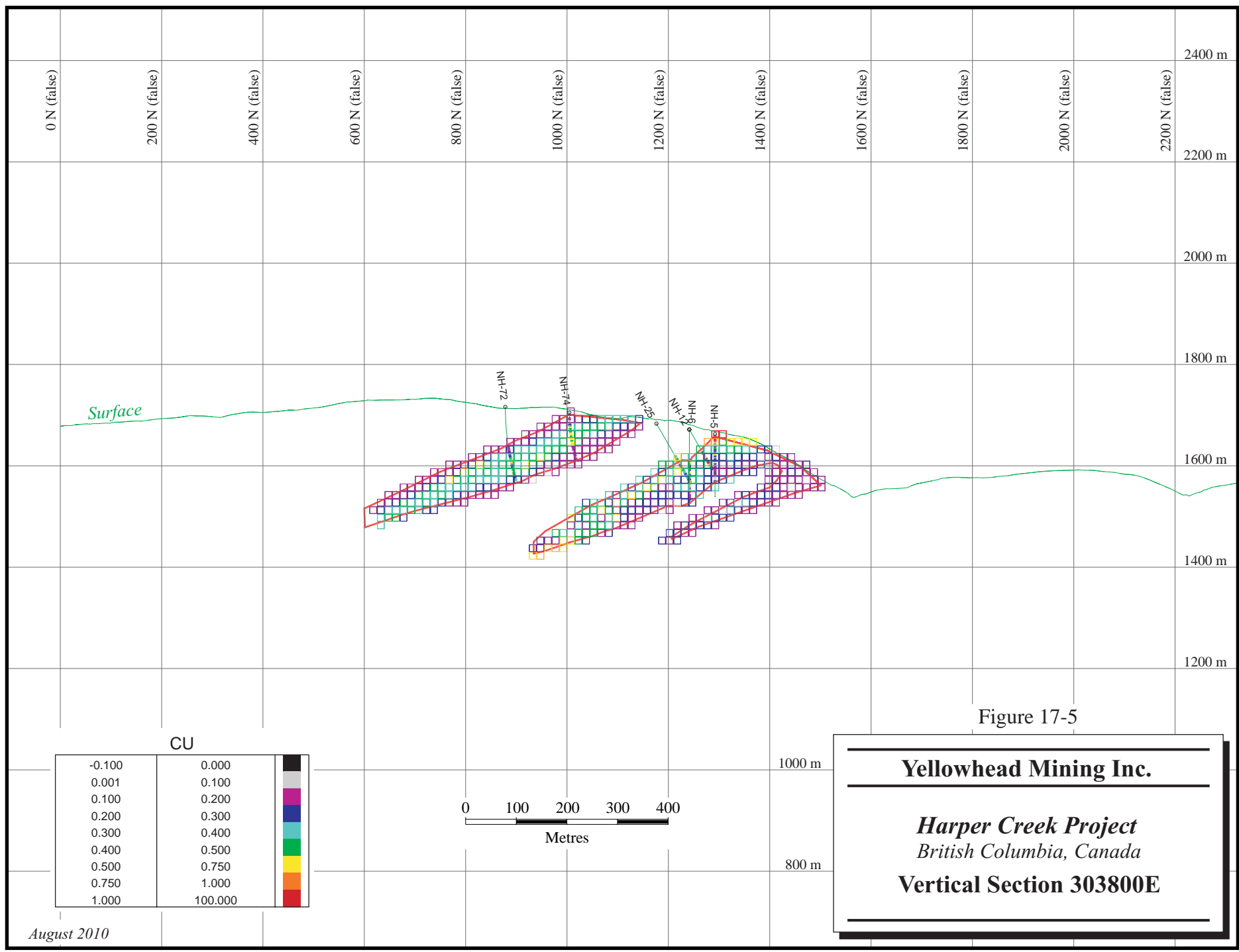
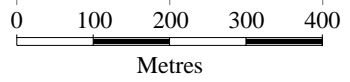


Figure 17-5

CU		
-0.100	0.000	Black
0.001	0.100	Grey
0.100	0.200	White
0.200	0.300	Blue
0.300	0.400	Light Blue
0.400	0.500	Green
0.500	0.750	Yellow
0.750	1.000	Orange
1.000	100.000	Red



**Yellowhead Mining Inc.**

*Harper Creek Project*  
*British Columbia, Canada*

**Vertical Section 303800E**

August 2010

17-14

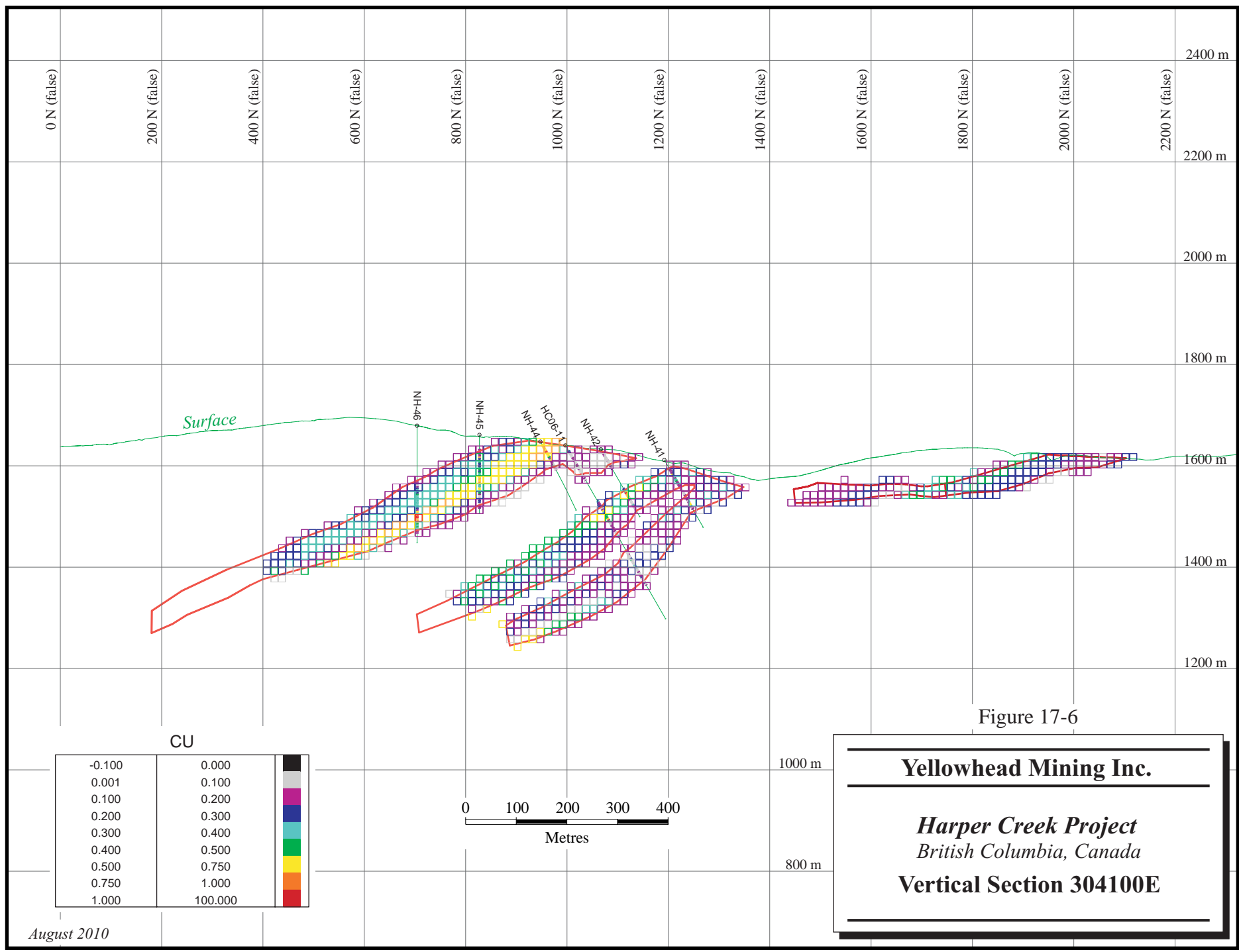


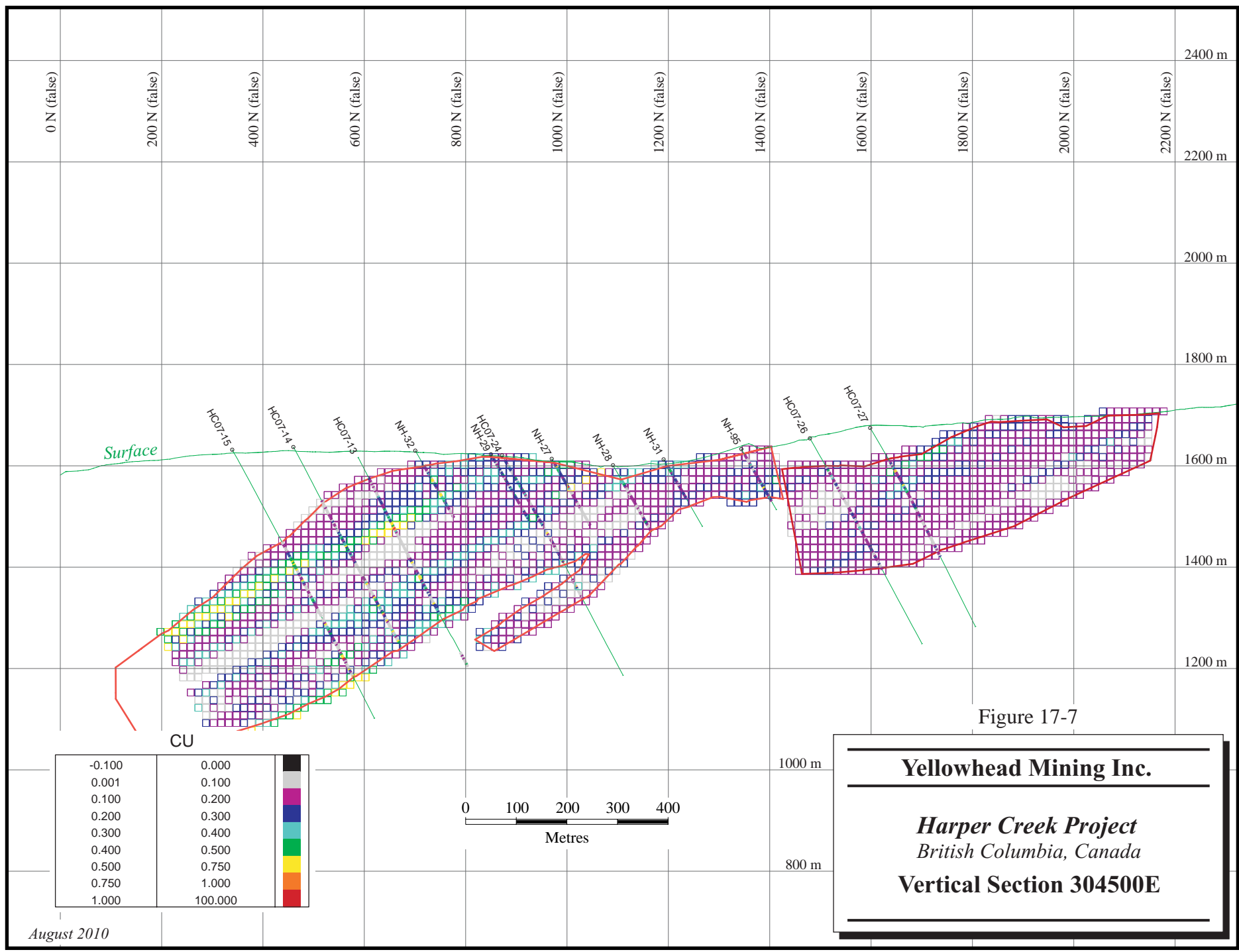
Figure 17-6

**Yellowhead Mining Inc.**

*Harper Creek Project*  
*British Columbia, Canada*

**Vertical Section 304100E**

17-15



CU

-0.100	0.000	
0.001	0.100	
0.100	0.200	
0.200	0.300	
0.300	0.400	
0.400	0.500	
0.500	0.750	
0.750	1.000	
1.000	100.000	

0 100 200 300 400  
Metres

Figure 17-7

**Yellowhead Mining Inc.**

*Harper Creek Project*  
British Columbia, Canada

**Vertical Section 304500E**

August 2010



**CLASSIFICATION**

The Mineral Resources were classified in accordance with the CIM Definition Standards for Mineral Resources and Mineral Reserves, adopted by the CIM Council on December 11, 2005. All of the Mineral Resources are classed as either Indicated or Inferred, and there were no Measured Mineral Resources.

The Mineral Resources were classified as follows:

- Indicated Mineral Resources are blocks within the resource shell estimated with a minimum of two drillholes (i.e., a minimum of four composites), with the anisotropic distance to the nearest composite less than or equal to 167 m.
- Inferred Mineral Resources are blocks within the resource shell estimated with a minimum of one composite out to a distance equal to the full variogram range.

**RESOURCE PIT SHELL**

The CIM Guidelines specify that Mineral Resources must have a reasonable prospect of economic extraction. In order to satisfy this constraint, Scott Wilson RPA generated a pit shell and reported as Mineral Resources only those blocks captured within this pit shell.

The key parameters used for the resource pit shell are listed below:

- General:
  - Density = 2.79 t/m<sup>3</sup>
  - Pit Wall Slope = 45°
- Mining Costs:
  - Waste Reference Mining Cost = US\$1.25/t
  - Mining Recovery = 100%
  - Mining Dilution = 0%
- Processing Costs:
  - Process Costs = US\$3.50/t
  - Tailings Management cost = US\$0.25/t
  - Cu Recovery = 87%
- G&A Costs:
  - US\$0.50/t
- Selling:
  - Cu Price = US\$3.25/lb
  - Exch. Rate = US\$1.00/C\$1.11

- Offsite Costs:
  - Cu Payable = 0.95%
  - Cu Selling Costs = US\$0.50/lb

The pit shell was generated using the Whittle optimization package in Surpac. Virtually all of the estimated resource blocks were captured within the pit shell, which, in Scott Wilson RPA's opinion, demonstrates that the deposit is potentially amenable to open pit mining.

### **CUT-OFF GRADE**

The cut-off grade for the Mineral Resource estimate is 0.2% Cu. In Scott Wilson RPA's opinion, this is a reasonable first-pass cut-off for an open pit Cu mine in British Columbia. However, additional economic studies are necessary to determine the appropriate cut-off grade for the Harper Creek Project.

## **18 OTHER RELEVANT DATA AND INFORMATION**

At the time of writing, the economic viability of the Harper Creek Project has not been established. However, Yellowhead has commenced socio-economic, mining engineering, metallurgical, geotechnical, and environmental studies in support of an economic assessment of the project. A consultant has been retained to work with local First Nations communities to engage them in the permitting process, and to facilitate participation in the project. Preliminary pit optimization studies have been carried out to begin to define appropriate mining parameters, production rates, and estimated costs. As stated in the Section 16 of this report, test work has been carried out which has demonstrated that the Cu can be recovered using conventional grinding/flotation, and a preliminary process flow sheet has been developed. A geotechnical consultant has conducted preliminary field studies for potential sites for tailings impoundment and other major infrastructure. Environmental monitoring, baseline studies, and site investigations have been under way since 2007. This work has included site hydrological studies, flora and fauna assessments, acid rock drainage potential, and socio-economic impacts.

Scott Wilson RPA is not aware of any issues that exist which would prevent the advancement of the project.

## 19 INTERPRETATIONS AND CONCLUSIONS

Scott Wilson RPA draws the following conclusions:

- The Harper Creek deposit is interpreted as a VHMS deposit, comprising Cu sulphide-bearing (chalcopyrite) horizons with significant Au and Ag values. The mineralization occurs in shallowly to moderately dipping tabular zones that appear from the drill results obtained to date to be reasonably coherent and predictable and broadly concordant with the stratigraphy.
- The drilling, logging, and sampling work by Yellowhead is being carried out in an appropriate fashion using conventional industry-standard protocols.
- The early drilling results have been validated to a standard that makes them acceptable for use in the estimation of Mineral Resources up to and including the Inferred and Indicated categories. Yellowhead has reassayed 4,375 of 14,242 older samples (approximately 31% of the total), and there has been good agreement between the older and newer data.
- In Scott Wilson RPA's opinion, the samples are representative and unbiased.
- Several holes are without complete downhole surveys, resulting in survey inaccuracies. In Scott Wilson RPA's opinion, the survey inaccuracies should not affect the global mineral resource estimate. However, local block grades will probably be affected.
- Limited Au and Ag assay work suggests that there are areas of the deposit where grades of these components will be high enough to affect project economics. Assaying for Au and Ag was not routinely done during earlier programs. Yellowhead assays the newer core for Au and Ag and has resampled a number of the older drillholes. Scott Wilson RPA recommends that grades for Au and Ag be estimated into the block model.
- Preliminary metallurgical test work suggests that the Yellowhead ore can be processed using conventional methods (i.e., grinding and froth flotation). Preliminary test work has been completed on a relatively high grade sample (0.76% Cu) and on a sample representative of an average head grade over a potential mine life (0.35% Cu). Based on this test work, Scott Wilson RPA projects that the lower grade material should obtain copper recovery of 88% at concentrate grades above 25% Cu, while the higher grade material should obtain copper recovery of 92% at similar concentrate grades.
- Indicated Mineral Resources at a cut-off grade of 0.2% Cu are estimated to be 569.0 Mt grading 0.32% Cu. Inferred Mineral Resources total 62.7 Mt grading 0.33% Cu. This represents an overall 5% increase in tonnes over the last estimate, carried out in 2008. The reason for the increase is that additional diamond drilling has added Mineral Resources.
- Scott Wilson RPA notes that the average grade of the Mineral Resources tends to be close to the cut-off grade. This indicates that the tonnage above cut-off will be quite sensitive to variations in cut-off grade.

- A cut-off grade of 0.2% Cu has been applied to the Mineral Resource estimate and this cut-off grade was derived from experience that Scott Wilson RPA has from similar deposits. Further economic studies are required to rigorously define the cut-off grade.
- In Scott Wilson RPA's opinion, there is significant exploration potential at Harper Creek. The deposit remains open ended to the north, and there are sparsely drilled sections in the central portion of the deposit area that have good potential for expansion of the mineralized zones. Also, at some distance from the main deposit, there are additional exploration targets on the property which may increase the current Mineral Resources.
- In Scott Wilson RPA's opinion, the Harper Creek deposit warrants additional engineering and economic studies to determine the feasibility of developing an open pit mining and milling operation on the property.

## **20 RECOMMENDATIONS**

Scott Wilson RPA makes the following recommendations:

- Further metallurgical test work should be undertaken to optimize the reagent scheme and improve the flotation performance, particularly with respect to gold recovery. Variability test work should be undertaken to test the response of different samples to the optimized reagent and grinding scheme.
- Further mineralogical work should be undertaken to investigate the mode of mineralized particle locking in the locked cycle test products, in order to better understand how mineral separation, of Au and Ag in particular, can be improved in future metallurgical test work.
- Property exploration work should continue in order to find additional Mineral Resources on the Harper Creek property and upgrade the present Mineral Resources.
- Engineering, environmental, and economic studies should continue in order to determine if the Harper Creek deposit is economically feasible to exploit.

Yellowhead proposes to advance the project to Feasibility Stage, and this work is to be financed through a public offering of shares in the company. The initial stage of the planned work is to include diamond drilling to expand and upgrade the known Mineral Resources, as well as metallurgical, environmental, geotechnical, hydrological, and general site field studies. A preliminary economic assessment is scheduled for completion in November 2010. Planned expenditures for the first six months total \$5 million, which includes the preliminary economic assessment. A summary of the budget is provided in Table 20-1. Field expenses are based on Yellowhead's experience on the property to date.

Scott Wilson RPA concurs with the planned work and budget, and recommends that the program be carried out.

**TABLE 20-1 PLANNED EXPENDITURES**  
**Yellowhead Mining Inc. – Harper Creek Property**

Item	C\$	Totals, C\$
<b>Geological Field Work</b>		
Personnel	350,000	
Mobilization	100,000	
Drilling and Related Fieldwork	300,000	
Camp Operations	300,000	
Equipment	100,000	
Construction	55,000	
Analyses	230,000	
Mineral Resource Report	60,000	
Reporting and Reproductions	20,000	
Contingency (15%)	227,250	
<b>Sub-Total</b>		<b>1,742,250</b>
<b>Other Technical Work</b>		
Environmental	200,000	
Geotechnical	15,000	
Project Management	550,000	
Metallurgy	200,000	
First Nations and Community Consultation	200,000	
Contingency (15%)	174,750	
<b>Sub-Total</b>		<b>1,339,750</b>
<b>Administration</b>		
Corporate Management	250,000	
Travel	100,000	
Legal	125,000	
Accounting	60,000	
Marketing and Promotion	75,000	
Office and Overhead	30,000	
US Steel Option Payment	500,000	
Contingency (15%)	171,000	
<b>Sub-Total</b>		<b>1,311,000</b>
Unallocated	500,000	
<b>Grand Total</b>		<b>4,893,000</b>
	say	<b>5,000,000</b>

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Schiarizza, P., and Preto, V. A., (1987): Geology of the Adams Plateau – Clearwater – Vavenby Area, BC Ministry of Energy, Mines and Petroleum Resources Paper 1987-2, 89 pp.

## **22 DATE AND SIGNATURE PAGE**

This report titled “Technical Report on the Harper Creek Project, Clearwater, British Columbia, Canada” and dated August 16, 2010, was prepared and signed by the following authors:

**(Signed & Sealed)**

Dated at Vancouver, BC  
August 16, 2010

David W. Rennie, P.Eng.  
Principal Geologist

**(Signed & Sealed)**

Dated at Vancouver, BC  
August 16, 2010

Kevin C. Scott, P.Eng.  
Principal Metallurgist

## **23 CERTIFICATES OF QUALIFIED PERSONS**

### **DAVID W. RENNIE**

I, David W. Rennie, P.Eng., as an author of this report entitled "Technical Report on the Harper Creek Project, Clearwater, British Columbia, Canada", prepared for Yellowhead Mining Inc., and dated August 16, 2010, do hereby certify that:

1. I am a Principal Geologist with Scott Wilson Roscoe Postle Associates Inc. of Suite 388, 1130 West Pender St., Vancouver, BC, V6E 4A4.
2. I am a graduate of the University of British Columbia, Vancouver, BC, Canada, in 1979 with a Bachelor of Applied Science degree in Geological Engineering.
3. I am registered as a Professional Engineer in the Province of British Columbia (Reg.# 13,572). I have worked as a Geological Engineer for a total of 31 years since my graduation. My relevant experience for the purpose of the Technical Report is:
  - Review and report as a consultant on numerous mining operations and projects around the world for due diligence and regulatory requirements.
  - Pre-Feasibility and Feasibility Study work on several projects.
  - Worked as a Geological Engineer at several mines and exploration projects in a number of countries.
4. I have read the definition of "qualified person" set out in National Instrument 43-101 (NI 43-101) and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101.
5. I visited the Harper Creek Property on May 23, 2007 and July 15, 2010.
6. I am responsible for all of the Technical Report except Section 16, and contributed parts of Sections 1, 19, and 20.
7. I am independent of the Issuer applying the test set out in Section 1.4 of NI 43-101.
8. I prepared a previous Mineral Resource estimate and Technical Report on the Harper Creel Project in 2007, and a Mineral Resource update in 2008.
9. I have read NI 43-101, and the Technical Report has been prepared in compliance with NI 43-101 and Form 43-101F1.

10. To the best of my knowledge, information, and belief, the Technical Report contains all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated this 16<sup>th</sup> day of August, 2010

**(Signed & Sealed)**

David W. Rennie, P.Eng.

**KEVIN C. SCOTT**

I, Kevin C. Scott, P.Eng., as the author of this report entitled "Technical Report on the Harper Creek Project, Clearwater, British Columbia, Canada", prepared for Yellowhead Mining Inc. and dated August 16, 2010, do hereby certify that:

1. I am a Principal Metallurgist with Scott Wilson Roscoe Postle Associates Inc. of Suite 388, 1130 West Pender Street, Vancouver, British Columbia, Canada V6E 4A4.
2. I am a graduate of University of British Columbia, Vancouver, Canada in 1989 with a Bachelor of Applied Science degree in Metals and Materials Engineering.
3. I am registered as a Professional Engineer in the Province of British Columbia (License # 25314) and the Province of Ontario (License # 90443342). I have worked as a metallurgical engineer for a total of 18 years since my graduation. My relevant experience for the purpose of the Technical Report is:
  - Reviews and reports as a metallurgical consultant on a number of mining operations and projects for due diligence and financial monitoring requirements
  - Process engineer at three Canadian base metals mineral processing operations
  - Senior metallurgical engineer working for three multi-national engineering and construction companies on feasibility studies and in engineering design of mineral processing plants in Canada and South America
  - Senior process manager in charge of process design and engineering for a metallurgical processing plant in South America
4. I have read the definition of "qualified person" set out in National Instrument 43-101 (NI 43-101) and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101.
5. I did not visit the Harper Creek property in the preparation of this report.
6. I am responsible for Section 16 and contributed to Sections 1, 19, and 20 of the Technical Report.
7. I am independent of the Issuer applying the test set out in Section 1.4 of NI 43-101.
8. I co-authored a previous Technical Report on the Harper Creek Project in 2007.
9. I have read NI 43-101, and the Technical Report has been prepared in compliance with NI 43-101 and Form 43-101F1.

10. To the best of my knowledge, information, and belief, the Technical Report contains all scientific and technical information that is required to be disclosed to make the technical report not misleading.

Dated this 16<sup>th</sup> day of August, 2010

**(Signed & Sealed)**

Kevin C. Scott, P.Eng.

## 24 APPENDIX 1

### MINERAL TITLES

**TABLE A1-1 MINERAL TITLES**  
**Yellowhead Mining Inc. – Harper Creek Property**

<b>Tenure Number</b>	<b>Area (ha)</b>	<b>Owner (100%)</b>	<b>Good To Date</b>	<b>Claim Type</b>
220877	25	Yellowhead	2011/nov/03	Legacy
220878	25	Yellowhead	2011/nov/03	Legacy
220879	25	Yellowhead	2011/nov/03	Legacy
501147	342.02	Yellowhead	2011/nov/03	MTO Cell
501225	301.71	Yellowhead	2011/nov/03	MTO Cell
501608	221.33	Yellowhead	2011/nov/03	MTO Cell
501799	181.05	Yellowhead	2011/nov/03	MTO Cell
502498	583.32	Yellowhead	2011/nov/03	MTO Cell
502603	603.43	Yellowhead	2011/nov/03	MTO Cell
502606	502.87	Yellowhead	2011/nov/03	MTO Cell
506422	562.99	Yellowhead	2011/nov/03	MTO Cell
509215	603.17	Yellowhead	2011/nov/03	MTO Cell
509217	422.21	Yellowhead	2011/nov/03	MTO Cell
513235	321.7	Yellowhead	2011/nov/03	MTO Cell
513237	80.43	Yellowhead	2011/nov/03	MTO Cell
513239	140.75	Yellowhead	2011/nov/03	MTO Cell
514183	40.22	Yellowhead	2011/nov/03	MTO Cell
517483	20.11	Yellowhead	2011/nov/03	MTO Cell
519327	502.43	Yellowhead	2011/nov/03	MTO Cell
519329	502.43	Yellowhead	2011/nov/03	MTO Cell
519330	502.43	Yellowhead	2011/nov/03	MTO Cell
519331	502.41	Yellowhead	2011/nov/03	MTO Cell
519332	502.47	Yellowhead	2011/nov/03	MTO Cell
519333	502.27	Yellowhead	2010/nov/03	MTO Cell
519334	462.09	Yellowhead	2010/nov/03	MTO Cell
530337	502.33	Yellowhead	2010/nov/03	MTO Cell
530338	502.67	Yellowhead	2010/nov/03	MTO Cell
532054	482.98	Yellowhead	2011/nov/03	MTO Cell
532057	241.48	Yellowhead	2011/nov/03	MTO Cell
538962	501.81	Yellowhead	2010/nov/03	MTO Cell
538963	501.61	Yellowhead	2010/nov/03	MTO Cell
538966	501.81	Yellowhead	2010/nov/03	MTO Cell
538968	501.88	Yellowhead	2010/nov/03	MTO Cell
538970	501.61	Yellowhead	2010/nov/03	MTO Cell
538971	421.49	Yellowhead	2010/nov/03	MTO Cell
538972	501.61	Yellowhead	2010/nov/03	MTO Cell
538973	501.61	Yellowhead	2010/nov/03	MTO Cell
538974	200.63	Yellowhead	2010/nov/03	MTO Cell
538996	502.01	Yellowhead	2010/nov/03	MTO Cell
538997	502.14	Yellowhead	2010/nov/03	MTO Cell
538999	421.77	Yellowhead	2010/nov/03	MTO Cell
539000	502.11	Yellowhead	2010/nov/03	MTO Cell
539001	421.73	Yellowhead	2010/nov/03	MTO Cell
539002	421.73	Yellowhead	2010/nov/03	MTO Cell
539004	281.14	Yellowhead	2010/nov/03	MTO Cell
539770	442.84	Yellowhead	2011/nov/03	MTO Cell
539771	322	Yellowhead	2011/nov/03	MTO Cell



Tenure Number	Area (ha)	Owner (100%)	Good To Date	Claim Type
564330	503.01	Yellowhead	2010/nov/03	MTO Cell
564331	503.01	Yellowhead	2010/nov/03	MTO Cell
564333	503.23	Yellowhead	2011/nov/03	MTO Cell
564334	503.34	Yellowhead	2011/nov/03	MTO Cell
564335	463.18	Yellowhead	2011/nov/03	MTO Cell
564337	362.59	Yellowhead	2010/nov/03	MTO Cell
564338	502.82	Yellowhead	2010/nov/03	MTO Cell
564339	502.78	Yellowhead	2010/nov/03	MTO Cell
564340	503.01	Yellowhead	2010/nov/03	MTO Cell
564341	442.81	Yellowhead	2010/nov/03	MTO Cell
564342	503.01	Yellowhead	2010/nov/03	MTO Cell
564343	502.78	Yellowhead	2010/nov/03	MTO Cell
564344	503.1	Yellowhead	2010/nov/03	MTO Cell
564346	442.55	Yellowhead	2010/nov/03	MTO Cell
564347	462.5	Yellowhead	2010/nov/03	MTO Cell
564348	402.03	Yellowhead	2010/nov/03	MTO Cell
564349	502.33	Yellowhead	2010/nov/03	MTO Cell
564350	502.33	Yellowhead	2010/nov/03	MTO Cell
564351	461.88	Yellowhead	2010/nov/03	MTO Cell
564352	502.1	Yellowhead	2010/nov/03	MTO Cell
564353	401.51	Yellowhead	2010/nov/03	MTO Cell
564354	501.69	Yellowhead	2010/nov/03	MTO Cell
564355	501.69	Yellowhead	2010/nov/03	MTO Cell
564356	461.55	Yellowhead	2010/nov/03	MTO Cell
564357	120.73	Yellowhead	2010/nov/03	MTO Cell
564358	401.23	Yellowhead	2010/nov/03	MTO Cell
564360	200.61	Yellowhead	2010/nov/03	MTO Cell
564361	501.59	Yellowhead	2010/nov/03	MTO Cell
564362	501.82	Yellowhead	2010/nov/03	MTO Cell
564363	502.05	Yellowhead	2010/nov/03	MTO Cell
564364	502.28	Yellowhead	2010/nov/03	MTO Cell
564365	502.51	Yellowhead	2010/nov/03	MTO Cell
564366	502.74	Yellowhead	2010/nov/03	MTO Cell
564367	502.97	Yellowhead	2010/nov/03	MTO Cell
564368	503.19	Yellowhead	2010/nov/03	MTO Cell
564370	322.09	Yellowhead	2010/nov/03	MTO Cell
569337	261.64	Yellowhead	2011/nov/03	MTO Cell
572094	503.39	Yellowhead	2010/nov/03	MTO Cell
572095	483.09	Yellowhead	2010/nov/03	MTO Cell
572096	483.09	Yellowhead	2010/nov/03	MTO Cell
572097	503.42	Yellowhead	2010/nov/03	MTO Cell
572098	382.56	Yellowhead	2010/nov/03	MTO Cell
572099	382.57	Yellowhead	2010/nov/03	MTO Cell
572100	463.18	Yellowhead	2010/nov/03	MTO Cell
582783	201.29	Yellowhead	2010/nov/03	MTO Cell
592574	503.12	Yellowhead	2011/nov/03	MTO Cell
592579	502.92	Yellowhead	2011/nov/03	MTO Cell
592580	462.54	Yellowhead	2011/nov/03	MTO Cell
592581	442.72	Yellowhead	2011/nov/03	MTO Cell
606977	415.44	Yellowhead	2010/jul/03	MTO Cell
627844	301.71	Yellowhead	2010/sep/03	MTO Cell

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<b>Tenure Number</b>	<b>Area (ha)</b>	<b>Owner (100%)</b>	<b>Good To Date</b>	<b>Claim Type</b>
663643	502.4	Yellowhead	2010/nov/02	MTO Cell
663658	401.97	Yellowhead	2010/nov/02	MTO Cell
220771	25	Cygnus	2011/nov/03	Legacy
220772	25	Cygnus	2011/nov/03	Legacy
220773	25	Cygnus	2011/nov/03	Legacy
220774	25	Cygnus	2011/nov/03	Legacy
220775	25	Cygnus	2011/nov/03	Legacy
220776	25	Cygnus	2011/nov/03	Legacy
220777	25	Cygnus	2011/nov/03	Legacy
220778	25	Cygnus	2011/nov/03	Legacy
220779	25	Cygnus	2011/nov/03	Legacy
220780	25	Cygnus	2011/nov/03	Legacy
220781	25	Cygnus	2011/nov/03	Legacy
220782	25	Cygnus	2011/nov/03	Legacy
220783	25	Cygnus	2011/nov/03	Legacy
220784	25	Cygnus	2011/nov/03	Legacy
220785	25	Cygnus	2011/nov/03	Legacy
220786	25	Cygnus	2011/nov/03	Legacy
220787	25	Cygnus	2011/nov/03	Legacy
220788	25	Cygnus	2011/nov/03	Legacy
220789	25	Cygnus	2011/nov/03	Legacy
220790	25	Cygnus	2011/nov/03	Legacy
220791	25	Cygnus	2011/nov/03	Legacy
220792	25	Cygnus	2011/nov/03	Legacy
220793	25	Cygnus	2011/nov/03	Legacy
220794	25	Cygnus	2011/nov/03	Legacy
220795	25	Cygnus	2011/nov/03	Legacy
220796	25	Cygnus	2011/nov/03	Legacy
220797	25	Cygnus	2011/nov/03	Legacy
220798	25	Cygnus	2011/nov/03	Legacy
220799	25	Cygnus	2011/nov/03	Legacy
220800	25	Cygnus	2011/nov/03	Legacy
220961	25	Cygnus	2011/nov/03	Legacy

## **25 APPENDIX 2**

### **SIGNIFICANT DRILLHOLE INTERCEPTS**

Table A2-1 contains all drillhole intercepts grading better than 0.2% Cu over a minimum apparent thickness of 6 m.

**TABLE A2-1 SIGNIFICANT DRILL INTERCEPTS**  
**Yellowhead Mining Inc. – Harper Creek Property**

Hole-ID	From	To	Length (m)	Cu (%)	Au (g/t)	Ag (g/t)
67-H-1	3.35	15.24	11.89	0.20	0.00	0.00
67-H-1	33.53	76.20	42.67	0.43	0.00	0.00
67-H-1	85.34	108.51	23.17	0.40	0.00	0.00
67-H-2	4.57	21.34	16.77	0.28	0.00	0.00
67-H-2	36.58	46.63	10.05	0.35	0.00	0.00
67-H-3	24.38	30.48	6.10	0.24	0.00	0.00
67-H-3	42.67	94.49	51.82	0.27	0.00	0.00
67-H-3	100.58	106.68	6.10	0.24	0.00	0.00
67-H-4	27.43	46.02	18.59	0.30	0.00	0.00
67-H-5	6.71	27.43	20.72	0.58	0.00	0.00
67-H-5	30.48	42.67	12.19	0.24	0.00	0.00
67-H-6	6.10	30.48	24.38	0.33	0.00	0.00
67-H-6	36.58	51.82	15.24	0.45	0.00	0.00
67-H-6	67.06	76.20	9.14	0.33	0.00	0.00
69-H-1	5.79	30.48	24.69	0.32	0.00	0.00
69-H-1	33.53	67.06	33.53	0.41	0.00	0.00
69-H-1	100.58	106.68	6.10	0.32	0.00	0.00
69-H-1	121.92	152.40	30.48	0.32	0.00	0.00
69-H-2	9.14	15.24	6.10	0.20	0.00	0.00
69-H-3	6.10	12.19	6.09	0.28	0.00	0.00
69-H-3	24.38	57.91	33.53	0.33	0.00	0.00
69-H-3	64.01	155.45	91.44	0.53	0.00	0.00
69-H-3	179.83	187.76	7.93	0.26	0.00	0.00
69-H-4	0.00	12.19	12.19	0.43	0.00	0.00
69-H-4	24.38	30.48	6.10	0.47	0.00	0.00
69-H-4	39.62	60.96	21.34	0.35	0.00	0.00
69-H-4	67.06	76.20	9.14	0.38	0.00	0.00
69-H-5	6.10	64.01	57.91	0.33	0.00	0.00
69-H-6	30.48	64.01	33.53	0.35	0.00	0.00
69-H-6	79.25	140.21	60.96	0.42	0.00	0.00
69-H-7	8.53	39.62	31.09	0.33	0.00	0.00
69-H-7	54.86	67.06	12.20	0.25	0.00	0.00
69-H-8	18.29	33.53	15.24	0.25	0.00	0.00
69-H-8	54.86	76.20	21.34	0.30	0.00	0.00
69-H-8	82.30	94.49	12.19	0.34	0.00	0.00
69-H-8	100.58	109.73	9.15	0.30	0.00	0.00
69-H-9	21.34	42.67	21.33	0.33	0.00	0.00
69-H-9	51.21	60.96	9.75	0.28	0.00	0.00
69-H-9	67.06	73.15	6.09	0.28	0.00	0.00
69-H-9	100.58	121.92	21.34	0.32	0.00	0.00
69-H-9	140.21	152.40	12.19	0.34	0.00	0.00
69-H-9	161.54	170.69	9.15	0.32	0.00	0.00
69-H-9	179.83	204.22	24.39	0.33	0.00	0.00
69-H-10	6.10	12.19	6.09	0.36	0.00	0.00
69-H-10	33.53	45.72	12.19	0.23	0.00	0.00
69-H-11	6.10	33.53	27.43	0.34	0.00	0.00

Hole-ID	From	To	Length (m)	Cu (%)	Au (g/t)	Ag (g/t)
69-H-12	51.82	60.96	9.14	0.27	0.00	0.00
69-H-13	15.24	45.72	30.48	0.41	0.00	0.00
69-H-13	64.01	70.10	6.09	0.45	0.00	0.00
69-H-13	73.15	94.49	21.34	0.45	0.00	0.00
69-H-13	115.82	121.92	6.10	0.30	0.00	0.00
69-H-13	128.02	137.16	9.14	0.26	0.00	0.00
69-H-15	12.19	18.29	6.10	0.36	0.00	0.00
69-H-15	24.38	48.77	24.39	0.36	0.00	0.00
69-H-15	67.06	94.49	27.43	0.47	0.00	0.00
69-H-15	97.54	106.68	9.14	0.36	0.00	0.00
69-H-19	24.38	30.48	6.10	0.52	0.00	0.00
69-H-19	33.53	39.62	6.09	0.26	0.00	0.00
69-H-19	48.77	70.10	21.33	0.28	0.00	0.00
69-H-19	85.34	112.78	27.44	0.35	0.00	0.00
69-H-19	121.92	128.02	6.10	0.47	0.00	0.00
69-H-19	170.69	176.78	6.09	0.37	0.00	0.00
69-H-20	10.67	27.43	16.76	0.36	0.00	0.00
69-H-20	54.86	91.44	36.58	0.27	0.00	0.00
69-H-20	131.06	146.30	15.24	0.52	0.00	0.00
69-H-20	152.40	164.59	12.19	0.28	0.00	0.00
69-H-21	21.34	33.53	12.19	0.40	0.00	0.00
69-H-21	42.67	51.82	9.15	0.27	0.00	0.00
69-H-21	73.15	82.30	9.15	0.24	0.00	0.00
69-H-21	91.44	106.68	15.24	0.34	0.00	0.00
69-H-21	112.78	118.87	6.09	0.23	0.00	0.00
69-H-21	124.97	140.21	15.24	0.22	0.00	0.00
69-H-22	48.77	54.86	6.09	0.33	0.00	0.00
69-H-22	70.10	82.30	12.20	0.27	0.00	0.00
69-H-22	94.49	124.97	30.48	0.27	0.00	0.00
69-H-22	128.02	170.69	42.67	0.27	0.00	0.00
69-H-22	173.74	182.88	9.14	0.35	0.00	0.00
69-H-22	185.93	195.07	9.14	0.38	0.00	0.00
69-H-22	204.22	222.50	18.28	0.28	0.00	0.00
69-H-22	225.55	237.74	12.19	0.40	0.00	0.00
69-H-22	243.84	271.27	27.43	0.43	0.00	0.00
69-H-22	274.32	286.51	12.19	0.27	0.00	0.00
69-H-22	289.56	295.66	6.10	0.27	0.00	0.00
69-H-23	39.62	45.72	6.10	0.31	0.00	0.00
69-H-23	57.91	64.01	6.10	0.28	0.00	0.00
69-H-23	88.39	167.64	79.25	0.54	0.00	0.00
69-H-23	170.69	176.78	6.09	0.21	0.00	0.00
69-H-23	210.31	274.32	64.01	0.53	0.00	0.00
69-H-23	277.37	286.51	9.14	0.32	0.00	0.00
69-H-24	18.29	27.43	9.14	0.22	0.00	0.00
69-H-24	57.91	67.06	9.15	0.32	0.00	0.00
69-H-24	88.39	109.73	21.34	0.31	0.00	0.00
69-H-24	115.82	124.97	9.15	0.30	0.00	0.00
69-H-24	134.11	152.40	18.29	0.33	0.00	0.00
69-H-24	161.54	185.93	24.39	0.51	0.00	0.00
69-H-24	198.12	207.26	9.14	0.28	0.00	0.00

Hole-ID	From	To	Length (m)	Cu (%)	Au (g/t)	Ag (g/t)
69-H-24	219.46	228.60	9.14	0.33	0.00	0.00
69-H-25	30.48	39.62	9.14	0.35	0.00	0.00
69-H-25	51.82	57.91	6.09	0.26	0.00	0.00
69-H-25	76.20	88.39	12.19	0.27	0.00	0.00
69-H-25	97.54	103.63	6.09	0.27	0.00	0.00
69-H-25	109.73	115.82	6.09	0.29	0.00	0.00
69-H-25	118.87	164.59	45.72	0.43	0.00	0.00
69-H-25	170.69	195.07	24.38	0.23	0.00	0.00
69-H-26	140.21	149.35	9.14	0.73	0.00	0.00
69-H-26	152.40	167.64	15.24	0.40	0.00	0.00
69-H-26	185.93	192.02	6.09	0.28	0.00	0.00
69-H-26	231.65	240.79	9.14	0.21	0.00	0.00
69-H-27	9.30	36.58	27.28	0.35	0.00	0.00
69-H-27	45.72	51.82	6.10	0.60	0.00	0.00
96-1	123.00	129.00	6.00	0.26	0.03	0.75
96-1	159.00	186.00	27.00	0.43	0.10	1.64
96-1	195.00	240.00	45.00	0.38	0.03	1.49
96-1	297.00	339.00	42.00	0.51	0.04	2.46
96-2	156.00	171.00	15.00	0.23	0.01	0.38
96-2	237.00	285.00	48.00	0.40	0.05	1.30
96-2	291.00	300.00	9.00	0.49	0.17	1.40
96-3	144.00	168.00	24.00	0.28	0.01	0.78
96-3	189.00	243.00	54.00	0.33	0.05	1.18
96-3	249.00	270.00	21.00	0.63	0.08	1.77
96-3	279.00	315.00	36.00	0.35	0.02	1.13
96-3	324.00	330.00	6.00	0.29	0.01	1.10
96-4	138.00	144.00	6.00	0.31	0.04	3.38
96-4	161.00	172.00	11.00	0.31	0.03	1.06
96-4	177.61	190.00	12.39	0.35	0.02	1.12
96-4	204.00	225.00	21.00	0.27	0.02	0.79
96-4	229.00	255.00	26.00	0.31	0.01	1.10
96-4	261.00	267.00	6.00	0.40	0.00	0.50
96-4	300.00	306.00	6.00	0.80	0.00	2.40
96-4	327.00	333.00	6.00	0.25	0.00	1.70
96-5	117.00	123.00	6.00	0.39	0.02	0.95
96-5	144.00	150.00	6.00	0.45	0.03	1.05
96-5	162.00	177.00	15.00	0.26	0.03	1.58
96-5	189.00	198.00	9.00	0.33	0.01	1.07
96-5	204.00	216.00	12.00	0.38	0.02	1.43
96-5	222.00	234.00	12.00	0.27	0.02	1.45
96-5	282.00	306.00	24.00	0.82	0.06	2.94
96-5	315.00	321.00	6.00	0.30	0.01	1.45
96-5	333.00	339.00	6.00	0.27	0.01	1.15
96-6	87.00	108.00	21.00	0.27	0.02	0.97
96-6	117.00	129.00	12.00	0.40	0.04	1.43
96-6	144.00	150.00	6.00	0.44	0.04	3.55
96-6	168.00	183.00	15.00	0.87	0.13	4.20
96-6	192.00	198.00	6.00	0.50	0.07	3.95
96-6	207.00	222.00	15.00	0.35	0.02	1.28
96-6	231.00	240.00	9.00	0.23	0.01	1.57

Hole-ID	From	To	Length (m)	Cu (%)	Au (g/t)	Ag (g/t)
96-7	345.00	363.00	18.00	0.39	0.02	1.07
HC06-01	40.35	50.75	10.40	0.45	0.07	3.00
HC06-01	69.80	79.74	9.94	0.40	0.04	2.70
HC06-01	90.25	108.51	18.26	0.47	0.08	3.54
HC06-02	7.53	17.07	9.54	0.62	0.13	1.97
HC06-02	21.12	52.75	31.63	0.73	0.16	2.79
HC06-02	230.00	236.00	6.00	0.43	0.03	2.00
HC06-03	3.05	66.10	63.05	0.29	0.04	0.70
HC06-03	72.10	81.10	9.00	0.41	0.04	1.00
HC06-03	90.10	112.90	22.80	0.55	0.08	1.67
HC06-03	118.35	131.05	12.70	0.66	0.07	1.87
HC06-03	134.60	175.70	41.10	0.35	0.04	1.36
HC06-03	181.70	214.60	32.90	0.47	0.04	2.10
HC06-03	235.80	247.80	12.00	0.42	0.04	1.43
HC06-03	262.80	272.10	9.30	0.38	0.02	1.97
HC06-04	18.20	29.20	11.00	0.25	0.05	0.84
HC06-04	41.20	82.95	41.75	0.30	0.04	0.79
HC06-04	89.77	166.70	76.93	0.50	0.07	1.85
HC06-04	175.70	187.15	11.45	0.52	0.06	2.06
HC06-04	210.40	225.70	15.30	0.31	0.02	0.83
HC06-04	230.20	244.10	13.90	0.29	0.03	1.23
HC06-04	250.10	264.75	14.65	0.29	0.03	1.12
HC06-05	21.10	43.90	22.80	0.24	0.04	0.46
HC06-05	54.00	63.75	9.75	0.26	0.04	0.80
HC06-05	78.00	104.60	26.60	0.34	0.04	0.95
HC06-05	120.70	182.95	62.25	0.39	0.05	1.29
HC06-05	309.00	316.00	7.00	0.29	0.02	1.68
HC06-06	0.00	34.16	34.16	0.58	0.08	2.33
HC06-06	47.92	55.79	7.87	0.27	0.01	0.89
HC06-06	136.10	143.95	7.85	1.31	0.07	5.74
HC06-06	171.05	177.46	6.41	0.29	0.11	1.48
HC06-06	182.28	194.47	12.19	0.87	0.12	5.31
HC06-06	206.91	214.52	7.61	0.28	0.01	1.79
HC06-07	43.11	102.69	59.58	0.53	0.08	2.01
HC06-07	130.40	140.58	10.18	0.28	0.05	1.60
HC06-07	261.21	274.00	12.79	0.39	0.07	3.96
HC06-12	6.10	28.20	22.10	0.43	0.05	1.40
HC06-12	32.34	62.12	29.78	0.68	0.17	2.26
HC06-12	185.01	191.11	6.10	0.72	0.03	3.12
HC06-12	201.51	209.07	7.56	1.11	0.05	5.59
HC06-12	215.59	232.13	16.54	0.48	0.04	2.37
HC06-12	304.43	319.35	14.92	0.44	0.02	2.48
HC06-12	330.80	340.21	9.41	0.37	0.03	1.34
HC06-12	361.37	370.12	8.75	0.95	0.04	4.31
J-1	36.58	42.67	6.09	0.23	0.00	0.00
J-1	109.73	115.82	6.09	0.21	0.00	0.00
J-1	118.87	134.11	15.24	0.32	0.00	0.00
J-2	76.20	82.30	6.10	0.48	0.00	0.00
J-3	36.58	48.77	12.19	0.25	0.00	0.00
J-3	54.86	60.96	6.10	0.50	0.00	0.00

Hole-ID	From	To	Length (m)	Cu (%)	Au (g/t)	Ag (g/t)
J-3	73.15	85.34	12.19	0.23	0.00	0.00
J-3	94.49	128.02	33.53	0.30	0.00	0.00
J-4	6.10	15.24	9.14	0.22	0.00	0.00
J-4	21.34	76.20	54.86	0.39	0.00	0.00
J-4	85.34	97.54	12.20	0.29	0.00	0.00
J-5	170.69	176.78	6.09	0.38	0.00	0.00
J-5	201.17	207.26	6.09	0.24	0.00	0.00
J-5	210.31	216.41	6.10	0.21	0.00	0.00
J-5	225.55	252.98	27.43	0.48	0.03	1.46
J-6	33.53	48.77	15.24	0.34	0.00	0.00
J-6	57.91	70.10	12.19	0.25	0.00	0.00
J-6	170.69	182.88	12.19	0.26	0.00	0.00
J-6	185.93	213.97	28.04	0.34	0.00	0.00
J-7	6.10	21.34	15.24	0.24	0.00	0.00
J-7	27.43	33.53	6.10	0.24	0.00	0.00
J-7	42.67	67.06	24.39	0.34	0.00	0.00
J-7	155.45	173.74	18.29	0.28	0.00	0.00
J-7	195.07	231.65	36.58	0.29	0.00	0.00
J-8	51.82	64.16	12.34	0.26	0.03	0.88
J-8	73.15	167.64	94.49	0.43	0.04	1.57
J-8	192.02	274.32	82.30	0.48	0.05	1.71
J-9	6.10	24.38	18.28	0.23	0.02	0.23
J-9	39.62	48.77	9.15	0.32	0.04	0.53
J-9	60.96	103.63	42.67	0.47	0.04	1.29
J-9	118.87	124.97	6.10	0.37	0.09	0.45
J-9	128.02	140.82	12.80	0.33	0.05	0.51
J-11	243.84	277.37	33.53	0.39	0.00	0.00
J-11	295.66	310.90	15.24	0.27	0.00	0.00
J-13	9.14	31.70	22.56	0.28	0.03	0.74
J-13	36.58	45.72	9.14	0.29	0.01	0.59
J-13	57.91	164.59	106.68	0.38	0.05	1.44
J-13	179.83	186.08	6.25	0.21	0.03	1.54
J-14	82.30	106.68	24.38	0.36	0.05	0.73
J-15	51.82	60.96	9.14	0.25	0.00	0.00
J-15	70.10	76.20	6.10	0.22	0.00	0.00
J-15	85.34	155.45	70.11	0.39	0.00	0.00
J-15	158.50	164.59	6.09	0.40	0.00	0.00
J-15	170.69	185.93	15.24	0.61	0.00	0.00
J-16	36.58	45.72	9.14	0.30	0.02	0.80
J-16	51.82	70.10	18.28	0.26	0.03	0.73
J-16	85.34	155.45	70.11	0.43	0.05	1.42
J-16	158.50	164.59	6.09	0.44	0.03	0.95
J-16	170.69	185.93	15.24	0.65	0.04	1.70
J-16	192.02	201.17	9.15	0.23	0.00	0.00
J-17	44.81	57.00	12.19	0.27	0.03	0.83
J-17	75.29	81.38	6.09	0.34	0.01	1.10
J-17	84.43	133.20	48.77	0.37	0.04	1.34
J-17	136.25	166.73	30.48	0.40	0.03	1.19
J-17	172.82	178.92	6.10	0.24	0.03	1.05
J-17	181.97	209.40	27.43	0.28	0.03	1.30



Hole-ID	From	To	Length (m)	Cu (%)	Au (g/t)	Ag (g/t)
J-17	215.49	252.07	36.58	0.50	0.04	1.36
J-17	255.12	294.74	39.62	0.39	0.02	1.86
J-18	51.82	57.91	6.09	0.23	0.00	0.00
J-18	112.78	118.87	6.09	0.26	0.00	0.00
J-19	51.82	73.15	21.33	0.34	0.00	0.00
J-19	79.25	88.39	9.14	0.24	0.00	0.00
J-19	118.87	133.50	14.63	0.32	0.00	0.00
J-20	64.01	94.49	30.48	0.28	0.00	0.00
J-20	97.54	109.73	12.19	0.28	0.00	0.00
J-21	6.10	12.19	6.09	0.30	0.00	0.00
J-21	82.30	88.39	6.09	0.39	0.00	0.00
J-21	94.49	103.63	9.14	0.32	0.00	0.00
J-22	24.38	45.72	21.34	0.32	0.00	0.00
J-22	48.77	67.06	18.29	0.27	0.00	0.00
J-22	115.82	124.97	9.15	0.24	0.00	0.00
J-23	10.97	30.48	19.51	0.29	0.00	0.00
J-23	33.53	42.67	9.14	0.35	0.00	0.00
J-24	109.73	128.02	18.29	0.36	0.00	0.00
J-24	140.21	161.54	21.33	0.25	0.00	0.00
J-25	139.60	148.74	9.14	0.37	0.02	1.10
J-25	154.84	162.76	7.92	0.44	0.03	0.91
J-25	165.81	214.88	49.07	0.43	0.03	1.10
J-26	73.15	94.49	21.34	0.27	0.02	0.41
J-26	118.87	128.02	9.15	0.26	0.03	0.83
J-26	134.11	146.30	12.19	0.37	0.07	1.27
J-26	152.40	161.54	9.14	0.38	0.00	0.36
J-26	164.59	216.41	51.82	0.59	0.08	1.72
J-26	219.46	228.60	9.14	0.51	0.02	1.57
J-27	48.77	57.91	9.14	0.44	0.05	1.83
J-27	100.58	112.78	12.20	0.36	0.05	1.08
J-27	118.87	192.02	73.15	0.51	0.05	1.66
J-28	48.77	57.91	9.14	0.26	0.00	0.00
J-28	85.34	115.82	30.48	0.32	0.00	0.00
J-28	124.97	170.69	45.72	0.50	0.00	0.00
J-28	176.78	195.07	18.29	0.43	0.00	0.00
J-28	204.22	210.31	6.09	0.25	0.00	0.00
J-29	39.62	54.86	15.24	0.36	0.00	0.00
J-29	73.15	91.44	18.29	0.39	0.00	0.00
J-29	97.54	118.87	21.33	0.42	0.00	0.00
J-29	134.11	146.30	12.19	0.28	0.00	0.00
J-29	155.45	167.64	12.19	0.31	0.00	0.00
J-30	100.58	146.30	45.72	0.38	0.00	0.00
J-30	167.64	179.83	12.19	0.38	0.00	0.00
J-30	192.02	204.22	12.20	0.24	0.00	0.00
J-31	112.78	131.06	18.28	0.26	0.00	0.00
J-31	164.59	207.26	42.67	0.29	0.00	0.00
J-31	219.46	274.32	54.86	0.46	0.00	0.00
J-31	280.42	286.51	6.09	0.33	0.00	0.00
J-32	100.58	131.06	30.48	0.29	0.00	0.00
J-32	167.64	246.89	79.25	0.52	0.00	0.00

Hole-ID	From	To	Length (m)	Cu (%)	Au (g/t)	Ag (g/t)
J-32	256.03	262.13	6.10	0.26	0.00	0.00
J-33	256.03	320.04	64.01	0.52	0.08	1.20
J-33	329.18	338.33	9.15	0.27	0.03	0.73
J-34	124.97	140.21	15.24	0.31	0.00	0.00
J-34	152.40	207.26	54.86	0.48	0.00	0.00
J-34	210.31	225.55	15.24	0.43	0.00	0.00
J-35	164.59	173.74	9.15	0.24	0.00	0.00
J-35	179.83	207.26	27.43	0.35	0.00	0.00
J-35	225.55	237.74	12.19	0.49	0.00	0.00
J-35	246.89	262.13	15.24	0.23	0.01	0.50
J-35	265.18	274.32	9.14	0.23	0.01	0.97
J-36	82.30	103.63	21.33	0.24	0.02	0.43
J-36	134.11	152.40	18.29	0.28	0.03	1.08
J-36	164.59	176.78	12.19	0.33	0.03	0.91
J-36	181.51	219.46	37.95	0.39	0.06	1.34
J-36	228.60	237.74	9.14	0.32	0.02	0.80
NH-1	30.48	36.58	6.10	0.38	0.00	0.00
NH-2	77.72	99.06	21.34	0.57	0.00	0.00
NH-2	103.63	109.73	6.10	0.25	0.00	0.00
NH-3	42.67	67.06	24.39	0.93	0.09	4.26
NH-3	71.63	83.82	12.19	0.50	0.06	3.39
NH-3	88.39	103.63	15.24	0.67	0.13	5.32
NH-4	121.92	137.16	15.24	0.23	0.00	0.00
NH-5	4.88	24.38	19.50	0.93	0.00	0.00
NH-5	36.58	51.82	15.24	0.34	0.00	0.00
NH-5	73.15	79.25	6.10	0.21	0.00	0.00
NH-6	57.30	115.82	58.52	0.42	0.00	0.00
NH-6	134.11	143.26	9.15	0.27	0.00	0.00
NH-7	33.53	39.62	6.09	0.37	0.00	0.00
NH-8	137.16	146.30	9.14	0.68	0.00	0.00
NH-10	94.49	100.58	6.09	0.21	0.00	0.00
NH-11	36.58	54.86	18.28	1.10	0.08	5.65
NH-11	64.01	97.54	33.53	0.30	0.04	2.41
NH-12	50.60	57.15	6.55	0.72	0.07	4.02
NH-12	71.32	80.16	8.84	0.77	0.09	5.06
NH-13	33.53	45.72	12.19	0.79	0.05	2.95
NH-13	60.96	70.10	9.14	0.32	0.03	3.03
NH-15	6.10	27.43	21.33	0.86	0.00	0.00
NH-15	30.48	39.62	9.14	0.27	0.00	0.00
NH-15	109.73	115.82	6.09	0.48	0.00	0.00
NH-16	79.25	85.34	6.09	0.52	0.05	1.80
NH-17	18.29	27.43	9.14	0.39	0.00	0.00
NH-17	30.48	36.58	6.10	0.24	0.00	0.00
NH-17	48.77	54.86	6.09	0.44	0.00	0.00
NH-17	97.54	109.73	12.19	0.33	0.00	0.00
NH-18	30.48	36.58	6.10	0.27	0.00	0.00
NH-18	45.72	57.91	12.19	0.24	0.00	0.00
NH-18	94.49	103.63	9.14	0.22	0.00	0.00
NH-19	9.14	24.38	15.24	0.31	0.00	0.00
NH-19	30.48	39.62	9.14	0.23	0.00	0.00

Hole-ID	From	To	Length (m)	Cu (%)	Au (g/t)	Ag (g/t)
NH-20	30.48	39.62	9.14	0.83	0.00	0.00
NH-20	45.72	64.01	18.29	0.26	0.00	0.00
NH-20	79.25	91.44	12.19	0.28	0.00	0.00
NH-21	60.96	85.34	24.38	0.34	0.00	0.00
NH-21	100.58	118.87	18.29	0.42	0.00	0.00
NH-23	15.24	42.67	27.43	0.73	0.00	0.00
NH-23	51.82	57.91	6.09	0.29	0.00	0.00
NH-24	106.68	128.02	21.34	0.61	0.00	0.00
NH-25	24.38	30.48	6.10	0.22	0.00	0.00
NH-25	73.15	94.49	21.34	0.37	0.00	0.00
NH-25	97.54	128.02	30.48	0.40	0.00	0.00
NH-27	10.97	39.62	28.65	0.35	0.03	1.70
NH-27	43.28	66.45	23.17	0.62	0.19	3.27
NH-27	91.14	97.54	6.40	0.23	0.01	1.56
NH-28	32.61	45.72	13.11	0.38	0.00	0.00
NH-29	6.10	18.29	12.19	0.25	0.00	0.00
NH-29	24.38	48.77	24.39	0.30	0.00	0.00
NH-29	57.91	64.01	6.10	0.35	0.00	0.00
NH-29	73.15	82.30	9.15	0.27	0.00	0.00
NH-29	91.44	103.63	12.19	0.31	0.00	0.00
NH-29	134.11	151.79	17.68	0.33	0.00	0.00
NH-31	15.24	39.62	24.38	0.30	0.03	0.67
NH-31	45.72	51.82	6.10	0.29	0.04	0.60
NH-31	60.96	88.39	27.43	0.21	0.03	0.98
NH-32	33.53	39.62	6.09	0.24	0.01	1.00
NH-32	48.77	59.89	11.12	0.31	0.02	0.84
NH-32	64.01	70.10	6.09	0.61	0.03	1.40
NH-32	73.15	82.30	9.15	0.23	0.02	0.73
NH-32	97.54	115.82	18.28	0.42	0.05	1.18
NH-32	118.87	128.02	9.15	0.32	0.03	1.07
NH-33	42.67	60.96	18.29	0.36	0.00	0.00
NH-33	70.10	76.20	6.10	0.23	0.00	0.00
NH-34	15.24	24.38	9.14	0.35	0.03	0.63
NH-34	27.43	45.72	18.29	0.26	0.03	0.85
NH-35	7.32	18.29	10.97	0.74	0.00	0.00
NH-35	21.34	30.48	9.14	0.31	0.00	0.00
NH-35	33.53	51.82	18.29	0.43	0.00	0.00
NH-35	57.91	97.54	39.63	0.32	0.00	0.00
NH-36	60.96	100.58	39.62	0.35	0.00	0.00
NH-36	109.73	118.87	9.14	0.38	0.00	0.00
NH-36	124.97	131.06	6.09	0.25	0.00	0.00
NH-37	97.54	103.63	6.09	0.27	0.00	0.00
NH-37	106.68	118.87	12.19	0.44	0.00	0.00
NH-37	124.97	137.16	12.19	0.38	0.00	0.00
NH-37	140.21	167.64	27.43	0.43	0.00	0.00
NH-38	10.06	30.48	20.42	0.31	0.00	0.00
NH-38	39.62	103.63	64.01	0.54	0.00	0.00
NH-38	106.68	121.92	15.24	0.24	0.00	0.00
NH-39	15.85	39.62	23.77	0.57	0.00	0.00
NH-39	45.72	57.91	12.19	0.28	0.00	0.00

Hole-ID	From	To	Length (m)	Cu (%)	Au (g/t)	Ag (g/t)
NH-39	134.11	143.26	9.15	0.49	0.00	0.00
NH-40	39.62	45.72	6.10	0.23	0.02	0.70
NH-40	48.77	57.91	9.14	0.23	0.01	0.73
NH-40	73.15	88.39	15.24	0.53	0.08	3.88
NH-41	42.67	48.77	6.10	0.40	0.09	3.00
NH-41	97.54	106.68	9.14	0.51	0.07	3.60
NH-42	88.39	109.73	21.34	0.74	0.08	4.76
NH-43	9.14	18.29	9.15	0.40	0.00	0.00
NH-43	60.96	67.06	6.10	0.47	0.00	0.00
NH-44	6.10	36.58	30.48	0.79	0.00	0.00
NH-45	42.67	115.82	73.15	0.50	0.00	0.00
NH-45	128.02	134.11	6.09	0.22	0.00	0.00
NH-46	121.92	201.17	79.25	0.51	0.09	1.60
NH-47	18.29	24.38	6.09	0.26	0.00	0.00
NH-47	27.43	79.25	51.82	0.61	0.00	0.00
NH-48	8.23	18.29	10.06	0.41	0.00	0.00
NH-48	21.34	30.48	9.14	0.36	0.00	0.00
NH-48	36.58	70.10	33.52	0.53	0.00	0.00
NH-49	57.91	94.49	36.58	0.37	0.00	0.00
NH-50	109.73	118.87	9.14	0.67	0.00	0.00
NH-51	134.11	185.93	51.82	0.44	0.00	0.00
NH-53	45.72	64.01	18.29	0.33	0.00	0.00
NH-53	76.20	112.78	36.58	0.42	0.00	0.00
NH-54	6.10	42.67	36.57	0.33	0.05	0.77
NH-55	94.49	124.97	30.48	0.29	0.00	0.00
NH-55	128.02	164.59	36.57	0.41	0.00	0.00
NH-58	64.01	106.68	42.67	0.41	0.05	0.44
NH-59	15.24	45.72	30.48	0.41	0.00	0.00
NH-60	106.68	137.16	30.48	0.42	0.00	0.00
NH-60	140.21	161.54	21.33	0.34	0.00	0.00
NH-61	45.72	51.82	6.10	0.34	0.00	0.00
NH-61	64.01	103.63	39.62	0.39	0.00	0.00
NH-62	24.38	30.48	6.10	0.37	0.00	0.00
NH-62	36.58	57.91	21.33	0.48	0.00	0.00
NH-63	134.11	143.26	9.15	0.26	0.00	0.00
NH-63	152.40	167.64	15.24	0.34	0.00	0.00
NH-65	4.57	18.29	13.72	0.44	0.00	0.00
NH-65	21.34	27.43	6.09	0.29	0.00	0.00
NH-65	30.48	42.67	12.19	0.47	0.00	0.00
NH-66	88.39	97.54	9.15	0.28	0.01	0.17
NH-66	103.63	109.73	6.10	0.31	0.03	0.45
NH-68	115.82	121.92	6.10	0.23	0.00	0.00
NH-69	30.48	36.58	6.10	0.29	0.01	0.10
NH-71	85.34	94.49	9.15	0.47	0.00	0.00
NH-72	88.39	149.35	60.96	0.39	0.00	0.00
NH-73	42.67	79.25	36.58	0.42	0.00	0.00
NH-74	21.34	70.10	48.76	0.45	0.00	0.00
NH-78	18.29	24.38	6.09	0.28	0.00	0.00
NH-78	70.10	79.25	9.15	0.33	0.00	0.00
NH-90	5.18	12.19	7.01	0.41	0.00	0.00

Hole-ID	From	To	Length (m)	Cu (%)	Au (g/t)	Ag (g/t)
NH-90	21.34	51.82	30.48	0.36	0.00	0.00
NH-91	45.72	118.87	73.15	0.44	0.00	0.00
NH-92	198.12	225.55	27.43	0.33	0.03	0.98
NH-92	240.79	265.18	24.39	0.65	0.00	0.00
NH-93	30.48	103.02	72.54	0.51	0.00	0.00
NH-94	88.39	94.49	6.10	0.87	0.00	0.00
NH-94	97.54	106.68	9.14	0.29	0.00	0.00
NH-95	33.53	42.67	9.14	0.22	0.01	0.87
NH-95	48.77	54.86	6.09	0.22	0.01	0.90
NH-95	70.10	103.63	33.53	0.29	0.02	1.24
NH-95	106.68	115.82	9.14	0.28	0.01	0.90
HC06-08	25.07	53.92	28.85	0.38	0.04	1.53
HC06-08	58.23	84.40	26.17	0.56	0.12	2.02
HC06-08	279.50	294.93	15.43	0.64	0.04	3.76
HC06-08	316.89	325.29	8.40	0.73	0.02	6.16
HC06-09	6.10	31.69	25.59	0.49	0.05	2.27
HC06-09	40.49	72.12	31.63	0.48	0.12	1.83
HC06-09	79.13	85.72	6.59	0.36	0.02	0.87
HC06-10	118.60	125.42	6.82	0.39	0.02	2.21
HC06-10	128.93	136.70	7.77	1.06	0.11	8.20
HC06-11	144.81	169.92	25.11	0.53	0.08	3.18
HC06-11	255.97	262.13	6.16	0.33	0.01	2.58
HC06-11	273.20	280.15	6.95	0.45	0.02	1.43
HC07-13	110.72	131.21	20.49	0.24	0.01	0.90
HC07-13	135.10	145.06	9.96	0.34	0.04	1.47
HC07-13	148.51	188.17	39.66	0.54	0.06	1.81
HC07-13	287.00	303.15	16.15	0.45	0.07	3.48
HC07-13	307.65	314.48	6.83	0.45	0.04	2.61
HC07-13	347.06	375.07	28.01	0.38	0.04	1.81
HC07-13	415.11	421.99	6.88	0.49	0.01	1.93
HC07-13	500.22	510.11	9.89	0.51	0.07	1.95
HC07-14	189.90	206.32	16.42	0.34	0.04	1.49
HC07-14	209.80	245.55	35.75	0.32	0.03	2.86
HC07-14	334.23	363.00	28.77	0.40	0.05	2.42
HC07-14	366.45	374.85	8.40	0.60	0.05	3.71
HC07-14	431.72	440.20	8.48	0.40	0.03	1.63
HC07-15	228.52	270.07	41.55	0.41	0.03	1.41
HC07-15	288.65	302.79	14.14	0.37	0.05	1.31
HC07-15	329.91	342.30	12.39	0.36	0.15	1.66
HC07-15	397.33	404.73	7.40	0.43	0.10	3.47
HC07-15	409.19	429.14	19.95	0.25	0.03	1.80
HC07-15	453.00	468.88	15.88	0.54	0.03	1.89
HC07-15	579.52	592.80	13.28	0.47	0.04	1.88
HC07-16	274.17	342.81	68.64	0.46	0.04	1.89
HC07-16	495.29	505.92	10.63	0.21	0.03	0.91
HC07-17	158.66	166.15	7.49	0.56	0.02	1.65
HC07-17	188.06	213.35	25.29	0.47	0.05	1.45
HC07-17	264.03	280.04	16.01	0.21	0.05	1.29
HC07-17	303.67	319.01	15.34	0.37	0.05	2.59
HC07-17	381.75	390.35	8.60	0.26	0.04	1.94

Hole-ID	From	To	Length (m)	Cu (%)	Au (g/t)	Ag (g/t)
HC07-17	449.15	458.55	9.40	0.50	0.01	2.05
HC07-17	580.53	589.20	8.67	0.26	0.02	1.12
HC07-18	92.00	98.31	6.31	0.42	0.05	1.49
HC07-18	105.80	116.14	10.34	0.25	0.02	0.65
HC07-18	120.14	159.48	39.34	0.36	0.04	1.15
HC07-18	163.35	175.83	12.48	0.54	0.05	2.46
HC07-18	221.26	229.40	8.14	0.46	0.05	5.49
HC07-18	244.09	256.80	12.71	0.26	0.03	1.35
HC07-18	261.21	274.22	13.01	0.35	0.02	2.17
HC07-18	370.21	376.40	6.19	0.37	0.03	1.45
HC07-19	101.05	109.59	8.54	0.43	0.05	0.81
HC07-19	130.22	144.60	14.38	0.34	0.03	1.11
HC07-19	150.60	174.25	23.65	0.42	0.04	1.63
HC07-19	184.76	198.40	13.64	0.22	0.04	0.94
HC07-19	208.35	216.14	7.79	0.39	0.03	1.80
HC07-19	219.96	227.44	7.48	0.26	0.01	1.19
HC07-19	233.60	240.85	7.25	0.29	0.01	0.99
HC07-19	484.05	506.10	22.05	0.44	0.03	2.21
HC07-20	16.46	51.90	35.44	0.26	0.03	0.69
HC07-20	77.52	87.54	10.02	0.28	0.02	8.43
HC07-20	93.33	99.90	6.57	0.44	0.03	1.99
HC07-20	211.14	221.49	10.35	0.28	0.02	0.70
HC07-21	25.27	35.12	9.85	0.54	0.04	2.22
HC07-21	116.26	125.15	8.89	0.50	0.02	0.99
HC07-22	26.00	34.20	8.20	0.32	0.03	1.03
HC07-22	62.10	72.24	10.14	0.50	0.08	2.27
HC07-22	105.40	115.93	10.53	0.31	0.05	2.36
HC07-22	119.97	130.45	10.48	0.48	0.10	3.13
HC07-22	153.14	165.77	12.63	0.56	0.02	2.24
HC07-22	185.80	192.53	6.73	0.27	0.01	2.32
HC07-22	286.50	301.30	14.80	0.29	0.05	1.03
HC07-23	38.84	46.12	7.28	0.25	0.02	1.39
HC07-23	53.08	60.95	7.87	0.37	0.03	1.30
HC07-23	96.98	112.01	15.03	0.35	0.03	1.39
HC07-23	115.42	122.67	7.25	0.71	0.05	7.25
HC07-23	176.04	185.00	8.96	0.42	0.07	4.13
HC07-23	188.66	201.16	12.50	0.48	0.02	2.99
HC07-23	230.64	245.97	15.33	0.52	0.02	2.91
HC07-24	12.37	18.43	6.06	0.29	0.02	1.09
HC07-24	26.52	33.78	7.26	0.34	0.03	1.44
HC07-24	50.33	81.71	31.38	0.32	0.03	2.60
HC07-24	130.15	139.70	9.55	0.46	0.02	3.81
HC07-24	145.18	159.28	14.10	0.28	0.03	3.25
HC07-24	236.91	244.04	7.13	0.65	0.05	5.06
HC07-24	295.62	302.00	6.38	0.55	0.02	4.50
HC07-25	96.76	104.55	7.79	0.27	0.02	0.27
HC07-25	121.32	131.87	10.55	0.38	0.00	0.64
HC07-25	135.87	143.65	7.78	0.44	0.03	1.31
HC07-25	151.60	159.79	8.19	0.32	0.01	1.00
HC07-25	163.61	173.80	10.19	0.31	0.02	0.62

Hole-ID	From	To	Length (m)	Cu (%)	Au (g/t)	Ag (g/t)
HC07-25	178.50	212.55	34.05	0.38	0.03	1.01
HC07-25	258.62	265.52	6.90	0.23	0.02	0.81
HC07-25	316.08	330.03	13.95	0.29	0.02	2.06
HC07-26	89.80	98.40	8.60	0.24	0.03	2.11
HC07-26	170.68	179.50	8.82	0.29	0.06	2.44
HC07-27	87.95	103.71	15.76	0.45	0.03	2.55
HC07-27	106.79	115.05	8.26	0.24	0.02	2.51
HC07-27	124.50	152.15	27.65	0.36	0.02	2.15
HC07-27	171.29	182.86	11.57	0.33	0.02	1.97
HC07-27	191.45	200.25	8.80	0.21	0.01	1.27
HC07-28	82.14	98.06	15.92	0.31	0.05	1.14
HC07-28	102.06	128.37	26.31	0.39	0.04	2.49
HC07-29	67.47	90.00	22.53	0.23	0.03	1.68
HC07-29	97.81	116.43	18.62	0.30	0.02	2.06
HC07-29	126.54	148.50	21.96	0.55	0.02	3.37
HC07-29	162.42	182.59	20.17	0.33	0.01	2.24
HC07-29	198.12	205.20	7.08	0.30	0.01	2.23
HC07-30	121.01	164.43	43.42	0.40	1.76	0.02
HC07-30	171.49	193.29	20.79	0.37	1.43	0.03
HC07-30	251.42	270.70	19.28	0.28	0.97	0.02
HC07-30	284.59	306.58	21.99	0.24	1.63	0.02
HC07-31	54.95	67.09	12.14	0.29	1.31	0.01
HC07-31	115.15	123.55	8.40	0.68	8.81	0.02
HC07-31	143.70	155.55	11.85	0.23	1.96	0.01
HC07-32	70.04	104.28	34.24	0.24	1.27	0.01
HC07-32	117.54	149.25	30.88	0.38	0.92	0.01
HC07-32	153.16	175.19	22.03	0.47	1.82	0.03
HC07-32	185.60	194.14	8.54	0.40	2.99	0.02
HC07-32	203.30	210.65	7.35	0.27	2.80	0.02
HC07-33	93.15	100.58	7.43	0.43	1.98	0.03
HC07-33	108.81	116.77	7.96	0.31	2.21	0.04
HC07-33	174.73	186.92	12.19	0.20	1.77	0.02
HC07-33	253.60	267.00	13.40	0.26	0.99	0.02
HC07-34	61.05	67.06	6.01	0.21	0.93	0.01
HC07-34	72.24	92.38	20.14	0.37	1.25	0.01
HC07-34	97.59	110.10	12.51	0.57	1.07	0.02
HC07-34	119.80	134.30	14.50	0.33	0.35	0.01
HC07-34	147.93	167.83	19.90	0.41	1.40	0.04
HC07-34	171.47	185.82	14.35	0.30	0.87	0.01
HC07-35	49.32	74.56	25.24	0.30	1.29	0.01
HC07-35	90.53	114.91	24.38	0.22	0.27	0.01
HC07-36	29.94	43.55	13.61	0.42	1.39	0.01
HC07-36	61.29	75.96	14.67	0.24	1.15	0.02
HC07-36	144.16	152.75	8.59	1.34	3.56	0.02
HC07-36	163.27	170.86	7.59	0.27	0.82	0.02
HC07-36	325.75	332.48	6.73	0.34	0.90	0.01
HC07-36	393.23	401.42	8.19	0.37	1.36	0.06
HC07-37	78.95	94.20	15.25	0.27	0.75	0.01
HC07-37	107.37	121.48	14.11	0.26	0.90	0.02
HC07-37	129.85	136.64	6.79	0.50	2.18	0.02

Hole-ID	From	To	Length (m)	Cu (%)	Au (g/t)	Ag (g/t)
HC07-37	142.36	169.77	27.41	0.60	2.35	0.02
HC07-37	193.33	210.99	17.66	0.49	2.61	0.01
HC07-37	223.70	236.15	12.45	0.31	0.92	0.01
HC07-37	243.23	267.02	23.79	0.25	1.43	0.01
HC07-38	115.15	128.00	12.85	0.36	1.00	0.02
HC07-38	141.20	151.02	9.82	0.27	1.36	0.02
HC07-39	19.43	42.35	22.92	0.37	1.39	0.01
HC07-39	124.01	145.39	21.38	0.38	2.02	0.02
HC07-39	161.24	174.25	13.01	0.36	1.07	0.02
HC07-39	269.28	294.56	25.28	0.25	1.19	0.02
HC07-39	299.52	314.69	15.17	0.31	0.73	0.03
HC07-39	328.94	343.80	14.86	0.23	1.32	0.01
HC07-40	81.98	98.30	16.32	0.30	0.86	0.01
HC07-40	102.45	113.68	11.23	0.23	0.47	0.01
HC07-40	128.89	138.60	9.71	0.50	1.29	0.01
HC07-40	177.36	196.11	18.75	0.40	0.62	0.01
HC07-40	199.60	219.06	19.46	0.58	1.14	0.02
HC07-40	230.66	258.11	27.45	0.44	1.65	0.03
HC07-41	89.50	125.17	35.67	0.30	1.32	0.02
HC07-41	130.50	142.80	12.30	0.27	1.27	0.02
HC07-41	155.46	166.28	10.82	0.40	0.77	0.03
HC07-41	172.62	193.03	20.41	0.34	3.63	0.02
HC07-41	206.35	227.69	21.34	0.42	2.80	0.02
HC07-41	234.80	243.45	8.65	0.55	3.25	0.02
HC07-41	260.14	293.63	33.49	0.35	2.37	0.02
HC07-41	299.01	317.36	18.35	0.29	1.28	0.01
HC07-42	92.30	98.85	6.55	0.21	0.69	0.02
HC07-42	102.58	116.91	14.33	0.31	0.53	0.01
HC07-42	130.72	153.14	22.42	0.32	1.25	0.01
HC07-42	162.75	169.40	6.65	0.35	1.25	0.01
HC07-42	215.88	241.60	25.72	0.35	1.17	0.02
HC07-42	264.00	274.08	10.08	0.29	2.34	0.02
HC07-43	52.09	60.75	8.66	0.26	1.03	0.01
HC07-43	64.73	73.30	8.57	0.21	0.61	0.02
HC07-43	92.84	110.10	17.26	0.39	1.99	0.01
HC07-43	113.18	128.56	15.38	0.35	1.25	0.01
HC07-43	146.00	158.86	12.86	0.25	1.00	0.01
HC07-43	163.00	182.66	19.66	0.58	1.83	0.03
HC07-43	185.95	220.49	34.54	0.35	2.03	0.03
HC07-44	77.48	83.94	6.46	0.28	1.21	0.02
HC07-44	133.20	151.80	18.60	0.24	0.61	0.01
HC07-44	158.47	204.26	45.79	0.30	1.32	0.03
HC07-44	224.16	245.97	21.81	0.20	1.57	0.01
HC07-45	44.50	63.23	18.73	0.45	1.62	0.01
HC07-45	66.80	74.83	8.03	0.24	1.56	0.01
HC07-45	78.33	87.43	9.10	0.41	1.88	0.02
HC07-45	111.48	119.52	8.04	0.33	1.08	0.01
HC07-45	136.96	147.10	10.14	0.39	1.07	0.03
HC07-45	151.31	158.99	7.68	0.32	0.82	0.02
HC07-46	6.10	47.39	41.29	0.49	1.67	0.02



Hole-ID	From	To	Length (m)	Cu (%)	Au (g/t)	Ag (g/t)
HC07-46	51.55	73.75	22.20	0.40	1.35	0.02
HC07-46	85.18	98.62	13.44	0.32	3.06	0.02
HC07-47	39.28	48.48	9.20	0.29	0.31	0.01
HC07-47	55.23	127.15	71.92	0.30	1.53	0.03
HC07-47	207.03	213.90	6.87	0.37	2.81	0.06
HC07-48	6.10	29.38	23.28	0.56	1.25	0.01
HC07-48	33.67	64.45	30.78	0.28	1.09	0.02
HC07-48	74.81	89.34	14.53	0.38	1.58	0.02
HC07-49	65.22	73.54	8.32	0.32	1.83	0.04
HC07-50	7.98	68.80	60.82	0.27	1.21	0.02
HC07-50	72.91	94.71	21.80	0.54	2.27	0.02
HC07-50	102.20	121.98	19.78	0.25	1.08	0.03
HC07-50	127.10	137.77	10.67	0.27	1.71	0.01
HC07-51	3.05	21.10	18.05	0.37	1.57	0.02
HC07-51	27.54	44.66	17.12	0.37	0.96	0.01
HC07-51	63.21	80.64	17.43	0.21	0.53	0.01
HC07-52	6.10	41.30	35.20	0.36	0.88	0.01
HC08-53	18.01	53.67	35.66	0.35	1.21	0.01
HC08-54	18.44	39.20	20.76	0.29	0.00	0.00
HC08-56	31.95	39.25	7.30	0.27	0.00	0.00
HC08-56	45.19	53.51	8.32	0.36	0.00	0.00
HC08-57	20.97	30.14	9.17	0.26	0.00	0.00
HC08-57	91.41	102.94	11.53	0.46	0.00	0.00
HC08-57	178.37	184.81	6.44	0.33	0.00	0.00
HC08-58	35.18	54.58	19.40	0.47	0.00	0.00
HC08-58	81.49	88.93	7.44	0.95	0.00	0.00
HC08-58	99.86	111.84	11.98	0.26	0.00	0.00
HC08-58	115.35	130.29	14.94	0.38	0.00	0.00
HC08-59	65.92	79.89	13.97	0.30	0.00	0.00
HC08-59	97.06	155.54	58.48	0.41	0.00	0.00
HC08-59	159.63	170.34	10.71	0.30	0.00	0.00
HC08-60	8.44	26.42	17.98	0.26	0.00	0.00
HC08-60	32.36	91.35	58.99	0.38	0.00	0.00
HC08-60	137.18	163.29	26.11	0.47	0.00	0.00
HC08-60	188.59	204.40	15.81	0.25	0.00	0.00
HC08-61	7.62	25.77	18.15	0.49	0.00	0.00
HC08-61	94.62	136.82	42.20	0.26	0.00	0.00
HC08-61	166.42	181.65	15.23	0.37	0.00	0.00
HC08-61	190.78	202.73	11.95	0.27	0.00	0.00
HC08-61	258.79	266.17	7.38	0.25	0.00	0.00
HC08-61	301.69	309.05	7.36	0.28	0.00	0.00
HC08-61	316.17	324.74	8.57	0.30	0.00	0.00
HC08-62	5.67	39.29	33.62	0.33	0.00	0.00
HC08-62	55.93	94.46	38.53	0.38	0.00	0.00
HC08-62	148.33	156.05	7.72	1.78	0.00	0.00
HC08-62	164.13	182.10	17.97	0.27	0.00	0.00
HC08-62	185.57	191.92	6.35	0.43	0.00	0.00
HC08-62	195.22	234.62	39.40	0.42	0.00	0.00
HC08-63	25.28	36.35	11.07	0.32	0.00	0.00
HC08-63	42.50	49.21	6.71	0.56	0.00	0.00

Hole-ID	From	To	Length (m)	Cu (%)	Au (g/t)	Ag (g/t)
HC08-63	124.82	134.83	10.01	0.33	0.00	0.00
HC08-63	139.98	176.11	36.13	0.21	0.00	0.00
HC08-63	195.93	205.26	9.33	0.47	0.00	0.00
HC08-63	228.20	239.38	11.18	0.20	0.00	0.00
HC08-63	244.74	262.63	17.89	0.41	0.00	0.00
HC08-63	266.78	332.47	65.69	0.38	0.00	0.00
HC08-63	350.29	358.31	8.02	0.26	0.00	0.00
HC08-63	361.36	377.04	15.68	0.31	0.00	0.00
HC08-63	380.55	390.90	10.35	0.27	0.00	0.00
HC08-64	9.14	22.61	13.47	0.39	0.00	0.00
HC08-64	136.20	142.39	6.19	0.31	0.00	0.00
HC08-64	150.68	174.07	23.39	0.24	0.00	0.00
HC08-64	181.73	188.02	6.29	0.30	0.00	0.00
HC08-64	232.37	248.57	16.20	0.34	0.00	0.00
HC08-64	256.96	319.30	62.34	0.36	0.00	0.00
HC08-64	322.48	368.20	45.72	0.41	0.00	0.00
HC08-65	6.10	19.26	13.16	0.32	0.00	0.00
HC08-65	122.75	131.46	8.71	0.23	0.00	0.00
HC08-65	135.25	153.00	17.75	0.23	0.00	0.00
HC08-65	166.63	181.38	14.75	0.37	0.00	0.00
HC08-65	224.95	246.72	21.77	0.39	0.00	0.00
HC08-65	250.39	271.21	20.82	0.45	0.00	0.00
HC08-65	275.61	322.49	46.88	0.35	0.00	0.00
HC08-65	326.14	341.95	15.81	0.57	0.00	0.00
HC08-65	346.82	358.75	11.93	0.33	0.00	0.00
HC08-66	10.44	53.83	43.39	0.36	0.00	0.00
HC08-66	57.72	70.79	13.07	0.39	0.00	0.00
HC08-66	78.67	172.72	94.05	0.43	0.00	0.00
HC08-67	3.05	27.79	24.74	0.36	0.00	0.00
HC08-67	33.92	44.50	10.58	0.40	0.00	0.00
HC08-67	54.27	125.72	71.45	0.51	0.00	0.00
HC08-67	149.77	168.53	18.76	0.37	0.00	0.00
HC08-67	171.68	178.47	6.79	0.39	0.00	0.00
HC08-67	186.96	224.53	37.57	0.36	0.00	0.00
HC08-68	19.43	50.90	31.47	0.33	0.00	0.00
HC08-68	100.81	137.90	37.09	0.43	0.00	0.00
HC08-68	174.98	184.00	9.02	0.28	0.00	0.00
HC08-68	323.55	331.01	7.46	0.25	0.00	0.00
HC08-69	6.10	23.47	17.37	0.34	0.00	0.00
HC08-69	26.52	96.62	70.10	0.32	0.00	0.00
HC08-69	110.87	173.26	62.39	0.46	0.00	0.00
HC08-69	184.88	190.88	6.00	0.39	0.00	0.00
HC08-69	200.21	207.91	7.70	0.51	0.00	0.00
HC08-69	212.92	244.71	31.79	0.31	0.00	0.00
HC08-69	254.25	261.21	6.96	0.21	0.00	0.00
HC08-70	15.01	25.79	10.78	0.33	0.00	0.00
HC08-70	73.67	81.38	7.71	0.39	0.00	0.00
HC08-70	84.43	98.65	14.22	0.26	0.00	0.00
HC08-70	104.00	110.30	6.30	0.49	0.00	0.00
HC08-70	117.59	135.54	17.95	0.35	0.00	0.00

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Hole-ID	From	To	Length (m)	Cu (%)	Au (g/t)	Ag (g/t)
HC08-70	142.04	165.13	23.09	0.31	0.00	0.00
HC08-70	175.02	194.49	19.47	0.27	0.00	0.00
HC08-71	36.40	45.35	8.95	0.44	0.00	0.00
HC08-71	52.90	86.96	34.06	0.31	0.00	0.00
HC08-71	93.96	115.81	21.85	0.56	0.00	0.00
HC08-72	4.80	22.16	17.36	0.25	0.00	0.00
HC08-72	25.72	76.56	50.84	0.42	0.00	0.00
HC08-72	85.29	97.81	12.52	0.30	0.00	0.00
HC08-72	101.24	134.97	33.73	0.39	0.00	0.00
HC08-73	23.80	30.32	6.52	0.24	0.00	0.00
HC08-73	34.33	69.19	34.86	0.30	0.00	0.00
HC08-73	81.02	121.88	40.86	0.50	0.00	0.00
HC08-73	125.29	143.31	18.02	0.33	0.00	0.00
HC08-73	186.98	201.63	14.65	0.38	0.00	0.00
HC08-73	211.95	258.86	46.91	0.42	0.00	0.00
HC08-73	264.95	284.42	19.47	0.29	0.00	0.00
HC08-74	15.65	29.57	13.92	0.32	0.00	0.00
HC08-74	34.18	60.25	26.07	0.45	0.00	0.00
HC08-74	142.97	163.47	20.50	0.43	0.00	0.00
HC08-74	203.30	220.51	17.21	0.25	0.00	0.00
HC08-74	224.12	231.86	7.74	0.24	0.00	0.00
HC08-74	249.59	268.01	18.42	0.47	0.00	0.00
HC08-74	295.63	302.77	7.14	0.27	0.00	0.00
HC08-74	308.56	328.16	19.60	0.30	0.00	0.00
HC08-74	363.73	382.12	18.39	0.39	0.00	0.00
HC08-75	26.70	41.94	15.24	0.24	0.00	0.00
HC08-75	108.65	155.77	47.12	0.36	0.00	0.00
HC08-75	181.57	197.50	15.93	0.25	0.00	0.00
HC08-75	224.30	273.12	48.82	0.32	0.00	0.00
HC08-75	343.43	351.25	7.82	0.33	0.00	0.00
HC08-75	356.17	366.95	10.78	0.34	0.00	0.00

## **26 APPENDIX 3**

### **SEMI-VARIOGRAM MODEL**

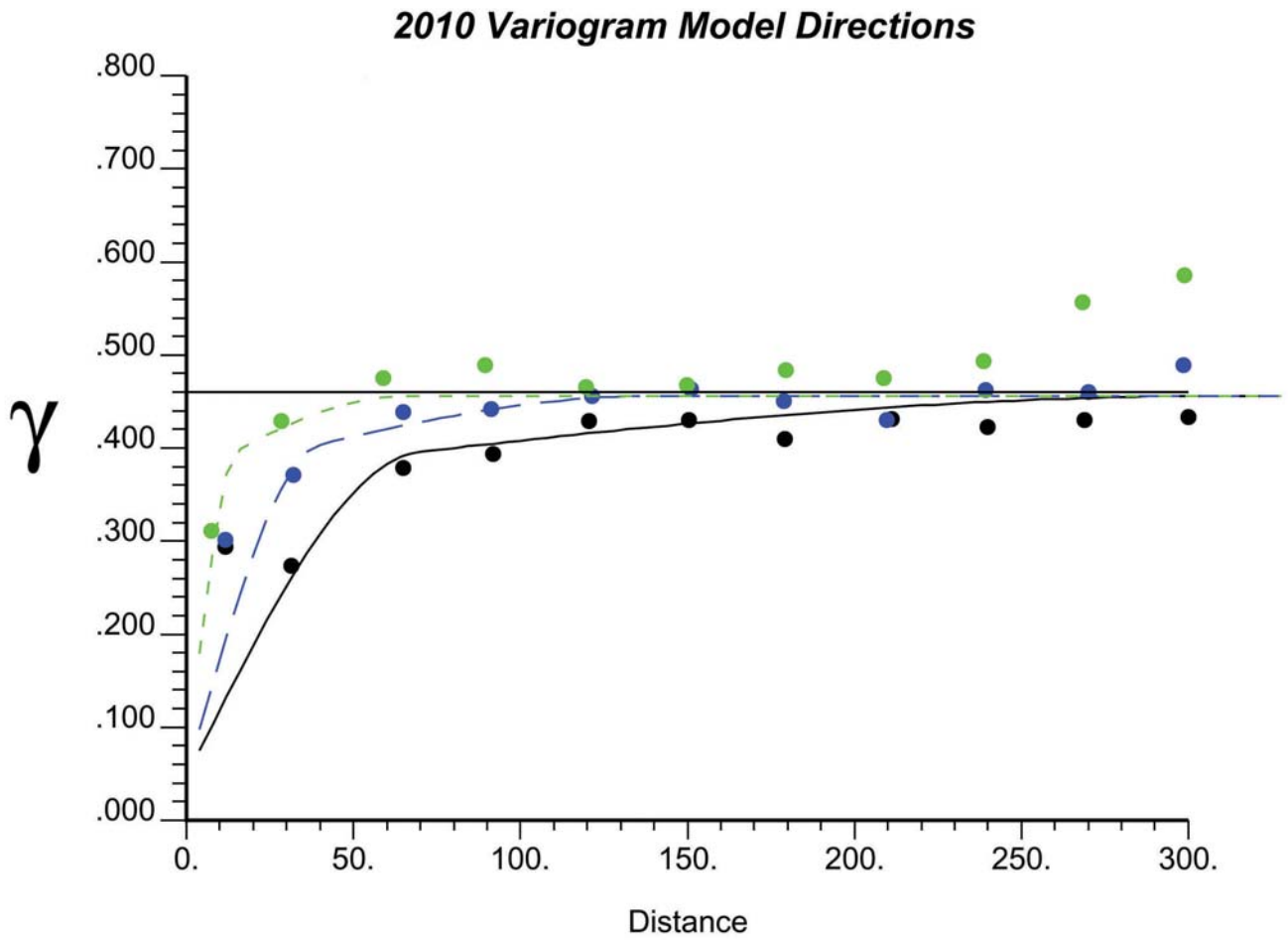


Figure A3-1

**Yellowhead Mining Inc.**  
*Harper Creek Project*  
*British Columbia Canada*  
**Variogram Model Directions**