



ASSESSMENT REPORT TITLE PAGE AND SUMMARY

TITLE OF REPORT : SOIL GEOCHEMICAL SURVEY – GRID EXTENSION – WEST – LINES K TO O

TOTAL COST: \$17,063.40

AUTHOR(S): Robert E. "Ned" Reid, P.Geo.; Fran Macpherson, M.A. SIGNATURE(S): "*signed*" NOTICE OF WORK PERMIT NUMBER(S)/DATE(S) STATEMENT OF WORK EVENT NUMBER(S)/DATE(S): 4921018 July 27, 2011

YEAR OF WORK: 2011 PROPERTY NAME: Weaver Creek Grid CLAIM NAME(S) (on which work was done): J1 204123 & STU1 204184

COMMODITIES SOUGHT: Gold (Au)

 MINERAL INVENTORY MINFILE NUMBER(S), IF KNOWN

 MINING DIVISION : Cariboo

 NTS / BCGS: 93A14 / 093A.073 & 093A.083

 LATITUDE __52_____o __47____' _30_____"

 LONGITUDE __121____o __27___' ____" (at centre of work)

 UTM Zone 10 EASTING 60300 NORTHING 5851000

OWNER(S): Noble Metal Group Incorporated MAILING ADDRESS: 1501-543 Granville St. Vancouver B.C. V6C 1X8

OPERATOR(S) [who paid for the work]: Noble Metal Group Incorporated MAILING ADDRESS

REPORT KEYWORDS (lithology, age, stratigraphy, structure, alteration, mineralization, size and attitude **do not use abbreviations or codes**)

REFERENCES TO PREVIOUS ASSESSMENT WORK AND ASSESSMENT REPORT NUMBERS See References in Report

SOIL GEOCHEMICAL SURVEY

GRID EXTENSION - WEST – LINES K to O

KEITHLEY CREEK AREA

WEAVER CREEK

CARIBOO MINING DIVISION

BRITISH COLUMBIA

EVENT NUMBER 4921018

NTS 93A/14W

BCGS 93A/73 & 93A/83

LATITUDE 52° 47" 30" LONGITUDE 121° 27'

UTM ZONE 10: 5851000 N 603000 E

FOR

NOBLE METAL GROUP INCORPORATED

November 25, 2011

Prepared by

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And

Fran Macpherson, M.A. Accurate Mining Services Ltd. 1282 March Road, Quesnel B.C. Phone: 250-992-2801 Email: <u>fmacpherson@accuratemining.com</u> BC Geological Survey Assessment Report 32521

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SUMMARY

Noble Metal Group Incorporated holds title to 73 mineral claims in the Cariboo Mining Division of British Columbia, Canada, NTS 93A/14W. northeast of the community of Likely, B.C.

Intermittent exploration has been carried out over portions of the property in past years.

This report presents the analytical results obtained from a soil sampling survey completed on the western extension of a portion of the of Weaver Creek grid carried out in July 2011. The survey was designed to test an area west of the previous survey grid, established in 2007 & 2008, straddling Weaver Creek in the north eastern sector of the property (AR by W. Timmins Event Numbers 4181754 & 4239018). The western extension of Lines K to O, filled in the "gap" between the original grid sampling and the road or "S" line sampling completed in June 2011 (AR by Timmins Event Number 4902826).

The results for gold are shown in ppb's on the accompanying Figure 4. Spot highs of 20 and 25 ppb Au were obtained and these sites will warrant further examination. The ICP analysis results for other elements are included in the Appendix, and indicate no values of anomalous significance.

Introduction and Term of Reference

The authors were requested by Dorothy Dennis, President of Noble Metal Group Incorporated, to present the results of a geochemical soil reconnaissance survey conducted on the Weaver Creek area within the company's wholly owned Cariboo Mineral Property in order to meet assessment requirements.

Survey information was supplied by William Timmins P.Eng., who usually undertakes the reporting, but due to illness within his family, was unavailable to complete the report according to the report submission deadline. This report relies upon data from several previous reports by Timmins.



PROPERTY DESCRIPTION AND LOCATION

The property is located approximately 21 kilometers north-northeast of the community of Likely, in the Cariboo Mining Division of British Columbia, Canada, NTS 93A/14, BCGS 093A073, 093A083 centered approximately at latitude 52 47'N, longitude 121 29'W (Figures 1 & 2).

The property consists of 73 contiguous located claims containing 11,214.79 hectares (27,711.37 acres).

A list of the claim tenure numbers and expiry dates are tabulated in Table 1 and illustrated on Figure 2.

This report covers work completed and filed as Event Number 4921018 on July 27, 2011 for the claims listed below and their new expiry dates.

Tenure No.	Claim Name	Area (ha)	New Good to Date
204123	J#1	500	2012/10/12
204184	STU 1	300	2012/06/15
204757	CAC II	500	2012/06/15
205123	CAC 3	500	2012/07/31
205124	CAC 4	500	2012/07/31
205125	CAC 5	500	2012/07/31



Tenure No	Name	Map No	Issue Date	Good To Date	Area (ha)
204123	J #1	093A073	1978/oct/12	2012/oct/12	500.0
204184	STU 1	093A083	1979/aug/17	2012/jun/15	300.0
204185	D.D. 2	093A073	1979/aug/17	2012/jun/15	150.0
204351	CASCA 1	093A073	1980/oct/02	2011/oct/02	200.0
204363	CASCA 3	093A073	1980/oct/23	2011/oct/23	400.0
204364	CASCA 4	093A073	1980/oct/23	2011/oct/23	400.0
204757	CAC II	093A073	1983/jul/12	2012/jun/15	500.0
205123	CAC 3	093A083	1986/apr/16	2012/jul/31	500.0
205124	CAC 4	093A083	1986/apr/16	2012/jul/31	500.0
205125	CAC 5	093A083	1986/apr/16	2012/jul/31	500.0
320311	NMG #13	093A073	1993/aug/07	2011/nov/15	25.0
320312	NMG #14	093A073	1993/aug/07	2011/nov/15	25.0
320313	NMG #15	093A073	1993/aug/07	2011/nov/15	25.0
320314	NMG #16	093A073	1993/aug/07	2011/nov/15	25.0
320315	NMG #17	093A083	1993/aug/07	2011/nov/15	25.0
320316	NMG #18	093A083	1993/aug/07	2011/nov/15	25.0
320317	NMG #19	093A083	1993/aug/07	2011/nov/15	25.0
320318	NMG #20	093A083	1993/aug/07	2011/nov/15	25.0
320319	NMG #21	093A083	1993/aug/07	2011/nov/15	25.0
320320	NMG #22	093A083	1993/aug/07	2011/nov/15	25.0
320321	NMG #23	093A083	1993/aug/08	2011/nov/15	25.0
320322	NMG #24	093A083	1993/aug/08	2011/nov/15	25.0
320323	NMG #25	093A083	1993/aug/08	2011/nov/15	25.0
320324	NMG #26	093A083	1993/aug/08	2011/nov/15	25.0
320325	NMG #27	093A083	1993/aug/08	2011/nov/15	25.0
320326	NMG #28	093A083	1993/aug/08	2011/nov/15	25.0
320327	NMG #29	093A083	1993/aug/09	2011/nov/15	25.0
320328	NMG #30	093A083	1993/aug/09	2011/nov/15	25.0
320329	NMG #31	093A083	1993/aug/09	2011/nov/15	25.0
320330	NMG #32	093A083	1993/aug/09	2011/nov/15	25.0
320331	NMG #33	093A083	1993/aug/09	2011/nov/15	25.0
320332	NMG #34	093A083	1993/aug/09	2013/aug/09	25.0
320338	NMG #40	093A073	1993/aug/10	2011/nov/15	25.0
349094	D.D. 3	093A083	1996/jul/14	2012/jun/15	300.0
410855	CASCA 5	093A073	2004/may/29	2011/nov/15	500.0
410856	DOT 1	093A083	2004/may/29	2011/nov/15	500.0
412720	CAC 6	093A073	2004/jul/23	2011/nov/15	500.0
412721	CAC 7	093A073	2004/jul/25	2011/nov/15	500.0
412722	CAC 8	093A073	2004/jul/24	2011/nov/15	500.0

 TABLE 1
 Claim Listing

ACCESSIBILITY, CLIMATE, LOCAL RESOURCES, INFRASTRUCTURE AND PHYSIOGRAPHY

The property is located in the Quesnel Highlands of Central British Columbia with elevations ranging from 1000 to 1500 meters above sea level (asl).

Topography varies from steep along Keithley and Snowshoe Creeks to moderate and gentle at higher elevations, up to the Pikes Peak area where steep rugged slopes occur.

Keithley Creek flows in a southeasterly direction through the centre of the property with many creeks such as Donaldson, Honest John, Rabbit, Snowshoe and Weaver Creeks which empty into Keithley Creek.

The area receives significant precipitation throughout the year occurring from both rain and snow. Accumulations of snow may reach three or more meters during the winter months. Temperatures can vary from -35° in winter to $+30^{\circ}$ in summer.

The natural vegetation is predominantly coniferous forest consisting of spruce, balsam, fir and cedar. Large portions of the property have been logged by clear cutting and most of these areas have been replanted. Many of the replanted areas contain second growth trees ranging from three to ten meters in height.

Access to the property is provided by an all-weather road to Keithley Creek from the community of Likely, B.C. From the old Keithley Creek settlement, a gravel logging road leads to the property. A network of logging and skid roads provide good access to all areas of the property, however road upgrading is often required.

A complete camp, consisting of trailers with built-on additions including kitchen-diner, three bedroom mobile, generator building, geological and core buildings, garage and tool shed is located on the J1 claim about 12 kilometers from the main road at Cariboo Lake.

The community of Likely, situated on Quesnel Lake, is reached by paved highway off Highway 97 about 12 kilometers southeast of the city of Williams Lake. Distance from Highway 97 to Likely is approximately 90 kilometers.

Williams Lake is a logging and lumber centre serviced by scheduled daily air service from Vancouver via Central Mountain Air. Necessary supplies and equipment as well as local labor and modern communications are readily available within the area.

Power for exploration purposes is supplied by portable generating units where required, while water is plentiful from the numerous creeks and rivers.

HISTORY

The Cariboo region of British Columbia is notable for the gold rush that began in 1860, which has continued to some degree to the present day. Placer gold was discovered in Keithley, Snowshoe, Little Snowshoe, and French Snowshoe Creeks around the same time.

Prospecting for lode deposits started shortly after the Cariboo gold rush began with production in the Wells-Barkerville area.

Noble Metal Group Incorporated and its predecessor company, Cascadia Mines and Resources Ltd., have been carrying out intermittent exploration for lode deposits since 1979.

Various work programs have been carried out on several areas of the property including soil geochemical surveys, magnetic, and electro-magnetic surveys, Induced Polarization (IP) surveys, trenching, and diamond drilling.

The most recent IP surveys were carried out by Pacific Geophysical Ltd. in 1995 and 1996. Several anomalies were tested by diamond drilling in 1996 and 2001 and anomalous values in gold, nickel, chromium, strontium, and vanadium were intersected.

A geochemical soil sampling survey was carried out over sections of the CAC 1, CAC 2 and CAC 3 mineral claims between May 20 and July 30, 2003 (Rabbit Creek Grid).

Geochemical soil sampling surveys were carried out in the Weaver Creek area in 2007and 2008. An electromagnetic and magnetometer survey was completed in 2009.

GEOLOGICAL SETTING

Regional Geology

The regional Geology is covered in GSC Memoir 421, Structural Geology of the Cariboo Gold Mining District, East-Central British Columbia, L.G. Struik 1988.

Property Geology

(Excerpted from W.G. Timmins, Report on Geochemical Survey, Keithley Creek Area, Weaver Creek)

The mineral claims are underlain by the rocks of the Ramos succession (Struik) of which interbedded quartzite and phyllite are the most abundant. The age of the Ramos succession is believed to be Hadrynian.

The quartzite is olive to grey on fresh surfaces, is poorly sorted and generally medium to coarse grained. The quartz clasts are predominately glass-clear and grey with minor blue. The quartzite is usually micaceous and sericite, epidote, muscovite, chlorite, and biotite occur along foliations. Some sections of the quartzite are weakly calcareous.

Graphitic schist containing pyritic sulphides was noted in proximity to anomalous gold values obtained by the Weaver Creek stream sediment survey in 2003 prompting the 2007and 2008 soil sampling surveys and the 2009 geophysical survey.

The phyllite varies from olive-gray to black with chlorite, graphite and accessory pyrite, and pyrrhotite. There is often rhythmic banding within the phyllite and contacts between the quartzite and phyllite are usually sharp.

The local area is underlain by the rocks of the Ramos succession containing phyllite, schist, calcsilicate rocks, and quartzite.

The main structure in the area is the Keithley Creek Thrust Fault that runs from Shoal's Bay on Quesnel Lake, northwest up Keithley Creek and along the lower portion of Rabbit Creek, carrying on to the northwest across Fontaine Creek. The dominant geological strike in the survey area is northwest however may be displaced by northeasterly trending faults.

Mineralization

Past geophysical surveys and diamond drill data reveals variable thicknesses of inter-bedded quartzite and green to black or grey phyllite intruded by diorite dikes, quartz-feldspar porphyry and altered ultramafic sill-like sections.

Sulphide enrichment, consisting of pyrite and pyrrhotite, occurs on chloritic and graphitic lamella and shear planes, quartz carbonate veins and veinlets and as disseminations and filling micro fractures.

Anomalous values in gold up to 0.07 oz/ton, nickel up to 1.0%, chromium up to 0.19% as well as anomalous values in strontium and vanadium have been encountered throughout past programs.

Significant iron oxide has been observed in minimal outcrop exposure west of Weaver Creek.

July 15 - 20, 2011 WORK PROGRAM (Figure 3)

A geochemical soil sampling program was carried out by Chart Ventures Inc., (E. Leimanis) for Noble Metal Group Incorporated from July 15 to July 20, 2011.

A total of 139 samples were collected from the "B" horizon, or the horizon below the root layer.

The samples were collected along grid lines spaced 100 meters apart and at 25 meter intervals. The grid lines are western extensions of the K to O lines of the previously established Weaver Creek Grid.

The samples were collected and placed in properly marked Kraft bags.

The samples were transported and stored each day in a secure building at the Noble camp where they were dried and packed. Upon completion of the program the samples were transported by the program supervisor, who delivered them to Eco Tech Laboratories in Kamloops, British Columbia.

Information for this report was supplied to the author by D. Dennis of Noble Metal Group Incorporated, W.G. Timmins, consultant to the company, and the analytical results received from Eco-Tech Laboratories in Kamloops, British Columbia.





ECO TECH: ANALYTICAL METHODOLOGY AND PROCEDURE

Sample Preparation

Samples (minimum sample size 250g) are catalogued and logged into the sample-tracking database. During the in process, samples are checked for spillage and general sample integrity. It is verified that samples match the sample shipment requisition provided by clients. The samples are transferred into a drying oven and dried.

Soils are prepared by sieving through an 80-mesh screen to obtain a minus 80-mesh fraction. Samples are unable to produce adequate minus 8-mesh material are screened at a coarser fraction. These samples are flagged with the relevant mesh.

Rock samples are crushed on a Terminator jaw crusher to -10 mesh ensuring that 70% passes through a Tyler 10 mesh screen.

Every 35 samples a re-split is taken using a riffle splitter to be tested to ensure the homogeneity of the crushed material.

A 250 gram sub sample of the crushed material is pulverized on a ring mill pulverizer ensuring that 95% passes through a -150 mesh screen. The sub sample is rolled, homogenized and bagged in a prenumbered bag. Barren gravel blank is prepared before each job in the sample prep to be analyzed for trace contamination along with the processed samples.

GOLD FIRE ASSAY: GEOCHEM (Au2-15,30,50)

A 15/30/50 g sample size is fired assay along with certified reference materials using appropriate fluxes. The flux used is pre-mixed, purchased from Anachemia which contains Cookson Granular Litharge. (Silver and gold free). The ratios are 66% Litharge, 24% Sodium Carbonate, 2.7% Borax, and 7.3% Silica. (The charges may be adjusted based on the sample). Flux weight per fusion is 150g. Purified Silver Nitrate or inquarts for the necessary silver addition is used for inquartation.

The resultant dore bead is parted and then digested with nitric acid followed by hydrochloric acid solutions and then analyzed on an atomic absorption instrument (Perkin Elmer/Thermo S-Series AA instrument).

Over-range geochem values (detection limit 5-1000ppb) for rocks are re-analyzed using gold assay methods (see below).

Appropriate certified reference material and repeat/re-split samples (Quality Control Components) accompany the samples on the data sheet for quality control assessment.

Results are collated by a computer and are imprinted along with accompanying quality data (repeats and standards). Results are emails, faxed or mailed to the clients.

ICP-AES AQUA REGIS DIGESTION (AR-ES)

A 0.5 gram is digested with a 3:1:2 (HCI: HNO3: H2O) solution in water bath at 95° C. The sample is then diluted to 10ml with water. All solutions used during the digestion process contain beryllium, which acts as an internal standard for the ICP run. The sample is analyzed on a Thermo IRIS Intrepid II XSP ICP unit. Certified reference material is used to check the performance of the machine and to ensure that proper digestion occurred in the wet lab. QC samples are run along with the client samples to ensure no machine drift occurred during the run procedure. Repeat samples (every batch of 10 or less) and re-splits (every batch of 35 or less) are also run to ensure proper weighing and digestion occurred.

Results are collated by a computer and are printed along with accompanying quality control data (repeats, re-splits, and standards). Any of the base metal elements (Ag, Cu, Pb, Zn) that are over limit (>1.0%) are immediately run as an ore grade assay.

SOIL GEOCHEMICAL RESULTS (Figure 4)

Gold assay results ranged from <5 ppb to 25 ppb. Two sites, containing the spot highs of 20 ppb (LK 3W) and 25 ppb (LM – 30W) are indicated on Figure 4.

Other elements analyzed exhibit background values.

CONCLUSIONS AND RECOMMENDATIONS

The 25 ppb result obtained from LM - 30 W is in close proximity to the 15 ppb value returned in a previous survey at LS #03. This area warrants further examination as does the spot high at LK - 3W.

It has been shown that "spot" highs, are significant in other areas of the Barkerville Gold Belt.

STATEMENT OF COSTS

Date of Work	July 15 – July 20 Inclusive, 2011
Work Performed on Tenures 204123(J#1) and 204184(STU 1)	
MOB and DEMOB	
Supervisor Truck Mileage – Kelowna/Property – Return 1,362k	m @\$0.65/km = \$ 885.30
Team Leader – Travel – Vancouver to property and return	= \$ 500.00

WORK PROGRAM:

Total		= \$	17,063.40
Report including typing, draftin	g, copying, binding and related costs	=\$4	,300.00
Assays		= \$ 5	5,357.06
Room and Board – 4 people (16	Person Days) @ \$100.00/Day	= \$ 1	1,600.00
Chain saw Rental	3 Days @ \$50.00 / Day	= \$	150.00
Fuel and Supplies		= \$	271.04
In Field Truck Rental	3 Days @ \$50.00/Day	= \$	150.00
2 Assistants	3 Days @ \$250.00/Day	= \$1	,500.00
Team Leader	3 Days @ \$250.00 / Day	=\$	750.00
Supervisor	4 Days @ \$400.00 / Day	= \$ 1	,600.00

Number of person days – 13

REFERENCES

Assessment Reports:

AR 08707: Mark D.G. 1981. Seismic Refraction Survey on PL1160 & PL 1161

AR 09719: Mark D.G. 1981. Seismic Refraction Survey on CASCA Claim Group.

AR 10209: Pattison E.F. 1981. Au Group, Report on Geology and Geochemistry.

AR 11117: Dibicki E.J. 1983.Geological, Geochemical and geophysical Report on the Au 1-7, 5-8, 10-13, 16-19 Claims.

AR 15847: Archanbault M, Timmins W.G. 1987. Drilling Assessment Report – CASCA Claims.

AR 16349: Timmins W.G. 1987. Drilling Assessment Report - Stu Claim Group

AR 17248: Davenport T. 1988. Assessment Report - Stu Claim Group

AR 18895: Lorimer M.K. 1989. Geochemical Report on the CAC Claim Group

AR 20502: Seywerd M.B. 1990. Induced Polarization Survey on the CAC Claim Group

AR 21523: Shearer J.T. 1991. Diamond Drilling on the CAC and J1 Groups

AR 21895: Seywerd M.B. 1990. Magnetometer and VLF EM Survey on the Stu Claim Group

AR 22524: Shearer J.T. 1991. Report on Sonic Drilling Program

AR 24085: Cartwright P. 1995. Induced Polarization and Resistivity Survey and Magnetometer Survey on the J1, CASCA 1-4 Claims

AR 24086: Cartwright P. 1995. Induced Polarization and Resistivity Survey and Magnetometer Survey on the DENND Claim

AR 24355: Crooker G. 1996. Diamond drilling Report on the J1 and CAB 3-5 mineral Claims

AR 24825: Schell B. 1997. Diamond Drilling Report on the J1 and NMG 29 Mineral Claims

AR 25192: Timmins W.G. 1997. Geological Report on the DID Claim group

AR Event Number 4239018: Timmins W.G. 2008. Report on the 2007-2008 Geochemical Soil Survey

AR Event number 4292657: Timmins W.G. 2009. Report on the 2009 Geophysical Survey

AR Event Number 4902826: Timmins W.G. 2011. Report on Geochemical Soil Survey

Hodgson, C.Jay. 1987. The Structure of Shear-Related, Vein-Type Gold Deposits: A Review. Ore Geology Reviews, 4 (1989) pp232-273. Elsevier Science Publishers B.V.

Holland, S.S. 1954. Geology of the Yanks Peak- Roundtop Mountain Area, Cariboo District, British Columbia Department of Mines, Bulletin 34.

Holland, S.S. 1950. Placer Gold Production of British Columbia; British Columbia Department of Mines, Bulletin 28 (reprinted 1986).

Johnston, W.A. and Uglow, W.L. 1926. Placer and Vein Gold Deposits of Barkerville, Cariboo District, British Columbia; Geological Survey of Canada, Memoir 149.

Levson, V.M. and Giles, T.R. 1993. Geology of Tertiary and Quaternary Gold-Bearing Placers in the Cariboo Region, British Columbia (93A, B, G, H); British Columbia Ministry of Energy, Mines and Petroleum Resources, Bulletin 89.

Robert, F., Poulsen, K.H. and Dube, B. 1994. Structural Analysis of Lode Gold Deposits in Deformed Terranes; Geological Survey of Canada, Open File Report #2850

Skerl, A.C. 1948. Geology of the Cariboo Gold Quartz Mine; Economic Geology, V.43. pp. 571-597.

Struik, L.C. 1988. Structural Geology of the Cariboo Gold Mining District, East-Central British Columbia; Geological Survey of Canada, Memoir 421. (O.F 1109 Outcrop Lithology Maps)

Statements of Qualification

Robert E. "Ned" Reid P.Geo. #16 - 231 Hartley Street Quesnel, BC V2J 1V8 Ph/Fax 250 992 3782

Certificate of Qualifications

I, Robert E. "Ned" Reid currently residing at apt #16 - 231 Hartley Street, Quesnel, British Columbia, do hereby certify that:

- 1. I am a graduate of the University of British Columbia, B.Sc. 1971, geology major.
- 2. I have been practicing my profession as an exploration and mine geologist / mine supervisor continuously since 1971.
- 3. I am a Professional Geoscientist registered with the Association of Professional Engineers and Geoscientists of British Columbia.(License # 20910) with sufficient relevant experience to be a "Qualified Person" as per National Instrument 43
- 4. I have prepared, along with Fran Macpherson, this report entitled "Soil Geochemical Survey: Grid Extension West Lines K to O" for assessment credit. I believe that this report accurately depicts the material obtained to date.
- 5. I have not been on the property, but have examined and reported upon several other properties in the Barkerville Gold Belt Area.
- 6. This report is compiled on data supplied by Dorothy Dennis, President of Noble Metal Group Inc., W.G. Timmins P.Eng., and a search of the numerous assessment reports available on the property

Dated at Quesnel B.C. this 22th day of November, 2011

"Signed and Sealed"

Robert E. "Ned" Reid P.Geo.

Frances J. 'Fran' Macpherson 1282 Marsh Road Quesnel, BC, Canada, V2J 6H3

Phone: (250) 992-2801 Fax: 888-515-9204 Email: <u>fmacpherson@accuratemining.com</u>

Statement of Qualifications

I, Frances J. (Fran) Macpherson, currently residing at 1282 Marsh Road, Quesnel, British Columbia, V2J 6H3, Canada, do hereby certify that:

- 1. I graduated with a B.A. (Psychology) from McGill University, P.Q. in 1972
- 2. I graduated with an M.A. (Clinical Psychology) from the University of New Brunswick, Fredericton NB in 1975
- 3. I have been employed in the mining industry since 1993
- 4. I was employed as mine manager on a large mineral exploration and bulk sample project in Wells, B.C. from 2000 to 2005 during which period I was involved in the drafting and compilation of numerous technical reports
- 5. I have owned and operated an independent consulting firm "Accurate Mining Services Ltd." since 2005
- 6. I have undertaken property management services for Noble Metal Group Incorporated, am familiar with the work and the claim group but have never visited the properties
- 7. I am not a partner or shareholder in Noble Metal Group Incorporated

Dated at Quesnel B.C. this 24th day of November 2011

alles

Fran Macpherson, M.A.

APPENDIX CERTIFICATE OF ANALYSIS



CERTIFICATE OF ANALYSIS AK 2011-0996

William Timmins Unit #3 - 950 Lanfranco Road Kelowna, BC V1W 3W8 6-Sep-11

No. of samples received: 139 Sample Type: Soil **Project: Weaver** Submitted by: William Timmins

		Au	
ET #.	Tag #	(ppb)	
1	LINE K 1W	10	ni ni ni hita ana in il na in in il na in in il na in in il na in in il na
2	LINE K 2W	<5	
3	LINE K 3W	20	
4	LINE K 4W	10	
5	LINE K 5W	10	
6	LINE K 6W	10	
7	LINE K 7W	10	
8	LINE K 8W	<5	
9	LINE K 9W	5	
10	LINE K 10W	10	
11	LINE K 11W	<5	
12	LINE K 12W	<5	
13	LINE K 13W	10	
14	LINE K 14W	15	
15	LINE K 15W	5	
16	LINE K 16W	10	
17	LINE K 17W	10	
18	LINE K 18W	10	
19	LINE K 19W	<5	
20	LINE K 20W	<5	
21	LINE K 21W	10	
22	LINE K 22W	5	
23	LINE K 23W	<5	
24	LINE K 24W	<5	
25	LINE K 25W	5	
26	LINE K 26W	5	
27	LINE K 27W	<5	
28	LINE K 28W	10	

All business is undertaken subject to the Company's General Conditions of Business which are available on request. Registered Office: Eco Tech Laboratory Ltd., 100041 Dallas Drive, Kamloops, BC V2C 6T4 Canada.

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William Timmins AK11-0996



6-Sep-11

		Au	
ET #.	Tag #	(ppb)	
29	LINE K 29W	<5	
30	LINE K 30W	5	
31	LINE K 31W	10	
32	LINE K 32W	5	
33	LINE K 33W	10	
34	LINE K 34W	10	
35	LINE L 1W	10	
36	LINE L 2W	10	
37	LINE L 3W	<5	
38	LINE L 4W	<5	
39	LINE L 5W	10	
40	LINE L 6W	<5	
41	LINE L 7W	<5	
42	LINE L 8W	10	
43	LINE L 9W	10	
44	LINE L 10W	<5	
45	LINE L 11W	<5	
46	LINE L 12W	<5	
47	LINE L 13W	<5	
48	LINE L 14W	5	
49	LINE L 15W	<5	
50	LINE L 16W	<5	
51	LINE L 17W	5	
52	LINE L 18W	<5	
53	LINE L 19W	<5	
54	LINE L 20W	<5	
55	LINE L 21W	<5	
56	LINE L 22W	5	
57	LINE L 23W	5	
58	LINE L 24W	<5	
59	LINE L 25W	<5	
60	LINE L 26W	5	
61	LINE L 27W	5	
62	LINE L 28W	5	
63	LINE L 29W	5	
64	LINE L 30W	10	
65	LINE L 31W	<5	
66	LINE L 32W	<5	
67	LINE M 1W	5	
68	LINE M 2W	<5	
69	LINE M 3W	5	

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William Timmins AK11-0996



6-Sep-11

			Au	
_	<u>ET #.</u>	Tag #	(ppb)	
	70	LINE M 4W	<5	
	71	LINE M 5W	5	
	72	LINE M 6W	<5	
	73	LINE M 7W	<5	
	74	LINE M 8W	5	
	75	LINE M 9W	5	
	76	LINE M 10W	5	
	77	LINE M 11W	<5	
	78	LINE M 12W	10	
	79	LINE M 13W	<5	
	80	LINE M 14W	<5	
	81	LINE M 15W	5	
	82	LINE M 16W	<5	
	83	LINE M 17W	<5	
	84	LINE M 18W	<5	
	85	LINE M 19W	5	
	86	LINE M 20W	<5	
	87	LINE M 21W	<5	
	88	LINE M 22W	15	
	89	LINE M 23W	10	
	90	LINE M 24W	10	
	91	LINE M 25W	10	
	92	LINE M 26W	<5	
	93	LINE M 27W	5	
	94	LINE M 28W	5	
	95	LINE M 29W	5	
	96	LINE M 30W	25	
	97	LINE N 1W	10	
	98	LINE N 2W	5	
	99	LINE N 3W	5	
	100	LINE N 4W	<5	
	101	LINE N 5W	<5	
	102	LINE N 6W	<5	
	103	LINE N 7W	10	
	104	LINE N 8W	5	
	105	LINE N 9W	5	
	106	LINE N 10W	<5	
	107	LINE N 11W	<5	
	108	LINE N 12W	10	
	109	LINE N 13W	<5	
	110	LINE N 14W	<5	

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William Timmins AK11-0996



06-Sep-11

		Au	
ET #.	Tag #	(ppb)	
111	LINE N 15W	5	
112	LINE N 16W	5	
113	LINE N 17W	<5	
114	LINE N 18W	10	
115	LINE N 19W	5	
116	LINE N 20W	5	
117	LINE N 21W	<5	
118	LINE N 22W	10	
119	LINE N 23W	5	
120	LINE N 24W	<5	
121	LINE N 25W	5	
122	LINE O 1W	<5	
123	LINE O 2W	<5	
124	LINE O 3W	10	
125	LINE O 4W	<5	
126	LINE O 5W	<5	
127	LINE O 6W	<5	
128	LINE O 7W	5	
129	LINE O 8W	5	
130	LINE O 9W	5	
131	LINE O 10W	<5	
132	LINE O 11W	<5	
133	LINE O 12W	10	
134	LINE O 13W	5	
135	LINE O 14W	5	
136	LINE O 15W	<5	
137	LINE O 16W	<5	
138	LINE O 17W	<5	
139	LINE O 18W	<5	
~~ ~ ~ ~ ~			
	<u>A:</u>		
Repeat			
1		10	
10	LINE K 10W	10	
22	LINE K 22W	10	
- 33	LINE K 33W	15	

33	LINE K 33W	15
37	LINE L 3W	5
47	LINE L 13W	5
54	LINE L 20W	5
67	LINE M 1W	5

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		Au	
ET #.	Tag #	(ppb)	
76	LINE M 10W	10	
83	LINE M 17W	5	
94	LINE M 28W	5	
99	LINE N 3W	10	
111	LINE N 15W	5	
116	LINE N 20W	5	
124	LINE O 3W	10	

Standard:

610
940
610
920

FA Geochem/AA Finish

NM/cr XLS/11

m

ECO TECH LABORATORY LTD. Norman Monteith B.C. Certified Assayer

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02-Sep-11

Stewart Group ECO TECH LABORATORY LTD. 10041 Dallas Drive KAMLOOPS, B.C. V2C 6T4

Phone: 250-573-5700 Fax : 250-573-4557 ICP CERTIFICATE OF ANALYSIS AK 2011-0996

William Timmins Unit #3 - 950 Lanfranco Road Kelowna, BC V1W 3W8

No. of samples received; 139 Sample Type; Soil **Project: Weaver** Submitted by: William Timmins

Values in ppm unless otherwise reported

		Ag	AI .	As	Ba	Be	Bi	Ca	a Cd	Ce	Co	Cr	Çu Fe	Ga	Ge	Hg K	La	Li Me	a Mn	Mo	Na	Nb	NI	Р	Pb	Rb	S	Sb	Sc S	ie :	Sn S	Sr -	la 1	Ĩe 🛛	ть ті	i	п	U	v	W	Y	Zn	Zr
Et #.	Tag #	ppm	% p	pm	ppm	ppm	ррп	n %	ррт	ррт	ppm	ppm	ppm %	ррт	ppm	opb %	ppm	ppm %	ppm	ppm	%	ppm	ppm_j	ррля	ppm	ppm	%	pm p	pm p	om p	pm p	om p	pm pp	от р	pm %	,F	opm p	pm p	opm	ppm	opm	ppm	ppm
1	LINE K 1W	0.2 (95	14.0	66.5	<0.1	0.22	2 0.1	4 0,17	45.6	11.3	3 34.0	17.6 2.57	4.2	2.5	15 0.06	26.0	9.6 0.3	2 458	1.63	0.039	0.20	21.2	319	24.5	8.1	<0.02	0.12	0.5	0.3	0.1 1	1.0 <).05 C	0.02	0.4 0.0	09 (0.06	1,1	26	0.3	4.3	48.5	0.62
2	LINE K 2W	1.9 2	1.15	19.8	145.5	0.5	0.34	4 0.5	5 1.39	76.7	20.1	45.5	37.9 4.03	6.4	4.3	125 0.13	39.0	20.0 0.3	4 1349	3.14	0.045	0.32	66.9	1467	34.5	12.3	0.08	0.20	1.5	0.9	0.2 3	7.5 <(0.05 0).04	0.8 0.0	08 C	0.10 1	13.8	32	0.3	28.0 1	56.4	1.62
з	UNE K 3W	0.2	.00	9.7	56.5	0.3	0.1€	6 0.1	3 0.28	52.2	9.4	1 32.5	23.6 2.11	4.1	2.1	40 0.06	26.0	11.0 0.3	3 243	1.05	0.041	0.22	28.0	413	19.3	8.4	0.02	0.18	0.5	0.4 <	:0.1 1	0.5 <(0.05 0).02	0.4 0.0	08 (0.06	1.3	20	0.2	4.3	67.4	0.54
4	LINE K 4W	0.4	.32	15.1	81.5	0.3	0.24	4 0.2	8 0.36	80.3	18,6	3 36.5	41.6 2.99	5.4	2.9	35 0.08	30.5	14.9 0.3	4 1212	1.75	0.041	0.22	45.5	548	27.1	11.2	0.04	0.26	0.6	0.5	0.2 2	1.0 <0	0.05 0).04	0.4 0.0	9 8 (0.08	2.8	28	0.2	7.9	97.4	0.56
5	LINE K 5W	0.1 (.46	6.0	51.0	0.2	0.10	0 0.0	6 0.25	54.1	3.3	3 12.0	22.4 1.27	3.4	1.3	t5 0.04	28.0	0.4 0.0	6 72	1.31	0.039	0.16	16.2	244	13.0	5.2 <	<0.02	0.14	0.3	0.3	0.1	7.0 <0	0.05 0	0.02	0.2 0.0	<u>)</u> 8 (0.04	0.8	20	0.2	3.2	35.0	0.49
6	LINE K 6W	0.1 (1.98	8.9	52.5	0.2	0.18	8 0.0	3 0.11	51.5	3.8	3 27.0	12.5 2.49	5.2	2.3	45 0.06	26.5	3.7 0.2	1 126	1.29	0.039	0.42	16.8	478	15.9	9.3 <	<0.02	0.14	0.9	0.3	0.2	5.5 <(0.05 <0	0.02	2.6 0.0	11 (0.06	0.5	26	0.2	2.0	45.9	0.77
· ·		<0.1 0	0.94	11.5	38.0	0.2	0.14	4 0.0	2 0.10	04.5	- 73	9 31.0	22.3 2.67	4.1	2.5	25 0.05	28.0	10.6 0.5	6 34/	1.38	0.039	0.20	28.0	428	15.4	/.2 <	<0.02	0.24	0.6	0.4 <	:0.1	4.5 <(0.05 <0).02	0.8 0.0	J7 (0.06	0.7	18	0.1	2.5	69.0	0.53
8		0.2	.03	8.3	40.0	0.4	0.24	4 0.2	0.24	81.5	11.1	30.0	29.1 2.25	5.4	2.3	20 0.07	38.5	9.8 0.1	8 794	1.36	0.041	0.20	28.4	472	22.4	13.7 ×	<0.02	0.14	0.5	0.3	0.2 1	7.5 <	0.05 0	2.04	0.3 0.0) 9 (0.06	1.9	28	0.2	7.5	60.8	0.46
40 Å	LINE K 10M	0.2 0	1.03 .00 ·	1.9	49.U	0.1	0.18	8 0.1 ¢ 0.0	0.0.10	91.0 40.1	8.0	3 22.3	10.4 2.12	5.0	2.0	45 0.05	20.0	8.1 0.1	7 700	1,13	0.037	0.24	19.4	350	22.2	10.3	<0.02	0.12	0.6	0.2	0.2 1	0.0 <).05 <0	3.02	0.4 0.0	16 (0.05	0.9	26	0.1	3.9	50.1	0.52
10	LINE N 1094	0.2	.00	13.2	90.D	0.1	0.10	0 U.U	0 0.20	49.1	1.0	29.0	20.7 3.20	3.0	2.0	45 0.04	25.0	11.2 0.2	9 298	1.44	0.039	0.30	27.0	1097	21.1	0.5	0.02	0.32	0.9	0.5 <	:0.1	6.0 <l< th=""><th>J.05 C</th><th>2.02</th><th>4.3 0.0</th><th>10 (</th><th>0.06</th><th>0.8</th><th>16</th><th>0.2</th><th>3.0</th><th>69.3</th><th>0.76</th></l<>	J.05 C	2.02	4.3 0.0	10 (0.06	0.8	16	0.2	3.0	69.3	0.76
11	LINE K 11W	⊰0.1.£	87	05	39.5	01	0.12	2.00	5 0 14	55.2	64	5 28 5	192 240	38	22	10 0.05	27.5	93.03	7 240	1 17	0.039	0.20	25.4	302	10.9	66.	-0.02	0.20	0.6	0.9.2	0.1	75 -1	05 -0	102	10.00	na i	0.04	0.6	16	0.1	99	50.2	0.62
12	LINE K 12W	0.1 (.77	8.7	42.5	0.3	0.16	6 0.0	8 0.11	59.0	6.8	3 24.5	20.0 2.25	3.7	2.1	10 0.05	29.5	83.03	4 280	0.94	0.042	0.16	26.7	308	9.3	6.5	-0.02	0.24	0.6	03 -	0.1	80 -1	105 0	0.02	08.00	11 (0.04	0.0	16	0.1	2.5	50.0	0.02
13	LINE K 13W	0.3	.43	15.5	89.0	0.3	0.24	4 0.1	1 0.70	57.1	9.6	5 43.0	43.6 3.04	5.3	3.0	25 0.10	39.5	14.5 0.3	9 295	1.37	0.042	0.20	42.0	619	23.2	11.2	0.02	0.18	0.9	0.5	01 1	20 <	105 0	02	0.0 0.0	08 (0.04	28	26	0.1	11.8	78.1	0.51
14	LINE K 14W	0.9	.24	10.6	125.5	0.5	0.22	2 0.6	0 1.20	68.6	17.0	31.5	43.7 2.27	4.7	3.2	120 0.10	80.0	8.1 0.2	8 1327	1.29	0.048	0.24	54.0	1216	30.0	9,9	0.12	0.42	0.5	0.9	0.2 4	0.5 <(0.05 0).02	0.1 0.0	05 (0.08	3.7	22	0.2	33.0	82.1	0.60
15	LINE K 15W	0.9	.49	8.1	93.0	0.3	0.22	2 0.1	1 0.36	55.4	8.3	3 41.5	27.9 2.18	5.4	2.3	70 0.10	37.5	16.2 0.3	8 289	0.98	0.041	0.20	38.2	716	24.1	10.9	0.04	0.14	0.5	0.4	0.1 1	3.0 <().05 0).02	0.2 0.0	0 6 (0.08	2.1	24	0.2	10.6	79.8	0.57
																																								-			
16	LINE K 16W	0.1 (.90	9.0	66.0	0.2	0.14	4 0.0	8 0.20	55.6	4.1	28.0	12.1 1.87	4.0	1.9	15 0.05	29.5	7.6 0.2	9 136	1.09	0.040	0.20	17.6	341	13.2	7.1 <	<0.02	0.10	0.5	0.2 <	0.1	8.0 <0	0.05 <0	0.02	0.6 0.0	08 (0.06	0.5	20	0.2	2.8	42.2	0.49
17	LINE K 17W	0.4 (.93	12.9	62.0	0.2	0.22	2 0.0	8 0.46	58.2	8.8	3 28.5	27.2 2.89	6.0	2,7	20 0.06	30.5	6.1 0.2	6 589	1.57	0.040	0.16	32.2	819	27.2	10.2 <	<0.02	0.24	0.4	0.4	0.2	9.0 <(0.05 <0).02	0.3 0.0	17 (0.06	0.9	32	0.1	3.3	82.0	0.58
18	LINE K 18W	0.8 (.48	9.1	53.5	<0.1	0.18	8 0.1	2 0.37	44.2	4.9	9 19.5	22.1 1.90	3.6	1.8	25 0.04	23.5	1.5 0.1	1 264	1.32	0.040	0.12	20.7	497	20.7	7.0 <	<0.02	0.30	0.3	0.3	0.1 1	0.0 <().05 <0	0.02	0.2 0.0	10 (0.04	0.7	22	0.1	2.7	63.9	0.49
19	LINE K 19W	0.9 (.45	2.8	69.0	0.1	0.08	9 0.0	0.31	45.1	6.3	3 11.0	10.7 1.03	3.5	1.1	20 0.03	22.5	1.2 0.0	7 1202	0.86	0.042	0.10	8.8	316	13.6	4.7 -	<0.02	80.0	0.2	0.2	0.2	7.0 <().05 <0).02	0.1 0.0	13 (0.10	0.4	16	0.1	2.3	29.9	0.45
20	LINE K 20W	0.5 (.75	11.8	40.0	0.2	0.16	B 0.0	3 0.27	51.0	5.4	1 24.0	17.0 2.20	5.2	2.1	25 0.05	26.0	5.4 0.1	9 322	1.38	0.038	0.24	21.6	629	14.3	6.1 <	<0.02	0.22	0.5	0.3	0.1	5.0 <(0.05 <0).02	0.5 0.0	15 (0.06	0.5	28	0.2	2.0	59.8	0.56
																							.																				
21	LINE K 21W	0.7 0	1.60	10.4	92.0	0.3	0.14	4 0.1	4 ().48	50.6	12.7	18.0	19.2 1.73	4.2	1.7	55 0.05	27.0	2.3 0.1	0 2059	1.13	0.039	80.0	20.7	684	30.2	7.5 <	<0.02	0.14	0.2	0.3	0.2 1	3.0 <(0.05 <0).02 <	0.1 0.0	J7 (9.08	1.1	20	0.1	4.1	48.1	0.41
22	LINE K 22W	0.4 (0.74	11.8	38.5	<0.1	0.20	0.0.0	6 0.21	48.2	4.	\$ 27.0	12.8 2.71	4.8	2.4	40 0.04	25.0	6.0 0.2	3 365	1.25	0.038	0.32	18.7	1377	20.6	4.5 <	< 0.02	0.22	0.6	0.4	0.1	6.0 <(0.05 0	0.02	0.8 0.0	14 (0.04	0.6	38	0.2	2.2	50.7	0.52
23		0.4 0	70 -	4.7	00.0 577 c	0.1	0.04	4 0.1	0.30	37.0	101	0.5	11.8 0.69 54.0 0.05	2.6	0.7	35 0.03	19.5	0.3 0.0	4 50	0.75	0.037	0.10	10.7	295	5.4	3.2 <	<0.02	0.10 •	c0,1	0.2	0.2 1	1.5 <().05 <0	0.02	:0.1 0.00	35 (0.04	0.5	10	0.1	2.0	28.9	0.48
24	LINE K 24VV	1.2	.70	10.9	177.0	0.7	0.34	4 U.U ¢ 0.0	6 0.63 6 1.00	47.0	10.0) 39.5) 69.5	24.9 3.93	0.0	3.5	90 0.15	31.0	11.2 0.2	0 031	2.24	0.042	0.36	47.2	953	40.4	14,4	0.04	0.36	0.9	0.5	0.3 1	4.0 <0	0.05 U	1.04	0.3 0.0	11 (20 i	0.10	2.9	36	0.4	9.8 1	11.0	0.62
2.7	LINE NZUW	1.976		10.0	172.0	0.9	0.30	0 0.2	.5 1.02	00.3	22.3	7 02.0	70.3 4.17	0.9	4.1	85 0.15	49.0	21.5 0.5	1 (20)	1.90	0.047	0.20	11.9	1020	49.7	0.01	0.06	0.02	1.0	0.8	0.2 2	0.0 <	0.05 U	.00	0.5 0.00	76 (2.12	Ð.Z	34	0.3	22.0 1	23.8	1.01
26	LINE K 26W	<0.1 1	.18	10.1	50.5	0.1	0.14	4 0.1	4 0.20	62.6	15.6	\$ 46.0	33.0 2.83	4.4	2.8	15 0.07	31.0	14.0 0.5	5 582	0.89	0.042	0.40	44.5	507	16.8	56 -	-0.02	0 24	21	03 -	0.1	05 <i>-</i> (05 0	0.02	72 00	40 (1.06	15	5 4	0.1	63	70 1	2 00
27	LINE K 27W	<0.1 (.60 1	13.9	31.5	<0.1	0.12	2 0.0	7 0.35	43.7	11.7	7 21.0	30.7 2.42	23	22	10 0.04	21.0	57.02	d 444	1.27	0.041	0.12	33.1	423	22.1	27.	<0.02 I	0.24	1.2	0.0 ~	0.1	70 A	0.05 0	ስ ሰፈ	56 0.0	na r	5.00 5.02	1.0	10	0.1	0.0	76.9	2.90
28	LINE K 28W	0.6 1	.86 1	17.6	128.5	0.9	0.26	6 0.2	4 0.63	109.9	22.6	5 51.5	69.5 3.67	5.8	3.7	40 0.12	49.5	29.2 0.4	1 841	1.29	0.042	0.30	84.7	570	35.0	11.9	0.02	0.28	1.4	0.7	02 2	0.5 ⊲0	105 0) 04	0.9 0.0	14 (1 08	55	32	12	1401	08.5	0.60
29	LINE K 29W	0.4 (.56	9.4	59.0	0.1	0.26	6 0.1	2 0.16	57.2	5.1	23.0	16.6 2.07	4.6	2.1	20 0.04	29.5	2.2 0.1	3 435	1.48	0.037	0.18	20.1	533	13.7	83 -	0.02	0.16	0.5	0.3	0.2 2	95 <(005 <0	102	07 00	16 (1.00	0.6	28	0.2	20	44 E	0.00
30	LINE K 30W	0.3 (.52	8.5	29.0	<0.1	0.20	0.0	5 0.09	51.8	3.2	2 19.0	12.6 1.77	4.6	1.8	35 0.04	26.0	2.7 0.1	1 111	1.07	0.037	0.34	12.9	533	11.7	5.3 <	<0.02	0.16	0.6	0.3	0.1	5.0 <0).05 <0	0.02	1.6 0.0	18 (0.06	0.5	28	0.2	20	33.9	0.10
																																				•		0,0	20	0.4		U U . U	0.70
31	LINE K 31W	0.6 (.69	9.3	40.0	0.1	0.18	8 0.0	2 0.12	60.2	3.8	3 22.0	13.6 2.19	4.8	2.1	30 0.05	30.5	4.4 0.1	5 306	1.13	0.039	0.24	15.2	7 79	13.3	8.2 <	<0.02	0.14	0.5	0.3	0.1	4.0 <().05 <0).02	1.2 0.0	12 (2.08	0.5	22	0.2	2.1	39.6	0 53
32	LINE K 32W	0.2 0	.41 1	2.2	27.0	<0.1	0.22	2 0.0	9 0.07	59.7	3.2	2 13.5	13.7 1.32	4.5	1.3	10 0 04	30.0	1.7 0.0	9 114	1.08	0.036	0.22	14.5	255	6. 6	6.4	<0.02	0.18	0.5	0.2	0.1	5.5 <0	0.05 0	.02	1.5 0.0	13 (9.06	0.6	28	0.2	2.0	34.5	0.66
33	LINE K 33W	0.3 1	.15 1	(4.7	78.5	0.1	0.22	2 0.1	3 0.f4	49.2	10.6	36.5	25.7 3.76	6.3	3.2	20 0.09	24.0	12.1 0.2	5 499	1,41	0.041	0.52	27.3	538	27.7	10.8 <	<0.02	0.22	1.2	0.3	0.2 1	0.5 <0	0.05 <0	0.02	2.5 0.02	22 r	0.08	8.0	36	0.2	2.4	69.0	0.76
34	LINE K 34W	1.1 2	.48 1	17.3	0.08	1.1	0.38	8 0.6	6 0.80	79.0	26.0	70.0	94.4 4.36	8.7	5.2	55 0.19	100.5	30.4 0.4	6 1260	1.29	0.049	0.54	86.9	821	44.0	21.9	0.04	0.28	2.8	1,1	0.3 4	2.5 <0	0.05 O	.04	1.8 0.0	16 C	0.08	9.5	44	0.3	38.9 1	15.8	0.90
35	LINE L 1W	0.4 1	.02 1	1.7	52.0	0.1	0.14	4 0.1	0 0.34	53.0	7.4	39.5	18.9 3.03	4.2	2.8	30 0.06	28.0	9.4 0.3	9 300	1.35	0.039	0.18	27.3	659	17.1	7.3	0.02	0.20	0.5	0.4 <	0.1	9.5 <0	0.05 <0	0.02	0.4 0.00	07 C	0.04	0.9	22	0.2	3.3	67.4	0.56

ICP CERTIFICATE OF ANALYSIS AK 2011-0996

William Timmins

Et#	. Taq #	Ag Al A	As Ba	Be	Si (Ca Col % nom	Ce	Co nom n	Cr -	Cu Fe	Ga nom r	Ge i	Hg K vab %a	La	Li Mg	Mn	Mo	Na l % n	Nb non n	NI I		Pb F	1b S	Sb	Sc	Se	Sn S	Sr 1	a Te) T	n Ti	n	U	V	w y	(Z	n Zr
36	LINE L 2W	0.3 1.21	9.8 92.0	0.2	0.26 0	.24 0.32	47.2	13.6	34.0	20.9 2.41	5.1	2.5	30 0.09	25.5	12.9 0.34	710	1.23 ().043 (0.20	26.5 f	594 2	23.3 1	1.3 0.	04 0.1	2 0.4	0.3	0.2 1	8.5 <(0.05 0.1	02 (0.2 0.007	0.06	1.9	24	0.2	5.2 G	0.6 0.63
37	LINE L 3W	0.9 1.01 1	1.3 65.5	0.2	0.16 0	0.05 0.19	53.4	6.0	30.5	18.6 2.88	4,4	2.7	45 0.04	27.0	10.4 0.31	258	1.38 0).037 (0.34	24.0 4	491 1	16.7	6.3 <0.	02 0.1	8 1.0	0.4	<0.1	6.5 <0	0.0 5 0.	04	4.0 0.010	0.04	0.7	20	0.2	2.4 6	5.5 0.81
39	LINE L 4W	0.2 0.66	5.2 121.0 8.6 59.0	0.9	0.34 0	0.05 0.54	52.4 55.9	28.1 3	38.5 21.0	43.5 3.89	4.5	3.6 20	55 0.11	26.0 29.5	34 0 11	2557	1.98 0	0.043 (0.039 (0.30 × 0.34	41.3 S 15.5 S	367 6 373 1	65.91 15.3	7.7 0. 76 <0	02 0.2	80.8 807	0.4	0.3	9.0 <0	0.05 D. 0.05 D.	04 (02 ·	0.5 0.013 1 8 0.016	0.10	2.3	38 24	0.3	5.7 10 27 1	9.6 0.55
40	LINE L 6W	0.1 0.48	5.2 23.0	<0.1	0.10 0	.14 0.07	51.1	2.1	12.0	10.4 0.89	3.7	1.0	15 0.05	26.0	2.7 0.09	73	0.84 0	0.038 (0.16	9.3 2	216	4.7	5.9 <0.	02 0.0	8 0.2	0.2	0.1 1	1.0 <0).05 <0.	02 (0.2 0.005	0.06	0.4	2⊶ 18	0.2	2.7 3 1.7 2	5.2 0.69 5.2 0.47
		0.0.070	<u>.</u>				50 Q		4 0 e																		•										
41		0.2 0.79	6.9 62.5	0.3	0.12 0	0.05 0.10	53.3 54.6	5.1 3.8	19.5 19.0	14.0 1.84	4.8 5.2	1.7	10 0.04	27.0	6.9 0.23	329 150	1,11 (0.038 0 0.038 0	0.24 0.40	16.7 0 14.6 0	388 1 396 1	10.9 10.6	6.2 <0. 4 9 <0	02 0.1	60.8 408	0.3	0.1	8.0 <0).05 <0. \05 ∠0	02 ·	1.0 0.018	0.08	0.5	26 24	0.1	2.8 4 25 4	5.7 0.56 22 0.65
43	LINE L 9W	0.4 1.44 1	4.9 76.5	0.6	0.20 0	0.09 0.33	63.0	29.7	33.0	37.1 2.87	4.7	2.7	50 0.07	35.0	20.5 0.34	739	1.53 (0.039 (0.30 :	37.7	730 3	31.7 1	3.3 0.	02 0.2	6 1.0	0.5	0.2	8.5 <0).05 <0.	02	1.4 0.011	0.08	1.5	22	0.2	7.68	6.6 0.55
44	LINE L 10W	0.1 0.97 1	0.5 46.5	<0.1	0.18 0	0.04 0.08	56.0	3.5	22.5	12.0 2.50	5.7	2.3	25 0.04	28.5	4.6 0.18	111	1.41 (0.038 0	0.52	14.8	573 1	10.8	5.8 <0.	02 0.2	0 1.1	0.3	0.2	4.5 <(0.05 0,	02 4	4.8 0.011	0.08	0.5	38	0.2	2.0 4	3.8 0.97
45	LINE L 11W	0.2 0.93	0.9 41.5	0.1	0.16 0	0.04 0.13	49.1	4.2	23.5	15.3 2.81	4,7	2.5	30 0.04	26.5	6.5 0.1 6	136	1.39 0	0.039 (0.44	18.0 f	549 1	15.6	7.2 <0.	02 0.2	0 0.8	0.3	0.2	6.0 <0).05 <0.	02 :	2.3 0.014	0.06	0.6	24	0.2	2.8 4	5.3 0.73
46	LINE L 12W	1.2 1.91 1	9.7 139.5	0.8	0.42 0	0.21 0.64	72.0	27.9	42.0	59.2 4.46	7.4	4.1	75 0.14	34.0	14.6 0.26	745	2.12	0.044 (0.46	54.8 13	278 5	54.6 1	4.3 0.	06 0.3	4 1.0	0. 6	0.3 2	3.5 <0	0.05 0.	04 (0.5 0.015	0.10	3.1	36	0.3 1	2.2 10	4.3 0.74
47	LINE L 13W	0.9 1.91 1	8.5 131.5	0.5	0.36 0	0.11 0.60	70.6	20.5	47.5	55.6 3.8 9	6.7	3.9	45 0.12	48.0	20.8 0.38	915	1.56 0	0.041 (0.28	59.5 9	913 4	40.9 1	4.6 0.	04 0.2	8 1.1	0.7	0.3 1	7.0 <(0.05 0.	04 (0.4 0.009	0.10	3.6	32	0.3 1	3.7 11	2.6 0.64
48 49	LINEL 14W	0.5 1.60 1	4.7 115.0 9.7 37.5) 0.5 : 0.2	0.32 0	0.15 0.76	64.9 53 1	20.6	42.5 22.5	41.0 3.24	6.1 4.2	3.1 2.0	30 0.10	40.0	19.9 0.38	989 275	1.19 (0.041 (0.22	46.6 7	783 3 504 4	38.9 1 12.7	3.4 0.	04 0.1) 01 0.0	8 0.7	0.5	0.2 1	5.5 <(0.05 0.	02 (0.3 0.008	0.08	2.6	30	0.2 1	3.2 9	8.1 0.59
50	LINE L 16W	0.2 0.50	6.6 37.5	0.1	0.14 0	0.04 0.10	55.1	4.5	16.0	9.1 1.27	4.4	1.3	15 0.04	28.0	4.0 0.13	283	1.10 0	0.039 (0.18 0.18	∡i.i s 11.6 4	425 1	13.7	9.2 <0. 8.2 <0.	02 0.2	0 0.4 8 0.3	0.3	0.1	5.0 <0).05 <0.).05 <0.	02 0	0.3 0.011	0.04	0.4	20 20	0.1	∠.a to 1.8 3	5.6 0.54
F 4	· (*)*** •																																- · ·				
52	LINEL 17W	0.2 0.55	8.0 36.0 67 31.5	0.1	0.14 0	1.06 0.14	52.3	3.6 2	20.5 14.0	10.9 1.53	4.1	1.5	15 0.04	26.5	4.9 0.18	213	0.88 (0.037 0	0.28	15.2 t 14.2 (561 1 250 1	11.3	7.2 <0.	02 0.1	6 0.6 6 0.5	0.2	0.1	5.5 <0).05 <0.	02 3	2.0 0.014	0.04	0.4	20	0.2 :	2.1 4	1.8 0.60
53	LINE L 19W	0.2 0.59 1	0.7 43.0	<0.1	0.18 0	0.04 0.38	45.5	6.1	22.5	14.2 2.25	4.5	1.9	20 0.04	23.0	4.4 0.10	469	1.19 0	0.038 (0.18	18.3 6	586 1	13.7	5.7 <0.	02 0.1	8 0.3	0.3	0.2	5.5 <0).05 0.	02 (0.3 0.010	0.06	0.4	24	0.2	1.7 5	3.7 0.59
54	LINE L 20W	0.8 2.04 1	9.5 114.5	0.9	0.38 0	0.29 0.32	108.7	39.0	47.5	57.8 4.21	6.5	4.0	85 0.12	48.5	21.0 0.34	1258	2.00 0	0.046 (0.24	60.0 11	195 5	58.3 1	2.1 0.	06 0.3	0 0.6	0.7	0.2 2	21.0 <0	0.05 0.	04 (0.5 0.006	0.10	3.8	28	0.2 1	5.5 10	1.3 0.70
55	LINE L 21W	0.2 0.33	5.8 24.0	<0.1	0.10 0	0.05 0.09	48.2	2.2	7.5	9.4 0.82	3.6	0. 9	10 0.03	24.0	1.2 0.04	60	0.75 (0.037 (0.12	8.1 2	223	4.9	4.3 <0.	02 0.1	2 0.1	0.2	0.1	4.5 <().05 <0.	02 (0.1 0.006	0.04	0.3	12	0.1	1.6 2	4.9 0.50
56	LINE L 22W	0.2 0.42	6. 9 34.0	<0.1	0.16 0	.06 0.17	43.5	3.2	14.0	11.3 1.43	3.3	1.3	25 0.04	22.0	2.2 0.10	200	1.03 0	0.035 0	0.18	14.5 6	578	8.4	3.9 <q.< th=""><th>02 0.1</th><th>6 0.3</th><th>0.2</th><th><0.1</th><th>5.0 <(</th><th>0.05 0.</th><th>04 (</th><th>0.4 0.007</th><th>0.04</th><th>0.4</th><th>16</th><th>0.1</th><th>1.5 3</th><th>3.0 0.52</th></q.<>	02 0.1	6 0.3	0.2	<0.1	5.0 <(0.05 0.	04 (0.4 0.007	0.04	0.4	16	0.1	1.5 3	3.0 0.52
57	LINE L 23W	<0.1 0.75	9.8 51.0	<0.1	0.16 0	0.08 0.15	43.1	5.4	27.5	15.2 2.76	4.3	2.4	30 0.04	21.5	7.2 0.25	331	1.07 0	0.036 (0.12	22.5 13	303 1	13.8	6.1 <0.	02 0.2	2 0.3	0.3	<0.1	6.0 <0	0.05 O.	02 (0.2 0.008	0.04	0.6	22	0.1	2.2 5	6.7 0.50
58	LINE L 24W	0.4 0.57	8.8 36.0 4 5 49.0	0.2	0.18 0	0.08 0.15	56.7 40 F	4.9	19.5	19.4 2.04	4.6	1.9	25 0.03	30.0	4.7 0.15	150	1.20 0	0.037 (0.36	19.0 «	418 1	11.8	6.6 <0.	02 0.1	8 0.8	0.3	0.1	7.0 <0	0.05 O.	02 3	3.2 0.020	0.06	0.6	24	0.1	3.9 4	3.6 0.87
60	LINE L 26W	0.7 1.64 2	0.4 102.0	0.5	0.16 0	0.08 0.46	68.9	24.3	49.5	63.3 3.67	4.5 5.8	2.5 3.5	40 0.10	25.0 36.5	19.3 0.41	1062	1.91 0	0.037 C	0.32	22.0 (52.0 (507 i 509 3	14.0 36.1 1	0.7 <0. 3.8 0.	02 0.1	0 0.9	0.a 0.6	0.1	9.5 <0	0.05 <0.	02 04 (0.5 0.009	0.06	0.6 3.2	24 30	0.2 1	2.3 5).9 9	3.2 0.50 9.5 0.58
61		06 069	77 046		0.00.0	1 0 07	46.0	71	14 0	210.202	4.1	2.0	25 A A6	00.0	10 0 10	100	4 40 0	000				nn c						/	ar a	~~ .							
62	LINE L 28W	0.7 1.30 1	7.7 94.3 2.6 107.0	0.2	0.20 0).14 0.67	40.2 56.9	22.9	24.0 33.5	51.6 3.26	4.1 5.7	2.0 3.2	35 0.06	30.0 41.5	11.4 0.24	430 2353	1.64 ()039 (0.14 . 0.16 ·	27.2 0 40.8 10	⊃roi ∠)346 4	∠3.5 47.5 1	9.0 0. 40 0.	02 0.2	2 0.2	0.3	0.2 1	5.5 <0 25 <0	1.05 U. 1.05 D	02 0 04 0	0.1 0.009	0.04	1.9 3.9	22	0.1 0	5.3 6 2 1 0	J.9 0.56 75 0.52
63	LINE L 29W	0.3 0.99 1	1.6 69.5	0.2	0.20 0	0.25 0.61	61.8	9.1	31.5	43.2 2.67	4.6	2.8	30 0.07	49.0	10.9 0.24	618	1.26 0	0.039 (0.18	44.0	741 2	22.4 1	0.1 0.	04 0.2	6 0.4	0.6	0.2 2	3.0 <0	0.05 0.	02 0	0.2 0.008	0.04	3.6	22	0.2 1	5.5 7	6.9 0.57
64	LINE L 30W	0.9 2.00 1	9.6 155.5	0.7	0.42 0	0.32 1.27	63.1	29.7	47.5	82.1 4.57	7.8	4.4	45 0.17	54.0	18.9 0.29	2174	2.26 0	0.043 (0.32	64.2 11	186 6	61.7 1	8.8 0.	04 0.3	8 1.0	0.7	0.3 2	4.5 <0	0.05 0,	06 (0.4 0.010	0.10	6.5	38	0.3 1	3.5 12	0.9 0.70
60		0.9 1.90 1	7.6 159.0	0.5	0.38 0	1.23 0.50	53.1	32.3	42.5	52.1 4.37	8.2	4.0	45 0.15	32.0	16.2 0.26	3381	2.13 0).042 (0.24	47.3 10	041 7	71.7 2	20.8 0.	04 0.3	0 0.6	0.5	0.4 2	20.0 <0	0.05 0.	04 (0.2 0.009	0.14	3.6	42	0.3 1	0.5 10	4.0 0.53
66	LINE L 32W	0.3 0.53	5.2 70.5	0.1	0.14 0	0.08 0.20	44.8	11.5	12.5	11.2 1.40	3.6	1.4	20 0.05	22.5	2.8 0.09	1265	0.66 0	0.037 (0.16	11.3 4	415 2	24.4	9.2 <0.	02 0.1	2 0.3	0.2	0.2	7.0 <0	0.05 <0.	02 0	0.3 0.014	0.06	0.4	16	0.1	2.1 3	5.5 0.44
67	LINE M 1W	0.3 1.28	9.3 87.5	0.1	0.22 0	0.13 0.17	47.0	7,7 3	38.5	20.5 2.21	5.2	2.0	30 0.11	24.5	10.5 0.33	372	1.38 0	0.041 (0.16	27.3 6	519 2	20.6 1	2.0 0.	02 0.1	4 0.4	0.3	0.2 1	3.5 <0	0.05 <0.	02 (0.2 0.005	0.08	1.9	24	0.3	3.5 7	1.1 0.51
69	LINE M 3W	0.4 0.73 1	0.6 56.0 9.4 62.5	0.1	0.14 0	0.24 0.24 0.08 0.50	53.4 42.5	4.8 6.5	∠4.≎ 25.0	10.5 2.20	4.7	2.1	30 0.04	27.0	69.022	187 584	1.35 0	0.039 (0.036 (0.16 3	22.3 4 22.9 8	470 1 562 1	11.0 16.1	5.0 <0. 67 0	02 0.10	8 0.3 4 n.4	0.3	0.1 1 20.1	75 -0	0.05 0. \As ∠0	02 (02 (0.2 0.006	0.06	0.5	22	0.1	2.2 6	3.4 0.51
70	LINE M 4W	0.1 1.26 2	0.9 80.5	0.4	0.16 0	0.06 0.34	63.5	13.9	37.0	42.4 3.30	4.3	3.1	30 0.10	31.5	12.7 0.40	519	1.53 0	0.038	0.18	54.7 8	587 2	26.3	6.6 <0.	02 0.5	2 1.9	0.6	<0.1	8.0 <0	0.05 0.	02 1	7.4 0.011	0.04	1.3	20	0.2	5.1 11	5.8 2.78
71	LINE M 5W	0.2 1.30 1	5.1 71.5	0.5	0.18 0	0.07 0.23	60.1	15.7	37.5	34.0 3.18	4.4	3.0	25 0.09	28.5	9.5 0.45	570	1.25 0	0.043 (0.24	45.7 6	304 2	26.6	7.3 <0,	02 0.3	4 1.6	0.5	0.1	6.5 <0	0.05 0.	04 9	5.1 0.011	0.06	1.0	22	0.3	3.6 9	7.8 1.30
72	LINE M 6W	<0.1 0.47	8.1 40.0	0.1	0.14 0	0.07 0.12	55.7	2.8	9.0	13.5 1.08	4.4	1.2	10 0.03	28.0	<0.1 0.06	63	1.17 0	0.038 0	0.20	11.4 2	265	7.2	6.2 <0.	02 0.1	4 0.3	0.3	0.2	5.0 <0	.05 0.	02 (0.3 0.008	0.06	0.4	22	0.2	1.8 3	7.5 0.44
73	LINE M 7W	0.3 1.11 1	0.8 98.5	0.3	0.24 0	0.10 0.12	50.5	18.1	29.5	23.0 2.17	5.0	2.1	40 0.09	26.0	8.7 0.23	640	1.07 0	0.040 (0.20	28.5 5	564 3	38.4 1	0.7 <0.	02 0.1	4 0.2	0.2	0.3	8.0 <0	.05 0.	02 (0.1 0.006	0.08	1.0	2 6	0.2 3	3.3 4	5.8 0.42
74	LINE M 9W	0.3 0.93 1	0.8 58.9 9.0 55.5	0.2	0.18 0	2.06 0.14	58.5 58.4	9.7 1	27.5	20.4 2.22	4.0 5.7	2.1	25 0.06	28.5	12.8 0.44	297	1.32 0	0.039 0 0.040 0	3.24 ; 3.42 ;	27.0 U 305 S	370 1 376 2	15.8 21.2 1	7.6 <0. 17 <0	02 0.2	0 0.6	0.3	0.1	6.0 <0 6.0 <0	0.05 0.0	02 (02 :	0.5 0.009	0.06	0.7	20	0.2 :	3.3 5	3.0 0.47
																			,						u	0.0	67. AL	0.0			1.1 0.010	0.00	0.0	20	0.1		3.3 0.00
76	LINE M 10W	0.2 0.94 1	3.1 52.0 3.1 30.0	<0.1	0.24 0	0.04 0.15	47.8	6.1	34.5	21.9 3.47	4.3	3.1	40 0.04	24.0	7.8 0.25	167	1.35 0	0.039 (0.38	26.0 9	902 1	14.3	6.4 <0.	02 0.2	2 1.2	0.4	0.1	3.5 <0	0.05 0.1	04	5.7 0.010	0.06	0.6	24	0.2 2	2.1 6	3.2 1.59
78	LINE M 12W	<0.1 0.53	2.1 30.0 9.2 49.5	<0.1	0.05 0	07 0.04	55.9 55.7	5.0	18.5	5.7 0.57 16.0 1.61	4.5 4.6	1.6	15 0.03	28.0 28.0	16 0 12	219	119.0	1039 C	שבע 128 י	5.1 1 177 1	192 377 1	4.2 10.8	2.3 <0. 4.0 >0	02 0.04 02 0.04	5 0.4 8 0.8	0.2	0.2	3.5 <0 4.5 ∠0	1.05 <0.1 1.05 - Au	02 (02 1	0.7 0.009	0.08	0.2	10	0.1	l.5 10 ⊧o 40	3.4 0.43 6 E 0.47
79	LINE M 13W	0.2 0.70	8.7 53.0	<0.1	0.16 0	.08 0.14	50.7	6.0	21.5	16.8 2.21	4.2	2.0	20 0.04	26.0	4.2 0.18	194	1.07 0	0.041 0	0.40	27.3 4	198 1	11.7	6.5 <0.	02 0.2	0.0	0.3	0.2	5.5 <0	.05 0.	04 a	4.4 0.016	0.06	0.5	20	0.1 2	2.0 5	3.6 0.91
80	LINE M 14W	0.6 1.05	7.9 96.0	0.4	0.22 0	.18 0.23	53.1	14.1	22.0	25.3 1.98	5.7	2.0	30 0.07	32.0	3.7 0.13	915	1.21 0).042 (0.30	22.8 8	572 3	33.1	8.6 <0.	02 0.2	0.7	0.3	0.3 1	3.0 <0	0.05 0.1	02 (0.3 0.014	0.08	1.1	28	0.2	5.0 5	3.2 0.44
81	LINE M 15W	0.6 0.94	9.1 103.5	0.3	0.24 0	.38 0.67	51.0	21.1	24.0	47.0 2.26	4.7	2.4	50 0.0B	40.0	6.0 0.17	1059	1.07 0	.043 0	0.24	40.6 F	966 3	38.3	9.5 O	04 0.2	2 0.4	0.4	0.2 2	4.0 <	05 0	04 (0.1.0.008	0.04	25	22	02 1	7 6	78 851
82	LINE M 16W	0.3 0.69 1	4.1 55.5	0.2	0.22 0	07 0.44	53.7	6.2 2	26.0	24.9 2.48	5.0	2.3	25 0.05	27.0	2.3 0,19	247	1.49 0	0.039 0	0.18	26.5 8	597 1	18.0	7.2 <0.	02 0.20	5 0.4	0.4	0.2	7.5 <0	.05 0.	04 (0.3 0.012	0.06	0.6	26	0.2 2	2.6 6	3.0 0.47
83	LINE M 17W	0.1 0.68	6.9 48.0	<0.1	0.18 0	08 0.16	62.3	3.8 2	22.5	10.4 1.88	5.0	1.9	20 0.04	31.0	1.6 0.17	125	0.79 0	.039 0	0.52	15.5 4	167 1	16.0	6.8 <0.	02 0.12	2 0.8	0.2	0.2	6.0 <0	.05 0.0	02 5	5.3 0.022	0.06	0.4	22	0.1 2	2.1 3	7.3 0.91
54 95	LINE M 18W	0.5 1.21 1	4.1 96.5 ว.4 หวะ	0.4	0.20 0	05 0.12	54.3 ⊿0 ≏	7,7 4 6 0 1	41.5	19.3 4.08	5.0 10	3.6 2.0	55 0.06	27.0 26 ⊑	10.5 0.34	315	1.51 0	0.041 0).38 ().4e (27.7 21	174 2	25.3	9.3 <0.	02 0.20	0 1.0	0.4	0.1	6.5 <0	05 0.0	04 2 04 7	2.0 0.011	0.06	0.6	28	0.7	2.4 6	3.2 0.50
00		0.0 1.01 1	a.n 40.0	0.2	U.10 U	.00 0.14	49.0	5.9 (06.U	21.0 0.47	4.3	3.0	00 0.04	24.3	a.U U.24	190	1.47 0	1.000 U	J.440 4	သေ၊ ရ	i Voq	11.4	a.r <0.	UZ U.ZI	5 1.2	0.4	U. I	ə.ə <q< th=""><th>.uo 0.0</th><th>94 5</th><th>5.1 0.012</th><th>0.06</th><th>0.6</th><th>22</th><th>0.2 2</th><th>£1 6∉</th><th>1.9 1.29</th></q<>	.uo 0.0	94 5	5.1 0.012	0.06	0.6	22	0.2 2	£1 6∉	1.9 1.29

ICP CERTIFICATE OF ANALYSIS AK 2011-0996

William Timmins

		Ag Al	As Ba	i Be	e Bi	Ça	Cđ	Çe	Co (Cr C	u Fe	Ga	Gel	ng K	La	Li Mg	Mn 1	Mo	Na Nb	N	Р	РЬ	Rb	5 9	SÞ SA	: Se	Sn	Sr	Ta	Te	Th	Π	<u>п</u> 1	י ט	V VI	Y Y	Zn	. Zr
Et #.	Tag #	ppm %	pom pon	n ppn	п рргп	% F	ppm p	opm p	pom po	om pp	m %	ppm g	opm p	pb %	ppm	ppm %	ppm p	i max	% рот	1 ppm	ppm	ppm	ppm	% p	pm pp	n ppm	ppm	ppm	opm :	ppm p	opm -	% F	opm pr	pm pp	ag me	in ppr	n ppr	m pom
26	LINE M 2016/	0.6 1.01	122 62	5 0	2 0 16	0.07	0.14	64.9	66 2	26 1	01 2 22	4.0	20	50 0.04		06002	222	1 20 0	040 0 40	1 72 7	1201	10.0	77.	0.02 /	1.24		1 1 C	6 O 3	-0.05	0.04	4 5 0	012 /		0.6	22	<u> </u>	0 60	0 0 7/
00		0.0 1.01	16.0 00		4 0.10	0.07	0.14	-4.0	0.0 0	0.J N	5.1 5.55	4.0	3.0	30 0.04	27.0	0.0 0.23	322	1.20 0.	040 0.40	5 23.1	1001	19.9	1.2 *	0.02 0).24 (.9 0.4	. 0.1	0.0	.0.03	0.04	4.5 0	1.012 (1.00	0.0	~~ ~	1.4. <u>2</u> .	Z 28	9 0.70
87	EINE M 21W	0.4 0.94	14.4 50	.5 <0.	.1 0.24	0.11	0.13	51.4	6.1 3	8.5 0	6.9 3.62	4./	3.3	30 0.05	26.0	6.7 0.31	302	1.13-0.	038 0.44	J 25.0	3373	21.3	0.8 <	0.02 (0.20	.0 0.4	0.1	7.5	0.05	0.04	2.3 0	0.014 (0.04	0.6	36 0	12 2	5 57.	.4 0.5/
88	LINE M 22W	0.3 0.46	5.9 34	.5 <0.	.1 0.14	0.02	0.14	48.9	5.4 1	4.0 tř	7.2 1.52	4.0	1.5	25 0.03	24.5	1.8 0.10	366 (0.89 0.	039 0.24	4 14.9	382	9.2	4.8 <	:0.02 (0.18 0	.5 0.4	0.2	3.0 •	:0.05	0.02	0.8 0	0.020 (0.06 /	0.5	18 0	2.1 1.	9 42.	.6 0.50
89	LINE M 23W	0.4 0.94	9.5 88	0 0.	.2 0.22	0.11	0.25	49.9	14.3 2	8.5 2	7.0 2.49	5.5	2.3	40 0.07	25.5	5.3 0.19	1008	1.21 0.	041 0.16	5 27.4	708	31.0	9.3 <	0.02 ().20 0	.4 0.3	0.3	9.0 •	<0.05	0.02	0.2 0	0.011 (0.06	0.9	28 0	1.1 - 2.	8 62.	.0 0.45
90	LINE M 24W	06 085	10.3 56	5 0.	2 0 18	0.04	0.25	58.4	59.2	70 1	90 2 63	43	2.5	55 0.04	28 Ö	67.023	394 (0.98.0	039 - 0.36	6 21 2	829	19.9	60 .	0.02	124 r	9 03	02	45 .	:0.05	0.02	26.0	014 (0 A4	0.6	20 0	12 2	4 59	0 0 60
20		0.0 0.00	10.0 00			0.04	0.20	00.7	0 .0 L	r.	0.0 L.00	H.U	c	00 0.04	20.0	0.7 0.20	004	0.00 0.	000 0.0		ULU	10.0	0.0 1	0.02 (<i></i>		0.2	T.D	0.00	0.04	2.0 0		J.04	0.0	20 0		- 30,	3 0.0.
<u>.</u>																																						
91	LINE M 25W	0.6 0.95	10.7 90	.0 0.	.3 0.18	0.15	0.41	53.Z	20.2 2	5.0 3	3.9 2.44	3.8	2.3	25 0.05	29.0	8.4 0.24	958	1.09 0.	039 0.18	5 36.2	606	20.5	6.8 <	:0.02 0	0.30 0	.6 0.4	0.1	9.5	<0.05	0.02	0.3 0).009 (0.04	1.5	16 C).2 9	.3 71.	.0 0.42
92	LINE M 26W	0.2 0.77	10.3 55	.5 0.	.1 0.18	0.05	0.17	56.0	4.1 2	1.5 1	2.7 2.15	4.4	2.0	25 0.04	28.5	2.6 0.20	129	0.82 0.4	038 0.3	2 16.4	508	13.7	4.9 <	(0.02 (0.14 C	.7 0.3	0.2	5.0	<0.05 -	<0.02	1.6 0	0.012 (0.04	0.5	20 0).2 2.	7 39.	.4 0.49
93	LINE M 27W	0.6 0.90	10.0 45	.5 0.	.1 0.22	0.06	0.27	54.7	4.8 2	7.5 1	4.9 3.08	5.4	2.9	35 0.03	27.5	5.9 0.23	176	1.01 0.	036 0.60	0 18.9	540	17.4	6.6 <	<0.02 ().14 C	.9 0.3	0.2	6.0 ·	<0.05	0.04	2.8 C).022 (0.04	0.5	32 0).2 2	4 43.	.5 0.76
94	LINE M 28W	07101	118 74	0 0	2 0 18	0.11	0.25	54.3	67 2	90 1	97 3 25	41	3.0	35 0.04	27.5	11.3 0.28	268	1.01.0	037 0.3	6 24 5	1085	15.3	87 .	0.02 0	1 20 1	0 04	0.1	70.	-0.05	0.04	520	1010	0.04	0.6	20 0	12 2	7 68	7 0.9
05	LINE M 20M	02 0 99	104 57	5 -0	1 0 20	0.02	0.14	52.4	57 2	60 1	1 2 2 70	4.0	26	35 0.05	26.6	4.2 0.24	450	1 12 0	027 04	6 16 2	001	16.0	0.7	.0.02 0	16 0	0 0.0	0.1	4.0	.0.00	0.00	260	0.010	0.00	0.0	20 0	<u>, , , , , , , , , , , , , , , , , , , </u>	0 44	3 0.9
		0.2 0.00	12.4 02		.1 0.20	0.00	0.14	52.7	3.1 2	0.0 1	1.0 2.73	4.3	£	33 0.05	20.0	4.2 0.24	400		0.41	Q 10.0	201	10.0	3.4	0.02 (<i>.</i>	.9 0.0	0.2	4.0 -	.0.03	0.02	5.5 0	0.010	0.00	0.4	20 0	<i>1.</i>	.0 44.	.5 0.00
90	LINE M 30W	0.4 0.94	8.9 79	.0 <0.	.1 0.18	0.06	0.34	50.0	9.3 2	4.5 1	7.4 2.93	5.2	2.7	30 0.05	26.5	5.0 0.21	656	0.90 0.	039 0.3	8 20.9	923	17.6	10.3	:0.02 ().18 C	9 0.3	0.2	6.0	<0.05	<0.02	1.5 0	0.017 (J.06	0.6	26 C	0.2 3	1 52	.2 0.4
97	LINE N 1W	0.3 0.94	13.0 44	.5 0.	.3 0.18	0.06	0.20	47.3	7.7 3	4.0 2	1.2 2.72	3.6	2.5	20 0.05	24.0	7.7 0.36	300	1.37 0.	039 0.10	6 29.2	491	17.1	5.2 <	-0.02 ().26 (.7 0.4	<0.1	5.5	-0.05	<0.02	0.8 0	0.010 (0.04	0.9	16 0).2 3.	5 72.	.7 0.54
98	LINE N 2W	0.3 0.51	6.0 88	0 <0.	.1 0.16	0.07	0.20	47.5	3.2 1	9.5 1:	2.3 0.94	3.6	1.1	20 0.04	25.0	<0.1 0.09	143 (0.85 0.	038 0.14	4 12.9	310	11,1	4.8 <	0.02 (0.12 0	.1 0.2	2 0.2	6.5	<0.05	<0.02	<0.1 0	0.006 (0.06	0.4	18 0).2 2	7 29.	.0 0.47
99	LINE N 3W	04 100	8.0 113	0 <0	1 0.16	0.05	0.44	56.0	112 3	05 2	06 189	<u> </u>	10.	25 0.07	29.0	59026	549	1.03.0	039 0.20	0 22 0	574	19.0	91 -	0.02 (114 E	7 0.2	02	65.	0.05	0.02	070	n oo a li	0.04	0.7	20 0	14 5	8 57	1 01
100		0.2 0.50	88 60	ις η.	2 0 14	0.05	0.01	69.6	40.4	70 1	7 5 1 01	37	4.4	20 0.04	22.0	-0.1 0.11	100	non n	000 0.1	0 100	270	16.7	73	-0.02 /	0.16 C	n 0.0	, 0.2 , 0.3	6.0 6.0	-0.05	-0.02	0.7 0	1000 ·	0.04	0.0	10 0		4 00	
100	LINE IN HAA	0.3 0.59	0.0 50	.5 0.	. <u>2</u> (7.14	0.05	0.21	56.5	4.2 (7.0	LO LOI	9.7	0.4	20 0.04	04.0	<0.1 0.11	122	0.09 0.	039 0.1	a 10.0	3/9	10,7	1.3 <	0.02 (J. 16 (.2 0.0	0.2	0.0	<0.05	<0.02	0.2 0	1.000 1	0.04	0.0	10 0	J. I J.	.4 .38.	.3 0,44
101	LINE N 5W	0.6 1.50	17.3 95	.5 0.	.3 0.26	0.21	0.35	62.0	16.3 4	5.0 4	5.8 3.41	5.0	3.3	30 0.11	37.0	13.8 0.37	751	1.81 0.	045 0.2	0 52.4	703	31.3	10.0	0.02 (0.32 (.8 0.6	i 0.2	15.0	<0.05	0.04	0.4 0	0.008 (0.08	3.5	26 ().2 8.	.2 97.	.8 0.53
102	LINE N 6W	0.9 2.85	25.7 219	0.0	.9 0.50	0.15	0.73	90.7	22.6 5	7.5 9	2.5 4.83	8.5	4.7	80 0.21	56.5	23.4 0.35	836	2.64 0.	046 0.4;	2 94.4	957	59.1	16.4	0.02 (0.36 1	.5 1.0	0.4	15.5	<0.05	0.06	1.1 0	0.010	0.12	7.7	42 0	0.4 16	7 153.	.5 1.06
103	LINE N 7W	04 091	11.3 65	5 0	2 0 18	0.07	0.19	55.7	82 2	7.5 1	7.6.2.50	42	2.4	25.0.06	28.0	4.7 0.25	384	1.09.0	041 0.2	2 24.1	552	22.4	80 <	0.02 (1.20 0	6 03	0.1	70	-0.05	0.02	07.0	1.009	0.04	0.6	20 0	12 2	5 66	9 0.5
104	LINE N 8W	07 219	20 7 120		6 0 36	0.20	0.21 1	00.0	A1 9 A	00 6	07 4 20	67	12	65 0 14	47.0	20.2 0.29	1076	104 0	042 0 2	6 64 0	1165	52.0	101		120 0	e 0.1	0.1	106	-0.05	0.04	040	1007	0.10	3.3	20 0	10 15	0 105	- 0.5L
10-4		0.7 2.10	40.7 100		.0 0.00	0.00	0.01	03.0	41.0 4	3.0 G		0.7	4.5	03 0.14	47.0	20.3 0.30	1270	1.54 0.	040 0.2	0 04.9	1100	00.9	10.1	0.00 0		.0 0.7	0.2	19.0	0.00	0.04	0.4 0	1.007	0.10	3.3	30 0	J.Z 15.	.2 105.	.1 0.54
105	LINE N AAA	0.5 0.98	12.5 62	.u U.	.4 0.10	0.13	0.22	57.8	11.3 3	5.0 Z	7.0 2.59	3.9	2.5	40 0.05	29.5	8.6 0.31	420	1.21 0.	039 0.2	0 34.6	629	22.8	6.3 <	:0.02 (J.28 (.7 0.4	÷ 0.1	8.0	<0.05	0.02	0.9 0	1.009	0.04	1.3	18 C).2 3	.8 71.	.7 0.50
106	LINE N 10W	0.4 1.13	16.8 103	.0 <0.	.1 0.26	0.23	0.31	44. 9	11.2 3	3.0 2	9.0 3.59	5. 6	3.6	35 0.09	22.5	7.5 0.23	541	1.78 0.	041 0.4	0 35.0	749	37.4	7.7	0.02 (0.28 (.8 0.4	0.3	11.5	<0.05	0.04	0.9 0	0.013 (0.06	0.7	32 0).2 2	1 81.	.6 0.81
107	LINE N 11W	0.2 0.41	6.1 24	.5 <0.	.1 0.08	0.07	0.09	39.9	2.9	7.0 1	1.3 0.93	3.6	1.0	15 0.03	20.0	0.3 0.04	60	1.15 0.	037 0.1	6 9.9	255	4.6	2.5 •	<0.02 (0.30 (.2 0.2	2 0.2	4.5	<0.05	<0.02	0.1 0	0.005	0.04	0.3	18 0	0.1 1	4 29.	.1 0.53
108	LINE N 12W	<0.1 0.50	4.9 20	.5 <û	1 0.10	0.09	0.08	50.4	35 2	8.0	96 0 97	47	12	10.0.03	25.0	12017	93.4	0.65.0	038 0.2	0 14.1	183	4.3	45 -	-0.02 0	112 0	7 03	0.2	50.	0.05	-0.02	110		0.06	03	26 0	12 1	A 54	3 0.6
100	LINE N 19M	0.0 1.00	15 7 80		2 0 10	0.00	0.00	60.4 60.6	110 0	70 1	1 1 0 07	10	2.0	00 0.00	00.0	16.6 0.00	070	104 0		0 40.0	200	00.0		.0.02 /	200 H	- 0.	. 0.2	0.0	0.00	0.02			0.00	1.0	20 0			0.52
103		0.2 1.30	10.7 69		.0 0.10	0.13	0.20	03.0	14.2 0	4 5 9	1.1 2.97	4.0	0.0	25 0.07	20.0	10.0 0.36	079	1.24 0.	040 0.3	0 40.0	020	20.0	7.4 <	0.02 0	J.20 I	.5 0.5	0.3	9.0 -	<0.05	0.02	5.1 0	5.012	0.06	1.3	24 (0.2 0.	. 1 / 5.	.3 1.00
110	LINE N 14W	0.6 0.74	4.1 50	0 <q.< th=""><th>.1 0.14</th><th>0.28</th><th>0.28</th><th>50.3</th><th>8.2 2</th><th>1.5 2</th><th>7.9 1.23</th><th>4.6</th><th>1.5</th><th>25 0.06</th><th>28.5</th><th>2.7 0.12</th><th>468</th><th>0.68 0.</th><th>042 0.3</th><th>0 14.9</th><th>368</th><th>22.0</th><th>5.8 <</th><th><0.02 (</th><th>0.10 C</th><th>.6 0.2</th><th>2 0.3</th><th>15.5</th><th><0.05</th><th>0.02</th><th>0.3 0</th><th>0.010</th><th>0.06</th><th>1.2</th><th>22 (</th><th>0.1 3</th><th>.4 39.</th><th>.8 0.60</th></q.<>	.1 0.14	0.28	0.28	50.3	8.2 2	1.5 2	7.9 1.23	4.6	1.5	25 0.06	28.5	2.7 0.12	468	0.68 0.	042 0.3	0 14.9	368	22.0	5.8 <	<0.02 (0.10 C	.6 0.2	2 0.3	15.5	<0.05	0.02	0.3 0	0.010	0.06	1.2	22 (0.1 3	.4 39.	.8 0.60
111	LINE N 15W	0.4 0.90	11.9 58	l.S <0,	,1 0.18	0.09	0.16	54.0	5.8 2	6.0 1	8.0 2.63	4.9	2.6	35 0.05	27.0	4.3 0.18	225	1.11 0.	040 0.3	8 19.5	1350	14.8	7.2 <	<0.02 (0.18 (.8 0.3	0.3	5.5	<0.05	0.04	1.8 0	0.011	0.06	0.5	28 0).1 2	2 51.	.4 0.64
112	LINE N 16W	0.3 0.96	12.3 55	.0 <0.	.1 0.20	0.13	0.14	57.3	6.9 4	1.0 1	8.6 2.99	4.8	2.9	35 0.06	28.5	6.8 0.32	243	1.15 0.	041 0.4	4 29.9	1308	15.6	5.1 <	:0.02 (0.24 1	2 0.4	0.2	65	<0.05	0.02	490	0.014	0.06	0.6	28 (1 2	4 63	9 0 9
113	LINE N 17W	02.060	29 50	5 20	1 0 10	0.19	0.08	49.6	16	75	69.058	5.0	0.8	25 0.03	24.5	0.5.0.05	121 0	0.46.0	030 0.2	2 56	101	40	30 -	-0.02 0	106 (9 03	0.3	60.	-0.05	~0.02	040	007	0.08	0.3	16 -0	1 1	7 20	3 0 4
114		04069	EE 20		0 010	0.07	0.07	6E 0	0.0 4	сс +	1 2 1 00	5.0	4 E	15 0.04	00 E	0.0 0.00	100			e 110	070	7.0	5.0 1	-0.02 (0.00 C	0.0		r.o.	.0.05	-0.00	0.4 0		0.00	0.0	00 10		., 20.	.0 0.47
145		0.4 0.00	10.0 177		.2 0.10	0.07	0.07	00.0		0.0 1	1.0 1.20	0.9	1.5	13 0.04	32.0		120	0.00 0.		0 11.0	372	1.0	3.9 <		J.14 (.a 0.0	0.3	3.0 4	<0.05	<0.02	0.4 0	1.009	0.00	0.4	20 <0		.3 20.	.1 0.53
115	LINE N 1999	0.8 2.20	18.0 177	.0 1.	.1 0.36	0.23	0.55 1	49.4 1	150.7 4	9.0 7	5.5 3.69	8.0	4.5	60 0.12	68.5	31.9 0.40	6849	1.90 0.	045 0.3	0 79.4	778	81.8	19.2	0.04 (0.30 1	3.0 0.8	0.4	17.5	<0.05	0.06	0.3 0	J.014 (0.16	3.2	40 0	0.2 22	5 94.	.5 0.5
116	LINE N 20W	0.2 0.49	1.7 26	.5 <0.	.1 0.08	0.09	0.06	58.6	1.2	8.0	3.4 0.31	5.3	0.6	10 0.03	29.5	0.4 0.04	59	0.23 0.	040 0.1	6 3.7	143	5.1	3.8 <	<0.02 (0.04 (.2 0.2	2 0.3	5.0	<0.05 -	<0.02	<0.1 0	0.009 (0.08	0.2	10 <0	2.1 1.	8 10.	.4 0.42
117	LINE N 21W	0.1 0.63	5.6 25	.5 0.	.1 0.14	0.06	0.04	58.4	2.8 1	3.5	9.9 1.08	5.2	1.2	20 0.04	28.5	2.6 0.12	159	0.72 0.	038 0.2	6 10.2	332	7.7	5.6 <	<0.02 (0.10 0	.5 0.2	2 0.3	4.5	<0.05	<0.02	0.8 0	0.014	0.06	0.4	22 0	0.1 2	1 23.	.6 0.56
118	LINE N 22W	0.7 0.89	10.9 45	0 0	2 0 18	0.03	0.16	55.3	64 2	15 1	65 2 47	45	25	40 0.05	27.5	75020	193	1.09.0	041 0.4	0 186	821	15.3	72 4	0.02 (n 16 - C	8 04	02	40	0.05	0.04	35.0	1011	0.06	0.6	20 0	1 2	2 47	4 07
119	LINE N 23W	0.3.074	47 46	0 -0	1 0 12	0.08	0.10	60.3	30.1	60	83155	5.2	17	25 0.04	30.0	34 0 14	113	0.50 0	037 0.2	8 10.2	762	9.0	18 -	0.02 0	108 0	κ ή:	0.3	55.	-0.05	~0.02	18.0		0.06	0.4	16 -4	1 2	1 06	0 0.67
100		0.0 0.14	10.7 97	E 0	0.10	0.00	0.10	60.0 60.6	16 4 3	0.0	0.0 1.00 0.E 0.00	3.0	0.0	15 0.04	20.0	10.4 0.14	577	0.38 U. 0.06 O.	007 0.2	0 10.2	640	20.0	4.0	0.02 0		.J 0.2	. 0.0	3.3	.0.05	0.02			0.00	1.0			- 20.	2 0.01
120	LINE IN 2444	0.1 1.10	10.7 57	.a 0.	.2 0.10	0.12	0.52	09.0	10.4 5	2.0 Ş	0.0 2.00	4.0	2.9	10 0.00	39.0	12.4 0.50	577	0.90 0.	041 0.2	ο 4 <i>μ</i> .4	012	20.5	4.0 <	(U.UZ (J.20 (.0 0.5	0.2	7.5 -	0.03	0.02	0.9 0	J.Q20 N	0.04	1.0	20 0	J. 1 4.	.5 08.	.8 1.97
				_																																		
121	LINE N 25W	0.3 1.12	12.5 46	.5 0.	.1 0.18	0.24	0.44	57.5	15.3 3	0.0 3	7.0 3.07	3.9	3.2	35 0.07	29.5	11.2 0.50	607	1.11 0.	043 0.5	0 41.4	744	19.0	4.4	0.02 (0.32 1	.4 0.5	6 0.2	12.0	<0.05	0.04	3.6 0	0.027 (0.04	1.1	20 0).1 5.	.5 78.	.2 0.88
122	LINE O 1W	1.7 0.92	9.9 114	.0 0.	.2 0.16	0.10	1.38	43.0	12.1 2	1.5 2	8.6 2.02	3.8	2.1	70 0.07	22.5	3.9 0.21	1657	1.19 0.	045 0.10	6 26.6	789	37.3	6.7	0.04 (0.30 0	.3 0.4	0.2	9.0	<0.05	0.02	0.2 0	0.006 (0.06	0.9	18 0	0.2 8	2 63.	.0 0.48
123	LINE O 2W	0.7 1.07	8.6 78	0.0	.2 0.18	0.03	0.30	51.5	7.3 2	3.5 2	3.9 2.23	4.3	2.3	40 0.07	27.0	6.0 0.27	245	1.24 0.	038 0.2	0 22.6	668	18.5	10.0 <	0.02 (0.18 0	4 0.4	02	45	c0 05	0.02	020	007 (0.06	0.9	18 0	12 5	6 56	9 0.50
124	LINE O 3W	09123	13.6 105	0 0	1 0 24	0.11	0.48	49.7	103.3	75 3	84286	4.0	27	45 0 11	35.0	63.031	556	1.62.0	038 0.2	0 322	702	27.6	0.2	0.02 (1.22 0	A 0.2	0.2	11.0	0.05	0.04	0.1 0	1007 0	0.00	0.0	24 0	10 7	6 60	0 0.00
105		0.5 1.20	10.0 100			0.10	0.00 4	107.0	170 4	n		- T. G	2.7	-0.0.10	00.0	14.5 0.00	007	1.02. 0.		0 00.0	7770	00.0	0.0 1			.4 0	. 0.2	0.5	0.03	0.04	0.1 0		0.00	e.r	24 0		.0 09.	2 0.48
120		Q.0 1.04	15.2 109	ι φ . ψ.	.4 0.24	Q. 10	Q.∠Q I	07.0	17.0 4	ပ္.၁ န	8.0 3.23	3 . i	3.4	50 0.10	30.0	14.0 0.00	037	1.49 0.	040 0.2.	2 30.5	116	32.0	9.3	0.02 (J.28 (.8 0.8	0.2	9.5	(0.05	Ų.04	0.4 C	006 (J.08 - 4	4.Ų	24 (13 9	.5 97.	.1 0.64
126	LINE O 5W	0.9 0.61	8.6 59	LQ 0,	.2 0.14	0.10	0.54	42.5	6.0 2	0.5 11	9.7 1.78	3.2	1.8	30 0.04	24.5	0.2 0.20	257	1.14 0.	038 0.1	6 21.4	460	14.5	4.8 <	:0.02 (0.24 (.5 0.4	0.1	8.0	<0.05	0.02	0.4 0	008 (0.04	0.7	14 (),1 4.	.0 54.	.7 0.48
127	LINE O 6W	0.9 0.85	7.9 76	.5 0.	.3 0.20	0.09	0.36	42.9	13.4 2	1.5 2	0.8 1.93	4.5	1.9	40 0.06	22.5	<0.1 0.14	969	1.14 0.	038 0.2	2 21.7	649	34.4	9.6 <	:0.02 ().20 (.5 0.3	0.3	6.5	<0.05	<0.02	0.2 0	0.012 (0.06	1.1	22 0).2 3.	2 53.	.9 0.47
128	LINE O 7W	10.0.77	6.8 62	.5 <0.	.1 0.18	0.05	0.29	43.4	15.4 2	05 1	42194	4.7	1.8	40 0.05	21.5	<01013	1305	1 15 0	038 0.2	8 16.0	685	36.0	10.5 <	0.02 (118 (6 02	0.3	55	0.05	<0.02	04.0	016 (0.08	0.6	22 (11 1	8 46	0 041
100		0.2.0.90	160 57	0 0	2 0 20	0.19	0.19	52.1	80.2	45 3	0.2.2.16	10	20	25 0.05	26.0	4 2 0 22	246	1 5 1 0	020 0.2	4 20.7	1510	00.0	70	.0.02 (<u> </u>	, 0,1	10.0	-0.0E	0.04	0.7 0	017	0.04	0.7	24		r 70.	7 0.47
123		0.2 0.05	10.5 37		.2 0.20	0.10	0.10	52.1	0.8 3	4.0 2	0.2 3.10	4.5	2.5	30 0.05	20.0	4.5 0.52	2-10	1.31 0.		4 20.7	1012	23.0	7.0 <	0.02 (J.32 I	.0 0.7	0.1	10.0 4	0.05	0.04	2.7 0	.017	5.04 4	0.7	34 C		5 73.	.7 0.56
130	LINE O 9W	0.5 0.67	10.0 47	.5 <0,	, 0.14	0.09	U.17	51.1	4.7 1	9.5 1:	5.4 1.83	4.Z	1.9	40 0.05	25.5	0.6 0.13	135	1.21 0.	039 0.3	2 16.0	660	14.2	5.1 <	<0.02 (J.22 C	.7 0.3	0.3	7.0 •	<0.05	0.02	2.9 0	1.012 (J.06 /	0.5	22 (0.2 1.	.8 39.	.1 0.70
131	LINE O 10W	0.5 1.31	12.5 50	.0 0.	.3 0.18	0.10	0.22	57.5	9.9 3	4.5 2	4.2 2.74	4.3	2.7	50 0.07	27.5	9.8 0.31	316	1.25 0.	041 0.3	6 36.3	1136	19.9	7.5 <	:0.02 (0.30 1	.1 0.4	0.2	6.5	<0.05	0.02	4.6 0	0.011 (0.06	0.8	20 0).1 3.	1 77.	.8 0.93
132	LINE O 11W	0.2 0.75	7.2 41	.0 <0.	.1 0.12	0.08	0.06	53.0	1.8 1	0.0	5.3 0.79	6.8	1.0	10 0.03	26.5	<0.1 0.06	51 0	0.54 0.	035 0.2	8 6.2	300	5.6	3.3 <	:0.02 (0.08	3 02	0.4	5.5	0.05	<0.02	0.2 0).007	0.08	0.2	20 0),1 1	5 20	1 0 4/
133	LINE O 12W	12100	11.6 120	5 n	7 0.32	0.41	0.35	63.8	35.8 2	05 A	13 250	70	28	45 0 10	39.5	156 0 24	1049	1 13 0	643 6 4	R 417	805	75.4	14.4	0.02 0	14 C	8 07	0.5	220	0.05	0.02	04.0	010 0	0.09	25	20 0	11 0	5 00	1 0.40
4714		33 464	21 4 104		л осо	0.70	0.00	16.0	617 5	16 7	20 200	7.0	47	105 0.10	60.0 66 m	34.0.0.24	1620	1.04 0	044 0.94	u ⇒1.0. ⊏ 1011 -	1000	FO 1	14.0	0.04	2.17 C			00.0	.0.07	0.02	0.40		7.00 / 0.40	£.0	02 1	, i 31.		4 7.46
1.34		2.3 2.59	21.4 104		0.50	0.70	0.83 1	10.3	01.7 5	1.3 /	J.9 J.90	1.2	4.7	100 0.10	00.0	24.9 0.34	1040	1.344 0.	044 0.3	0 123.1	1099	09.1	14.3	0.10 0	1.310 1	0 1.3	0.3	39.0	<u.u5< th=""><th>0.06</th><th>0.5 0</th><th>1.00/ 0</th><th>J.1U !</th><th>5.8</th><th>32 0</th><th>12 34</th><th>.0 133.</th><th>.4 0.87</th></u.u5<>	0.06	0.5 0	1.00/ 0	J.1U !	5.8	32 0	12 34	.0 133.	.4 0.87
135	LINE O 14W	0.5 1.05	11.4 91	.5 Q.	.3 0.22	0.24	0.30	60.3	13.2 2	9.5 3	2.5 2.39	4.7	2.5	45 0.06	33.0	6.8 0.24	468	1.20 0.	040 0.3	2 34.3	431	26.9	7.5	0.02 (3.20 C	.7 0.4	0.2	17.0 -	<0.05	0.04	0.8 0	0.009 (J.06	1.5	22 Ç	0.1 6.	3 60.	.4 0.55

ICP CERTIFICATE OF ANALYSIS AK 2011-0996

William Timmins

		Ag Al	Ás	Ba	Be	Bi	Ċa	Cd	Сө	Co	Cr	Cu Fe	Ga	Ge	Hg H	(La	i L	.i Mg	Mn	Mo	Na	Nb	NE	P	Pb	Rb	s	Sb	Sc	Se :	Sn S	Sr 1	ġ.	Te	Th	п	TI	U	v	w	Y	Zn	Zr
Ët #.	Tag #	ppm %	ppm	ppm	ppm	ppm	% j	րա հ	ppm	ppm	ppm	ppm %	ppm	ppm	ррб 🤊	6 рр	n pp	<u>m %</u>	ppm	ppm	%	ppm	ppm	ppm	ppm	ррт	%	opm	ppm p	pm p	pm p	om p	in p	pm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm
136	LINE O 15W	2.8 2.36	3 18.1	103.0	1.4	0.40	0.34	0.62 1	07.5	78.7	44.5	97.7 3.8	3 6.4	4.6	145 0.	11 74	.0 10	5.3 0.28	3122	2.31	0.042	0.36	75.7	1114	136.7	12.8	0.06	0.46	1.1	1.3	0.3 2	0.5 <0	.05	0.04	0.6 0	800.0	0.14	6.8	24	0.2	39.3	81.0	0.61
137	LINE O 16W	2.3 2.04	17.0	127.0	1.1	0.38	0.42	0.81 1	10.8	64.9	43.5	102.1 3.6	7 7.1	4.5	80-0.	12 91	.5 14	1.1 0.32	2910	2.04	0.044	0.32	81.4	1015	99.3	14.6	0.06	0.36	1,1	1.2	0.3 2	6.0 <0	05	0.04	0.5 0	3.008	0.08	5.8	28	0.2	41.4	96.4	0.63
138	LINE O 17W	0.7 0.70	8.2	57.0	≪0.1	0.14	0.17	0.13	57.9	4.2	17.5	15.1 1.6	3 4.8	1.8	40_0/	04 29	.o 2	2.0 0.14	160	0.88	0.040	0.22	14.3	518	8.4	5.7	<0.02	0.14	0.4	0.3	0.2	9.5 <0	.05	0.04	0.4 (0.005	0.06	0.4	20	0.1	2.1	38.1	0.51
139	LINE O 18W	0.3 1.4	13.2	55.5	0.3	0.20	0.10	0.17	64.3	9.2	40.5	25.4 3.9	8 5.4	3.9	40 0.1	05 32	.5 14	4.0 0.48	3 500	1.08	0.038	0.38	32.9	635	15.5	8.2	0.02	0.22	1.2	0.4	0.1	6.5 <0	.05 <	0.02	4.8 (0.010	0.04	0.7	22	0.1	3.1	72.5	0.89

OC DATA: Repeat:

LINE K 1W 0.3 0.99 11.8 70.0 0.1 0.20 0.15 0.19 49.4 9.6 34.0 18.6 2.49 4.4 2.3 15 0.07 28.0 10.1 0.32 436 1.55 0.042 0.18 21.4 327 29.5 9.0 <0.02 0.10 0.5 0.3 0.1 12.5 <0.05 0.02 0.4 0.007 0.04 1.2 24 0.3 4.6 50.0 0.58 1 317 1.49 0.039 0.32 30.3 1154 23.3 6.8 0.02 0.30 1.0 0.5 <0.1 6.5 <0.05 0.04 4.0 0.011 0.06 0.8 18 3.3 74.5 0.75 10 LINE K 10W 0.2 1.07 13.3 40.0 0.2 0.18 0.07 0.26 47.4 8.2 31.5 26.5 3.40 3.9 3.2 50 0.04 24.0 12.8 0.35 0.1 1.1 20 0.03 24.0 1.1 0.08 1145 0.84 0.041 0.08 13.8 4.9 <0.02 0.10 0.2 0.2 0.2 7.5 <0.05 <0.02 5.7 13.0 11.6 1.10 3.8 9.7 336 0.2 0.012 0.10 0.5 16 < 0.1 2.4 32.8 0.49 19 LINE K 19W 1.0 0.48 3.0 66.0 <0.1 0.10 0.07 0.32 47.9 28 LINE K 28W 0.7 1.97 19.2 129.0 0.6 0.28 0.28 0.73 111.7 21.6 52.5 72.7 3.81 6.3 3.9 45 0.13 51.5 31.7 0.43 860 1.44 0.042 0.32 86.1 596 37.2 13.0 0.02 0.28 1.5 0.7 0.2 21.0 <0.05 0.04 1.0 0.014 0.08 6.1 34 0.2 16.0 113.3 0.63 5.2 2.2 25 0.10 26.5 15.5 0.34 679 1.10 0.042 0.18 25.8 664 21.1 11.9 0.02 0.12 0.4 0.3 0.2 19.0 <0.05 0.02 0.2 0.007 0.06 36 LINE L 2W 0.3 1.22 8.7 84.0 0.3 0.26 0.24 0.33 48.7 12.0 33.5 20.6 2.27 2.0 24 0.2 5.4 62.1 0.52 2.6 35 0.05 27.0 6.6 0.18 151 1.45 0.040 0.46 17.7 674 15.3 7.9 0.02 0.18 0.3 0.2 7.0 <0.05 2.3 0.015 0.06 45 LINEL 11W 0.2 0.95 10.3 45.0 0.3 0.16 0.05 0.16 50.8 4.6 26.0 15.9 3.00 5.0 0.9 0.02 0.626 0.2 3.0 48.5 0.81 54 6.8 4.3 90 0.13 52.5 21.1 0.36 1306 2.18 0.042 0.24 62.6 1246 62.4 13.0 0.08 0.30 0.7 0.8 0.2 23.5 <0.05 0.04 0.6 0.006 0.10 32 0.2 17.5 108.2 0.66 LINE L 20W 0.8 2.15 20.8 122.0 0.8 0.38 0.31 0.34 116.3 42.5 51.0 59.4 4.30 4.1 63 LINE L 29W 0.4 1.06 11.7 73.5 0.5 0.22 0.27 0.62 66.5 9.5 32.0 45.2 2.76 4.8 3.0 30 0.07 52.5 10.5 0.25 623 1.27 0.039 0.18 46.4 768 23.7 10.7 0.04 0.26 0.4 0.6 0.2 25.0 <0.05 0.02 0.3 0.007 0.04 3.8 22 0.2 16.6 78.6 0.56 LINE M 5W 0.2 1.25 14.2 70.0 0.2 0.18 0.07 0.21 58.9 15.3 38.0 33.1 3.08 4.2 2.9 25 0.09 28.5 8.8 0.43 557 1.18 0.041 0.22 45.8 575 25.6 7.1 <0.02 0.34 1.5 0.5 0.1 6.5 <0.05 0.04 5.1 0.010 0.06 1.0 20 0.2 3.4 94.0 1.15 71 LINE M 14W 0.4 1.02 7.3 89.0 0.2 0.22 0.15 0.21 51.4 12.7 21.0 24.3 1.96 5.5 1.9 25 0.07 30.5 4.0 0.13 884 1.22 0.042 0.28 23.2 547 32.4 8.7 <0.02 0.18 0.7 0.3 0.3 11.5 <0.05 0.02 0.3 0.015 0.08 1.0 28 0.2 4.7 56.8 0.44 80 5.5 2.5 40 0.07 26.0 4.7 0.20 1028 1.19 0.041 0.16 27.4 735 32.1 9.6 <0.02 0.18 0.4 0.3 0.3 9.5 <0.05 0.02 0.2 0.011 0.06 0.9 28 LINE M 23W 0.5 0.97 9.8 91.5 0.2 0.24 0.11 0.24 52.1 14.6 29.5 27.2 2.55 0.1 2.9 63.9 0.40 89 1.1 25 0.05 26.0 <0.1 0.09 159 0.92 0.039 0.16 12.6 335 12.0 5.2 <0.02 0.20 0.2 0.2 0.2 7.5 <0.05 0.02 <0.1 0.007 0.06 0.4 98 LINE N 2W 0.3 0.55 6.9 92.5 <0.1 0.18 0.09 0.24 47.9 3.4 20.0 11.6 0.97 3.8 20 0.2 2.9 30.9 0.41 5.7 3.4 30 0.10 24.0 6.4 0.23 513 1.71 0.040 0.40 33.5 741 37.5 8.1 <0.02 0.26 0.8 0.3 0.3 11.5 < 0.05 0.04 1.0 0.013 0.06 0.7 32 0.2 2.3 80.9 0.62 LINE N 10W 0.3 1.12 16.9 103.5 0.3 0.26 0.22 0.30 47.3 10.9 33.0 27.3 3.59 106 115 LINE N 19W 1.0 2.30 18.8 184.0 1.4 0.38 0.25 0.63 151.6 160.3 50.5 79.4 3.87 8.5 4.7 66 0.13 71.0 33.7 0.41 6903 2.01 0.044 0.30 81.4 799 83.7 21.0 0.04 0.30 1.1 0.9 0.4 19.5 < 0.05 0.04 0.3 0.014 0.18 3.4 40 0.2 24.4 97.5 0.55 1.0 1.36 14.4 114.0 0.3 0.24 0.13 0.52 52.0 11.6 40.5 40.8 2.97 5.4 2.9 45 0.12 38.5 7.7 0.35 573 1.70 0.039 0.22 37.0 724 28.9 9.9 0.02 0.24 0.4 0.5 0.3 12.5 <0.05 <0.02 0.2 0.007 0.06 2.9 26 0.3 8.1 72.4 0.55 124 LINE O 3W

Standard:

TILL3 1.4 1.03 77.8 35.0 0.1 0.24 0.58 0.09 30.0 9.1 58.5 21.3 1.99 4.7 1.9 105 0.08 14.0 15.9 0.53 307 0.59 0.036 1.04 31.2 447 18.8 8.8 <0.02 0.49 2.9 0.3 1.0 18.0 <0.05 0.02 3.1 0.064 0.06 11 36 0.2 6.8 38.6 1.66 300 0.59 0.034 0.96 30.4 430 18.3 8.4 0.02 0.48 2.8 0.3 1.0 18.0 <0.05 <0.02 2.7 0.061 0.06 TILL3 1.4 1.02 84.5 35.0 0.2 0.24 0.57 0.10 30.2 9.3 58.5 22.0 1.94 4.5 1.8 110 0.07 14.0 15.1 0.53 1.1 38 0.2 6.3 38.5 1.72 9.6 59.0 20.3 2.03 4.3 1.9 115 0.08 15.5 14.8 0.52 296 0.59 0.037 0.98 30.1 459 18.2 8.1 0.02 0.46 2.7 0.3 0.9 17.5 < 0.05 < 0.02 3.2 0.059 0.06 **TILL3** 1.5 1.02 84.1 38.0 0.1 0.24 0.58 0.08 31.0 1.0 38 0.2 5.8 40.0 1.86 1.4 1.00 78.7 38.0 0.2 0.22 0.57 0.10 28.4 9.6 59.0 22.0 2.03 4.3 1.8 105 0.07 13.5 14.7 0.51 314 0.57 0.035 0.94 30.3 475 18.6 8.0 0.02 0.50 2.7 0.2 1.2 17.5 < 0.05 0.02 2.9 0.058 0.06 36 6.7 39.7 1.78 TILL3 0.9 0.2

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